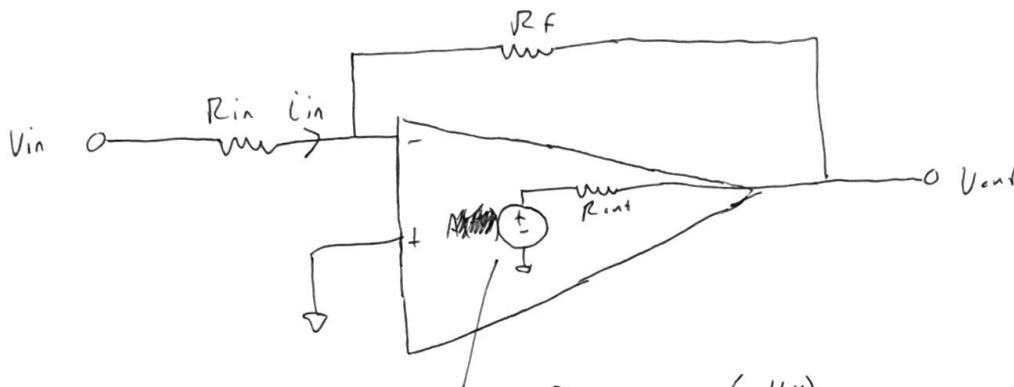


- ① f. for this question parts a and b I will just solve for a generalized transfer function first and then I can adjust  $s$  and  $A$  as necessary to get results for ~~all~~ different parts
- for a generalized transfer function, we will ~~use~~ describe the amp as follows:
- $$A(s) = \frac{A_0}{1 + \frac{s}{\omega_p}}, \quad A_0 = DC \text{ gain}, \quad \omega_p = pole \text{ frequency}$$



$$A(s) \cdot (V^+ - V^-) = A(s) \cdot (-Vx)$$

$$\frac{V_{in} - V_{out}}{R_{in} + R_f} = i_{in}, \quad V_{out} - i_{in}R_{out} = A(s)(-Vx), \quad Vx = V_{in} - i_{in}R_{in}$$

$$V_{out} - i_{in}R_{out} = A(s)(-V_{in} + i_{in}R_{in})$$

$$V_{out}(s) - \frac{V_{in}(s) - V_{out}(s)}{R_f + R_{in}} R_{out} = A(s) \left[ -V_{in}(s) + \frac{V_{in} - V_{out}}{R_f + R_{in}} R_{in} \right]$$

$$V_{out}(s) - \frac{V_{in}(s)R_{out}}{R_f + R_{in}} + \frac{V_{out}(s)}{R_f + R_{in}} R_{out} = -A(s)V_{in}(s) + \frac{A(s)R_{in}V_{in}(s)}{R_f + R_{in}} - \frac{A(s)R_{in}V_{out}(s)}{R_f + R_{in}}$$

$$(R_f + R_{in}) \left[ V_{out}(s) \left[ 1 + \frac{R_{out}}{R_f + R_{in}} + \frac{A(s)R_{in}}{R_f + R_{in}} \right] \right] = V_{in}(s) \left[ -A(s) + \frac{A(s)R_{in}}{R_f + R_{in}} + \frac{R_{out}}{R_f + R_{in}} \right]$$

$$V_{out}(s) \left[ R_f + R_{in} + R_{out} + A(s)R_{in} \right] = V_{in}(s) \left[ -A(s)(R_f + R_{in}) + A(s)R_{in} + R_{out} \right]$$

$$V_{out}(s) \left[ R_f + R_{out} + R_{in}(1 + A(s)) \right] = V_{in}(s) \left[ R_{out} - A(s)R_f \right]$$

$$\boxed{\frac{V_{out}(s)}{V_{in}(s)} = \frac{R_{out} - A(s)R_f}{R_f + R_{out} + R_{in}(1 + A(s))}}$$

(a) set  $s = 0, A_0 = \infty, R_{out} = 0$

$$\therefore A(s) = A_0 = \infty$$

$$\boxed{\frac{V_{out}}{V_{in}} = \frac{R_{out} - A_0 R_f}{R_f + R_{in}(1 + A_0)}}$$

~~as~~ as  $A \rightarrow \infty$

$$\boxed{\frac{V_{out}}{V_{in}} = \frac{-A_0 R_f}{R_{in} A_0} = -\frac{R_f}{R_{in}}}$$

$$\boxed{\frac{V_{out}}{V_{in}} = -5}$$

b) Now,  $A_o = 1000$ ,  $\omega_p = 2\pi \cdot 10^7$

$$\begin{aligned}
 \frac{V_{out}(s)}{V_{in}(s)} &= \frac{R_{out} - A(s)R_f}{R_f + R_{out} + R_{in}(1 + A(s))} \\
 &= \frac{R_{out} - \left(\frac{A_o}{1 + \frac{s}{\omega_p}}\right)R_f}{R_f + R_{out} + R_{in} + \frac{R_{in}A_o}{1 + \frac{s}{\omega_p}}} \quad | + \frac{\frac{s}{\omega_p}}{1 + \frac{s}{\omega_p}} \\
 &= \frac{R_{out}\left(1 + \frac{s}{\omega_p}\right) - A_oR_f}{(R_f + R_{out} + R_{in})\left(1 + \frac{s}{\omega_p}\right) + R_{in}A_o} \\
 &= \frac{R_{out} + \frac{R_{out}s}{\omega_p} - A_oR_f}{(R_f + R_{out} + R_{in}) + \frac{(R_f + R_{out} + R_{in})s}{\omega_p} + A_oR_{in}} \\
 &= \frac{\frac{R_{out}s}{\omega_p} + (R_{out} - A_oR_f)}{(R_f + R_{out} + R_{in})s + R_f + R_{out} + R_{in} + A_oR_{in}}
 \end{aligned}$$

To find the closed loop gain we can set  $s=0$

$$\frac{V_{out}(s=0)}{V_{in}(s=0)} = \frac{100 - 1000 \cdot 5000}{1000 + 5000 + 100 + 1000 \cdot 1000}$$

$$\frac{V_{out}(s=0)}{V_{in}(s=0)} = -4.97$$

↳ closed loop gain

Note that this is the closed-loop gain

$$\begin{aligned}
 &\boxed{\left[ \left( \frac{R_{out}}{\omega_p} \right) \left( \frac{1}{R_{out} - A_oR_f} \right) s + 1 \right] i \left( R_{out} - A_oR_f \right)} \\
 &= \boxed{\left[ \left( \frac{R_f + R_{out} + R_{in}}{\omega_p} \right) \left( \frac{1}{R_f + R_{out} + R_{in} + A_oR_{in}} \right) s + 1 \right] i \left( R_f + R_{out} + R_{in} + A_oR_{in} \right)}
 \end{aligned}$$

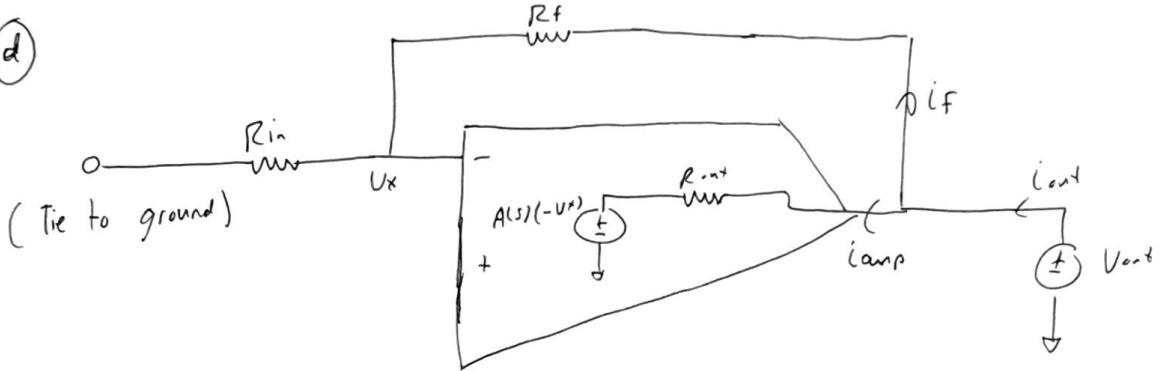
$$\begin{aligned}
 \omega_z^1 &= \frac{(\omega_p)(R_{out} - A_oR_f)}{R_{out}} \\
 &= \frac{(2\pi \cdot 10^7)(100 - 1000 \cdot 5000)}{100} = -3.14 \cdot 10^{12} \frac{\text{rad}}{\text{sec}}
 \end{aligned}$$

$$\begin{aligned}
 \omega_p^1 &= \frac{(\omega_p)(R_f + R_{out} + R_{in} + A_oR_{in})}{R_f + R_{out} + R_{in}} = \\
 &= \frac{(2\pi \cdot 10^7)(1000 + 100 + 5000 + 1000 \cdot 1000)}{1000 + 100 + 500} = 10.36 \cdot 10^9 \frac{\text{rad}}{\text{sec}}
 \end{aligned}$$

$$\frac{V_{out}(s)}{V_{in}(s)} = \frac{\left( \frac{-s}{3.14 \cdot 10^{12}} + 1 \right)}{\left( \frac{s}{10.36 \cdot 10^9} + 1 \right)} (-4.97)$$

c) fractional error =  $\left| \frac{-5 + 4.97}{5} \right| = \frac{0.03}{5} = 0.006 = 0.6\%$

(d)



$$\frac{V_x(s)}{V_{out}(s)} = \frac{V_{out}(s) \cdot R_{in}}{R_{in} + R_f}$$

$$i_f^{(s)} = \frac{V_{out}(s) \cdot \cancel{R_{in}}}{R_{in} + R_f}$$

$$V_{out}(s) - i_{amp} R_{out} = A(s)(-V_x)$$

$$V_{out}(s) - i_{amp} R_{out} = A(s) \left( \frac{-V_{out} \cdot R_{in}}{R_{in} + R_f} \right)$$

$$V_{out}(s) \left[ 1 + A(s) \frac{R_{in}}{R_{in} + R_f} \right] = i_{amp} R_{out}$$

$$\frac{V_{out}(s)}{R_{out}} \left[ 1 + \frac{A(s) R_{in}}{R_{in} + R_f} \right] = i_{amp}(s)$$

Output resistance

$$R_{out}^* = \frac{V_{out}(s)}{i_{out}(s)}, \quad i_{out}(s) = i_f(s) + i_{amp}(s)$$

$$= \frac{V_{out}(s)}{\frac{V_{out}(s) R_{in}}{R_{in} + R_f} + \frac{V_{out}(s)}{R_{out}} \left[ 1 + \frac{A(s) R_{in}}{R_{in} + R_f} \right]} \cdot \frac{R_{in} + R_f}{R_{in} + R_f}$$

$$= \frac{\frac{R_{in} + R_f}{R_{in} + R_f R_{in}}}{\frac{R_{in} + R_f}{R_{in} + R_f R_{in}}} + \frac{\frac{R_{in} + R_f + A(s) R_{in}}{R_{in} + R_f}}{\frac{R_{in} + R_f}{R_{in} + R_f}}$$

$$= \frac{(R_{in} + R_f)(R_{out})}{R_{out} + R_{in} + R_f + A(s) R_{in}}$$

$$= \frac{(100 + 5000)(100)}{100 + 1000 + 5000 + 1000 \cdot 1000}$$

$$= 0.596 \Omega$$

Output  
impedance

Problem 2.

$$(a) \quad A(s) = \frac{A_0}{(1 + \frac{s}{\omega_0})}$$

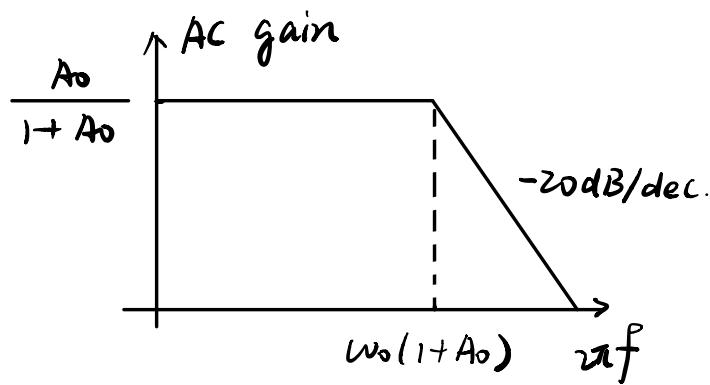
$$\text{loop gain} = A(s) \quad \text{So} \quad V_{out}/V_{in} = \frac{A(s)}{1 + A(s)}$$

$$\text{or } \beta = 1$$

$$= \frac{A_0}{(1 + \frac{s}{\omega_0}) + A_0}$$

$$= \frac{A_0 / (1 + A_0)}{1 + \frac{s}{(1 + A_0)\omega_0}}$$

Thus the pole is modified as  $(1 + A_0)\omega_0$ , but the gain is also modified as  $A_0 / (1 + A_0) \approx 1$



$$\text{loop gain} = \frac{1}{10} A(s)$$

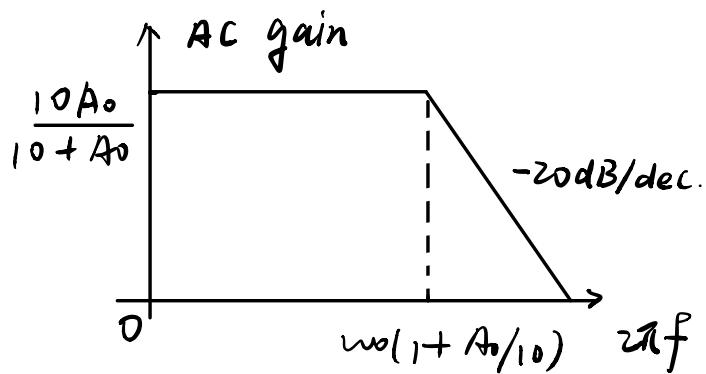
$$(b) \quad \frac{V_{out}}{V_{in}} = \frac{A(s)}{1 + \beta A(s)} = \frac{A_0 / (1 + \frac{s}{\omega_0})}{1 + 1/10 \cdot A_0 / (1 + s/\omega_0)}$$

$$= \frac{A_0}{(1 + s/\omega_0) + 1/10 \cdot A_0}$$

$$= \frac{A_0}{A_0/10 + 1 + s/\omega_0}$$

$$= \frac{A_0 / (1 + A_0/10)}{1 + s/\omega_0(1 + A_0/10)}$$

Bode plot see the next page.



$$\begin{aligned}
 (c) \quad \text{loop gain} &= \frac{1/Cs}{R + \frac{1}{Cs}} \cdot A(s) \\
 &= \underbrace{\frac{1}{Rcs + 1} A(s)}_{A(s)} \\
 \text{gain} &= \frac{A(s)}{1 + \frac{1}{Rcs + 1} A(s)} \\
 &= \frac{A_0 / (1 + \frac{s}{\omega_0})}{1 + \frac{1}{Rcs + 1} A_0 / (1 + \frac{s}{\omega_0})} \\
 &= \frac{A_0 (Rcs + 1)}{(Rcs + 1) (\frac{s}{\omega_0} + 1) + A_0} \quad \text{denote } \frac{1}{Rc} = \omega_1 \\
 &= \frac{\left(\frac{s}{\omega_1} + 1\right)}{\frac{1}{A_0} \frac{s}{\omega_1} \cdot \frac{s}{\omega_0} + \frac{1}{A_0} \left(\frac{s}{\omega_1} + \frac{s}{\omega_0}\right) + \frac{A_0 + 1}{A_0}}
 \end{aligned}$$

Let the denominator = 0.

$$\frac{1}{(A_0 + 1) \omega_0 \omega_1} s^2 + \frac{\omega_0 + \omega_1}{(A_0 + 1) \omega_0 \omega_1} s + 1 = 0$$

One can use the dominant pole approximation - so that the coefficient of  $s$  is roughly  $1/w_p$ ,

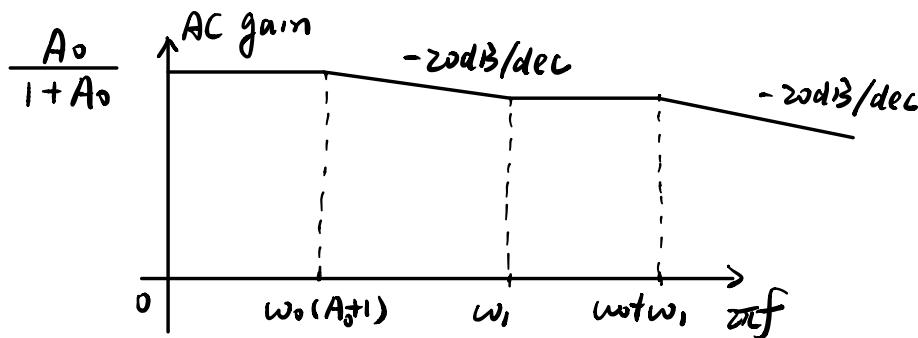
$$\therefore \begin{cases} \frac{1}{w_{p_1}} = \frac{\omega_0 + \omega_1}{(A_0+1)\omega_0\omega_1} \Rightarrow w_{p_1} = \frac{(A_0+1)\omega_0\omega_1}{\omega_0 + \omega_1}, \\ \frac{1}{w_{p_1} w_{p_2}} = \frac{1}{(A_0+1)\omega_0\omega_1} \Rightarrow w_{p_2} = \omega_0 + \omega_1, \end{cases}$$

Assume  $\omega_0 \ll \omega_1$ ,

Note  $w_{p_1} \ll w_{p_2}$

$$\begin{cases} w_{p_1} = \frac{(A_0+1)\omega_0}{1 + \frac{\omega_0}{\omega_1}} \approx (A_0+1)\omega_0 \\ w_{p_2} \approx \omega_1 + \omega_0. \end{cases}$$

We need to make sure that  $(A_0+1)\omega_0 \ll \omega_1 + \omega_0$   
so that our approximation is valid.



A more exact solution:

$$\Rightarrow w_{p_{1,2}} = \frac{-\left(\frac{1}{\omega_0} + \frac{1}{\omega_1}\right) \pm \sqrt{\left(\frac{1}{\omega_0} + \frac{1}{\omega_1}\right)^2 - 4(A_0+1)\frac{1}{\omega_0\omega_1}}}{2\frac{1}{\omega_0\omega_1}}$$

Since we use the notation  $(1 + \frac{s}{\omega})$ ,

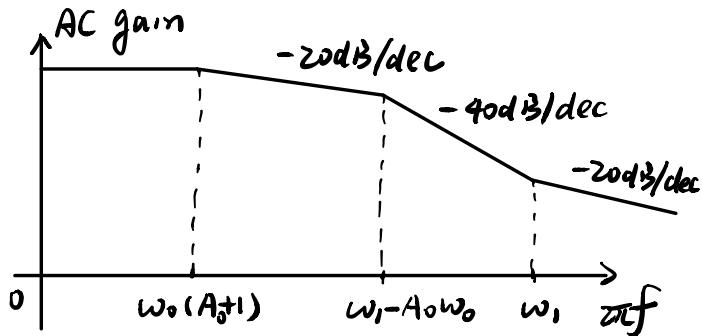
$$w_{p_{1,2}} = -\omega_{1,2}$$

$$\left(\frac{1}{\omega_0} + \frac{1}{\omega_1}\right) \pm \sqrt{\left(\frac{1}{\omega_0} + \frac{1}{\omega_1}\right)^2 - 4(A_0+1)\frac{1}{\omega_0\omega_1}}$$

$$\begin{aligned}
 &= \frac{\omega_0 + \omega_1 - \sqrt{\omega_0 \cdot \omega_1} \pm \sqrt{(\omega_0 \cdot \omega_1)^2 - 4(A_0+1)\omega_0\omega_1}}{2} \\
 &= \frac{(\omega_0 + \omega_1) \pm \sqrt{(\omega_0 + \omega_1)^2 - 4(A_0+1)\omega_0\omega_1}}{2}
 \end{aligned}$$

let's consider the case where  $\omega_1 \gg \omega_0$ .

$$\begin{aligned}
 &\approx \frac{(\omega_0 + \omega_1) \pm \omega_1 \sqrt{(\omega_0/\omega_1 + 1)^2 - 4(A_0+1)\omega_0/\omega_1}}{2} \\
 &\approx \frac{(\omega_0 + \omega_1) \pm \omega_1 \sqrt{2(\omega_0/\omega_1) + 1 - 4(A_0+1)\omega_0/\omega_1}}{2} \\
 &\approx \frac{(\omega_0 + \omega_1) \pm [\omega_1 - (2A_0+1)\omega_0]}{2} \\
 &= \omega_1 - A_0\omega_0 \quad \text{or} \quad (A_0+1)\omega_0
 \end{aligned}$$



Note also that this topology adds a zero at  $\omega_1 = \frac{1}{RC}$

