1. Executive Summary

Roads play an important role in our daily lives. Accidents and their consequences are inevitable, but they can be minimised by making our roads safer by implementing appropriate safety measures. Safer Roads UK, a pressure group dedicated to social responsibility, is studying historical accident data from 2017 to observe how UK roads may be made safer.

The purpose of this coursework is to investigate the variations of accidents across UK's geography, identify the factors that contribute to accidents and their severity with suitable graphical and statistical evidence. It also aims at providing necessary recommendations to improve the roads, techniques to be adopted to make UK roads safer.

The data set majorly contains the geographical coordinates of each accident, date and time of occurrence, accident severity, casualties, and other attributes defining the spot of the incident.

2. Data Cleaning

Dataset has missing values and errors. Hence, it's essential to clean the data before the commencement of analysis. Initially, the encoded data was recoded in R replacing the missing values with NA characters followed by converting the attributes to appropriate data types. Literature has cited several imputation methods for handling missing values, most common being- dropping, replacing with mode, employing neural networks, etc (Margot Peeters et al., 2015). Imputation methods can inject bias into the data hence need to be chosen wisely. Percentage of NA's and unknown values were analysed for each attribute for choosing the best imputation method as shown in the table below. If the total percentage of NA and unknown values was less than 2%, then they were dropped during analysis. For percentages < 8, they were replaced with mode values. Attributes with NA% >40 were not considered for analysis.

Table 1: Missing data analysis

| | | Ing data anary | 010 | | |
|---|----------------|----------------|--------------|--------------|---------|
| Categorical variable | No. of missing | Unknown | % of missing | % of unknown | Total % |
| Road Type | 0 | 2552 | 0.00% | 1.96% | 1.96% |
| Junction_Detail | 609 | 0 | 0.47% | 0.00% | 0.47% |
| Junction_Control | 56296 | 0 | 43.31% | 0.00% | 43.31% |
| Road Class 2 nd | 54412 | 0 | 41.86% | 0.00% | 41.86% |
| Pedestrian Crossing Human Control | 2574 | 0 | 1.98% | 0.00% | 1.98% |
| Pedestrian Crossing Physical Facilities | 2765 | 0 | 2.13% | 0.00% | 2.13% |
| Road Surface Conditions | 1937 | 0 | 1.49% | 0.00% | 1.49% |
| Special Conditions at Site | 2206 | 0 | 1.70% | 0.00% | 1.70% |
| | 2073 | 0 | 1.59% | 0.00% | 1.59% |
| Carriageway Hazards | 2073 | U | 1.3970 | 0.0070 | 1.3970 |
| Weather Conditions | 1 | 7354 | 0.00% | 5.66% | 5.66% |

3. Results and Discussions

Question 1

The preliminary data analysis entailed the study of the cleaned dataset and its continuous and categorical variables, to look for patterns, variations, and association with other variables. The geographical attributes are used to plot a GIS map and create a 'big picture' of the problem.

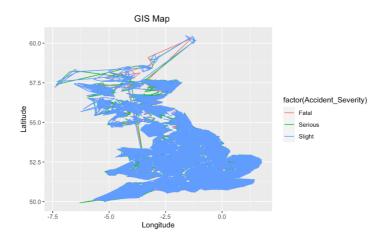


Figure 1: GIS mapping of accidents in UK

The major metrics to categorize the accidents are the number of casualties and the number of vehicles. However, their distributions are highly skewed to the right proving most of the accidents are of slight severity. Hence, we use the statistic 'casualties per accident' to analyse various scenarios. The above statistic is normally distributed with a mean of 1.315 and a standard deviation of 0.76. The skewness of -1.75 indicates slight left skewness and a kurtosis greater than 3 (5.94) indicates the leptokurtic condition. The z-value of skewness (skew/standard error) falls within the range -7 to +7 (-5.11) for n>300 implies that the skew is not too much to consider the variable normally distributed.

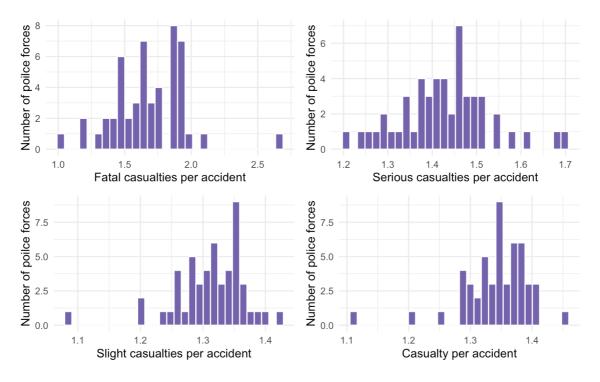


Figure 2: Casualty rate histograms

To analyse the variation of accident severity across the police forces, a chi-squared test was conducted assuming the below hypothesis:

H0: Accident severities are the same across the police forces HA: Accident severities are different across the police forces

The results yield a p-value < 0.05 (2.2E-16) proving that there is a very small probability that the null hypothesis is true. Therefore, be rejected. The standardized residuals (in the appendix) depict that even though the "Metropolitan Police" force has the highest number of accidents, fewer fatal and serious accidents have occurred than expected (std. res<1.96) (Harris, Jenine K., 2021)

To statistically prove significant variations across the police forces, analysis of variance was done assuming the sample means are equal. The hypothesis formulations are as follows:

H0: The sample means are equal HA: The sample means are not equal

Table 2: ANOVA summary

| | Df | Sum Sq | Mean Sq | F value | Pr(>F) |
|-------------------|-----|-----------|----------|---------|----------|
| Police Force | 50 | 227261752 | 4545235 | 1.559 | 0.0306 |
| Accident Severity | 2 | 118951621 | 59475811 | 20.399 | 3.72E-08 |
| Residuals | 100 | 291561061 | 2915611 | | |

The p-value 0.0306 and 3.72E-08 are < 0.05 and are sufficient to reject the null hypothesis inferring that these groups likely came from a population with different means making the variations statistically significant.

Question 2

It was found that 97,779 accidents have occurred on weekdays and 32,203 accidents have occurred on weekends. The number of accidents represent each observation in the dataset, it wouldn't be the right metric to perform the hypothesis testing as it's not possible to compute the mean and standard deviation. Hence, various statistics have been made use of to analyse the situation.

Initially, we consider the proportion of accidents occurring on weekdays and weekends instead of counting.

Let P1 be the proportion of accidents occurring on weekdays = 0.7522 Let P2 be the proportion of accidents occurring on weekends = 0.2477

Then, our null and alternate hypothesis would be,

H0: P2-P1=0 HA: P2-P1≠0

$$Z = \frac{\textit{Observed value-Expected value}}{\textit{Standrad Error}}$$

$$Z = \frac{(P2-P1)-0}{\sqrt{(SE(P1))^2 + (SE(P2))^2}}$$

Substituting proportion values and using SE(P) = $\sqrt{\frac{P(1-P)}{n}}$ where n is the number of observations, we get Z= 297. Since the Z-value is very high p-value \rightarrow 0 <<0.05. Hence, rejecting the null hypothesis.

Similarly, we consider two other statistics - Number of vehicles and number of casualties and computed t-test in R. If X1 and X2 are the numbers of vehicles/ number of casualties occurring on weekdays and weekends respectively. The null, alternate hypothesis, and p-values are as follows:

Table 3: Hypothesis and p-value summary

| | Number of vehicles | Number of casualties | | | | |
|----------------------|--------------------|----------------------|--|--|--|--|
| Null hypothesis | X1-X2=0 | X1-X2=0 | | | | |
| Alternate hypothesis | X1-X2! =0 | X1-X2! =0 | | | | |
| p-value | 8.35E-16 | 2.20E-16 | | | | |

The null hypothesis is rejected as p-value < 0.05 implying that the difference in the number of accidents occurring on weekdays and weekends is statistically significant.

Question 3

It was observed that fatal accidents occur majorly during the day. 986 accidents with 1625 casualties have occurred in the day and 690 accidents with 1198 casualties in the night. The lighting condition characteristic was used to distinguish between day and night. Even though more fatal accidents occur in the day, casualties per accident are higher at the night (1.73). This can be due to various other contributing factors such as higher cases of alcohol consumption, weather conditions, etc. Maximum fatal casualties happen inroads with a speed limit of 60 miles/hour during day and night with casualty per accident of 1.89 and 1.96 respectively

To check if the difference is statistically significant, a t-test was performed assuming:

H0: Mean differences of casualties are the same in day and night HA: Mean differences of casualties are different in day and night

The null hypothesis is rejected as p-value <0.05 implying that mean differences of casualties are different in day and night and are statistically significant

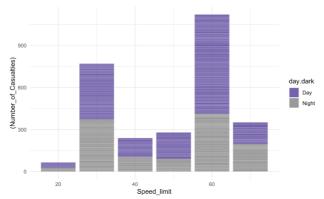


Figure 3: Stacked bar graph representing number of casualties across various speed limits and daytime

Question 4

Uni-variate analysis of various road types was performed to establish whether certain road types are dangerous, comparing the number of casualties across various factors. Single carriageways were found to be the most dangerous, with a highest number of accidents (122424 casualties) and casualty per accident of 1.3. It could be due of the lack of a divider that separates the traffic in opposite directions. However, dual carriageways have the highest casualty rate of 1.44. ANOVA results yielded a p-value <0.05 implying the mean casualties which are different across road types is statistically significant and not occurring by chance.

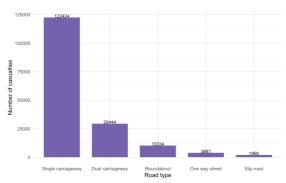


Figure: 4: Casualties across road types

A large number of accidents do occur in 'A' class and unclassified roads with a casualty rate of 1.35 and 1.24 respectively. Owing to broad motorways, the vehicle per accident is high as 2.28. It is observed that higher speed limit roads have higher casualty rates which are evident from the below figure.

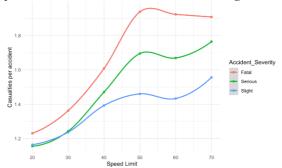


Figure 5: Variation of speed limit with casualty rate

Question 5

Some of the explanatory factors contributing to a number of accidents include certain junctions. Around 60% of the accidents occur at the junctions with staggered, crossroads, and roundabouts being major contributors. Slip roads have the highest casualty rate of 1.43. 80% of the accidents occur where there are no pedestrian crossing facilities within 50m. On the contrary, lesser accidents have occurred in traffic junctions and zebra crossings. High winds and rains are major causes of accidents. However, the casualty rates are almost the same across all weather conditions. The lack of dividers in single carriage roads can be another factor as over 73% of the accidents occur here. Even though over 70% of the accidents occur in dry road conditions, wet roads and floods over 3cm have high casualty rates of 1.35 and 1.45 respectively. ANOVA was conducted for each of the above contributing factors above whose p-values were <0.05 implying the difference of mean casualties across various factors was statistically significant and did not occur by chance.

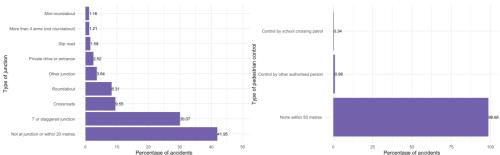


Figure 6: Analysis of accidents at junctions

Figure 7: Pedestrian crossing controls

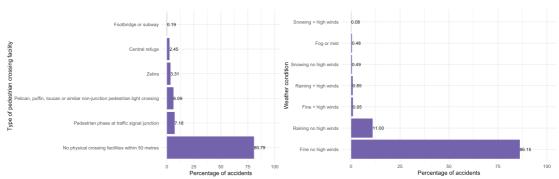


Figure 8: Pedestrian crossing facilities.

Figure 9: Accidents across weather conditions

Bi-variate analysis of road surface-weather, pedestrian crossing facilities-road type, and pedestrian control-road types was conducted to analyse the association through the chi-squared test. In all three cases, the p-value was <0.05 indicating their association is statistically significant. Residual analysis proved that the number of accidents is more than expected when roads are dry and no high winds. Also, they occur more than expected in single carriage ways without crossing facilities, subways in a slip road, traffic junctions in dual carriageways, and one-way streets.

4. Recommendations

Various contributing factors for road accidents in the UK are junction controls, pedestrian crossing facilities, weather conditions, etc. Junctions being a major contributor of accidents (60%) it's essential to install junction controls such as traffic signals at least in the staggered, crossroads and roundabouts. However, it has been observed that the remaining 40% of the accidents that don't occur at junctions are due to a lack of pedestrian crossing controls or lack of pedestrian crossing facilities. Hence, pedestrian crossing controls such as signals, authorized persons need to be deployed. As 58% of the accidents in places without pedestrian crossing control within 50m have occurred at the junctions themselves, it is essential to prioritise junction controls.

Histogram of accidents across the day depicts that a maximum number of accidents occur during the evening rush hour of 4 pm to 5 pm followed by morning peak hours around 8 am inroads with speed limit 30miles/hour with single carriageways being the highest. This implies that it's not speed rather the rush/volume of traffic that causes accidents. Also, it is evident from the below figure that the volume of traffic is higher on unclassified roads. Hence, it is recommended to divert the traffic to broader roads during rush hours to prevent accidents due to congestion.

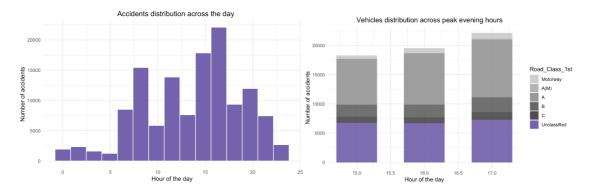


Figure 10: Histogram of accidents across the day

Figure 11: Vehicles involved in accident during peak hours

Although the casualty rate is almost the same in all weather conditions, more than 70% of accidents occur in dry road conditions due to drivers letting their guard down. Therefore, it is recommended to construct more placards for cautious driving on the roadside and strengthen the safety education for drivers regularly. The frequency of accidents on single carriage roads may be due to the lack of dividers. It is recommended to build a little vegetation separation belt in the centre of the road to separate the two side lanes. Although there are more fatal accidents during the day, the average number of casualties (1.73) is higher at night. This may be due to people's restricted vision when driving at night. It is recommended to improve road lighting conditions, increase streetlights, reflective strips, and other facilities.

5. References

- [1] Margot Peeters, Mariëlle Zondervan-Zwijnenburg, Gerko Vink & Rens van de Schoot (2015), How to handle missing data: A comparison of different approaches, European Journal of Developmental Psychology, 12:4, 377-394
- [2] Harris, Jenine K.(2021), Statistics with R: solving problems using real-world data. Sage, London, UK

6. Appendix

Code repository: https://github.com/kbkn11597/FBAMS/blob/master/Code/FBAMS_R_CODE.pdf

1. Below table explains the fact that even though maximum accidents occur in the metropolitan area, the fatal accidents are fewer than expected (with a std. res. Value <-1.96)

| | ======== | | | ==== |
|--|----------|-------------|------------|-------|
| ## | Accident | .cleaned\$A | cident_Sev | erity |
| <pre>## Accident.cleaned\$Police_Force</pre> | Fatal | Serious | Slight | Total |
| ## | | | | |
| ## Metropolitan Police | 129 | 3566 | 23052 | 26747 |
| ## | 344.9 | 4636.9 | 21765.2 | |
| ## | 0.005 | 0.133 | 0.862 | 0.206 |
| ## | -11.625 | -15.727 | 8.722 | |
| ## | | | | |

2. Skewness and kurtosis values of casualties per accidents across accident severity

```
skew.fatal
## skew (g1)
                    se
## 0.4198722 0.3429972 1.2241272 0.2209043
skew.serious
## skew (g1)
                    se
## 0.3010081 0.3429972 0.8775819 0.3801707
skew.slight
       skew (g1)
                            se
## -1.438620e+00 3.429972e-01 -4.194262e+00 2.737613e-05
kurtosis.fatal
## Excess Kur (g2)
                                 se
      2.3385613722
                      0.6859943406
                                       3.4090097161
                                                       0.0006519916
kurtosis.serious
## Excess Kur (g2)
                                 se
         0.6420749
                         0.6859943
                                          0.9359770
                                                          0.3492850
kurtosis.slight
## Excess Kur (g2)
                                 se
                                                  z
      4.339628e+00
                      6.859943e-01
                                       6.326041e+00
                                                       2.515306e-10
```

3. Test of significance for accidents occurring in day and night

```
## Welch Two Sample t-test
##
## data: Accident.cleaned$Number_of_Casualties by Accident.cleaned$day.dark
## t = -7.8674, df = 67093, p-value = 3.674e-15
## alternative hypothesis: true difference in means between group Day and group
Night is not equal to 0
## 95 percent confidence interval:
```

t.test(formula=Accident.cleaned\$Number_of_Casualties~Accident.cleaned\$day.dark)

```
## -0.04669795 -0.02807086
## sample estimates:
## mean in group Day mean in group Night
## 1.304786 1.342171
```

4. Standard residual table for road surface condition and weather

| ======== ## | Accident | : .cleaned\$Road | Surface Co | ======= onditions | | ===: |
|-------------------------|------------------|---------------------|----------------|----------------------|---------------|------|
| ## Accdn.\$W_C Total | | Wet or dmp | | | Fld o 3. d | |
| ## - | | | | | | |
| ## Fn n hgh w 110075 | 91370 | 16633 | 81 | 1979 | 12 | |
| ## ## | 79628.5 0.830 | 27993.9 0.151 | 367.9 0.001 | 1993.5 0.018 | 91.1 0.000 | |
| 0.860 ## ## | 41.609 | -67.902 | -14.959 | -0.326 | -8.289 | |
| "" | | | | | | |
| ## Rnng n h w 14274 | 259 | 13855 | 14 | 83 | 63 | |
| ## ## | 10325.8 0.018 | 3630.1 0.971 | 47.7 0.001 | 258.5 0.006 | 11.8 0.004 | |
| 0.111 ## ## | -99.067 | 169.706 | -4.881 | -10.916 | 14.890 | |
| - - | | | | | | |
| ## Snwn n h w 637 | 17 | 238 | 273 | 109 | 0 | |
| ## ## | 460.8 0.027 | 162.0 0.374 | 2.1 0.429 | 11.5 0.171 | 0.5 0.000 | |
| 0.005 ## ## | -20.674 | 5.971 | 185.632 | 28.695 | -0.726 | |
| - - | | | | | | |
| ## Fn + hgh w 1235 | 875 | 337 | 5 | 18 | 0 | |
| ## ## | 893.4 0.709 | 314.1 0.273 | | 22.4 0.015 | 1.0 0.000 | |
| 0.010 ## | -0.616 | 1.293 | 0.429 | -0.923 | -1.011 | |
| ## - | | | | | | |
| ## Rnng + h w 1102 | 16 | 1042 | 2 | 12 | 30 | |
| ## | 797.2 0.015 | 280.3 0.946 | 3.7 0.002 | 20.0 0.011 | 0.9 0.027 | |
| 0.009 ## ## | -27.668 | 45.502 | -0.877 | -1.781 | 30.454 | |
| ## - | | | | | | |
| ## Snwn + h w 99 | 3 | 26 | 50 | 20 | 0 | |
| ## ## | 71.6 0.030 | 25.2 0.263 | 0.3 0.505 | 1.8 0.202 | 0.1 0.000 | |
| 0.001 ## | -8.108 | 0.164 | 86.343 | 13.597 | -0.286 | |

| ## | | | | | | |
|---------------|-----------|--------|-----------|-----------|-----------|--|
| _ | | | | | | |
| ## Fog or mst | 88 | 433 | 3 | 98 | 1 | |
| 623 | | | | | | |
| ## | 450.7 | 158.4 | 2.1 | 11.3 | 0.5 | |
| ## | 0.141 | 0.695 | 0.005 | 0.157 | 0.002 | |
| 0.005 | | | | | | |
| ## | -17.084 | 21.813 | 0.636 | 25.816 | 0.674 | |
| ## | | | | | | |
| - | | | | | | |
| ## Total | 92628 | 32564 | 428 | 2319 | 106 | |
| 128045 | | | | | | |
| ## ======== | .======== | | :======:: | ========= | ========= | |

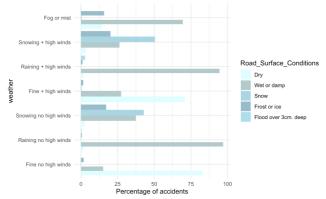


Figure: Comparison of weather and road surface conditions

5. Standard residual table for road types and pedestrian crossing facilities

| ========= | ========= | | | | | ===== |
|------------------------|-------------|----------------------------|-----------|-----------|-----------|-----------|
| ## | Accident.cl | .eaned\$Road_ ⁻ | Гуре | | | |
| ## A.\$P_C_P_ Total | Roundabot | On wy str | Dl crrgwy | Sngl crrg | Slip road | |
| ## | | | | | | |
| - | | | | | | |
| ## N p c f w | 6667 | 2284 | 15750 | 76653 | 1292 | |
| 102646 | | | | | | |
| ## | 6780.0 | 2727.5 | | | 1188.9 | |
| ## | 0.065 | 0.022 | 0.153 | 0.747 | 0.013 | |
| 0.806 | 4 2-2 | 0.461 | 4 05 1 | 2 05 5 | 2 252 | |
| ## | -1.372 | -8.491 | -4.954 | 3.956 | 2.989 | |
| ## | | | | | | |
| - ## 7absa | 242 | 254 | 205 | 2200 | 21 | |
| ## Zebra 4223 | 343 | 254 | 305 | 3290 | 31 | |
| 4223 ## | 278.9 | 112.2 | 674.1 | 3108.9 | 48.9 | |
| ## | 0.081 | 0.060 | 0.072 | 0.779 | 0.007 | |
| 0.033 | 0.001 | 0.000 | 0.072 | 0.775 | 0.007 | |
| ## | 3.836 | 13.385 | -14.215 | 3.248 | -2.561 | |
| ## | | | | | | |
| _ | | | | | | |
| ## P, p, t o | 433 | 379 | 1573 | 5449 | 43 | |
| 7877 | | | | | | |
| ## | 520.3 | 209.3 | 1257.3 | 5798.9 | 91.2 | |
| ## | 0.055 | 0.048 | 0.200 | 0.692 | 0.005 | |
| 0.062 | | | | | | |
| ## | -3.827 | 11.730 | 8.903 | -4.594 | -5.050 | |
| ## | | | | | | . – – – – |
| | | | | | | |

| ## Ppats | 308 | 399 | 2342 | 6141 | 82 | |
|---|--|--|---|---|--|------|
| 9272 ## | 612.4 | 246.4 | 1480.0 | 6825.8 | 107.4 | |
| :# !# | 0.033 | 0.043 | 0.253 | 0.662 | 0.009 | |
|).073 | 0.055 | 0.045 | 0.233 | 0.002 | 0.005 | |
| # | -12.302 | 9.724 | 22.408 | -8.289 | -2.451 | |
| # | | | | | | |
| | | | | | | |
| # Ftbrd o s | 73 | 5 | 81 | 67 | 12 | |
| 238 | 45.7 | 6.3 | 20.0 | 475.0 | 2.0 | |
| !# !# | 15.7 0.307 | 6.3 0.021 | 38.0 0.340 | 175.2 0.282 | 2.8 0.050 | |
| .002 | 0.307 | 0.021 | 0.340 | 0.202 | 0.030 | |
| t# | 14.447 | -0.526 | 6.978 | -8.175 | 5.567 | |
| :# | | | | | | |
| | | | | | | |
| ## Cntrl rfg | 593 | 65 | 289 | 2211 | 16 | |
| 3174 | | | | | | |
| # | 209.6 | 84.3 | 506.6 | 2336.6 | 36.8 | |
| # | 0.187 | 0.020 | 0.091 | 0.697 | 0.005 | |
|).025 !# | 26.476 | -2.106 | -9.669 | -2.599 | -3.425 | |
| +# ‡# | 20.4/0 | -2.100 | -9.009 | -2.599 | -3.425 | |
| | | | | | | |
| ш т.т.1 | 8417 | 3386 | 20340 | 93811 | 1476 | |
| ## lotal | | | | | | |
| ## Total 127430 ## ======== 7. Standard residua ========== | | surface condition | and road types | | | === |
| 127430 ## =================================== | al table for road s ======= Accident.cl | -======= Leaned\$Road_ ⁻ | ===================================== | | | === |
| 127430 ## =================================== | al table for road s ======= Accident.cl | -======= Leaned\$Road_ ⁻ | | Sngl crrg | Slip road | === |
| .27430 ## =================================== | al table for road s ======= Accident.cl | -======= Leaned\$Road_ ⁻ | ===================================== | Sngl crrg | Slip road | === |
| .27430 ## =================================== | al table for road s ======= Accident.cl | -======= Leaned\$Road_ ⁻ | ===================================== | Sngl crrg | Slip road | === |
| 127430 ## =================================== | al table for road s ======= Accident.cl | -======= Leaned\$Road_ ⁻ | ===================================== | Sngl crrg | Slip road | ==== |
| .27430 !# ========= /. Standard residua !========= !# !# Ac.\$R_S_C Total !# !# Dry 1358 | al table for road s ==================================== | Leaned\$Road_ On wy str | ===================================== | 67129 | 1063 | ==== |
| 127430 ## =================================== | al table for road s ==================================== | Leaned\$Road_ On wy str 2596 | Type Dl crrgwy 14520 14610.5 | 67129 67250.7 | 1063 1054.4 | === |
| 127430 ## ================================== | al table for road s ==================================== | Leaned\$Road_ On wy str | ===================================== | 67129 | 1063 | === |
| 27430 ## ========= #. Standard residua ## Ac.\$R_S_C Total ## ## Dry 1358 ## 0.723 | al table for road s ==================================== | Leaned\$Road_ On wy str 2596 | Type Dl crrgwy 14520 14610.5 0.159 | 67129 67250.7 0.735 | 1063 1054.4 | ==== |
| 127430 ## =================================== | Al table for road selection and table for road selection and selection are selected as a selection and selection are selected as a selection a | Leaned\$Road_ On wy str 2596 2408.0 0.028 | Type Dl crrgwy 14520 14610.5 0.159 | 67129 67250.7 0.735 | 1063 1054.4 0.012 | ==== |
| 27430 ## =================================== | Accident.c. Roundabot 6050 6034.4 0.066 | 2596 2408.0 0.028 | 14520 14610.5 0.159 | 67129 67250.7 0.735 -0.469 | 1063 1054.4 0.012 0.265 | |
| 127430 ## ================================== | Al table for road selection and table for road selection and selection are selected as a selection and selection are selected as a selection a | Leaned\$Road_ On wy str 2596 2408.0 0.028 | Type Dl crrgwy 14520 14610.5 0.159 | 67129 67250.7 0.735 | 1063 1054.4 0.012 | |
| 27430 ## =================================== | al table for road s ==================================== | 2596 2408.0 0.028 3.832 | Type Dl crrgwy 14520 14610.5 0.159 -0.749 | 67129 67250.7 0.735 -0.469 | 1063 1054.4 0.012 0.265 | ==== |
| 27430 ## =================================== | al table for road s | Leaned\$Road_ On wy str 2596 2408.0 0.028 3.832 705 849.7 | Type Dl crrgwy 14520 14610.5 0.159 -0.749 5295 | 67129 67250.7 0.735 -0.469 | 1063 1054.4 0.012 0.265 374 372.0 | ==== |
| 27430 ## =================================== | al table for road s ==================================== | 2596 2408.0 0.028 3.832 | Type Dl crrgwy 14520 14610.5 0.159 -0.749 | 67129 67250.7 0.735 -0.469 | 1063 1054.4 0.012 0.265 | ==== |
| 27430 ## =================================== | al table for road s | Leaned\$Road_ On wy str 2596 2408.0 0.028 3.832 705 849.7 | Type Dl crrgwy 14520 14610.5 0.159 -0.749 5295 | 67129 67250.7 0.735 -0.469 | 1063 1054.4 0.012 0.265 374 372.0 | ==== |
| 127430 ## =================================== | al table for road s | 2596 2408.0 0.028 3.832 705 849.7 0.022 | Type Dl crrgwy 14520 14610.5 0.159 -0.749 5295 5155.4 0.164 | 67129 67250.7 0.735 -0.469 23673 23729.7 0.734 | 1063 1054.4 0.012 0.265 374 372.0 0.012 | ==== |
| 27430 ## ========= ## Ac.\$R_S_C Total ## Dry 1358 ## ## Ac.\$R 1358 ## 10.723 ## 14.50 15.723 15.723 15.723 15.723 15.723 15.723 15.723 | al table for road s ==================================== | 2596 2408.0 0.028 3.832 705 849.7 0.022 | 14520 14610.5 0.159 -0.749 5295 5155.4 0.164 1.945 | 67129 67250.7 0.735 -0.469 -23673 23729.7 0.734 -0.368 | 1063 1054.4 0.012 0.265 374 372.0 0.012 0.101 | |
| 27430 ## ========= ## Ac.\$R_S_C Total ## Dry 1358 ## 20723 ## ## Wt or dmp 32236 ## ## 3.255 ## ## Snow | al table for road s | 2596 2408.0 0.028 3.832 705 849.7 0.022 | Type Dl crrgwy 14520 14610.5 0.159 -0.749 5295 5155.4 0.164 | 67129 67250.7 0.735 -0.469 23673 23729.7 0.734 | 1063 1054.4 0.012 0.265 374 372.0 0.012 | |
| 127430 ## ================================== | al table for road s ==================================== | 2596 2408.0 0.028 3.832 705 849.7 0.022 -4.963 | Type Dl crrgwy 14520 14610.5 0.159 -0.749 5295 5155.4 0.164 1.945 | 67129 67250.7 0.735 -0.469 -23673 23729.7 0.734 -0.368 | 1063 1054.4 0.012 0.265 374 372.0 0.012 0.101 | |
| 27430 ## ================================== | al table for road s ==================================== | 2596 2408.0 0.028 3.832 705 849.7 0.022 -4.963 | Type Dl crrgwy 14520 14610.5 0.159 -0.749 5295 5155.4 0.164 1.945 81 67.8 | 67129 67250.7 0.735 -0.469 23673 23729.7 0.734 -0.368 | 1063 1054.4 0.012 0.265 374 372.0 0.012 0.101 7 4.9 | ==== |
| 127430 ## ================================== | al table for road s ==================================== | 2596 2408.0 0.028 3.832 705 849.7 0.022 -4.963 | Type Dl crrgwy 14520 14610.5 0.159 -0.749 5295 5155.4 0.164 1.945 | 67129 67250.7 0.735 -0.469 -23673 23729.7 0.734 -0.368 | 1063 1054.4 0.012 0.265 374 372.0 0.012 0.101 | |
| 127430 ## ================================== | al table for road s ==================================== | 2596 2408.0 0.028 3.832 705 849.7 0.022 -4.963 | Type Dl crrgwy 14520 14610.5 0.159 -0.749 5295 5155.4 0.164 1.945 81 67.8 | 67129 67250.7 0.735 -0.469 23673 23729.7 0.734 -0.368 | 1063 1054.4 0.012 0.265 374 372.0 0.012 0.101 7 4.9 | |

| - | | | | | |
|--------------|--------|--------|--------|--------|--------|
| ## Frst or i | 94 | 27 | 279 | 1877 | 15 |
| 2292 | | | | | |
| ## | 151.4 | 60.4 | 366.5 | 1687.2 | 26.5 |
| ## | 0.041 | 0.012 | 0.122 | 0.819 | 0.007 |
| 0.018 | | | | | |
| ## | -4.664 | -4.299 | -4.573 | 4.621 | -2.227 |
| ## | | | | | |
| - | | | | | |
| ## Fl o 3. d | 2 | 0 | 42 | 61 | 0 |
| 105 | | | | | |
| ## | 6.9 | 2.8 | 16.8 | 77.3 | 1.2 |
| ## | 0.019 | 0.000 | 0.400 | 0.581 | 0.000 |
| 0.001 | | | | | |
| ## | -1.874 | -1.664 | 6.152 | -1.853 | -1.101 |
| ## | | | | | |
| - | | | | | |
| ## Total | 8350 | 3332 | 20217 | 93057 | 1459 |
| 126415 | | | | | |
| ## | | | | | |

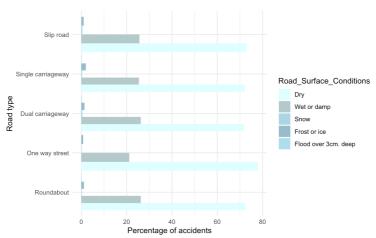


Figure: Comparison of road surface conditions and road types

8. ANOVA test for junction detail

```
oneway.test(formula = Number_of_Casualties~Junction_Detail,data=Accident.c
leaned,var.equal = TRUE)

##
## One-way analysis of means
##
## data: Number_of_Casualties and Junction_Detail
## F = 56.535, num df = 8, denom df = 129364, p-value < 2.2e-16</pre>
```

9. ANOVA test for pedestrian human control

```
oneway.test(formula = Number_of_Casualties~Pedestrian_Crossing_Human_Contr
ol,data=Accident.cleaned,var.equal = TRUE)

##
## One-way analysis of means
##
## data: Number_of_Casualties and Pedestrian_Crossing_Human_Control
## F = 8.7893, num df = 2, denom df = 127405, p-value = 0.0001525
```