#### Note

# THE METHOD OF CALCULATION OF KINETIC PARAMETERS AS A POSSIBLE CAUSE OF APPARENT COMPENSATION EFFECTS

# J.M. CRIADO and M. GONZALEZ

Departamento de Química Inorgánica de la Facultad de Química de la Universidad de Sevilla y Departamento de Investigaciones Físicas y Químicas, Centro Coordinado del C.S.I.C., Seville (Spain)

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#### INTRODUCTION

The study of the significance of the compensation effect between the logarithm of the Arrhenius pre-exponential factor and the activation energy of heterogeneous reactions has received a great deal of attention [1—6]. Recent papers [7—11] have shown that very often the compensation effects reported in the literature are rather apparent and motivated by the influence of secondary effects on the reactions that leads to apparent kinetic parameters. The experimental errors, the effect of the particle size distribution and the heat and mass transfer phenomena have been considered as the major causes leading to the observation of an apparent compensation effect [12].

However, little, if any, attention has been paid to the study of whether the use of different methods of calculation for obtaining the kinetic parameters of one and the same reaction would be a possible source of apparent compensation effects. We think that this study merits attention after considering that compensation effects between the kinetic parameters obtained by different authors for the same reaction have been reported in several reviews [6,13]. Moreover, chemical interpretations of the phenomenon have been given in spite of the fact that the assumed reaction mechanism has not always been the same.

The scope of the present paper is to explore the influence of both the method of calculation and the kinetic law assumed for performing the analysis of single TG—DTG traces of CdCO<sub>3</sub>, MnCO<sub>3</sub> and PbCO<sub>3</sub> on their kinetic parameters in order to determine if they are correlated through a compensation effect.

# **EXPERIMENTAL**

CdCO<sub>3</sub>, MnCO<sub>3</sub> and PbCO<sub>3</sub>, d'Hemio AR were used. The TG and DTG curves were obtained simultaneously under a vacuum of 10<sup>-4</sup> torr using a

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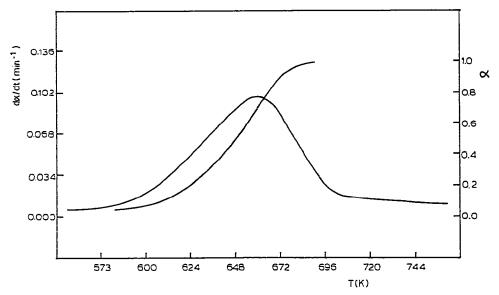


Fig. 1. TG and DTG curves of the thermal decomposition of CdCO<sub>3</sub>.

Cahn electrobalance, model RG, equipped with a derivatograph Mark II. Sample weights of about 23 mg and a heating rate of 6°C min<sup>-1</sup> were used.

# RESULTS AND DISCUSSION

The TG and DTG curves of the thermal decomposition of CdCO<sub>3</sub>, MnCO<sub>3</sub> and PbCO<sub>3</sub> are included in Figs. 1, 2 and 3, respectively. Kinetic analysis of

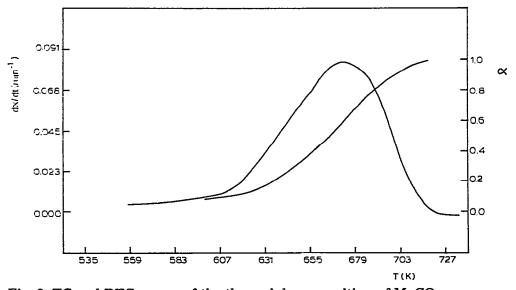


Fig. 2. TG and DTG curves of the thermal decomposition of MnCO<sub>3</sub>.

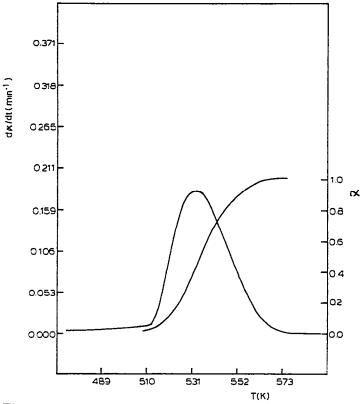


Fig. 3. TG and DTG curves of the thermal decomposition of PbCO<sub>3</sub>.

the above data has been carried out by means of the Coats and Redfern [14] method

$$\ln g(\alpha) - 2 \ln T = \ln \frac{AR}{E\beta} \times \frac{E}{RT}$$
 (1)

and that of Achar et al. [15]

$$\ln \frac{(\mathrm{d}\alpha/\mathrm{d}t)}{f(\alpha)} = \ln A - \frac{E}{RT} \tag{2}$$

where  $\alpha$  is the reacted fraction at time t,  $\beta$  is the heating rate, E is the activation energy, A is the Arrhenius pre-exponential factor and  $f(\alpha)$  and  $g(\alpha)$  are mathematical functions depending on the reaction mechanism.

When the functions  $f(\alpha)$  and  $g(\alpha)$  fit the experimental data, plots of the left-hand side of eqns. (1) and (2) against the reciprocal of the absolute temperature give straight lines whose slopes and intercepts yield the apparent activation energy and the apparent Arrhenius pre-exponential factor, respetively.

The results obtained from kinetic analysis of the data included in Figs. 1—3, by taking into account the  $f(\alpha)$  and  $g(\alpha)$  functions corresponding to the mechanisms more commonly used in the literature for describing the thermal decomposition of solids, are included in Tables 1—3. We can see that the experimental data fit most of the kinetic equations tested.

TABLE 1

Kinetic parameters obtained from analysis of the curves in Fig. 1 by different methods of calculation and different kinetic laws

Mechanism	Integral method			Differential method		
	E(kcal mole 1)	$A(\min^{-1})$	Regression coefficients	E(kcal mole <sup>-1</sup> )	$A(\min^{-1})$	Regression coefficients
R <sub>1</sub>	25.2	$2.7 \times 10^{7}$	-0.99678	9.5	$1.2 \times 10^{2}$	-0.89177
R <sub>2</sub>	31.9	$7.0 \times 10^{9}$	-0.99957	26.8	$1.3 \times 10^{8}$	-0.99951
R <sub>3</sub>	34.4	$5.6 \times 10^{10}$	-0.99974	32.6	$1.3 \times 10^{10}$	-0.99885
$F_1(\alpha)$	39.8	$5.1 \times 10^{12}$	-0.99912	44.2	$1.3 \times 10^{14}$	-0.99493
$A_2$	37.3	$4.3 \times 10^{10}$	-0.99902	45.9	$2.9 \times 10^{13}$	-0.98694
$A_3$	34.7	$1.8 \times 10^{8}$	-0.99888	47.6	$4.1 \times 10^{12}$	-0.97631
$\mathbf{D_1}$	53.0	$6.2 \times 10^{16}$	-0.99712	37.3	$2.8 \times 10^{11}$	-0.98427
$D_2$	61.1	$2.4 \times 10^{19}$	-0.99902	52.0	$1.7 \times 10^{16}$	-0.99779
$D_3$	71.3	$2.2 \times 10^{22}$	-0.99976	69.6	$4.7 \times 10^{21}$	-0.99964
$D_4$	64.5	$8.4 \times 10^{19}$	-0.99946	58.0	$1.1 \times 10^{18}$	-0.99942

Figures 4—6 show that plots of the logarithms of Arrhenius pre-exponential factor vs. the corresponding values of the activation energy lead to compensation effects represented by the equations quoted in Table 4.

The above results show that the differences in the kinetic parameters reported for a reaction would be motivated by both the method of calculation used and/or the kinetic law previously assumed. Moreover, in such a case  $\ln A$  and E seem to be connected through a compensation effect.

TABLE 2
Kinetic parameters obtained from analysis of the curves in Fig. 2 by different methods of calculation and different kinetic laws

Mechanism	Integral method			Differential method		
	$E(\text{kcal mole}^{-1})$	$A(\min^{-1})$	Regression coefficients	E(kcal mole <sup>-1</sup> )	$A(\min^{-1})$	Regression coefficients
$R_1$	19.7	2.0 × 10 <sup>5</sup>	-0.99420	7.8	2.8 × 10 <sup>1</sup>	-0.85459
R <sub>2</sub>	23.9	$7.0 \times 10^{6}$	-0.99758	18.3	1.1 × 10 <sup>5</sup>	-0.99258
$R_3$	25.5	$2.6 \times 10^{7}$	-0.99813	21.7	$1.8 \times 10^{6}$	-0.99751
$F_1(\alpha)$	28.8	$4.1 \times 10^{8}$	-0.99847	28.7	$4.7 \times 10^{8}$	-0.99887
$A_2$	26.2	$2.3 \times 10^{6}$	-0.99816	25.9	$3.5 \times 10^{6}$	-0.99777
$A_3$	23.6	$6.1 \times 10^{3}$	-0.99774	23.2	$1.6 \times 10^4$	-0.99452
$\mathbf{D_{i}}$	42.1	$4.7 \times 10^{12}$	-0.99495	30.2	$6.1 \times 10^{8}$	-0.97663
$\overline{D_2}$	47.3	$1.7 \times 10^{14}$	-0.99699	39.3	$4.3 \times 10^{11}$	-0.99247
$D_3$	53.6	$6.5 \times 10^{15}$	-0.99832	49.9	$4.4 \times 10^{14}$	-0.99835
D <sub>4</sub>	49.4	$2.1 \times 10^{14}$	-0.99759	42.9	$3.9 \times 10^{12}$	-0.99558

TABLE 3
Kinetic parameters obtained from analysis of the curves in Fig. 3 by different methods of calculation and different kinetic laws

Mechanism	Integral method			Differential method		
	E(kcal mole <sup>-1</sup> )	A(min <sup>-1</sup> )	Regression coefficients	E(kcal mole <sup>-1</sup> )	A(min <sup>-1</sup> )	Regression coefficients
$R_1$	33.5	$8.0 \times 10^{12}$	-0.98458	<del>-9</del> .6	$2.0 \times 10^{-5}$	-0.83812
R <sub>2</sub>	41.3	$1.8 \times 10^{16}$	-0.99029	10.1	$3.2 \times 10^{3}$	-0.92843
$R_3$	44.2	$3.1 \times 10^{17}$	-0.99166	16.6	$1.7 \times 10^{6}$	-0.97651
$F_1(\alpha)$	50.4	$1.4\times10^{20}$	-0.99372	29.7	$5.0 \times 10^{11}$	-0.99155
$A_2$	48.3	$2.3 \times 10^{18}$	-0.99314	6.9	$3.2 \times 10^{1}$	-0.87509
$A_3$	46.2	$2.1 \times 10^{16}$	-0.99249	-15.9	$1.2 \times 10^{-9}$	-0.94398
$D_1$	69.1	$2.8 \times 10^{27}$	-0.98551	26.0	$6.8 \times 10^{9}$	-0.91167
$D_2$	78.7	$1.6 \times 10^{31}$	-0.98898	42.9	$4.0 \times 10^{16}$	-0.97126
$D_3$	90.5	$3.5 \times 10^{35}$	-0.99205	62.9	$1.9 \times 10^{24}$	-0.98922
$D_4$	82.6	$1.6 \times 10^{32}$	-0.99018	49.8	$1.4 \times 10^{19}$	-0.98057

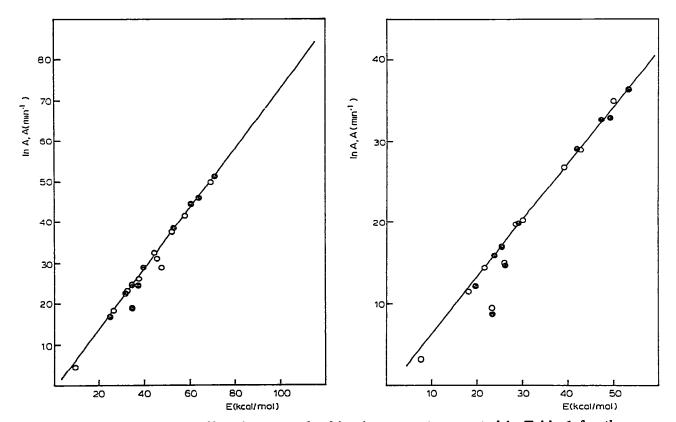


Fig. 4. Compensation effect between the kinetic parameters quoted in Table 1 for the thermal decomposition of CdCO<sub>3</sub>. O, Differential method; , integral method.

Fig. 5. Compensation effect between the kinetic parameters quoted in Table 2 for the thermal decomposition of MnCO<sub>3</sub>.  $\circ$ , Differential method;  $\bullet$ , integral method.

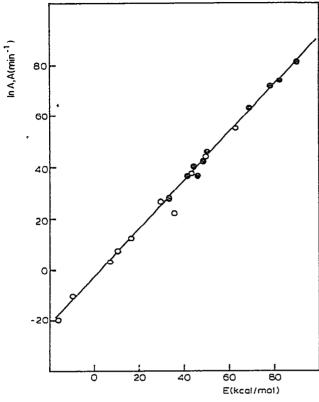


Fig. 6. Compensation effect between the kinetic parameters quoted in Table 3 for the thermal decomposition of PbCO<sub>3</sub>.  $\circ$ , Differential method;  $\bullet$ , integral method.

TABLE 4 Mathematical expressions of the compensation effect

Sample	Equation	
CdCO <sub>3</sub> MnCO <sub>3</sub> PbCO <sub>3</sub>	$\ln A = 0.75E - 2.30$ $\ln A = 0.76E - 3.81$ $\ln A = 0.92E - 1.56$	

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