

# Contact wrench set

$$W = \begin{bmatrix} f \\ p \times f \end{bmatrix}$$

linearized friction cone

$$W \in K = \text{Convex Cone} \left( \begin{bmatrix} e_1 \\ p_1 \times e_1 \end{bmatrix}, \dots, \begin{bmatrix} e_n \\ p_n \times e_n \end{bmatrix} \right)$$

$(2,2) \times (-1,1)$   
 $= 2(1) - 2(-1)$   
 $= 4$

Aggregated contact wrench set is in CWS,  
Minkowski sum of each individual wrench set  
 $CWS = K_1 \oplus K_2 \dots$

Sum of sets:  $A \oplus B = \{a+b | a \in A, b \in B\}$   
 vs. union

ex.  $A = \{1,2\}, B = \{3,4\}$   
 $A \oplus B = \{1+3, 1+4, 2+3, 2+4\}$   
 $A \cup B = \{1,2,3,4\}$

Feasibility?

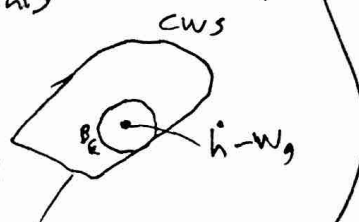
$\dot{h} - W_g \in CWS$  gravity wrench  
 $W_g = \begin{bmatrix} mg \\ r \times mg \end{bmatrix}$   
 $\dot{h} \in \mathbb{R}^6$  total robot momentum  
 $\dot{h} \approx \ddot{x}$

Once contact wrench  $(f, \tau)$  is within CWS, we  
 can compute necessary joint torques. May not meet torque constraints

## Contact wrench set margin

Analogous to  $\epsilon$ -ball in grasping  
 smallest magnitude of wrench disturbance that robot  
 cannot resist, given contact locations and constraints  
 Goal: find motion s.t. CWS margin is maximized

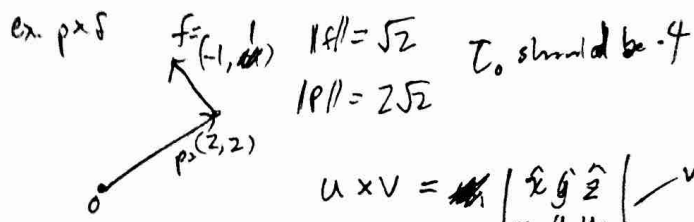
Atlas can ignore this



How to check this?

Transform CWS convex hull  $\rightarrow$   $\cap$  of halfspaces  
 use double description method [44]  
 or  
 $Q$ -hull [4]  $CWS = \{w | a_i^T w \leq 0, i=1, \dots, N_c\}$   
 normal vectors

Can we do a weighted cost  
 between  $B_e$  and  $B_c$ ?  
 $(\dot{h}_{des} - \dot{h})$   
 min max



$$u \times v = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ u_x & u_y & u_z \\ v_x & v_y & v_z \end{vmatrix}$$

vector

$$u \times v = \det(uv) = u_x v_y - u_y v_x$$

magnitude

$$a \times b = \|a\| \|b\| \sin(\theta) n$$

Decision variables  
 $r, \dot{r}, \ddot{r}, k_0, \dot{k}_0$   
 ↑  
 com pos  
 ↑  
 angular momentum  
 minimize  
 ZMP assumes zero

Feasible:

$$a_i^T \begin{bmatrix} m \ddot{r} - mg \\ \dot{k}_0 - r \times mg \end{bmatrix} \leq 0, i=0, \dots, N_c$$

$$\epsilon_{max} = \min_{a_i} \bar{a}_i \begin{bmatrix} \dots \\ \dots \end{bmatrix}$$

concave!  
 check  
 minimize among linear functions of decision variables  
 max this is convex  
 just have to make sure it can be minimized!  
 References for costs (ex-PD) can be arbitrary?

Are there constraints on the costs?  
 Costs have to be quadratic

# Centroidal momentum - stability criterion

$$\begin{aligned} \mathbf{f}_G &= M(\mathbf{g} - \ddot{\mathbf{p}}_G) \quad \mathbf{p}_G = \mathbf{p}^{com} \\ \mathbf{\tau}_G &= \mathbf{p}_G \times M(\mathbf{g} - \ddot{\mathbf{p}}_G) - \dot{\mathbf{L}} \end{aligned}$$

COG = COM when gravitational field is uniform across object  
 gravity + inertia forces  
 $\mathbf{p}$ : position wrt world frame  $\Sigma_w$

where

$$M = \sum_{i=1}^N m_i$$

This term incorporate current momentum?  
 Or coriolis forces from links ← ?

$$\mathbf{L} = [\mathbf{L}_x \mathbf{L}_y \mathbf{L}_z]^T = \sum_{i=1}^N [m_i(\mathbf{p}_i - \mathbf{p}_G) \times \dot{\mathbf{p}}_i + \mathbf{I}_i \boldsymbol{\omega}_i]$$

$$\mathbf{g} = [0 \ 0 \ -g]^T$$

Make balance task by trying to move towards "center" of this convex cone?

Contact forces and torques

$$\mathbf{f}_c = \sum_{k=1}^K \sum_{l=1}^L \epsilon_k^l (\mathbf{n}_k + \mu_k \mathbf{t}_k^l)$$

$$\mathbf{\tau}_c = \sum_{k=1}^K \sum_{l=1}^L \epsilon_k^l \mathbf{p}_k \times (\mathbf{n}_k + \mu_k \mathbf{t}_k^l)$$

These form "polyhedral convex cone in the space of the contact force and torque"  
 "contact wrench"

Friction cone approximation

~~weighting factors~~  
 nonnegative scalar



$L = 4$  usually

stable = sufficient friction exists at contact

- Arbitrary forces, independent of normal force
- Stability is wrt specific  $(\mathbf{f}, \boldsymbol{\tau})$

Stably stable if  $(-\mathbf{f}_G, -\boldsymbol{\tau}_G)$  is inside polyhedral convex cone of contact wrench

Kind of like grasp map?

Convex hull of vectors:

$$\text{conv}(\{\mathbf{V}_i\}) = \left\{ \sum k_i \mathbf{V}_i \mid k_i \geq 0, \sum k_i = 1 \right\}$$

Set of vectors positively spans  $\mathbb{R}^n$  iff origin is in interior of convex hull

$$\text{pos}\{\mathbf{V}_i\} = \mathbb{R}^n \iff \mathbf{0} \in \text{int}(\text{conv}(\{\mathbf{V}_i\}))$$

It takes at least  $n+1$  vectors to positively span  $\mathbb{R}^n$   
 vectors will be wrenches

$$\mathbf{w} = \begin{bmatrix} \mathbf{f} \\ \mathbf{p} \times \mathbf{f} \end{bmatrix}$$

from arbitrary reference frame

stability  
 SVDs to compute ~~grasp maps~~  
 non-zero singular values to check for force closure

PHZ: Think of human as object to be manipulated?

Does this help ~~stability~~  
 deal with contact changes?

ai these

- maximize contact wrench set margin
- minimize upper bound of centroidal angular momentum
- smooth motion

convex function ~~the~~ linear constraints  
 $0 \leq \bar{a}_i \leq \bar{a}_i^{\max}$

QP!

when polytope

or second-order cone program when ellip so.v

How do they set reference for the optimization?

or in contact positions

convex function

linear programs or second-order cone, depending on representation of constraints

desired motion  
 slack variable for angular momentum

here?

$$\min_{\substack{r, \dot{r}, \ddot{r}, s, \\ \epsilon, k_0, \dot{k}_0}} \sum_i \left( C_s s[i] - C_\epsilon \epsilon[i] + C_{\ddot{r}} \ddot{r}[i]^T \ddot{r}[i] \right)$$

weighting terms

convex quadratic function of decision variables

This is over trajectory, like most other works

Can we make this reactive?

in motion retargeting (real-time)  
 Because contact points are defined, but we don't know where they will be (?)

What's the application of this?

~~If we know where they'll be~~

If we don't need real-time?

We know where the contacts will be over entire trajectory and we ~~still~~ don't have to optimize locally

Human-robot collaboration  
 Teleoperation?

our  
 In QP:  $X = \begin{cases} u : \text{motor torques} \\ \ddot{q} : \text{joint accelerations} \\ f : \text{control forces (replaced by } \lambda, \text{ friction cone vector weights)} \end{cases}$

Basically all tasks formulated in terms of task Jacobian  $J_g$

How  $\ddot{q}$  affects task. — linearized approximation

Can we do that here?

$$\frac{1}{2} \ddot{x}^T Q \ddot{x} + C^T \ddot{x} + C^T C$$

$$CW S = \{ W | a_i^T W \leq 0, i=1, \dots, n_a \}$$

$$a_i^T (\dot{h} - w_g) \leq 0, i=1, \dots$$

$$\dot{h} = \begin{bmatrix} m \ddot{r} \\ \dot{k}_0 \end{bmatrix}, w_g = \begin{bmatrix} mg \\ r \times mg \end{bmatrix}$$

feasible if  $a_i^T \begin{bmatrix} m \ddot{r} - mg \\ \dot{k}_0 - r \times mg \end{bmatrix} \leq 0$  this is what we control

→ Add robustness by maximizing  $\epsilon$ -ball

6x6 matrix that transforms wrench at  $p_w$  to origin at world frame

$$B_\epsilon = \{ \dot{h} - w_g + T(p_w, I) W | W^T Q W \leq \epsilon^2 \} \cap CW$$

$$\epsilon_{\max} = \min_{i=1, \dots, n_a} \bar{a}_i \begin{bmatrix} m \ddot{r} - mg \\ \dot{k}_0 - r \times mg \end{bmatrix}$$

where

$$\bar{a}_i = -[a_i^T T(p_w, I) Q W^{-1} T^T(p_w, I) a_i]^{-\frac{1}{2}} a_i^T$$