Chapter 4:

Thermodynamics of Electrochemical Systems

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Chapter 4: Thermodynamics of Electrochemical Systems

Thermodynamics is the study of equilibria states. Thus, it provides us information on systems which do not carry current. Thermo applies also to pseudo-steady states, i.e., systems whose response time is faster (shorter) than the imposed change (perturbation), and therefore if the reaction is fast, thermo will still apply. However, electrochemical systems are often characterized by sluggish electrode kinetics and slow diffusion, hence; one should apply themodynamic analysis with care to such systems, since it can be misleading. Accordingly, thermo indicates that we cannot plate zinc out of acidic solutions, the lead acid battery cannot exist, and that we cannot plate InSb, GaAs and other compounds from aqueous solutions – all of which are wrong.

Nonetheless, thermo provides the 'base line' – i.e., the ideal or the basis from which we start to analyze our system. This relates primarily to the standard potential, direction of spontaneous reactions, energy content in chemicals, etc.

We focus our discussion on electrochemical systems, i.e., systems involving ionic species in contact with electrodes.

Energy Expressions used in thermo:

- G = Gibbs Free energy
- A = Helmholtz free energy

We can determine the change in Gibbs Free energy of a system undergoing a reaction readily from thermodynamic measurable and tabulated values:

$$\Delta G = \Delta H - T \Delta S \tag{4-1}$$

Where ΔH is the change in the enthalpy (\sim heat content) of the system, and ΔS , the change in its entropy. The latter term is typically quite small at ambient temperatures.

We shall also see that ΔG is directly linked to the standard potential of the electrode reaction, E:

$$\Delta G = -nFE \tag{4-2}$$

Where n is the number of electrons transferred in the electrode reaction, and F is Faraday's constant.

The Gibbs free energy can be viewed (imprecisely) as the chemical energy stored in a system. Hence a change in the Gibbs free energy will tell us if the system will react spontaneously (negative ΔG for the reaction).

Criterion for Spontaneity:

AG provides a criterion for determining the spontaneous direction a chemical reaction will take.

The change in free energy for any process is either negative or remains constant, at constant temperature and pressure, for any closed system. The change in ΔG provides the clue whether a reaction will <u>spontaneously</u> proceed in a particular direction. This is why G is also called the thermodynamic or chemical potential. It is analogous as far as equilibrium and changes are concerned to potential energy in mechanical systems.

Note:

- 1. ΔG determines the possibility and direction of change in a chemical system not its rate.
- 2. Never try to propose a process in which ΔG increases.
- 3. ΔG and direction of the chemical reaction can change with the temperature. (Why do we often heat systems where ΔG is already negative?)
- 4. Will reaction "1" proceed more readily than reaction "2" if $\Delta G_1 < \Delta G_2$ both being negative.

[define "readily" faster (no) or to a further extent (yes)].

5. In electrochemical systems $\Delta G = -nFE$, hence we can drive any reaction to any extent by externally applying the appropriate voltage.

Gibbs Equation and the Chemical Potential

Gibbs free energy is a function of the temperature, pressure and chemical composition of the system:

$$G = G(T, P, n_i)$$
 [4-3]

A complete differential becomes,

$$dG = \left(\frac{\partial G}{\partial T}\right)_{P,n_i} dT + \left(\frac{\partial G}{\partial P}\right)_{T,n_i} dP + \sum \left(\frac{\partial G}{\partial n_i}\right)_{T,P,n_i} dn_i$$
 [4-4]

Gibbs defined the chemical potential of species i, μ_i ,

$$\mu_{i} = \left(\frac{\partial G}{\partial n_{i}}\right)_{T,P,n_{i}} = \left(\frac{\partial A}{\partial n_{i}}\right)_{T,V,n_{i}}$$
[4-5]

We can now re-write the Gibbs equation 4-4,

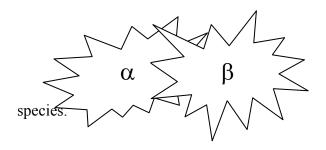
$$dG = -SdT + VdP + \sum \mu_i dn_i$$
 [4-6]

Reversible Work

$$dW=dG$$
 const. T,P at equilibrium, no work \rightarrow dG=0

The chemical potential provides the criterion for phase equilibrium:

For two phases α and β , in contact, in which species can transfer from one to the other,



at equilibrium:

$$\mu_i^{\alpha} = \mu_i^{\beta}$$

For all species, including charged

Also:
$$T^{\alpha} = T^{\beta}$$

 $P^{\alpha} = P^{\beta}$

Activity

We cannot measure directly the chemical potential and also its mathematical behavior is inconvenient (goes to negative infinity when a species is absent), hence we want to account for it in terms of another parameter, the activity.

Availability of a species in solution for a chemical reaction is equal to its concentration only in the absence of any intermolecular forces In any non-ideal solution such forces will exist between the -solvent and the solute molecules. In the case of ionic solutions, in particular those of strong electrolytes, strong long range coulombic forces also exist between the ions. Therefore, in all these practical solutions we must replace the concentration with an "effective concentration" which we will designate as the activity, a. Hence for the reaction

$$A + B \rightleftharpoons C + D$$

$$K = \frac{a_C \cdot a_D}{a_A \cdot a_B} \neq \frac{C_C \cdot C_D}{C_A \cdot C_B}$$

Also, when the ionic solution is extremely dilute the activity approach the concentration:

$$a_i \sim C_i$$
 as $C \rightarrow 0$

We would like to speak about the absolute activity of a species i, a_i (dimensionless) irrespective of the concentration units used. We will say that the absolute activity is equal to the concentration times an activity coefficient.

$$a_i = f_i C_i$$

Since we have two major concentration systems:

or

c - molarity [gr moles solute/liter solution]

We must define two systems of activity coefficients:

$$a_i = \gamma_i m_i$$
 or $ai = f_i C_i$

We relate the activity to the chemical potential:

$$\mu_i = RT \ln a_i$$
 (absolute activity according to Gugenheim)

$$\mu_i = \mu_i^0 + RT \ln a_i$$
 (activity defined by Lewis and Randall)

Mean Properties

While conceptually we may discuss the activity of an ionic species, in reality, we are always faced with a solution containing multiple species (as required by electroneutrality). Since the activity of an ion is strongly affected by its neighboring ions, we must therefore discuss (and measure) the activity of an ion in combination with the other constituents of the solution. We do this by defining the mean properties of the neutral combination:

$$a_{+/-} = \gamma_{+/-} m_{+/-}$$

Calculating the activity

Consider the salt: $BaCl_2 \rightarrow Ba^{++} + 2Cl^{-}$

Or in a general form: $A_{\nu^+}B_{\nu^-} \rightarrow \nu^+ A + \nu^- B$

Define: $v = v^+ + v^-$

Mean molality $m_{+/-} = m \left(v_+^{v^+} \cdot v_-^{v^-} \right)^{1/v}$

Mean activity $a_{+/-} = \gamma_{+/-} m_{+/-}$

Activity: $a = (a_{+/-})^{\nu}$

Determining the activity coefficients:

- a. Use tabulated values (hard to find, but available)
- b. Use the Debye-Huckel limiting law: $\log \gamma_{+/-} = -0.51 |z_+ \cdot z_-| \sqrt{I}$ Where I is the ionic strength of the solution, given by: $I = \frac{1}{2} \sum_{i} z_i^2 C_i$

Example:

Determine the activity of 0.1 m H_2SO_4 given that $\gamma_{+/-} = 0.265$

$$H_2SO_4 \rightarrow 2H^+ + SO_4^{-2}$$

(Always assume complete dissociation, even if you know [as the case here is] this to be incorrect. The activity coefficient takes care of this 'wrong' assumption)

$$v^{+} = 2; \quad v^{-} = 1$$

$$y = y^{+} + y^{-} = 2 + 1 = 3$$

$$m_{+/-} = m \left(\nu_{+}^{\nu^{+}} \bullet \nu_{-}^{\nu^{-}} \right)^{1/\nu} = 0.1(2^{2} * 1^{1})^{1/3} = 0.1587$$

$$a_{+/-} = \gamma_{+/-} m_{+/-} = 0.265 * 0.1587$$

$$a = (a_{+/-})^{\nu} = (0.1587 * 0.265)^{3} = 7.4 * 10^{-5}$$

Standard Electrode Potentials

Measured vs. Normal Hydrogen Electrode.

In Practice, we use secondary 'reference electrodes'

Expresses the relative tendency of an electrode to give up or accept electrons and change its oxidation state.

Conventionally written as reduction potentials for the half-cell reaction:

$$M_1^{z+} + ne^- \rightarrow M_1^{(z-n)+} \quad \Delta G_1 = (\Delta H_1 - T\Delta S_1) = -nFE_1^0 \rightarrow E_1^0 = -\Delta G_1/nF$$

or:

 $Cu^{++} + 2e^{-} \rightarrow Cu^{0}$ (cupric ion being reduced to metallic copper) $E^{0}=0.34 \text{ V}$ $E^{0}=\text{`Standard'}$ Electrode potentials; refers to potential of electrode in contact with unit activity solution (a $_{Mn^{+}}=1$)

Related definitions for: Equilibrium potentials, Galvani potentials, Open circuit potential (OCP), EMF:

Because of the need for a charge balance we must have an accompanying oxidation reaction which provides the electrons. E.g.:

$$M_2 \rightarrow M_2^{n+} + ne^-$$

Standard electrode potentials:

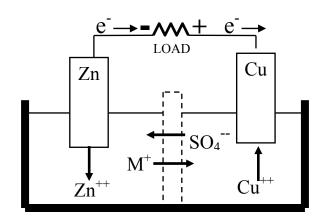
Active (anodic)

$Li^+ + e \rightarrow Li^0$	-3.045 V		$H^+ + e \rightarrow 1/2H_2$	0 V
$K^+ + e \rightarrow K^0$	-2.935		$^{\circ}$ HgO +H ₂ O +2e → Hg+2OH $^{\circ}$	0.098
$Ca^{2+} + 2e \rightarrow Ca^{0}$	-2.866		$Cu^{++} + e \rightarrow Cu^{+}$	0.153
$Na^+ + e \rightarrow Na^0$	-2.714		$AgCl + e \rightarrow Ag+Cl^{-}$	0.2224
$Mg^{++} + 2e \rightarrow Mg^0$	-2.363		$HgCl_2 + 2e \rightarrow 2Hg + 2Cl^-$	0.2676
$Al^{+3} + 3e \rightarrow Al^{0}$	-1.662		$Cu^{++} + 2e \rightarrow Cu^{0}$	0.337
Ti ⁺⁺ +2e →Ti ⁰	-1.628		$Fe(CN)_6^{-3} + e \rightarrow Fe(CN)_6^{-4}$	0.36
$Zn(OH)_2 + 2e$ $\rightarrow Zn^0 + 2OH^-$	-1.245		$I_2 + 2e \rightarrow 2I^-$	0.536
$Mn^{++} + 2e \rightarrow Mn^0$	-1.180		$O_2 + 2H^+ + 2e \rightarrow H_2O_2$	0.682
2H ₂ O +2e →H ₂ +2OH	-0.822		$Fe^{+3} + e \rightarrow Fe^{+2}$	0.771
$Zn^{++} + 2e \rightarrow Zn^0$	-0.764		$Ag^+ + e \rightarrow Cu^0$	0.9
$Cr^{3+} + 3 e \rightarrow Cr$	-0.744		$Br_2 + 2e \rightarrow 2Br^-$	1.065
$Fe^{++} + 2e \rightarrow Fe^{0}$	-0.441		$O_2 + 4H^+ + 4e \rightarrow 2H_2O$	1.229
$Cd^{++} + 2e \rightarrow Cd^{0}$	-0.403		$Cl_2 + 2e \rightarrow 2Cl^-$	1.358
$Ni^{++} + 2e \rightarrow Ni^{0}$	-0.250		$PbO_2 + 4H^+ + e \rightarrow Pb^{+2} + 2H_2O$	1.455
$\operatorname{Sn}^{++} + 2e \rightarrow \operatorname{Sn}^{0}$	-0.136		$Ce^{+4} + e \rightarrow Ce^{+3}$	1.61
$Pb^{++} + 2e \rightarrow Pb^0$	-0.126	1	$Au^+ + e \rightarrow Au^0$	1.692
$H^+ + e \rightarrow 1/2H_2$	0		$F_2 + 2e \rightarrow 2F$	1.87

Nobel (Cathodic)

These are half cell potentials. Obviously, for a process we require two half cells: one with anodic reaction, the other with cathodic (why?)

For example consider the Zn/Cu cell



Battery or Fuel-Cell

A spontaneous chemical reaction is used to produce electrical energy

Anodic Oxidation:

Cathodic Reduction:

$$Zn \longrightarrow Zn^{++} + 2e \qquad Cu^{++} + 2e \longrightarrow Cu$$

$$Cu^{++} + 2e \longrightarrow Cu$$

Assume:

$$Cu^{++}+2e \rightarrow Cu^{0}$$
 $E^{0} = 0.34 \text{ V}$
 $Zn^{++}+2e \rightarrow Zn^{0}$ $E^{0} = -0.76 \text{ V}$

We must reverse one of the reactions (Why?). Note also, that when we add the standard potentials we get -0.42 and hence ΔG will be positive. This indicates impossible reaction. We will pick the half cell reaction with the lower standard potential and reverse it:

Cathode:
$$Cu^{++}+2e \rightarrow Cu^{0}$$
 $E^{0} = 0.34 \text{ V}$
Anode: $Zn^{0} \rightarrow Zn^{++}+2e$ $-E^{0} = +0.76 \text{ V}$

Now we can sum up the reactions and the standard potentials:

$$Cu^{++} + Zn^{0} \rightarrow Cu^{0} + Zn^{++}$$
 $V = +1.1 \text{ V} \rightarrow \Delta G = -nFE^{0} < 0$

We note that the cell voltage is: $V_{Cell} = E_{Anoder}^0 - E_{Cathode}^0$

Materials that are active (very negative) tend to get easily oxidized. This will reverse the cathodic reaction and yield a positive E^0 corresponding to negative (spontaneous) ΔG . They are suitable to be anodes in batteries.

The other electrode reaction in the battery during discharge will be cathodic reduction. However, here we have a problem, since we do not want the proton to be reduced to hydrogen gas, which will tend to explode the battery. Possible materials are those that inhibit hydrogen evolution kinetically – Zinc, and lead, or mercury, or Cd. Alternatively, if we want to e.g., use Li, we must use non-aqueous (a-protic) solvents.

Note: Battery applications - Cathodes
$$Li = -3 \text{ V}$$

 $Zn = -0.176$
 $Pb = -0.126$

The highest voltage: Li-F Battery: 1.87 V - (-3.045 V) = 4.91 V

Leclanche Cell (Zn-Carbon)

Anode:
$$\operatorname{Zn}(s) \to \operatorname{Zn}^{2+}(aq) + 2 e^{-}$$

Cathode: $\operatorname{2MnO}_2(s) + 2 \operatorname{H}^+(aq) + 2 e^{-} \to \operatorname{Mn}_2\operatorname{O}_3(s) + \operatorname{H}_2\operatorname{O}(l)$
 $[\operatorname{Mn}^{+4} \to \operatorname{Mn}^{+3} + e]$

We find for Mn:

i.	Mn ⁺⁺ + 2 e → Mn	-1.185
ii.	$Mn^{3+} + 3e \rightarrow Mn^{2+}$	1.5415
iii.	$MnO_2 + 4 H^+ + 2 e \rightarrow Mn^{2+} + 2 H_2O$	1.224
iv.	$MnO^{4-} + e \rightarrow MnO4^{2-}$	0.558
V.	$MnO_{4^{-}} + 4 H^{+} + 3 e \rightarrow MnO_{2} + 2 H_{2}O$	1.679
vi.	$MnO_{4^{-}} + 8 H^{+} + 5 e \rightarrow Mn^{2+} + 4 H_{2}O$	1.507
vii.	$MnO_4^- + 2 H_2O + 3 e \rightarrow MnO_2 + 4 OH^-$	0.595
viii.	$MnO_{42-} + 2 H_2O + 2 e \rightarrow MnO_2 + 4 OH$	0.60
ix.	$Mn(OH)_2 + 2 e \rightarrow Mn + 2 OH^-$	-1.56

x.
$$Mn(OH)_3 + e \rightarrow Mn(OH)_2 + OH_-$$
 0.15
xi. $Mn_2O_3 + 6 H^+ + 2e \rightarrow 2 Mn^{2+} + 3 H_2O$ 1.485

2 iii.
$$2MnO_2 + 8 H^+ + 4 e \rightarrow 2Mn^{2+} + 4 H_2O$$
 $\Delta G = -4F(1.224)$
xi. $2 Mn^{2+} + 3 H_2O \rightarrow Mn_2O_3 + 6 H^+ + 2 e$ $\Delta G = -2F(-1.485)$

$$2MnO_2 + 8 H^+ + 4 e^+$$
. $2 Mn^{2+} + 3 H_2O \rightarrow \Delta G = F(-4x1.224 + 2x1.485)$
 $2Mn^{2+} + 4 H_2O + Mn_2O_3 + 6 H^+ + 2 e$

When considering energetics we never add voltages. We add and subtract energies or ΔG . When n is identical in the two reactions, we may add and subtract voltages, since ΔG =-nFE. However when adding half cell reactions with different n we must add or subtract ΔG .

Combining identical terms:

Cathode:
$$2MnO_2 + 2 H^+ + 2 e \rightarrow Mn_2O_3 + H_2O$$

$$\Delta G = F(-4x1.224+2x1.485) = F(-1.926)$$

Switching back to voltage:

$$E = -\Delta G/nF = 1.926/2 = 0.963 \text{ V}$$

Combining with the Zinc reaction:

$$Zn^{2+}(aq) + 2 e^{-} \rightarrow Zn(s)$$
 E = -0.764 V

Reversing the zinc reaction:

Anode:
$$Zn(s) \to Zn^{2+}(aq) + 2e^{-}$$
 E= + 0.764

Summing the anode and cathode reactions we get:

$$Zn(s) + 2MnO_2 + 2 H^+ \rightarrow Mn_2O_3 + H_2O + Zn^{2+}(aq)$$

$$E = 0.963 + 0.764 = 1.727 \text{ V}$$
 (in reality we have $V \sim 1.5 \text{ V}$)

This difference is mainly due to the fact that the proton comes from ammonia:

$$NH_4^+(aq) \rightarrow H^+(aq) + NH_3(aq)$$
 E=?

Corrosion implications:

All very negative material 'love' to give electrons (are readily oxidized). All very positive materials tend to be reduced (accept electrons). This is why we find in nature the alkali metals only as cations, and all 'active' metals are found as oxides. On the other hand, noble metals such as gold or platinum might be found in nature in the reduce form, as e.g., gold metallic nuggets (if we are lucky to find them). We will never find active metal as a reduced (non oxidized) species.

By the same token, we never want to have an active element in its reduced form (e.g., Li, zinc, or even iron) in contact with a 'noble' species in its oxidized form. The active metal will readily give its electrons to the noble material.

This is why we never want to store CuSO₄ solution in zinc or iron container. We will have the reaction:

$$Zn + Cu^{++} \rightarrow Zn^{++} + Cu$$

which will have a Positive E (or negative ΔG), indicating a spontaneous reaction.

Dissimilar metal corrosion

The Cementation reaction

$$Fe + Cu^{++} \rightarrow Fe^{++} + Cu \quad E^0 > 0$$

Copper (in the form of carbonates, sulfates, etc.) is dug from the ground and leached with sulfuric acid, producing impure copper sulfate. Iron scrap is then thrown into the bath, causing the reaction above. The copper 'mud' precipitates, with codeposits of irom. Gold. Silver..

The copper 'mud' is then used as anode in a copper refining cell.

Nernst equation:

Correcting for activities different from unity:

$$v_A A + v_B B \rightarrow v_C C + v_D D$$

$$E = E^{0} - \frac{RT}{nF} ln \frac{a_{C}^{\nu_{C}} \cdot a_{D}^{\nu_{D}}}{a_{A}^{\nu_{A}} \cdot a_{B}^{\nu_{B}}} \sim E^{0} - \frac{RT}{nF} ln \frac{C_{C}^{\nu_{C}} \cdot C_{D}^{\nu_{D}}}{C_{A}^{\nu_{A}} \cdot C_{B}^{\nu_{B}}}$$
(assuming $\gamma_{i}=1$)

For the half cell reaction:

$$vM^{n+} + ne \rightarrow M_v$$

$$E = E^{0} - \frac{RT}{nF} ln \frac{a_{M_{v}}}{a_{M^{n+}}^{v}} = E^{0} - \frac{RT}{nF} ln \frac{a_{reduced}}{a_{oxidized}^{v}} = E^{0} - \frac{RT}{nF} ln \frac{a_{right}}{a_{left}^{v}}$$

At 25 C = 298 K:

$$\frac{RT}{F} = 0.02565 V$$

$$\frac{RT}{F}\ln X = 0.02565 \ln X = 2.3 \cdot 0.02565 \log X = 0.0591 o g X$$

$$E = E^{0} - \frac{0.02565}{n} \ln \frac{a_{M_{v}}}{a_{M^{n+}}^{v}} = E^{0} - \frac{0.059}{n} \log \frac{a_{M_{v}}}{a_{M^{n+}}^{v}}$$

Also,

 $a_{element} = 1$

 $\ln a^{\upsilon} = \upsilon \ln a$

$$\ln \frac{1}{X} = -\ln X$$

$$\ln a - \ln b = \ln \frac{a}{b}$$

$$E = E^{0} - \frac{RT}{n} \ln \frac{a_{M_{\upsilon}}}{a_{M^{n+}}^{v}} = E^{0} - \frac{RT}{n} \ln \frac{1}{a_{M^{n+}}^{v}} = E^{0} + \frac{RT}{n} \ln a_{M^{n+}}^{v} = E^{0} + \frac{RT}{\upsilon n} \ln a_{M^{n+}}^{v}$$

Cells with Varying Concentrations

A. Identical Species

 $Cu \mid CuSO_4(a_1) \parallel CuSO_4(a_2) \mid Cu$

$$Cu^{++}(a1) + 2e \rightarrow Cu^{0}$$
 $E(a1)$

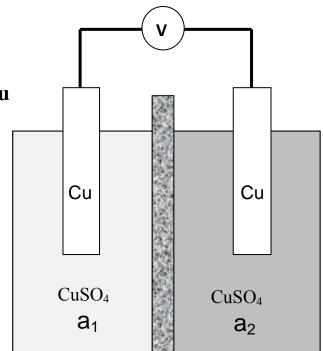
$$Cu^{++}(a2) + 2e \rightarrow Cu^{0}$$
 E(a2)

Reverse the more negative:

$$Cu^0 \rightarrow Cu^{++}(a1) + 2e - E(a1)$$

Add up:

$$Cu^{++}(a2) \rightarrow Cu^{++}(a1)$$



$$E(a1) = E^{0}-(RT/nF)\ln(1/a1)$$
 $a_1 < a_2$

$$E(a2) = E^{0}-(RT/nF)ln(1/a2)$$

-
$$E(a1) = -E^0 + (RT/nF)ln(1/a1)$$

Add up potentials (ΔG):

$$E=-E(a1)+E(a2) = -E^0+(RT/nF)\ln(1/a1)+E^0-(RT/nF)\ln(1/a2)$$

E = (RT/nF)ln(a2/a1) > 0 [Spontaneous]

a1 = anode (dissolves)

a2= cathode (plates)

Cells with Varying Concentrations

B. Non- Identical Species

 $Cu \mid Zn \mid ZnSO_4 (a=0.2) \mid | CuSO_4 (a=0.5) \mid Cu \mid Cu$

$$\mathbf{E}_{\text{Cell}}=?$$

$$Cu^{++}(a=0.5) + 2e \rightarrow Cu^{0}$$
 $E(Cu)$

$$Zn^{++}(a=0.5) + 2e \rightarrow Zn^{0}$$
 E(Zn)

Reverse the more negative:

$$Zn^0 \rightarrow Zn^{++}(a=0.2) + 2e$$
 -E(Zn)

Add up:

$$Cu^{++}(a=0.5) + Zn^{0} \Rightarrow$$

 $\Rightarrow Cu^{0} + Zn^{++}(a=0.2)$

$$E_{Cu} = E_{Cu}^{0} - \frac{RT}{2F} \ln \frac{a_{Cu^{0}}}{a_{Cu^{++}}}$$

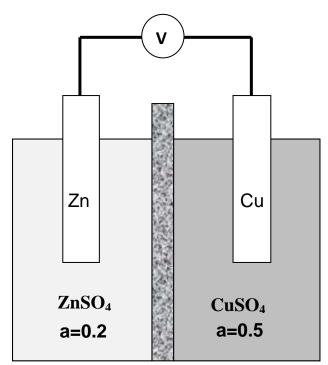
$$E_{Zn} = E_{Zn}^0 - \frac{RT}{2F} \ln \frac{a_{Zn^0}}{a_{Zn^{++}}}$$

$$-E_{Zn} = -E_{Zn}^{0} + \frac{RT}{2F} \ln \frac{a_{Zn^{0}}}{a_{Zn^{++}}}$$

$$E_{Cell} = E_{Cu} + \left(-E_{Zn}\right) = E_{Cu}^{0} - E_{Zn}^{0} - \frac{RT}{2F} \ln \frac{a_{Cu^{0}}}{a_{Cu^{++}}} + \frac{RT}{2F} \ln \frac{a_{Zn^{0}}}{a_{Zn^{++}}}$$

$$E_{Cell} = \left(E_{Cu}^{0} - E_{Zn}^{0}\right) + \frac{RT}{2F} \ln \frac{a_{Zn^{0}} a_{Cu^{++}}}{a_{Zn^{++}} a_{Cu^{0}}} = \left(E_{Cu}^{0} - E_{Zn}^{0}\right) + \frac{RT}{2F} \ln \frac{a_{Cu^{++}}}{a_{Zn^{++}}}$$

$$E_{Cell} = (0.34 - [-0.784]) + \frac{0.059}{2} \log \frac{0.5}{0.2} = 1.115 + 0.03 * 0.398 = 1.127V$$



Determine now the concentrations upon short circuit:

$$E_{cell} = 0 V$$

$$\begin{split} E_{Cell} &= 0 = \left(E_{Cu}^{0} - E_{Zn}^{0}\right) + \frac{RT}{2F} \ln \frac{a_{Cu^{++}}}{a_{Zn^{++}}} = \\ &= \left(0.34 - \left[-0.784\right]\right) + \frac{0.059}{2} \log \frac{a_{Cu^{++}}}{a_{Zn^{++}}} = 1.115 + 0.03 * \log \frac{a_{Cu^{++}}}{a_{Zn^{++}}} \\ &= \frac{a_{Cu^{++}}}{a_{Zn^{++}}} = 10^{-37} \end{split}$$

$$\frac{a_{Cu^{++}}}{a_{Zn^{++}}} = 10^{-37}$$

Since a_{zn} cannot be significantly larger than 1, very few atoms of cupric ions remain in solution

Industrial application: Copper displacement by iron scrap.

E-pH diagrams (Pourbaix diagrams)

Water may be electrolytically decomposed (= 'electrolyzed') according to:

Cathodic reduction: $4 \text{ H}^+ + 4 \text{ e} \rightarrow 2 \text{ H}_2$ $E_1^0 = 0 \text{ V}$

Anodic Oxidation: $\underline{2 \text{ H}_2\text{O} \rightarrow \text{O}_2 + 4\text{H}^+ + 4\text{e}} \qquad \underline{\text{E}^0}_2 = 1.23 \text{ V}$

Overall: $2 \text{ H}_2\text{O} \rightarrow \text{H}_2 + \text{O}_2$ $E^0 = E^0_1 - E^0_{2} = -1.23 \text{ V}$

The negative standard potential tells us that the reaction is not spontaneous (positive ΔG). Acidic medium has been assumed at pH=0, however a similar reaction can be written for neutral or basic environment, remembering that under neutral conditions we have both H⁺ and OH⁻ species, and in base environment we only have OH⁻ and water.

In base environment (pH= 14) we have:

Cathodic reduction: $4 \text{ H}_2\text{O} + 4 \text{ e} \rightarrow 2\text{H}_2 + 4 \text{ OH}^2$ $\text{E}^0_1 = -0.826 \text{ V}$

Anodic Oxidation: $\underline{4 \text{ OH}^- \rightarrow O_2 + 2 \text{H}_2 \text{O} + 4 \text{ e}} \qquad \underline{\text{E}^0_2} = +0.404 \text{ V}$

Overall: $2 \text{ H}_2\text{O} \rightarrow \text{H}_2 + \text{O}_2$ $E^0 = E^0_1 - E^0_2 = -1.23 \text{ V}$

Obviously, both reactions exhibit the same overall standard potential (- 1.23 V), and it should be so, because the overall reaction is the same, and does not involve the pH.

It is instructive to write the potential for each of the electrode reactions separately. We will assume, here, arbitrarily for this illustration) that we are in acidic environment (pH=0).

Cathodic reduction: $4 \text{ H}^+ + 4 \text{ e} \rightarrow 2 \text{ H}_2$ $E_1^0 = 0 \text{ V}$

$$E = E^{0} - \frac{RT}{nF} \log \frac{\Pi a_{products}^{v}}{\Pi a_{reactants}^{v}}$$

$$E_{H_2} = 0 - \frac{0.059}{4} \log \frac{p_{H_2}}{a_{H^+}^4} = -\frac{0.059}{4} \log a_{H^+}^{-4} \cdot p_{H_2} = +0.059 \log a_{H^+} \cdot p_{H_2}$$

Since: $pH \equiv -\log a_{\mu^+}$

$$E_{H_2} = -0.059 \cdot pH \cdot \log p_{H_2}$$

Assuming that the partial pressure of hydrogen is 1 $(p_{H2}=1)$,

$$E_{H_2} = -0.059 \cdot pH$$

We can show, similarly, for the oxygen:

$$E_{O_2} = 1.23 - 0.059 \cdot pH$$

The overall reaction, $E_{H2} - E_{O2}$

$$E_{H_2} - E_{O_2} = -1.23$$

The same as before. Clearly, from Nernst Eq., only reactions that exhibit explicitly either H^+ or OH^- will show a dependence of E on the pH.

We now will plot a diagram of the dependence of each of the electrode reactions on the pH:

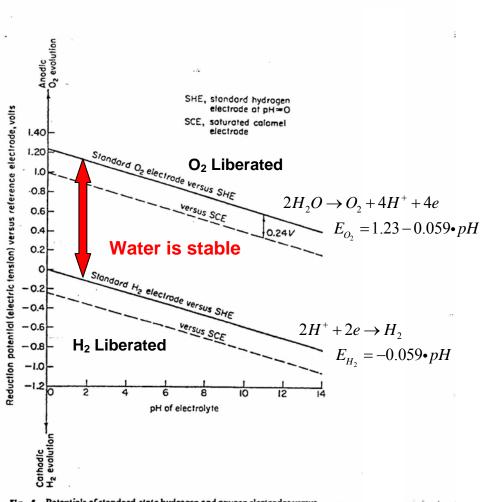
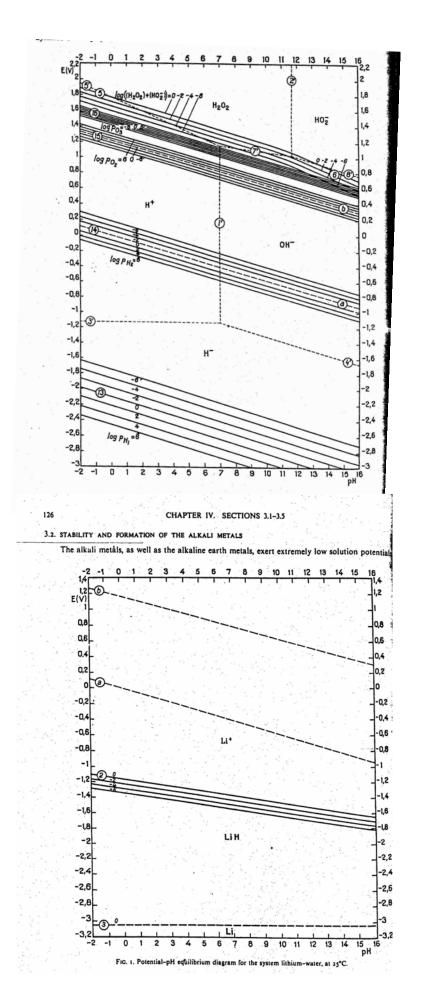


Fig. 4 Potentials of standard-state hydrogen and oxygen electrodes versus pH of electrolyte, using the reduction potential sign convention.



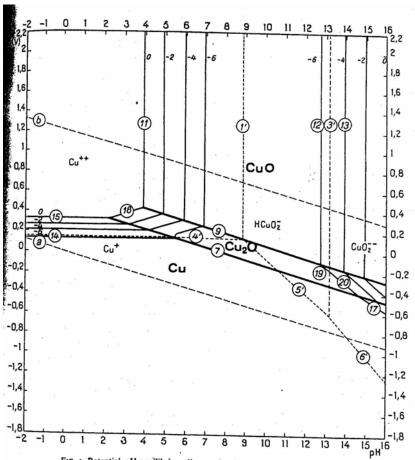
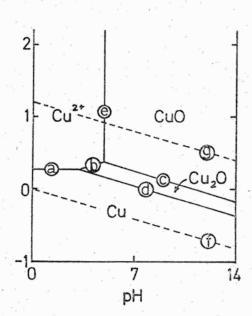
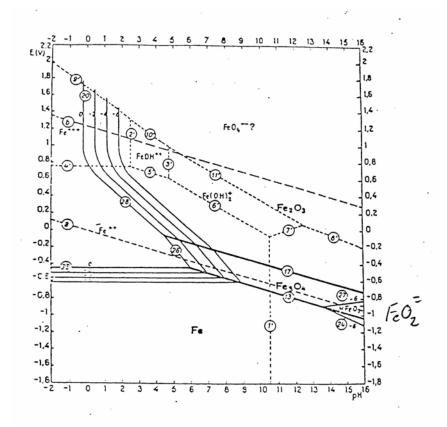


Fig. 1. Potential-pH equilibrium diagram for the system copper-water, at 25°C. [Considering the solid substances Cu, Cu₂O and CuO. Cu(OH)₂ is not considered.]



Pourbaix Diagram for the System ${\rm Cu-Cu}^{2+}{\rm -Cu}_2{\rm O-CuO-H}_2{\rm O}$. Activity of Cupric Ion is assumed to be 0.01.

-		
	Line	Reaction
	a	$Cu = Cu^{2+} + 2e^{-}$
,	b	$Cu_2O + 2H^+ = 2Cu^{2+} + H_2O + 2e^-$
	С	$Cu_2^0 + H_2^0 = 2Cu_0 + 2H^+ + 2e^-$
	d	$2Cu + H_2O = Cu_2O + 2H^+ + 2e^-$
	e	$Cu^{2+} + H_2O = CuO + 2H^+$
	f	$H_2 = 2H^{+} + 2e^{-}$
	g	$H_2O = 1/2 O_2 + 2H^+ + 2e^-$



Potential pH Diagram of iron-water system based on the oxides of iron. (adapted from Pourbaix.)

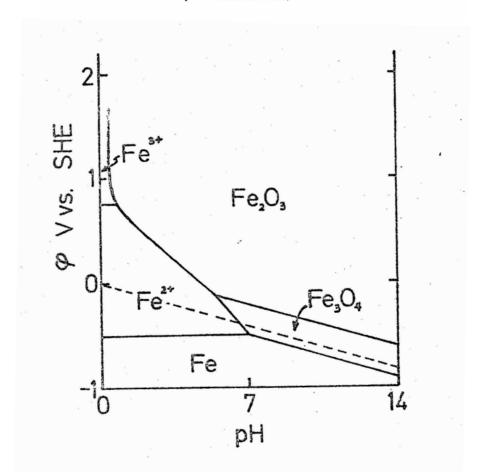


FIGURE III-10. Pourbaix Diagram for Iron.

Effect of complexing agents on codeposition of alloys.

The normal deposition potentials for copper and zinc are far apart. Nevertheless, it is possible to plate brass (a Cu-Zn alloy) directly by electrolysis. Suggest how simultaneous deposition of these two metals is possible:

$$Zn^{++} + 2\bar{c} \rightarrow Zn$$
 $E^{\circ} = -0.758$
 $Cu^{++} + 2\bar{c} \rightarrow Cu$ $E^{\circ} = +0.344$

This is clearly too much of a difference

(107)
$$E_{\frac{1}{2}} = E_{1}^{\circ} + \frac{RT}{2F} \ln Zn^{++}$$

(108)
$$E_2 = E_2^{\circ} + \frac{RT}{2F} \ln Cu^{++}$$

(109)
$$E_1 = E_2$$
: for codeposition

(110)
$$-0.758 + \frac{0.059}{2}$$
 lg Zn⁺⁺ = +0.344 + $\frac{0.059}{2}$ lg Cu⁺⁺

(111)
$$\lg \frac{[Zn^{++}]}{[Cu^{++}]} = \frac{2.204}{0.059}$$
; $\frac{[Zn^{++}]}{[Cu^{++}]} = 1.7 \times 10^{37}$

Clearly, not many copper ions are allowed to be in the solution. A "permissible" concentrations ratio can be obtained by the addition of a complexing agent such as cyanide. The cupocyanide anion dissociates into cuprous and cyanide ions according to:

$$Cu(CN)_3^{2-} \neq Cu^+ + 3CN^-$$

$$k = 5.6 \times 10^{-28}$$

And for the zinc:

$$Zn(CN)_4^{2-} \stackrel{?}{+} Zn^{++} + 4CN^{-}$$

$$k = 1.3 \times 10^{-17}$$

Assume 0.05 M copper cyanide solution and 0.025 M Zn $(CN)_4^{2-}$

(112)
$$\frac{\left[\text{Cu}^{+}\right]\left[\text{CN}^{-}\right]^{3}}{\left[\text{Cu}\left(\text{CN}\right)_{2}^{-2}\right]} = \frac{\left[x\right]\left[3x\right]^{3}}{\left[0.05-x\right]} = 5.6 \times 10^{-28}$$

$$[Cu^{+}] = 3.19 \times 10^{-8}$$

 $[CN^{-}] = 9.57 \times 10^{-8}$

for the Zn:

$$[Zn^{+2}] = 6.62 \times 10^{-5};$$
 [CN] = 2.65 x 10⁻⁴

When the two solutions are mixed the cyanide concentration will be mostly due to the An complex dissociation. Calculate again the cuprous ion conc.:

(113)
$$\frac{\left[\text{Cu}^{+}\right]\left[2.65 \times 10^{-4}\right]^{3}}{0.05} = 5.6 \times 10^{-28} \left[\text{Cu}^{+}\right] = 1.50 \times 10^{-18}$$

The new deposition potentials are:

For Zn:
$$E_1 = -0.758 + \frac{0.059}{2}$$
 lg $6.62 \times 10^{-5} \approx -0.90V$
For Cu: $E_1 = +0.52 + \frac{0.059}{1}$ lg $1.5 \times 10^{-18} \approx -0.54V$
 E° Cu⁺/Cu $\Delta V \approx 0.36V$

This ΔV is considerably closer than 1.1 V, and can be "bridged over" by surface overpotential terms.

Temperature Effects on the EMF

(114)
$$\Delta G = \Delta H - T\Delta S = \Delta H + T(\frac{\partial \Delta G}{\partial T})_{p}$$
; $\Delta G = -nF\epsilon$
(115) $-nFE = \Delta H - nFT(\frac{\partial E}{\partial T})_{p}$

(115)
$$-nFE = \Delta H - nFT(\frac{\partial E}{\partial T})$$

(116)
$$\Delta H = -nF \left[E - T(\frac{\partial E}{\partial T})\right]_{p}$$

Note that:

(117)
$$\Delta S = nF \left(\frac{\partial E}{\partial T}\right)_{P}$$
 slope of E vs. T gives entropy change on the order of 0.5mV/°C

(118)
$$\Delta Cp = nFT(\frac{\partial^2 E}{\partial T^2})_p$$
 Difficult to determine accurately

$$\left(\frac{\partial E}{\partial T}\right)_{P} = \frac{\Delta S}{nF}$$

 ΔS can be either negative or positive, but it is a small number under ambient temperatures

(119)
$$\left(\frac{\partial E}{\partial p}\right)_T = -\frac{\Delta V}{nF}$$
 For solids and liquids pressure dependence of volume is normally negligible

Considering only the volume change of a gas:

(120)
$$E_p = E_1 - \frac{1}{nF} \int_1^P \Delta V dp$$
 dependence of V on P must be specified

Assuming ideal gas behavior PV = NRT

$$E_p = E_1 - \frac{NRT}{nF} \int_1^P d \ln P = E_1 - \frac{4NRT}{nF} \ln P$$

Values of N and n have to be established with care.

Example: Decomposition potential of water at 25°C and 100 At.

$$^{2H_2O}(L) + ^{O}2 + ^{2H}2$$
 $^{4}N = 3$ $n = 4$ $E_{100} = -1.23 - \frac{3 \times 0.059}{4} \log_{10}100 = -1.23 - 0.09 = -1.32$

The negative sign is indicative that this reaction (decomposition of water) is not spontaneous, ΔE is positive.

Current Flow and Heat Effects

The potential of a cell under equilibrium is called the "EMF". Equilibrium implies that there is no current flow. When current flows the cell deviates from equilibrium and for a case of a galvanic cell the terminal voltage $E_{\overline{1}}$ will be lower than the EMF because of ohmic dissipation on the internal cell resistance.

The current flowing through the cell:

$$i = \frac{EMF}{R_e + R_i}$$

where R_e - external resistance

R_i - internal resistance

The component i $R_e = E_T = Terminal voltage$.

The relationship between EMF and E_T :

$$\frac{E_T}{EMF} = \frac{R_e}{R_e + R_i}$$

for <u>n</u> cells in series $i = \frac{nEMF}{R_e \div nR_i}$

(same as for single if
$$R_i >> R_e$$
; $i = \frac{EMF}{R_i}$

if $R_i << R_e$; $i = n \cdot \frac{EMF}{R_e}$

$$i = \frac{EMF}{Re + \frac{R_i}{n}}$$

(for batteries $R_i = 0.05 - 0.5 \Omega$)

if
$$R_i >> R_e$$
, $i = n \frac{EMF}{R_1}$ current prop. to number of cells if $R_1 << R_e$, $i = \frac{EMF}{R_e}$ current same as for single cell

Heat Effects in Cells

Heat effects are measured either in terms of either:

Q [cal/mole] - heat of reaction

or

q [cal/sec] - rate of heat flow

The two are related through:

$$q = Q \dot{m} = \frac{cal}{mole} \frac{mole}{sec} = \frac{cal}{sec}$$

Where m, the rate of material reacted is related to the current through Faraday's law:

$$\dot{m} = \frac{w}{Mt} = \frac{I}{Fz} \left[\frac{mole}{sec} \right]$$

In order to analyze the heat effects we must first assign a sign convention. Accordingly, heat evolved (giving rise to cell temperature) will be considered with a negative sign. Conversely, heat absorbed (causing cell cooling) will be positive.

Heat effects (cooling or heating) of electrochemical cells are due to two classes of phenomena:

- a. Reversible ("thermodynamic") heat effects
- b. Heat due to irreversible (dissipative processes).

The heat associated with the thermodynamic (reversible) process is associated with electrical work

or

Ι

 $q_{rev} = \dot{m} T \Delta S$

 ΔS can either be positive or negative hence the cell may heat or cool down due to reaction. ΔS , however, is typically a small quantity and unless the temperature is very high the reversible heat effect is rather small.

b. The heat associated with the irreversible processes is always negative (heat evolved). It is given by the various dissipative processes in the cell, including diffusion, kinetics and ohmic migration. Typically the later, given by Iη_Ω or I²R, is dominant. Hence,

$$q_{irr} = -0.24 |I\eta_{\Omega}| = -0.24 I^2 R = -0.24 \frac{\eta_{\Omega}^2}{R}$$
 [$\frac{cal}{tee}$]

The factor of 0.24 is due to the conversion from joules to calories:

1 joule = 0.24 cal.

Lastly,

 $q \text{ total} = q \text{ rev.} + q \text{ irr} = \text{rin } T \Delta S - 0.24 | I \eta_{\Omega} | \text{ [cal/sec]}$

I. THERMODYNAMIC POTENTIALS AND REFERENCE ELECTRODES

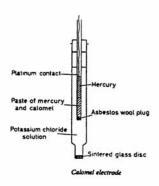
- A. REFERENCE ELECTRODES FOR AQUEOUS SOLUTIONS

 - 2. SECONDARY REFERENCES: FOR USE WITHOUT LIQUID JUNCTIONS

A) TABLE I: TYPICAL REFERENCE ELECTRODES

- 3. SECONDARY REFERENCES: FOR USE WITH SALT BRIDGES TO MINIMIZE LIQUID JUNCTION POTENTIALS
 - REQUIREMENTS OF SALT BRIDGE TO MINIMIZE LIQUID JUNCTION POTENTIALS
 - 1) HIGH CONCENTRATION
 - 2) TRANSFERENCE NO. t+ = t_
 - B) TYPICAL ELECTROLYTES: KC1, NH4 NO3

TABLE II: CALOMEL REFERENCES WITH SALT BRIDGES



A STANDARD REDUCTION POTENTIALS IN ACCUEOUS SYSTEMS. NOTE THAT THE REDUCTION POTENTIALS AND ELECTRODE POTENTIALS HAVE THE SAME SIGNS. ALL POTENTIALS VS. SHE.

B
H2 GENERATED BY SMALL CATHODIC POLARIZING CURRENT ON HIGH AREA PE
CATHODE. POTENTIAL SHOULD BE CHECKED AGAINST A KNOWN REFERENCE.
POTENTIAL USUALLY CLOSE TO REVERSIBLE H2 H ELECTRODE.

REFERENCE ELECTRODES FOR NON AGUEOUS SYSTEMS

TABLE III: APPLICATIONS OF REFERENCE ELECTRODES

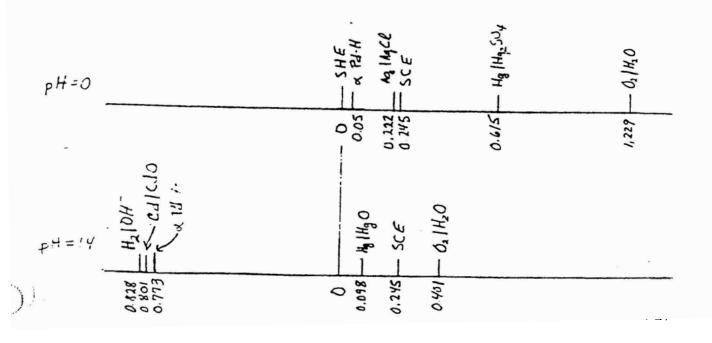
	Suitability					
Electrode	Aqueous solutions	Organic	Fused salts	Biological systems	Special applications	
standard hydrogen	****	••	•	•	Electrode standardization	
silver-silver halide	**** .	***	•••	•••	Secondary reference standard; thermo	
calomel	****	••	•	•	Thermodynamic studies	
glass	••••	••	•	•••	pH measurement; potentiometric titra	
quinhydrone	****	•		••	Potentiometric studies	
metal-metal oxide and sulfide	•••	•	•••	**	Alkaline systems; high-temperature studies	
metal-metal halide	••	00	***	••	Thermodynamics of molten inorgan halides	
metal-metal sulfate	***	••		••	Thermodynamic studies	
membrane	•••	••	•	••	Membrane performance studies; co	
halogen	•	•	**	•	Molten inorganic halides	
oxygen	••	•	•	••	Oxygen tension measurement	
thiol	•	•	•	••	Biological oxidation—reduction e	

Key: **** generally applicable
*** applicable to selected systems
** occasionally suitable

· insufficiently explored and/or inapplicable

G. Janz and F. Kelly in Encyclopedia of Electrochemistry, C. Hampel, ed., Reinhold, NYC, 1964, p. 1015.

5. COMPARISON OF REFERENCE ELECTRODE POTENTIALS



Liquid Junction Potential (LJP)

- A small (few mV) potential that typically exists over regions of electrolyte with varying concentrations.
- The origin of liquid Junction potential is in diffusion and electrostatics, and it is present in cells without current passage (equilibrium), hence it lies in the border region between thermo and transport.
- The liquid junction potential is a function of the electrolyte type and the structure of the region of varying concentrations; hence it is typically a constant value for a given system.
- The determination of the LJP is complicated since it requires detailed knowledge of the concentration profile in the junction region
- LJP is always present when using reference electrodes, since those involve a concentration gradient across a salt bridge.
- LJP is of little importance to engineers. Areas where it is important are:
 - o The determination of accurate absolute equilibrium potentials
 - o Biological systems (e.g., cell membranes) that are characterized by a small potential.

Consider a two compartment cell, separated by a diaphragm.

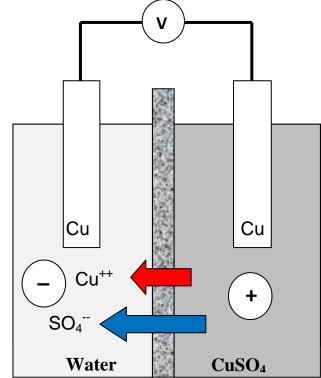
One compartment contains copper sulfate; the other water.

Clearly, Cupric and sulfate ions will diffuse From the right compartment to the left one.

However their properties are different:

Cu:
$$\lambda_{Cu} = 54$$
 $D \sim 5*10^{-6}$

SO₄:
$$\lambda_{SO4}$$
= 80 D ~ 7.4*10⁻⁶



As a consequence of the different diffusivity, the Sulfate ion will diffuse faster that the cupric ion. Since the sulfate is negatively charged, the left compartmen 4-66 ld-up a negative charge, the right one will become positive.

The different charge gives rise to a potential. The potential will now slow down the fast moving sulfate ion and will enhance (electrostatically) the transport of the slow moving copper. This potential difference which causes both ions to continue diffusing at the same speed is the LJP.

The preferred salt in salt bridges for reference electrodes is KCl. The reason being is that

$$\lambda_K \sim \lambda_{Cl}$$

Hence both ions diffuse at about the same rate, minimizing the LJP.