Assignment 03

EE 538 Spring 2020 Analog Circuits for Sensor Systems University of Washington Electrical & Computer Engineering

Due: April 25, 2020 Author: Kevin Egedy

```
In [1]: # Imports
         import os
         import sys
         import cmath
         import math
         import matplotlib.pyplot as plt
         import matplotlib
         import numpy as np
import pandas as pd
         import ltspice
         import sympy as sp
from scipy import signal
         %matplotlib inline
         from IPython.core.interactiveshell import InteractiveShell
         InteractiveShell.ast_node_interactivity = "all'
In [2]: def read_ltspice_tran(file_name):
             cols = []
             arrs = []
             with open(file_name, 'r',encoding='utf-8') as data:
    for i,line in enumerate(data):
                      if i==0:
                          cols = line.split()
                          arrs = [[] for _ in cols]
                          continue
                      parts = line.split()
                      for j,part in enumerate(parts):
                          arrs[j].append(part)
             df = pd.DataFrame(arrs,dtype='float64')
             df = df.T
             df.columns = cols
             return df
In [3]: def RoundNonZeroDecimal(num, place, rnd='ceil'):
             # Requires numpy library
                 RoundNonZeroDecimal(0.0004512,1,'floor') -> 0.0045
                RoundNonZeroDecimal(0.0004512,1,'ceil') -> 0.0046
             tmp = num # implement so that num can be array
             mag = 0
             if rnd=='ceil':
                 while(abs(tmp)<1):</pre>
                      tmp*=10
                      mag+=1
                 for i in range(place):
                      tmp*=10
                 return int(np.ceil([tmp])[0])/(10**(mag))
             if rnd=='floor':
                 while(abs(tmp)<1):</pre>
                      tmp*=10
                      mag+=1
                 for i in range(place):
                      tmp*=10
                      mag+=1
                 return int(np.floor([tmp])[0])/(10**(mag))
```

raise ValueError('Invalid argument')

return None

Problem 1: Common-emitter versus common-source amplifier

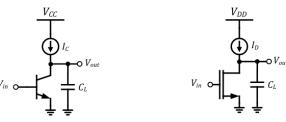


Figure 1a. Common-emitter (CE) amplifier

Figure 1b. Common-source (CS) amplifier

For the following, T = 300K, $V_A = 100$ V, $V_{GS} - V_{th} = 500$ mV, $\lambda = 0.1$ V $^{-1}$, $C_L = 10$ pF and $I_C = I_D = 1$ mA.

- a) (5 points) Calculate the DC voltage gain v_{out}/v_{in} for each structure. Determine the ratios g_m/I_C and g_m/I_D (transconductance efficiency).
- b) (5 points) For each structure, determine the small-signal transfer function v_{out}/v_{in} as a function of frequency. Plot the Bode magnitude and phase (by hand or using MATLAB/Python). For each, calculate the transit frequency f_T, the frequency at which the magnitude of the transfer function is equal to 1V/V.
- c) (5 points) The so-called "square-law" model of the FET incorrectly predicts that current becomes arbitrarily small (and g_m arbitrarily large) as $V_{GS} V_{th}$ approaches zero. For values of V_{GS} smaller than V_{th} (subthreshold operation), the drain current is better described as

$$I_D = I_S e^{V_{GS}/nV_T},$$

where I_S and n are technology parameters related to the device structure. For n=1.5, calculate the transconductance efficiency (g_m/I_D) of the FET assuming subthreshold operation. How does it compare to your answers in Part a)?

Part A

Structure A: $T=300K, V_A=100, C_L=10 \mathrm{pF}, I_C=1 \mathrm{mA}$

$$I_{C0}=I_S(e^{V_{
m BE}/V_T}-1)$$

$$I_C = I_{C0}(1 + rac{V_{CE}}{V_A}), V_A \gg V_{CE}
ightarrow I_C pprox I_{C0}$$

$$egin{aligned} ext{Find} & rac{v_{ ext{out}}}{v_{ ext{in}}} \ V_{in} &= V_{ ext{BE}} \ V_{T} &= rac{kT}{q}igg|_{T=300K} \ &= 25.86 ext{mV} \ &g_{m} &= rac{I_{CO}}{V_{T}} \ &r_{0} &= rac{V_{A}}{I_{C0}} \ &i_{C} &= g_{m}v_{ ext{be}} \end{aligned}$$

$$v_{
m out}\,=\,-\,i_c r_0=-g_m v_{
m in} r_0$$

$$egin{aligned} rac{v_{
m out}}{v_{
m in}} &= -\,g_m r_0 \ &= rac{V_A}{V_T} = -3867 \end{aligned}$$

Find transconductance efficiency $\frac{g_m}{I_C}$

$$g_m = rac{I_{C0}}{V_T} \ rac{g_m}{I_C} = rac{I_{C0}}{I_C V_T} pprox rac{1}{V_T} = 38.67 ext{V}^{-1}$$

Structure B $T=300K, C_L=10 {
m pF}, I_D=1 {
m mA}, V_{{
m GS}-V_{
m th}}=500 {
m mV}, \lambda=0.1 {
m V}^{-1}$ Given

$$I_Dpprox I_{D0}$$

Find
$$\frac{v_{\mathrm{out}}}{v_{\mathrm{in}}}$$

$$i_D \; = g_m v_{
m gs}$$

$$v_{
m out}\,=\,-\,i_D r_0=-g_m v_{
m in} r_0$$

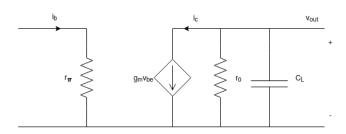
$$egin{align} rac{v_{
m out}}{v_{
m in}} &= -\,g_m r_0 \ &= rac{-2I_{D0}}{\lambda I_{D0}(V_{
m GS}-V_{
m th})} \ &= rac{-2}{\lambda(V_{
m GS}-V_{
m th})} \ &= -\,40 \ \end{array}$$

Find transconductance efficiency $\frac{g_m}{I_D}$

$$g_m = rac{2I_{D0}}{V_{
m GS} - V_{
m th}}$$

$$rac{g_m}{I_D} pprox rac{2}{V_{
m GS}-V_{
m th}} = 4 {
m V}^{-1}$$

Part B



In [4]: def parallel(Z1,Z2):
 return 1/((1/Z1)+(1/Z2))

Structure A:
$$T=300K, V_A=100, C_L=10 {
m pF}, I_C=1 {
m mA}$$
 $V_{in}=V_{
m BE}$

$$V_{in} = V_{
m BH}$$

$$i_C = g_m v_{
m be}$$

$$g_m = rac{I_{CO}}{V_T} = 0.03867$$

$$r_0 = rac{V_A}{I_{C0}} = 100000$$

$$v_{
m out}~=~-i_c r_{
m eq} = -g_m v_{
m in}(r_0 \| C_L)$$

$$rac{v_{
m out}}{v_{
m in}} \ = \ - \, g_m(r_0 \| C_L)$$

$$=\,-\,g_mrac{r_0}{1+sr_0C}$$

$$\left|rac{v_{
m out}}{v_{
m in}}
ight|=g_mrac{r_0}{\sqrt{1+(2\pi f r_0C)^2}}
ightarrow f_T=6.15\cdot 10^8{
m Hz}$$

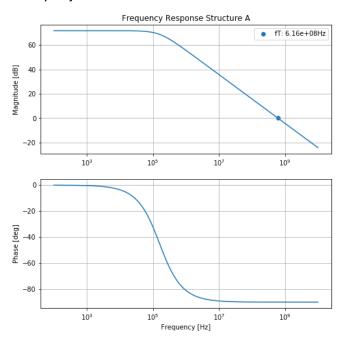
```
In [5]: f1 = np.linspace(1e2,1e6,100000)
f2 = np.linspace(1e6,1e10,100000)
             f = np.concatenate((f1,f2))
             w = 2*np.pi*f
             s = 1j*w
             gm = 0.03867
                                                   # change
             r0 = 100000
                                                    # change
             C = 10e-12
             Z_C = 1/(s*C)
             H = gm*parallel(r0,Z_C)
             #H = gm*r0/(1+s*r0*C)
             #Find fT, frequency where magnitude is 1V/V.
             mag = abs(H)
             x0 = np.where(mag<=1)[0][0]
label = "{:.2e}".format(f[x0])
print(f"fT frequency at {label}")</pre>
             # Plot the frequency response
             fig, axs = plt.subplots(2,figsize=(8,8))

axs[0].set_title('Frequency Response Structure A')

axs[0].semilogx(f, 20*np.log10(abs(H)))

axs[0].scatter(f[x0], 20*np.log10(mag[x0]),label=f"fT: {label}Hz")
             axs[0].set_ylabel('Magnitude [dB]')
             axs[0].grid()
             axs[0].legend()
             axs[1].semilogx(f, np.angle(H,deg=True),label='Ideal')
axs[1].set_ylabel('Phase [deg]')
axs[1].set_xlabel('Frequency [Hz]')
             axs[1].grid()
             #axs[1].legend()
             plt.show();
```

fT frequency at 6.16e+08



Structure B
$$T=300K, C_L=10 \mathrm{pF}, I_D=1 \mathrm{mA}, V_{\mathrm{GS-}V_{\mathrm{th}}}=500 \mathrm{mV}, \lambda=0.1 \mathrm{V}^{-1}$$
 $V_{\mathrm{in}}=V_{\mathrm{GS}}$ $i_D=g_m v_{\mathrm{gs}}$ $g_m=\frac{\partial I_D}{\partial V_{\mathrm{GS}}}=\frac{2I_{D0}}{V_{\mathrm{GS}}-V_{\mathrm{th}}}=0.004$ $r_0=\frac{1}{\lambda I_{D0}}=10000$ $v_{\mathrm{out}}=-i_D r_{\mathrm{eq}}=-g_m v_{\mathrm{in}}(r_0 \| C_L)$ $\frac{v_{\mathrm{out}}}{v_{\mathrm{out}}}=-g_m (r_0 \| C_L)$

$$egin{array}{l} rac{v_{
m out}}{v_{
m in}} &= -\,g_m(r_0\|C_L) \ \\ &= -\,g_mrac{r_0}{1+sr_0C} \end{array}$$

$$\left|rac{v_{
m out}}{v_{
m in}}
ight|=g_mrac{r_0}{\sqrt{1+(2\pi f r_0 C)^2}}
ightarrow f_T^{}~=6.36\cdot 10^7 {
m Hz}$$

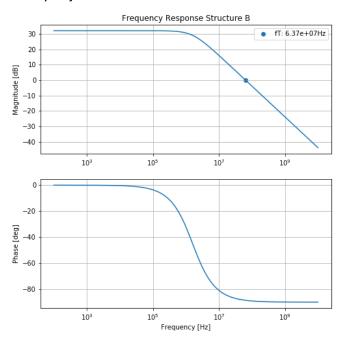
```
In [6]: f1 = np.linspace(1e2,1e6,100000)
f2 = np.linspace(1e6,1e10,100000)
              f = np.concatenate((f1,f2))
              w = 2*np.pi*f
              s = 1j*w
              gm = 0.004
                                                         # change
              r0 = 10000
                                                         # change
              C = 10e-12
              Z_C = 1/(s*C)
              H = gm*parallel(r0,Z_C)
              #H = gm*r0/(1+s*r0*C)
              #Find fT, frequency where magnitude is 1V/V.
              mag = abs(H)
             x0 = np.where(mag<=1)[0][0]
label = "{:.2e}".format(f[x0])
print(f"fT frequency at {label}")</pre>
              # Plot the frequency response
             fig, axs = plt.subplots(2,figsize=(8,8))

axs[0].set_title('Frequency Response Structure B')

axs[0].semilogx(f, 20*np.log10(abs(H)))

axs[0].scatter(f[x0], 20*np.log10(mag[x0]),label=f"fT: {label}Hz")
              axs[0].set_ylabel('Magnitude [dB]')
              axs[0].grid()
axs[0].legend()
             axs[1].semilogx(f, np.angle(H,deg=True))
axs[1].set_ylabel('Phase [deg]')
axs[1].set_xlabel('Frequency [Hz]')
              axs[1].grid()
#axs[1].legend()
              plt.show();
```

fT frequency at 6.37e+07



$$\begin{aligned} & \text{Given } I_D = 1 \text{mA}, V_{\text{GS}} - V_{\text{th}} = 500 \text{mV} \\ & \frac{g_m}{I_D} \approx \frac{2I_{D0}}{I_D(V_{\text{GS}} - V_{\text{th}})} \bigg|_{I_D = 1 \text{mA}, V_{\text{GS}} - V_{\text{th}} = 500 \text{mV}} = 4 \text{V}^{-1} \end{aligned}$$

$$\begin{split} \operatorname{Given} I_D &= I_s e^{V_{\mathrm{GS}}/nV_T} \bigg|_{n=1.5, V_T = 25.86 \mathrm{mV}} \\ g_m &= \frac{\partial I_D}{\partial V_{\mathrm{GS}}} = \frac{\partial}{\partial V_{\mathrm{GS}}} I_s e^{V_{\mathrm{GS}}/nV_T} = \frac{I_s}{nV_T} e^{V_{\mathrm{GS}}/nV_T} \\ \frac{g_m}{I_D} &= \frac{\frac{I_s}{nV_T} e^{V_{\mathrm{GS}}/nV_T}}{I_s e^{V_{\mathrm{GS}}/nV_T}} \\ &= \frac{1}{nV_T} \\ &= 25.78 \mathrm{V}^{-1} \end{split}$$

This model is $\frac{25.78}{4}=6.45 \mathrm{x}$ larger.

Problem 2: Temperature-independent voltage reference (BJT DC analysis)

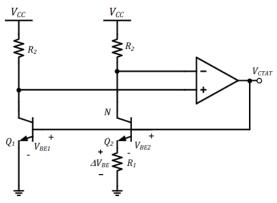


Figure 2. PTAT Voltage Generator

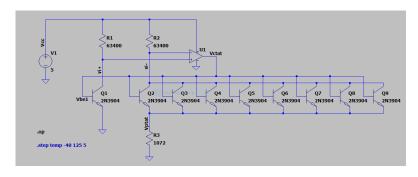
Temperature-insensitive voltage and current references are critical components of precision sensor systems. A temperature-independent reference is created by combining something (e.g. a voltage) that has a positive temperature coefficient (proportional-to-absolute-temperature, PTAT) with something that has a negative temperature coefficient (complementary-to-absolute-temperature, CTAT). When biased with a constant current, the V_{BE} of a BJT exhibits a slope of approximately -2mV/°C (CTAT). Combining this with the difference of the V_{BE} 's of two BJT's biased with different current densities (which is PTAT), properly scaled, will yield a voltage that is (approximately) independent of temperature:

$$V_{BG} = V_{CTAT} + V_{PTAT} = V_{BE}(T) + M \times \Delta V_{BE}(T)$$

Note that different current densities for Q_1 and Q_2 are achieved by connecting N transistors in parallel for Q_2 .

For the following, use the 2N3904 npn transistor ($I_S=10^{-14}$ A, $\beta=300$, $V_A=100$) and the UniversalOpamp2 models in Ltspice. Use $V_{CC}=5$ V for the supply voltage.

- a) (5 points) Determine values for N and R_I such that $I_{CI} = I_{CZ} = 50\mu\text{A}$ at room temperature (27C).
- b) (5 points) Determine the temperature slope of V_{BEI} via simulation and calculate the value of M that would satisfy the above equation.
- c) (5 points) Verify the design of the PTAT generator in Ltspice, plotting the expression $V_{BE}(T)+M\times \Delta V_{BE}(T)$ as a function of temperature. Include your schematic in your submission, showing all relevant voltages and currents at room temperature. Evaluate
 - 1. the value of $V_{\it BG}$ at room temperature, and
 - 2. the maximum deviation from this value over the temperature range –40C to 125C.



voltage	5	V(vcc)
voltage	1.829	V(vi+)
voltage	1.82901	V(vi-)
voltage	0.577333	V(vbe1)
voltage	0.0537948	V(vptat)
device_current	5.00171e-05	Ic(Q1)
device_current	1.64682e-07	lb(Q1)
device_current	-5.01817e-05	le(Q1)
device_current	5.01817e-05	I(R3)

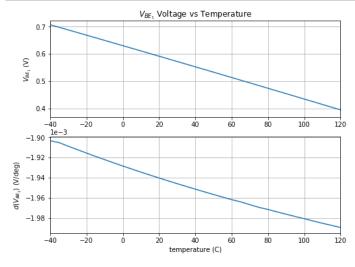
Dart A

Given:
$$I_S=10^{-14}{
m A}, \beta=300, V_A=100, V_{CC}=5, N=8$$
 Find: R_1 such that $I_{C1}=I_{C2}=50\mu{
m A}$

$$\begin{split} V_T &= \frac{kT}{q} \bigg|_{T=27C=300K} &= 25.86 \text{mV} \\ V_{\text{BE}_2} &= V_T \ln \big(\frac{I_{\text{bias}}}{NI_S} \big) \bigg|_{\text{N parallel BJTs}} \\ \Delta V_{\text{BE}} &= V_{\text{BE}_1} - V_{\text{BE}_2} \\ &= V_T [\ln \big(\frac{I_{C1}}{I_S} \big) - \ln \big(\frac{I_{C2}}{NI_S} \big)] \bigg|_{N=8} \\ &= 0.05377 \text{V} \\ I_B &= \frac{I_C}{\beta} &= \frac{50 \mu \text{A}}{300} \\ I_E &= (\beta+1)I_B &= 50.17 \mu \text{A} \\ \Delta V_{\text{BE}} &= I_E R_1 \rightarrow R_1 = \frac{\Delta V_{\text{BE}}}{I_E} \\ R_1 &= \frac{\Delta V_{\text{BE}}}{I_E} &= 1072 \Omega \\ R_2 &= \frac{V_{CC} - V_{\text{BE}_1}}{I_C} \bigg|_{V_{\text{BE}_1} = 0.578} &= 88440 \Omega \end{split}$$

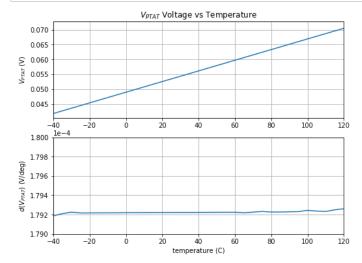
Part B

```
In [8]: fig, axs = plt.subplots(2,figsize=(8,6))
    axs[0].set_title('$V_{{BE}_1}$ Voltage vs Temperature')
    axs[0].plot(df['temperature'], df['V(vbe1)'],label='$V_{{BE}_1}$')
    axs[0].set_ylabel('$V_{{BE}_1}$ (V)')
    axs[0].set_xlim(-40, 120)
    axs[0].grid()
    #xs[0].legend()
    axs[1].plot(df['temperature'], df['d(V(vbe1))'],label='$d(V_{{BE}_1})$')
    axs[1].set_ylabel('$d(V_{{BE}_1})$ (V/deg)')
    axs[1].set_xlabel('temperature (C)')
    axs[1].set_xlim(-40, 120)
    axs[1].ticklabel_format(style='sci', axis='y', scilimits=(-2,-3))
    plt.show();
```



```
In [9]: temp = df['temperature'].to_numpy()
    x0 = np.where(temp<=27)[0][-1]
    v1 = df.iloc[x0]['d(V(vbe1))']
    print(f'Derivative value of Vbe1 at 27 Celcius is {round(le3*v1,3)}mV')</pre>
```

Derivative value of Vbel at 27 Celcius is -1.943mV



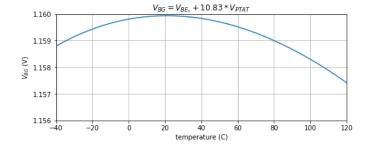
```
In [11]: v2 = df.iloc[x0]['d(V(vptat))']
    print(f'Derivative value of Vptat at 27 Celcius is {round(le3*v2,3)}mV')
```

Derivative value of Vptat at 27 Celcius is 0.179mV

```
In [12]: print(f'M = 1.943/0.179 = {round(-v1/v2,3)}')
M = 1.943/0.179 = 10.843
```

Part C

```
In [13]: fig, ax = plt.subplots(figsize=(8,3))
    ax.set_title('$V_{BG} = V_{{BE}_1}+10.83*V_{PTAT}$')
    ax.plot(df['temperature'], df['V(vbe1)+10.83*V(vptat)'],label='$V_{{BE}_1}$')
    ax.set_ylabel('$V_{BG}$ (V)')
    ax.set_ylim(1.156, 1.16)
    ax.set_xlim(-40, 120)
    ax.set_xlabel('temperature (C)')
    ax.grid()
    #ax.legend()
    plt.show();
```



```
In [14]: v3 = df.iloc[x0]['V(vbe1)+10.83*V(vptat)']
    df['delta'] = df['V(vbe1)+10.83*V(vptat)']-v3
    print(f'V_BG at 27 Celcius is {round(v3,4)}V')
    print(f'Maximum deviation is {RoundNonZeroDecimal(max(df["delta"]),4)}V')
```

V_BG at 27 Celcius is 1.1599V Maximum deviation is 4e-06V

Problem 3: Nonlinear distortion in a common-source amplifier

The output voltage of a resistor-loaded common-source amplifier is expressed (neglecting λ) as

$$V_{out} = V_{DD} - \kappa (V_{in} - V_{th})^2 R_D$$

a) (5 points) Assuming the amplifier is driven with a sinusoidal voltage $V_{in} = a_{in} \times \sin(2\pi f_0 \cdot t) + V_{DC}$ where $V_{DC} = V_{th} + 500$ mV, determine expressions for the *amplitudes* of the fundamental (sinusoid at f_0 with amplitude a_1) and second harmonic (sinusoid at $2f_0$ with amplitude a_2) using the trigonometric relationship

$$\sin^2(x) = \frac{1}{2} [1 - \cos(2x)]$$

b) (5 points) Calculate the ratio of a_2/a_1 for a_{in} = 1mV and a_{in} = 10mV.

Part A

$$\begin{split} V_{\text{out}} &= V_{DD} - \kappa (V_{\text{in}} - V_{\text{th}})^2 R_D \\ V_{\text{in}} &= a_{\text{in}} \sin \left(2\pi f t \right) + V_{DC} \bigg|_{V_{DC} = V_{\text{th}} + 500 \text{mV}} \\ V_{\text{out}} &= V_{DD} - \kappa R_D [a_{\text{in}} \sin \left(2\pi f_0 t \right) + V_{\text{th}} + 500 \text{mV} - V_{\text{th}}]^2 \\ V_{\text{out}} &= V_{DD} - \kappa R_D [a_{\text{in}} \sin \left(2\pi f t \right) + 0.5]^2 \\ &= V_{DD} - \kappa R_D [a_{\text{in}}^2 \sin^2 \left(2\pi f_0 t \right) + a_{\text{in}} \sin \left(2\pi f_0 t \right) + 0.25] \bigg|_{w = 2\pi f_0} \\ &= V_{DD} - \kappa R_D [a_{\text{in}}^2 \sin^2 \left(w t \right) + a_{\text{in}} \sin \left(w t \right) + 0.25] \\ &= V_{DD} - \kappa R_D [\frac{a_{\text{in}}^2}{2} \left(1 - \cos(2wt) \right) + a_{\text{in}} \sin \left(w t \right) + 0.25] \\ &= V_{DD} - \kappa R_D \frac{a_{\text{in}}^2}{2} + \kappa R_D \frac{a_{\text{in}}^2}{2} \cos(2wt) - \kappa R_D a_{\text{in}} \sin \left(w t \right) - \kappa R_D 0.25 \\ &= \left(V_{DD} - \kappa R_D \left(\frac{a_{\text{in}}^2}{2} + 0.25 \right) \right) - \kappa R_D a_{\text{in}} \sin \left(w t \right) + \kappa R_D \frac{a_{\text{in}}^2}{2} \cos(2wt) \right) \\ &= \text{DC} + \text{fundamental sinusioid} + 2\text{nd harmonic} \\ a_1 &= -\kappa R_D a_{\text{in}} \\ a_2 &= \kappa R_D \frac{a_{\text{in}}^2}{2} \end{split}$$

Part B

$$egin{aligned} rac{a_2}{a_1} &= rac{\kappa R_D rac{a_{
m in}^2}{2}}{-\kappa R_D a_{
m in}} &= rac{-a_{
m in}/2}{1} rac{({
m V})}{({
m V})} \ &= rac{-a_{
m in}/2}{1}igg|_{
m 1mV} &= -0.5 \cdot 10^{-3} = 0.05\% \ &= rac{-a_{
m in}/2}{1}igg|_{
m 10mV} &= -5 \cdot 10^{-3} &= 0.5\% \end{aligned}$$