

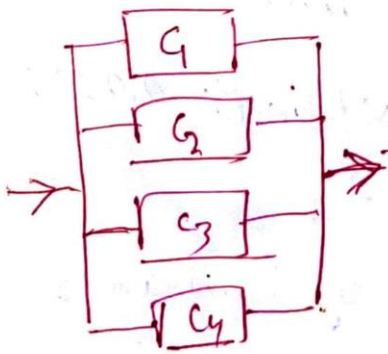
<u>Costs</u>	12000	4000	3000	1750	800	Total = \$21550
<u>Percent</u>	55.7	18.6	13.9	8.1	3.7	
<u>Cum. %</u>	55.7	74.2	88.2	96.3	100.0	

Pareto chart for error categories.

$$\text{Budget} = \$18000 = \frac{18000}{21550} = 83.53\%$$

Areas to Tackle = Inadequate Binding,
 Paper Tension,
 Paper misalignment (66.66%)
 Rectification

Q2



$$\begin{aligned}
 n &= 4, & p &= 0.9 \\
 P(\text{System Functioning}) &= P[X \geq 1] \\
 P(\text{System Failing}) &= 1 - P[X = 0] \\
 &= 1 - P(\text{Sys Fnc}) &= 1 - 4 \cdot 0.9^3 \cdot 0.1^1 \\
 &= 0.0001 &= 1 - 0.0001 \\
 &= 0.9999
 \end{aligned}$$

Q3

Outside diameter = quality issues. ΣX

$$\mu = 40 \text{ mm}, \sigma = 2.5 \text{ mm}$$

Specification limits are (36, 45)

$$Z_1 = \frac{36 - 40}{2.5} = -1.60$$

$$Z_2 = \frac{45 - 40}{2.5} = \frac{5}{2.5} = 2.00$$

$$\frac{x - \mu}{\sigma}$$

$$\text{Daily cost of scrap} = 2000 \times 0.0548 \times 0.50 \\ = \$54.80$$

$$\Phi(z_1) = \Phi(-1.60) = \cancel{\Phi(-1)} \cancel{\Phi(-1)} 0.0548$$

$$\Phi(z_2) = \Phi(2.00) = \cancel{0.9772} 0.9772$$

$$\text{Daily cost of ~~repair work~~ rework} \\ = 2000 \times 0.2 \times \cancel{0.0548} 0.0228$$

$$\text{Total ~~daily cost~~ daily costs of rework \& scrap} = \$63.92$$

$$\mu = 4000 \text{ Kg}$$

$$\sigma = 25 \text{ Kg.}$$

$$Z = \frac{4050 - 4000}{25}$$

$$= 2$$

$$1 - \Phi(Z) = 0.0228$$

Not meeting the requirement.

Only 2.28% of the products has a strength that exceeds 4050 kg.

$$Z = \frac{x - \mu}{\sigma}$$

$$-1.645 = \frac{4050 - \mu}{25}$$

$$\mu = 4050 + 1.645 \times 25 = 4091.125 \text{ kg.}$$

$$\begin{aligned} P[X > 4050] &= 0.95 \\ \Rightarrow 1 - \Phi(Z) &= 0.95 \\ \Rightarrow \Phi(Z) &= 0.05 \\ \Rightarrow Z &= -1.645 \end{aligned}$$

$$Z = \frac{x - \mu}{\sigma}$$

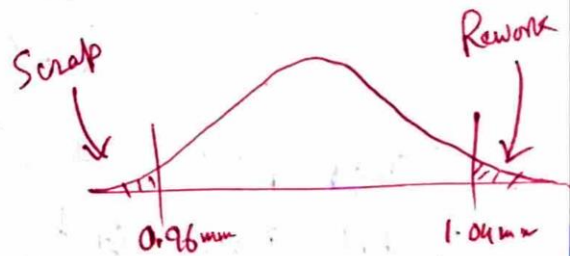
$$\begin{aligned} & \checkmark 1 - P[X \leq 4050] \\ &= 1 - P[Z\sigma + \mu \leq 4050] \\ &= 1 - P\left[Z \leq \frac{4050 - \mu}{\sigma}\right] \\ &= 1 - P[Z \leq -2.00] \\ &= 1 - \Phi(-2) \end{aligned}$$

— α —

$$1.0 \pm 0.04 \text{ mm}$$

$$USL = 1.04 \text{ mm}$$

$$LSL = 0.96 \text{ mm}$$



(a) $X \sim N(0.98 \text{ mm}, 0.02 \text{ mm})$ $N(\mu, \sigma)$
 $\mu =$ $\sigma =$

Proportion of conforming washers

$$Z_1 = \frac{USL - 0.98}{0.02} = \frac{1.04 - 0.98}{0.02} = 3$$

$$Z_2 = \frac{LSL - 0.98}{0.02} = \frac{0.96 - 0.98}{0.02} = -1$$

$$= 1 - (\underbrace{0.1587}_{\text{Scrap}} + \underbrace{0.0013}_{\text{Rework}}) = 0.84$$

$$\text{Daily cost of rework} = 10000 \times 0.0013 \times 0.1$$

$$= \$1.30$$

$$\text{Daily cost of scrap} = 10000 \times 0.1587 \times 0.15$$

$$= \$238.05$$

$$\text{Daily total cost} = \$239.35$$

(b) $\mu = 1.0, \sigma = 0.02$

$$z_1 = \frac{0.96 - 1}{0.02} = -2.00$$

$$z_2 = \frac{1.04 - 1}{0.02} = 2.00$$

Proportion of rework = $0.0228 = 1 - \Phi(z_2)$

" " (scrap) = $0.0228 = \Phi(z_1)$

Total Daily cost = $10000 \times 0.0228 (0.15 + 0.10)$
 $= \$57$

(c) $\mu = 1.0, \sigma = 0.015$

$$z_1 = \frac{0.96 - 1}{0.015} = -2.67$$

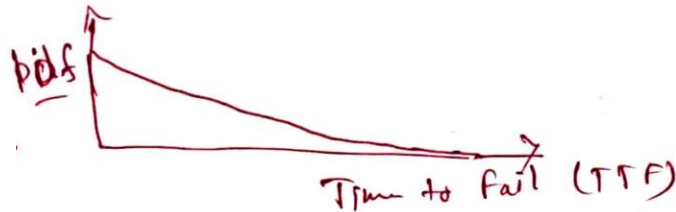
$$z_2 = \frac{1.04 - 1}{0.015} = +2.67$$

Scrap portion = 0.0038 , Rework = 0.0038

Total Daily cost Scrap + Rework = $10000 \times 0.0038 \times (0.15 + 0.10)$
 $= \$9.5$

% decrease = 98.03%

— α —



$$f(x) = \lambda e^{-\lambda x} \quad \text{PDF}$$

$$f(t) = \lambda e^{-\lambda t}$$

$$M_T = \frac{1}{\lambda} = 10000 \text{ hr.}$$

$$\begin{aligned} \int_0^{\infty} t f(t) dt &= \int_0^{\infty} t \lambda e^{-\lambda t} dt \\ &= \frac{1}{\lambda} \end{aligned}$$

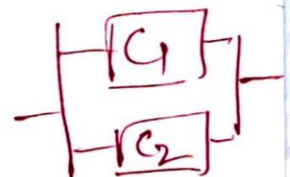
$$\begin{aligned} \text{C.D.F} &= \int_0^t f(t) dt \\ &= 1 - e^{-\lambda t} \end{aligned}$$

$$\begin{aligned} \text{(a)} \quad P(T > 8000) &= 1 - P(T \leq 8000) \\ &= 1 - (1 - e^{-\lambda \times 8000}) \\ &= 0.449 \end{aligned}$$

$$\begin{aligned} \text{(b)} \quad P(T > 15000 | T > 9000) &= \frac{P(T > 15000)}{P(T > 9000)} \\ &= \frac{e^{-\lambda 15000}}{e^{-\lambda 9000}} \\ &= e^{-\lambda 6000} \\ &= P(T > 6000) = 0.549 \end{aligned}$$

$$\begin{aligned} \text{(c)} \quad A &\equiv \text{Comp 1 operates } 12000 \text{ hr} \\ B &\equiv \text{Comp 2 " } 12000 \text{ hr.} \\ P(A) &= 1 - (1 - e^{-\lambda \times 12000}) = 0.30119 \\ P(B) &= 0.30119 \end{aligned}$$

$$P(A \cup B) = P(A) + P(B) - P(A \cap B) = 0.5117$$





* Probability of Type I error = $P[X < \mu - 3\sigma] + P[X > \mu + 3\sigma]$

$$= P\left[\frac{X - \mu}{\sigma} < -3\right] + P\left[\frac{X - \mu}{\sigma} > 3\right]$$

$$= P[Z < -3] + P[Z > 3]$$

$$= \Phi(-3) + (1 - \Phi(3))$$

From standard normal CDF / Z table \rightarrow

$$= 0.00135 + (1 - 0.99865)$$

$$= 0.00135 + 0.00135$$

$$= 0.0027$$

* Probability of two out of three consecutive points falling outside the 2σ limits \Rightarrow

$$= {}^3C_2 p^2 (1-p) \quad \text{where } p = P[X < \mu - 2\sigma] + P[X > \mu + 2\sigma]$$

$$= {}^3C_2 \times 0.0455^2 \times (1 - 0.0455)$$

$$= 3 \times 0.0455^2 \times (1 - 0.0455)$$

$$= 0.005928$$

$$= P\left[\frac{X - \mu}{\sigma} < -2\right] + P\left[\frac{X - \mu}{\sigma} > 2\right]$$

$$= P[Z < -2] + P[Z > 2]$$

$$= \Phi(-2) + (1 - \Phi(2))$$

$$= 0.02275 + (1 - 0.97725)$$

$$= 0.02275 + 0.02275$$

$$= 0.0455$$

* Probability of 4 out of 5 consecutive points falling outside the one-sigma limits \Rightarrow

$$= {}^5C_4 \times p^4 \times (1-p) \quad \text{where } p = P[X < \mu - \sigma] + P[X > \mu + \sigma]$$

$$= 5 \times 0.31732^4 \times (1 - 0.31732)$$

$$= 0.0346804$$

$$= P[Z < -1] + P[Z > 1]$$

$$= \Phi(-1) + [1 - \Phi(1)]$$

$$= 0.15866 + 0.15866 = 0.31732$$

Average diameter = 15 mm $\mu = \bar{x} = \mu$

Std. dev. of diameter = 0.8 mm $\sigma = \sigma$

$$CL = \bar{x} = 15 \text{ mm}$$

$$\text{Std. dev. of sample mean} = \sigma_{\bar{x}} = \frac{\sigma}{\sqrt{n}} = \frac{0.8}{\sqrt{4}} = 0.4 \text{ mm}$$

(a) One-sigma control limits: $\mu \pm 1\sigma_{\bar{x}} = 15 \pm 0.4 = (14.6, 15.4) \text{ mm}$

Two-sigma control limits: $\mu \pm 2\sigma_{\bar{x}}$

$$= 15 \pm (2 \times 0.4)$$

$$= 15 \pm 0.8$$

$$= (14.2, 15.8) \text{ mm}$$

(b) 3- σ control limits = $\mu \pm 3\sigma_{\bar{x}}$ mm

$$= 15 \pm (3 \times 0.4) \text{ mm}$$

$$= 15 \pm 1.2$$

$$= (13.8, 16.2) \text{ mm}$$

(c) Probability of false alarm = Prob. of Type I error

$$= P[X < \mu - 3\sigma] + P[X > \mu + 3\sigma]$$

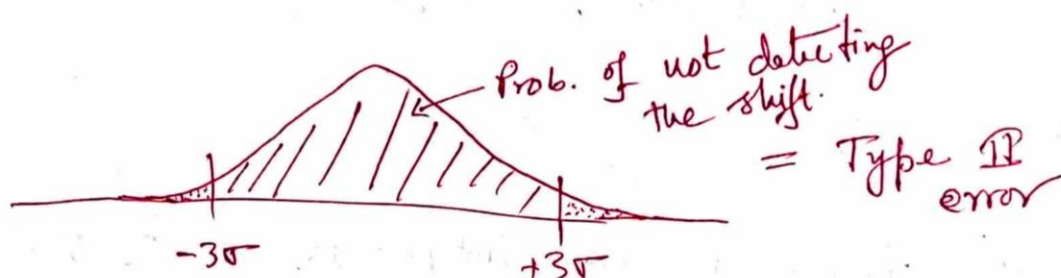
$$= P\left[\frac{X - \mu}{\sigma} < -3\right] + P\left[\frac{X - \mu}{\sigma} > 3\right]$$

$$= \Phi(-3) + (1 - \Phi(3))$$

$$= 0.0027$$

(d) Standardized normal values at the control limits after the shift:

$$z_1 = \frac{16.2 - 14.5}{0.4} = 4.25 \quad \left| \quad z_2 = \frac{13.8 - 14.5}{0.4} = -1.75$$



$$\begin{aligned} \text{Prob.} &= \Phi(z_1) - \Phi(z_2) \\ &= \Phi(4.25) - \Phi(-1.75) \\ &= 1 - 0.04006 \\ &= 0.9599 \end{aligned}$$

$$ARL = \frac{1}{1 - 0.9599} = 24.9626$$

(e) Prob. of detecting at second sample = Prob. of not detecting on first shift \times Prob. of detecting on second shift

$$= 0.9599 \times (1 - 0.9599)$$

$$= 0.0385 \quad \text{** Prob. of failing to detect by the second sample}$$

Prob. of detecting by second sample = $(1 - 0.9599) + 0.0385 = 1 - 0.0786 = 0.9214$

$$= 0.0401 + 0.0385 = 0.0786 \quad \text{--- } \alpha \text{ ---}$$

25 Samples = m Sample / Batch Size = $4 = n$

$$\bar{\bar{x}} = \frac{1000}{25} = 40$$

$$\bar{R} = \frac{250}{25} = 10$$

(a) \bar{x} -Chart control limits

$$CL = \bar{\bar{x}} = 40 \text{ minutes.}$$

$$UCL = \bar{\bar{x}} + A_2 \bar{R} = 40 + (0.7286) \times 10 = 47.286 \text{ min.}$$

$$LCL = \bar{\bar{x}} - A_2 \bar{R} = 40 - (0.7286) \times 10 = 32.714 \text{ min}$$

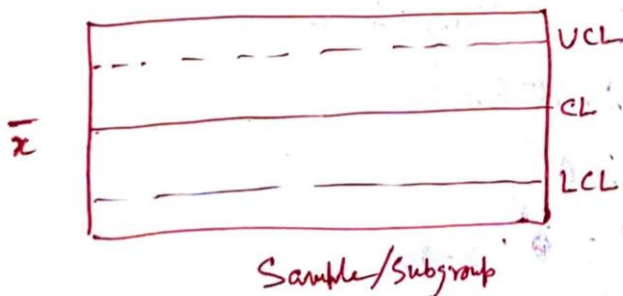
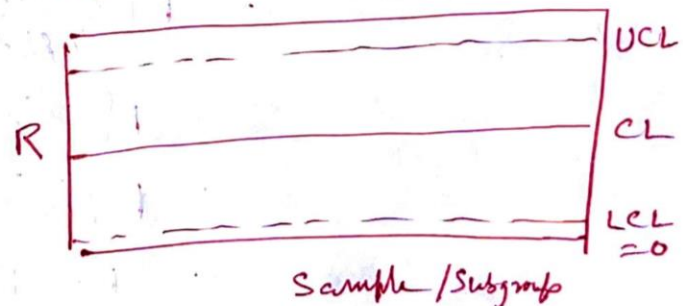
R-Chart control limits

$$CL = \bar{R} = 10 \text{ min}$$

$$R_i = x_{\max}^i - x_{\min}^i$$

$$UCL = \bar{R} D_4 = 10 \times 2.2821 = 22.821 \text{ min}$$

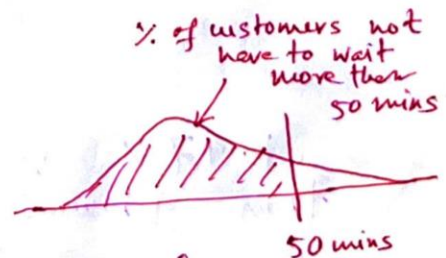
$$LCL = \bar{R} D_3 = 10 \times 0.000 = 0 \text{ min}$$

 \bar{x} -ChartR-Chart(b) Waiting time = X (Random variable)

Process mean = 40 min.

Process standard deviation = $\frac{\bar{R}}{d_2}$

$$= \frac{10}{2.0588} = 4.8572 \text{ min.}$$



$$P[X < 50] = P\left[\frac{X - 40}{4.8572} < \frac{50 - 40}{4.8572}\right] = P[Z < 2.06] = \Phi(2.06)$$

$$P[X < 50] = \Phi(2.06) = 0.98030$$

→ 98.03% of customers will not wait more than 50 mins.

(c) 2-σ limits for \bar{x} -chart

$$\begin{aligned} 40 \pm 2 \times \frac{4.8572}{\sqrt{4}} &= 40 \pm 4.8572 \\ &= (35.143, 44.857) \text{ min} \end{aligned}$$

(d) New process average waiting time = 30 min.

$$\begin{aligned} P[X > 40] &= P\left[\frac{X - \mu}{\sigma} > \frac{40 - \mu}{\sigma}\right] \\ &= P\left[\frac{X - 30}{4.8572} > \frac{40 - 30}{4.8572}\right] \\ &= P[Z > 2.0588] \\ &= P[Z > 2.06] \\ &= 1 - P[Z \leq 2.06] \\ &= 1 - \Phi(2.06) \\ &= 1 - 0.9803 \\ &= 0.0197 \end{aligned}$$

→ 1.97% of customers will have to wait more than 40 mins.

$$P[X > 50] = P\left[Z > \frac{50 - 30}{4.8572}\right] = P[Z > 4.12] = 1 - \Phi(4.12) \approx 0.0000$$

Proportion of customers have to wait more than 50 mins is negligible.

— X —

Specifications on baking time = 10 ± 0.2 min.

$$USL = 10.2 \text{ min}; \quad LSL = 9.8 \text{ min}$$

20 Samples: $m = 20$; Sample / Batch Size = 6 ; $n = 6$

(a) \bar{x} -Chart

$$CL = \bar{\bar{x}} = \frac{199.8}{20} = 9.99 \text{ min}$$

$$UCL = \bar{\bar{x}} + A_3 \bar{s}$$

$$= 9.99 + 1.287 \times 0.07$$

$$= 10.080 \text{ min}$$

$$LCL = \bar{\bar{x}} - A_3 \bar{s}$$

$$= 9.99 - 1.287 \times 0.07$$

$$= 9.90 \text{ min}$$

s -Chart

$$CL = \bar{s} = \frac{1.40}{20} = 0.07 \text{ min.}$$

$$UCL = B_4 \bar{s}$$

$$= 1.970 \times 0.07$$

$$= 0.1379 \text{ min.}$$

$$LCL = B_3 \bar{s}$$

$$= 0.030 \times 0.07$$

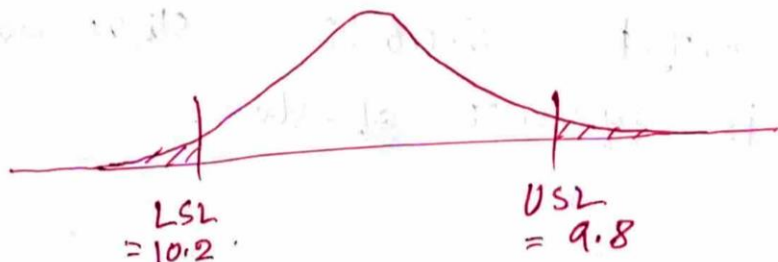
$$= 0.0021 \text{ min}$$

(b) Process mean = $9.99 \text{ min} = \bar{\bar{x}}$

$$\text{Process standard deviation} = \frac{\bar{s}}{C_4} = \frac{0.07}{0.9515} = 0.0736$$

Shewhart
constant

(c)



$$P[X < LSL] + P[X > USL] = \Phi\left(\frac{LSL - 9.99}{0.0736}\right) + \left[1 - \Phi\left(\frac{USL - 9.99}{0.0736}\right)\right]$$

$$= \Phi\left(\frac{9.8 - 9.99}{0.0736}\right) + \left[1 - \Phi\left(\frac{10.2 - 9.99}{0.0736}\right)\right]$$

$$= 0.0049 + 0.0022$$

$$= 0.0071$$

Non conforming output = 0.71 %

The process is 99.29% capable.

(d) If the process mean shifts to 10 min, the standardized normal values at the specification limits are:

$$Z_1 = \frac{9.8 - 10}{0.0736} = -2.72$$

$$Z_2 = \frac{10.2 - 10}{0.0736} = 2.72$$

$$P[X < LSL] + P[X > USL]$$

$$= \Phi(-2.72) + [1 - \Phi(2.72)]$$

$$= 0.0033 + 0.0033$$

$$= 0.0066$$

Non conforming output = 0.66 % (slight reduction)

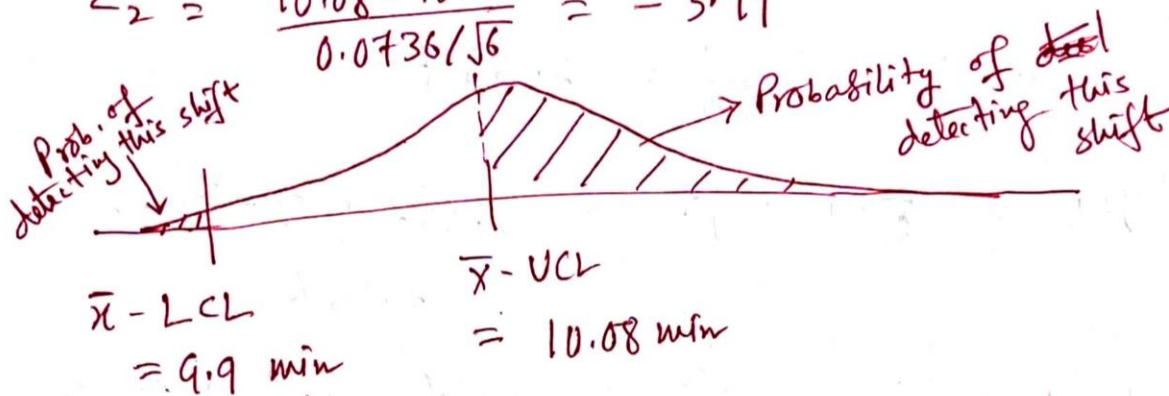
The process is 99.34% capable.

e)

Standardized normal values:

$$Z_1 = \frac{9.90 - 10.2}{(0.0736/\sqrt{6})} = -9.98$$

$$Z_2 = \frac{10.08 - 10.2}{0.0736/\sqrt{6}} = -3.99$$



Prob. of detecting this shift:

$$P[\bar{x} < LCL] + P[\bar{x} > UCL]$$

$$\Rightarrow \Phi(-9.98) + (1 - \Phi(-3.99))$$

$$\Rightarrow \approx 1.0000$$

Probability of detection in the first sample taken $\approx 1.0000 \approx 100.00\%$

— α —

Count of nonconformances chart

→ c-chart

$$CL = \bar{c} = \frac{80}{30} = 2.667$$

$$UCL = \bar{c} + 3\sqrt{\bar{c}} = 2.667 + 3 \times \sqrt{2.667} \\ = 7.566$$

$$LCL = \bar{c} - 3\sqrt{\bar{c}} = 2.667 - 4.899 \approx 0.0$$

For the specified. ~~goal~~ goal:

$$CL = 0.5 = \bar{c}$$

$$UCL = 0.5 + 3\sqrt{\bar{c}} = 0.5 + 3\sqrt{0.5} \\ = 0.5 + 2.121 \\ = 2.621$$

$$LCL = 0.5 - 3\sqrt{\bar{c}} = 0.5 - 2.121 \approx 0$$

[Count of nonconformances
can not be negative]

$$\text{Process mean} = \frac{2.667}{3} = 0.889 \text{ blemishes per } 100 \text{ m}^2$$

$$\text{std. dev.} = \sqrt{0.889} = 0.943$$

$X \equiv$ No. of blemishes per 100 cm^2

\rightarrow A Poisson random variable.

$$P[X < \text{UCL}] = P[X < 2.621] = P[X \leq 2]$$
$$= \sum_{x=0}^2 \frac{e^{-\lambda} \lambda^x}{x!} \quad (\lambda = 0.889)$$

$$= e^{-0.889} \times \left(1 + 0.889 + \frac{0.889^2}{2!} \right)$$

$$= e^{-0.889} \times (1 + 0.889 + 0.3952)$$

$$= e^{-0.889} \times 2.2842$$

$$= 0.41107 \times 2.2842$$

$$= 0.93896$$

So, about 6.1% of the time, the process will be out of control.

— α —

Natural Tolerance limits = $3\text{-}\sigma$ limits
 $= 44 \pm 3(3) = (35, 53) \text{ ppm.}$

$$z_1 = \frac{40 - 44}{3} = -1.33$$

$$z_2 = \frac{55 - 44}{3} = 3.67$$

$$\begin{aligned} P[X < LCL] + P[X > UCL] &= \Phi(z_1) + (1 - \Phi(z_2)) \\ &= \Phi(-1.33) + (1 - \Phi(3.67)) \\ &= 0.0918 \end{aligned}$$

$$C_p, PCR = \frac{USL - LSL}{6\sigma} = \frac{55 - 40}{6 \times 3} = 0.833$$

$$C_p < 1$$

$$\frac{1}{C_p} = 1.2 = 120\%$$

The process uses up 120% of the specification range.

Process mean should be shifted to 47.5 ppm — mid point between the specification limits.

~~2) $\frac{40 - 47.5}{3} = -2.5 = z_2$~~

$$\frac{55 - 47.5}{3} = +2.5 = z_1$$

$$\frac{40 - 47.5}{3} = -2.5 = z_2$$

$$z_1 = z_2 = \pm 2.5$$

$$\begin{aligned} \text{Proportion non conforming} \\ &= 0.0062 \times 2 \\ &= 0.0124 \end{aligned}$$

— α —

