

EE 332: Devices and Circuits II

Lecture 7: Feedback

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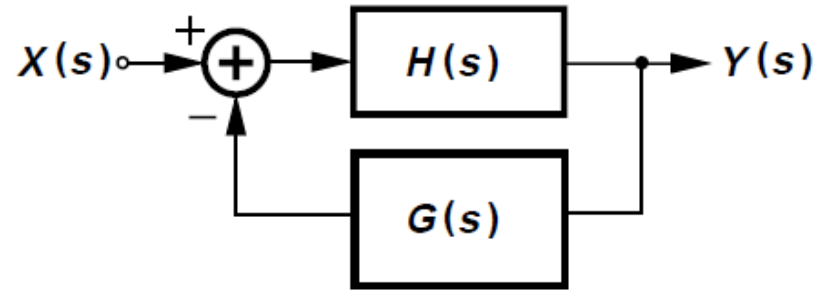
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Feedback Systems

- Feedback Examples?
- Positive vs. Negative Feedback

General Considerations



- Above figure shows a negative feedback system
- H : Feedforward network & G : Feedback network
- Feedback error is given by $X(s) - G(s)Y(s)$

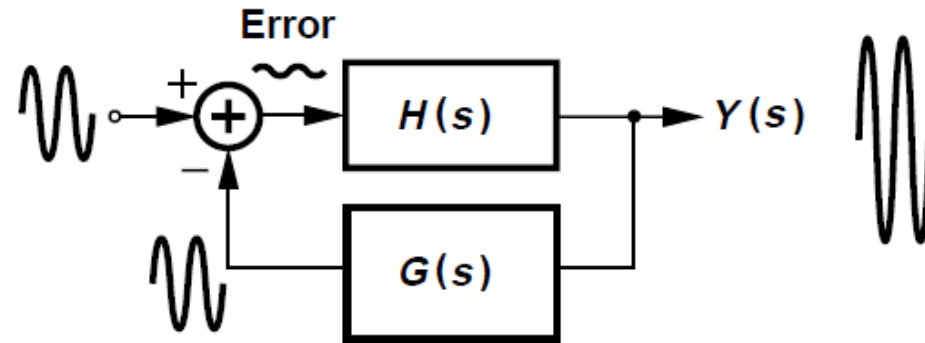
$$Y(s) = H(s)[X(s) - G(s)Y(s)]$$

- Thus

$$\frac{Y(s)}{X(s)} = \frac{H(s)}{1 + G(s)H(s)}$$

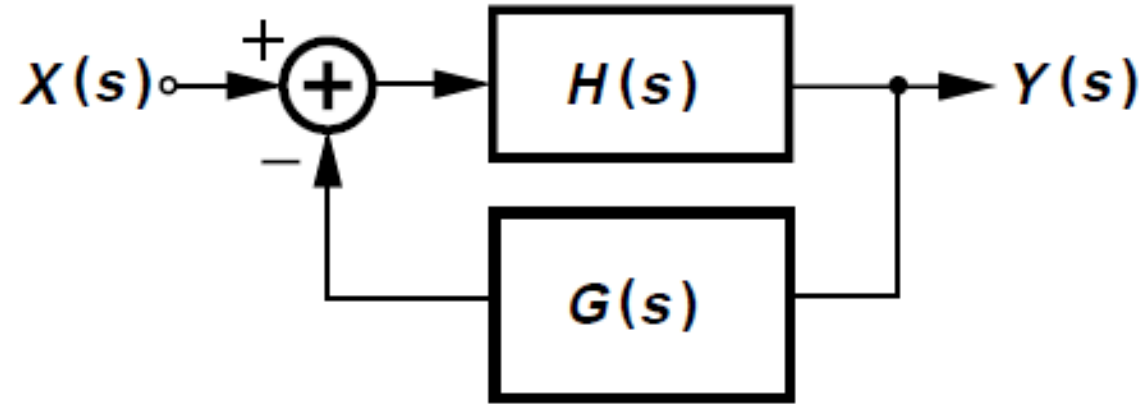
- $H(s)$ is called the “open-loop” transfer function, $Y(s)/X(s)$ is called the “closed-loop” transfer function, and $G(s)H(s)$ is the “loop-gain”

General Considerations



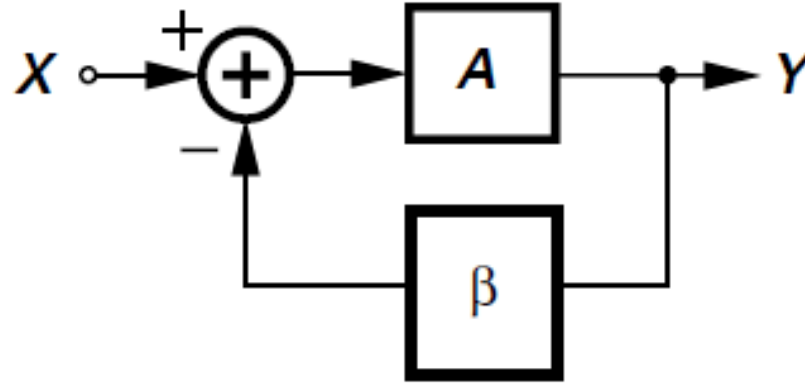
- In most cases, $H(s)$ represents an amplifier and $G(s)$ is a frequency-independent quantity
- In a well-designed negative feedback system, the error term is minimized, making the output of $G(s)$ an “accurate” copy of the input and hence the output of the system a faithful (scaled) replica of the input
- In subsequent developments, $G(s)$ is replaced by a frequency-independent quantity β called the *feedback factor*

General Considerations



- Four elements of a feedback system
 - The feedforward amplifier
 - A means of sensing the output
 - The feedback network
 - A means of generating the feedback error, i.e., a subtractor (or an adder)

Properties of Feedback Circuits

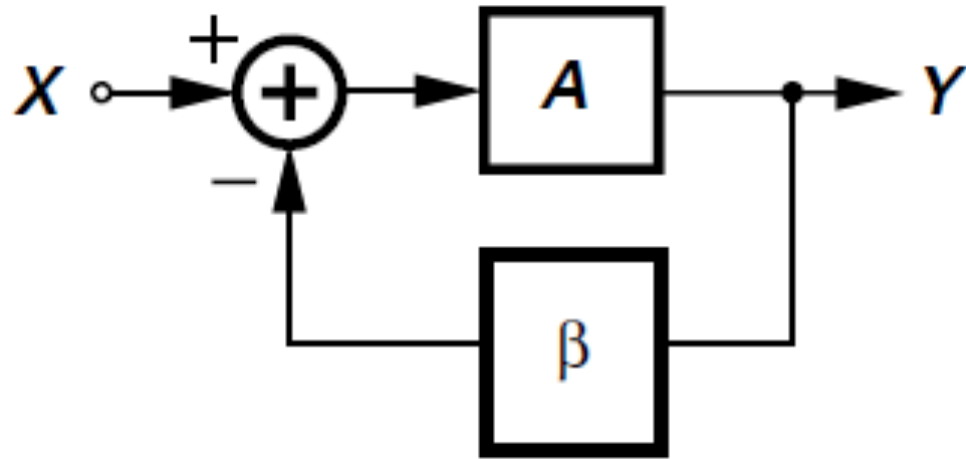


- For a more general case, gain desensitization is quantified by writing

$$\begin{aligned}\frac{Y}{X} &= \frac{A}{1 + \beta A} \\ &\approx \frac{1}{\beta} \left(1 - \frac{1}{\beta A} \right)\end{aligned}$$

- It is assumed $\beta A \gg 1$; even if open-loop gain A varies by a factor of 2, Y/X varies by a small percentage since $1/(\beta A) \ll 1$

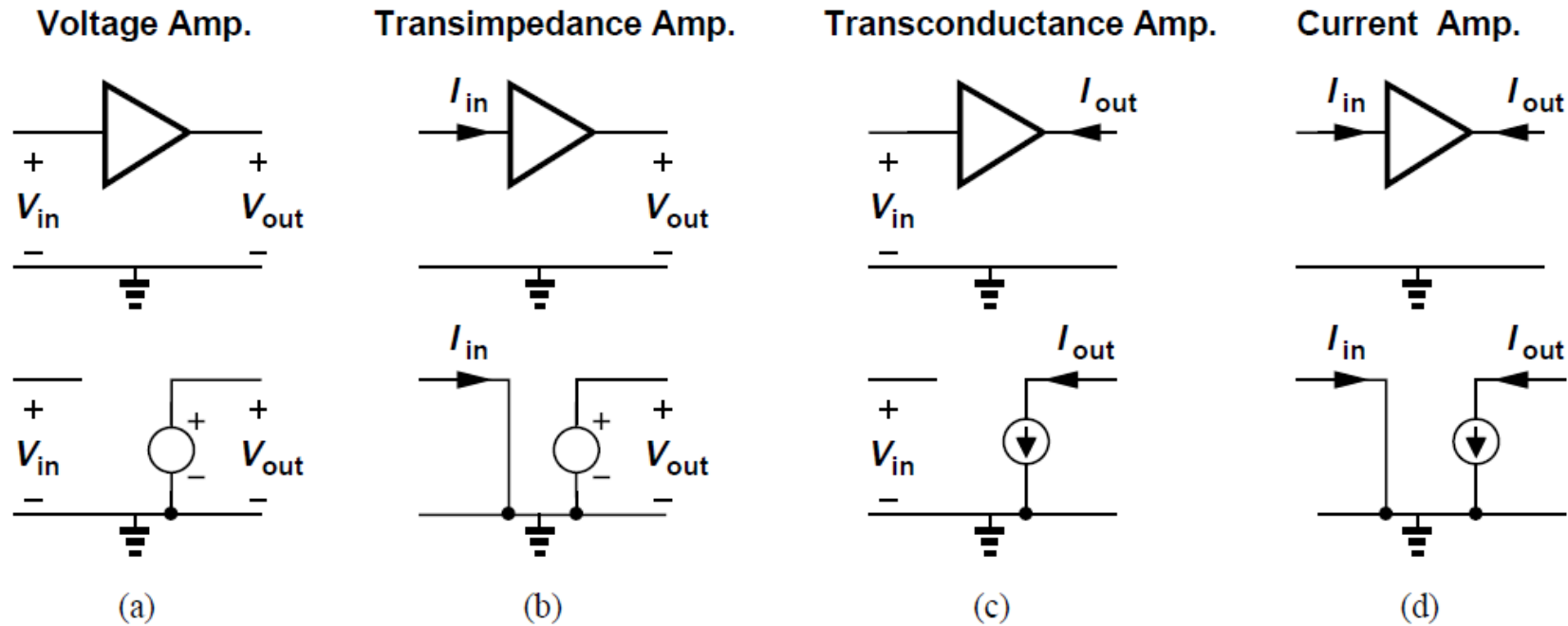
Properties of Feedback Circuits



- The quantity βA is called the “loop gain”
- The output of the feedback network is equal to $\beta Y = X \cdot \beta A / (1 + \beta A)$ approaching X as βA becomes much greater than unity

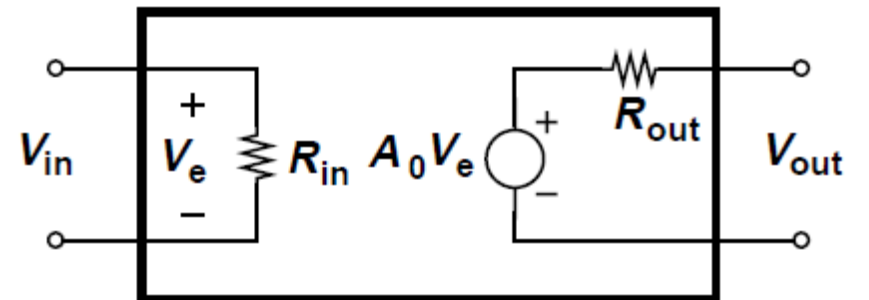
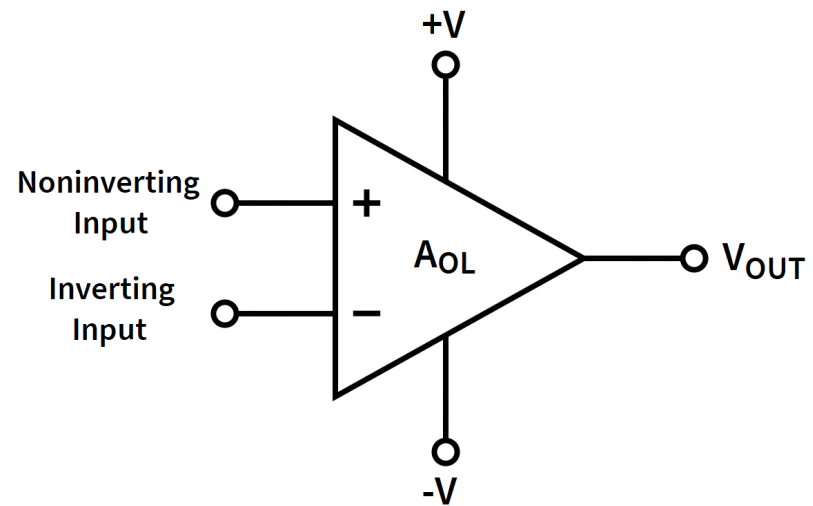
Types of Amplifiers

- Four possible amplifier configurations depending on whether the input and output signals are voltage or current quantities



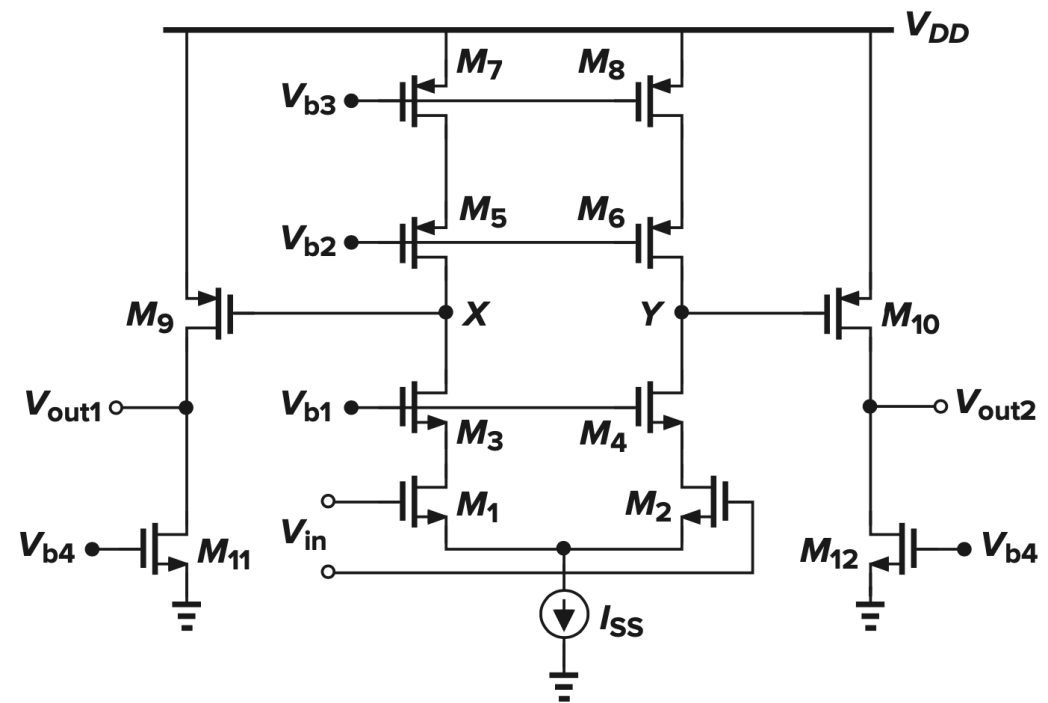
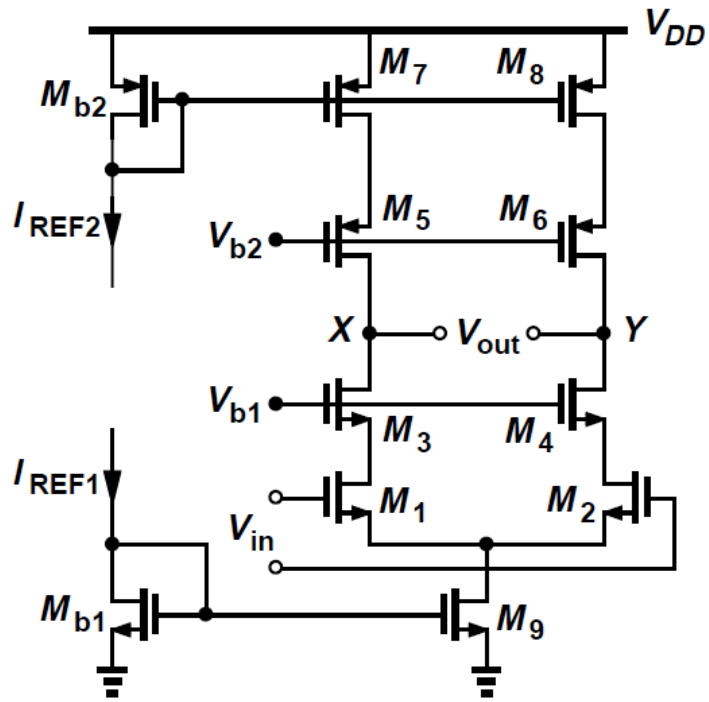
- Figs. (a) – (d) show the four amplifier types with the corresponding idealized models

OpAmp



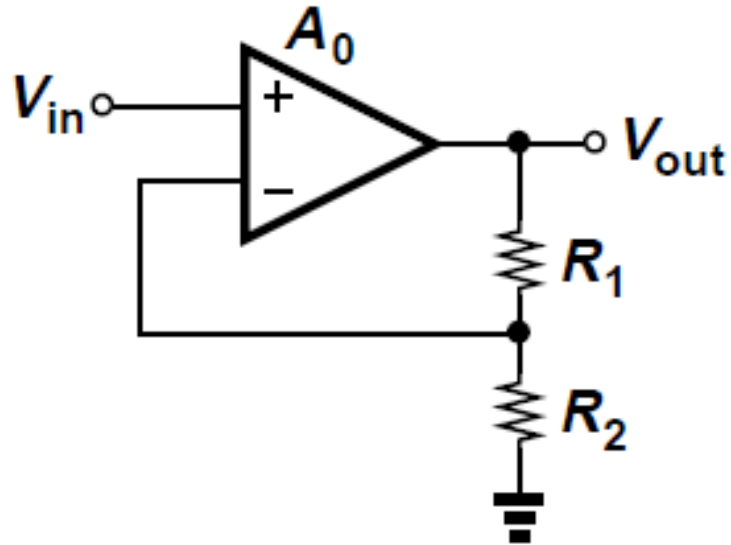
OpAmp

- **Providing large-gain by:**
 - Cascoding technique
 - Cascading multiple stages
 - etc.



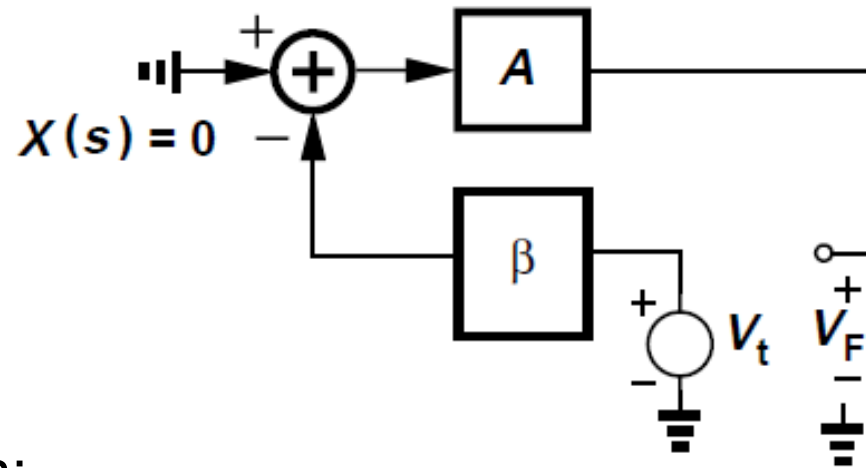
Properties of Feedback Circuits

- **Gain Desensitization:** (Non-inverting feedback amplifier example)



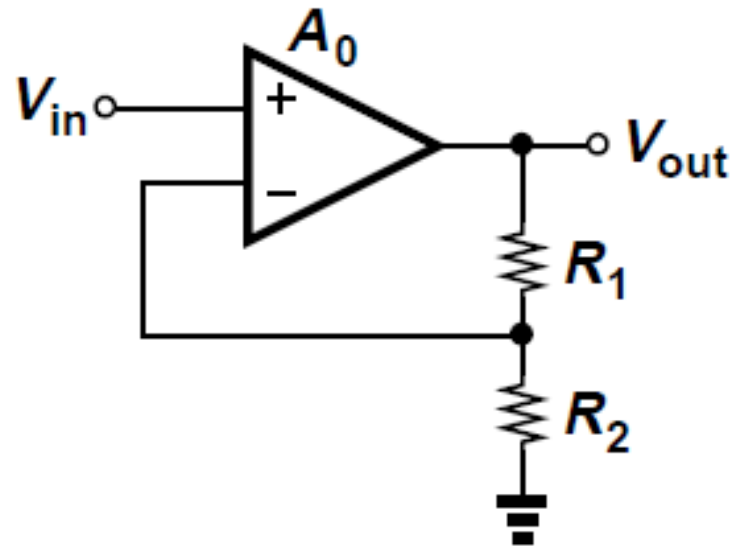
- Gain can be controlled with higher accuracy unaffected by PVT variations
- Closed-loop gain is less sensitive to device parameters than the open-loop gain, hence called “gain desensitization”

Calculation of Loop Gain



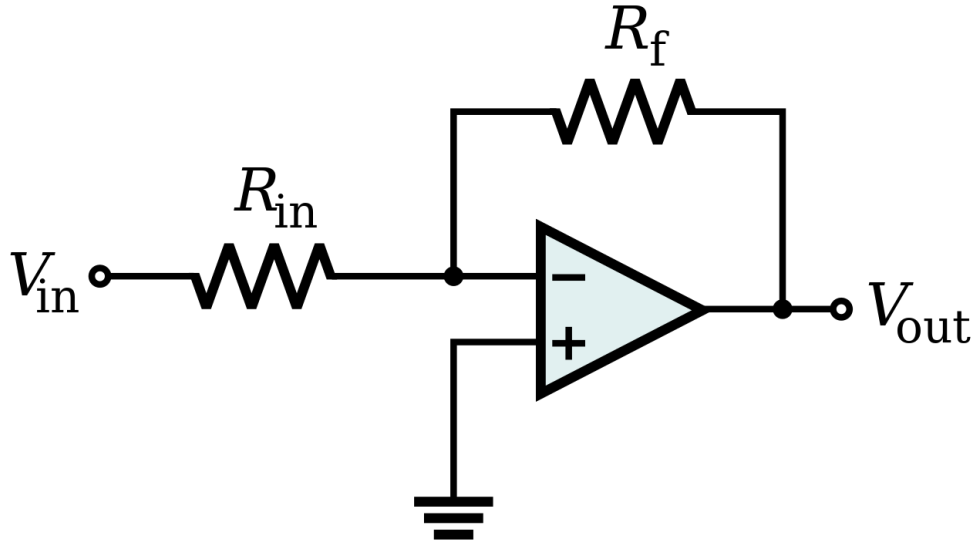
- To calculate the loop gain:
 - Set the main input to (ac) zero
 - Inject a test signal in the “right” direction
 - Follow the signal around the loop and obtain the value that returns to the break point
 - Negative of the transfer function thus obtained is the loop gain
- Loop gain is a dimensionless quantity
- In above figure, $V_t \beta (-1) A = V_F$ and hence $V_F / V_t = -\beta A$

Calculation of Loop Gain: Example



Calculation of Loop Gain: Example

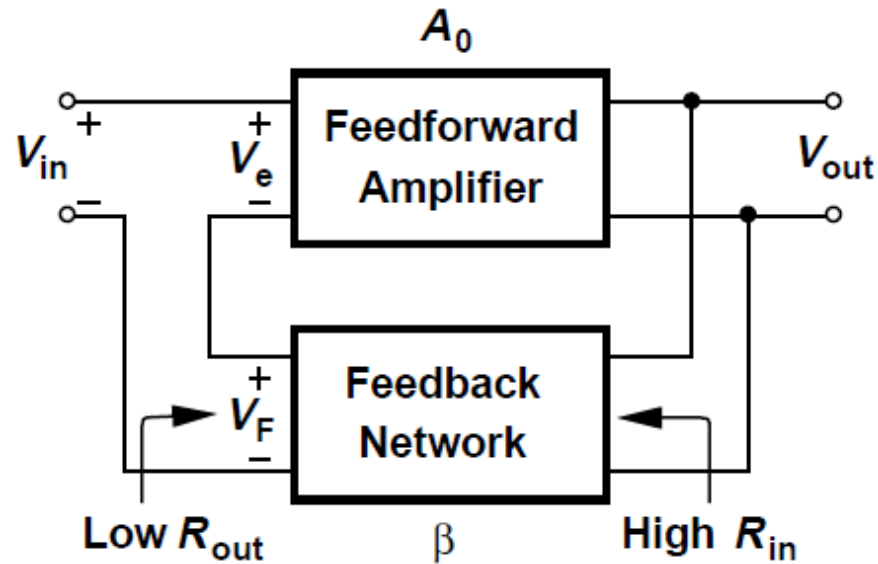
(inverting feedback amplifier example)



Sense and Return Mechanisms

- Placing a circuit in a feedback loop requires sensing an output signal and returning a fraction of it to the summing node at the input
- Four types of feedback:
 - Voltage-Voltage (*We only cover this type in our lecture, Sec. 8.2.1*)
 - Voltage-Current
 - Current-Current
 - Current-Voltage
- **First term is the quantity sensed at the output, and the second term is the type of signal returned to the input**

Voltage-Voltage Feedback

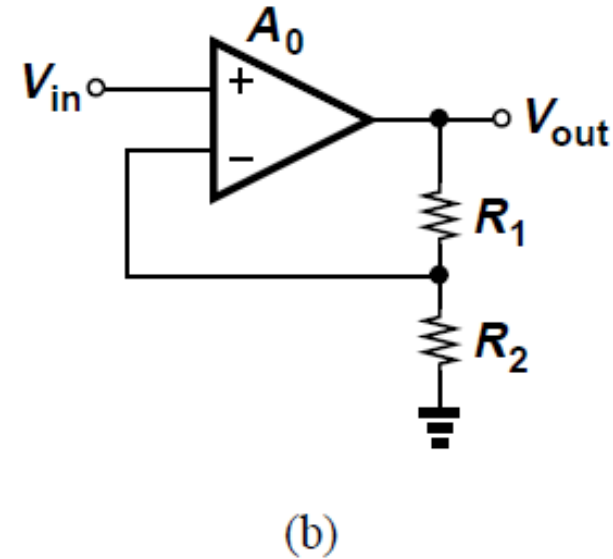
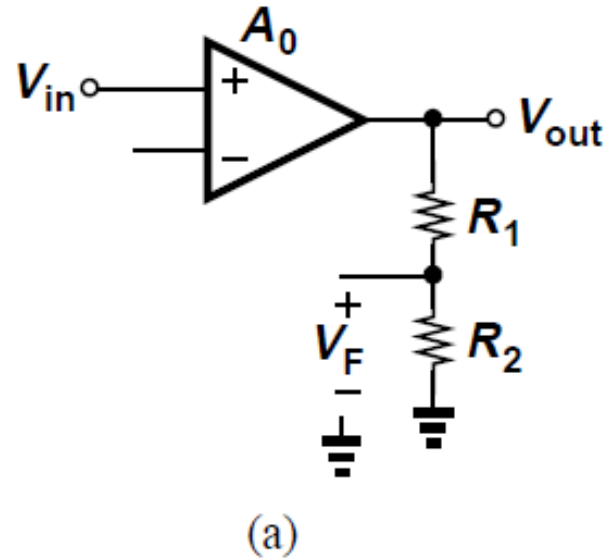


- Also called “series-shunt” feedback; first term refers to the *input* connection and second to the *output* connection
- We can write $V_F = \beta V_{out}$, $V_e = V_{in} - V_F$, $V_{out} = A_0(V_{in} - \beta V_{out})$, and hence

$$\frac{V_{out}}{V_{in}} = \frac{A_0}{1 + \beta A_0}$$

- βA_0 is the loop gain and the overall gain has dropped by $1 + \beta A_0$

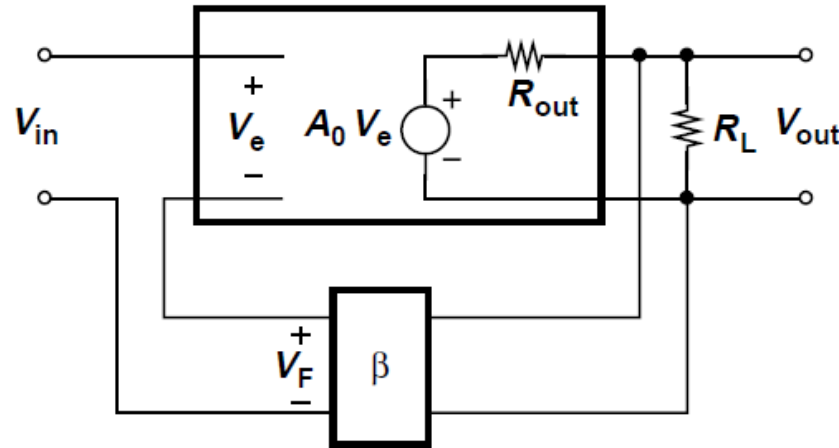
Voltage-Voltage Feedback



- As an example of voltage-voltage feedback, a differential voltage amplifier with single-ended output can be used as the forward amplifier and a resistive divider as the feedback network [Fig. (a)]
- The sensed voltage V_F is placed in series with the input to perform subtraction of voltages

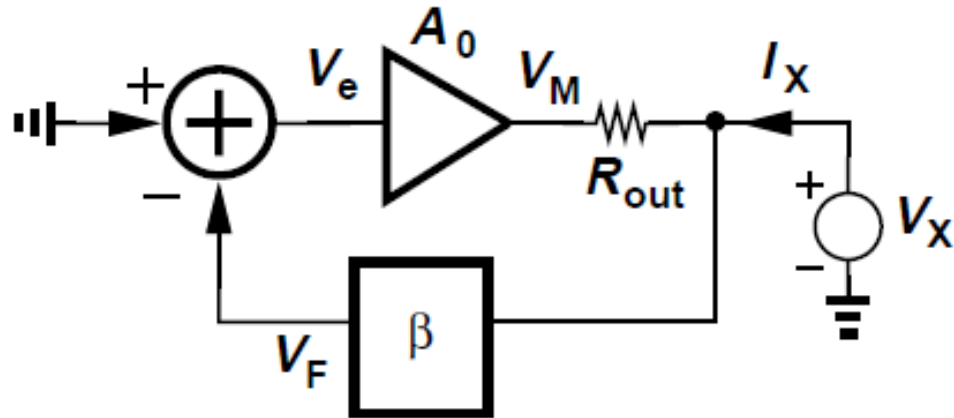
Properties of Feedback Circuits

- Terminal Impedance Modification (output impedance)



- If output is loaded by resistor R_L , in open-loop configuration, output decreases in proportion to $R_L/(R_L + R_{out})$
- In closed-loop V_{out} is maintained as a constant replica of V_{in} regardless of R_L as long as loop gain is much greater than unity
- Circuit “stabilizes” output voltage despite load variations, behaves as a voltage source and exhibits low output impedance

Voltage-Voltage Feedback: Output Resistance

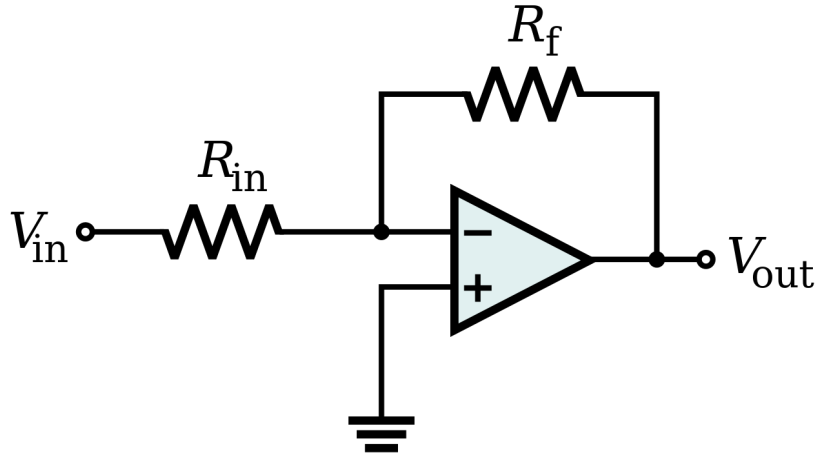


- In the above model, R_{out} represents the output impedance of the amplifier
- Setting input to zero and applying a voltage at the output, we write $V_F = \beta V_X$, $V_e = \beta V_X$, $V_M = \beta A_0 V_X$ and hence $I_X = [V_X - (-\beta A_0 V_X)]/R_{out}$ (*if current drawn by feedback network is neglected)

$$\frac{V_X}{I_X} = \frac{R_{out}}{1 + \beta A_0}$$

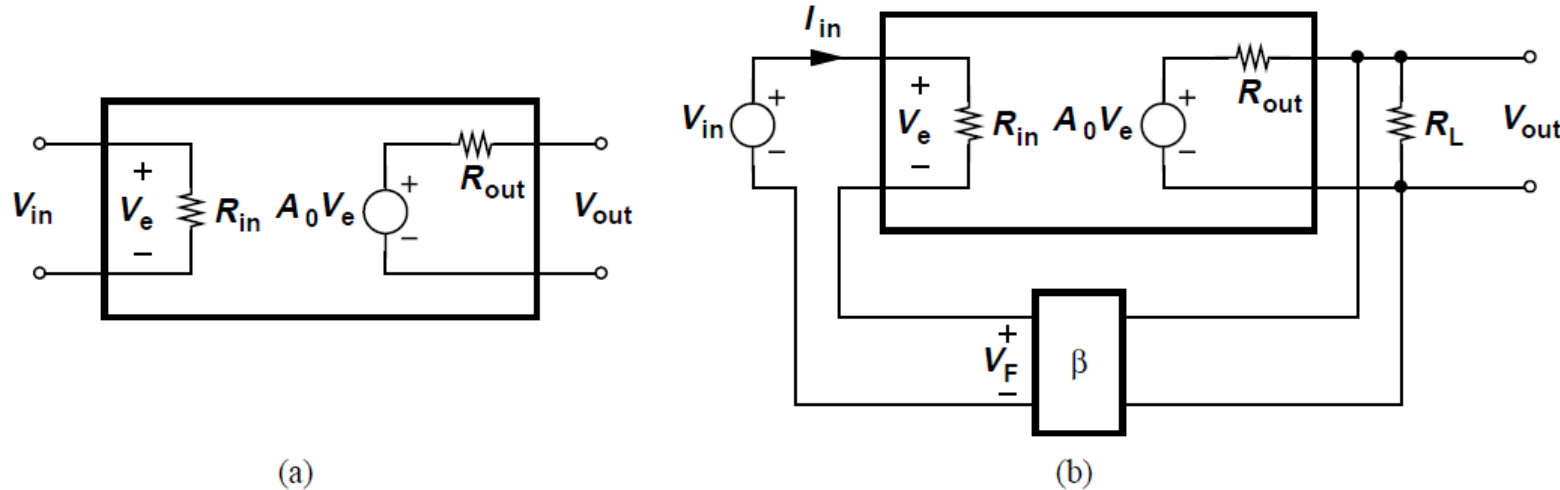
- Output impedance and gain are lowered by the same factor

Calculation of Output Impedance: Example



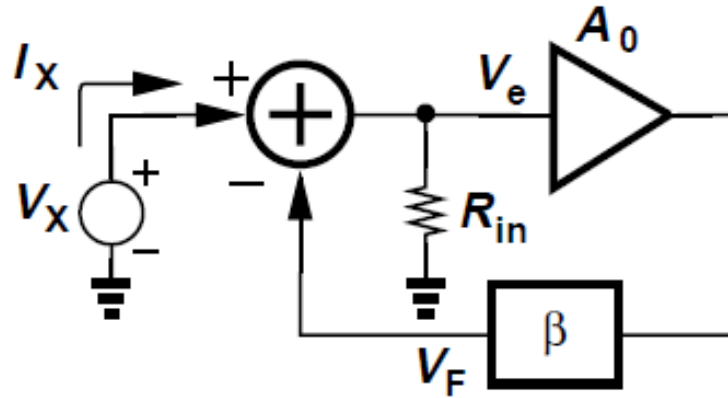
Properties of Feedback Circuits

- Terminal Impedance Modification (input impedance)



- Voltage-voltage feedback also modifies input impedance
- In Fig. (a) [open-loop], R_{in} of the forward amplifier sustains the entire V_{in} , whereas only a fraction in Fig. (b) [closed-loop]
- I_{in} is less in the feedback topology compared to open-loop system, suggesting increase in the input impedance

Voltage-Voltage Feedback: Input Resistance



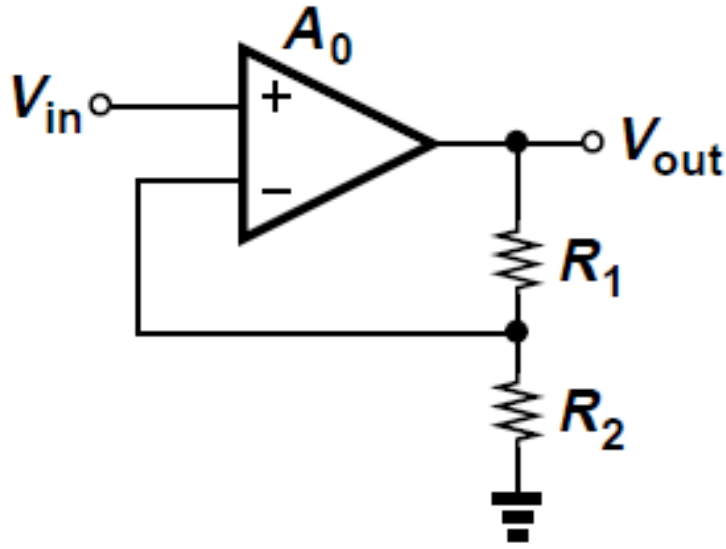
- $V_e = I_X R_{in}$ and $V_F = \beta A_0 I_X R_{in} \Rightarrow V_e = V_X - V_F = V_X - \beta A_0 I_X R_{in}$
- Hence, $I_X R_{in} = V_X - \beta A_0 I_X R_{in}$ and

$$\frac{V_X}{I_X} = R_{in}(1 + \beta A_0)$$

- Input impedance increases by the factor $1 + \beta A_0$, bringing the circuit closer to an ideal voltage amplifier
- Voltage-voltage feedback decreases output impedance and increases input impedance, useful as a buffer stage

Properties of Feedback Circuits

- Terminal Impedance Modification

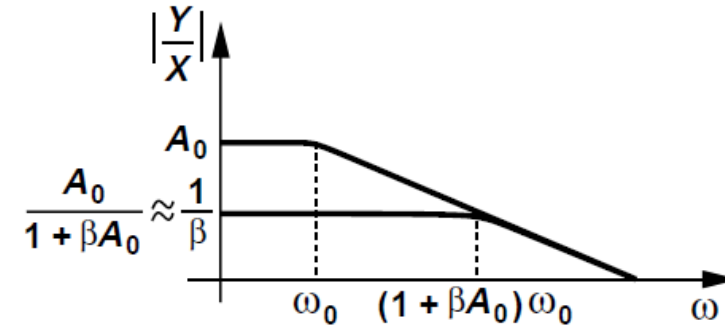
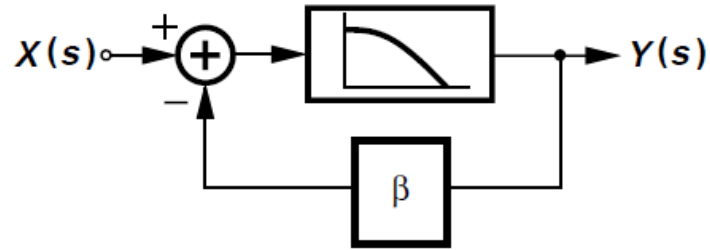


Feedback modifies input & output impedances (by a factor of $1 + \beta A$)

- increase or decrease of impedances depend on the feedback type
 - Feedback always improves the impedance ...

Properties of Feedback Circuits

- Bandwidth Modification:**



- Suppose the feedforward amplifier above has a one-pole transfer function with A_0 as the low-frequency gain and ω_0 as the 3-dB bandwidth

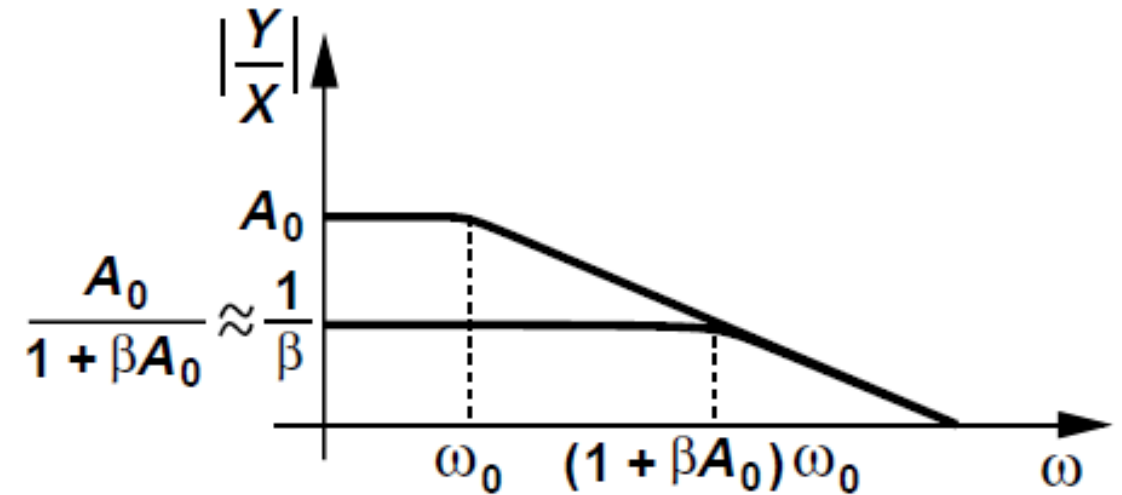
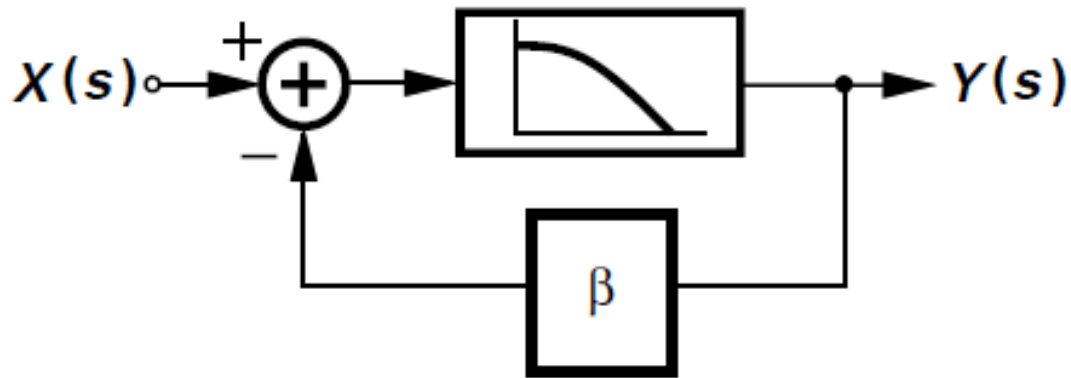
$$A(s) = \frac{A_0}{1 + \frac{s}{\omega_0}}$$

- Transfer function of the closed-loop system is

$$\frac{Y}{X}(s) = \frac{\frac{A_0}{1 + \frac{s}{\omega_0}}}{1 + \beta \frac{A_0}{1 + \frac{s}{\omega_0}}} = \frac{A_0}{1 + \beta A_0 + \frac{s}{\omega_0}} = \frac{\frac{A_0}{1 + \beta A_0}}{1 + \frac{s}{(1 + \beta A_0)\omega_0}}$$

Properties of Feedback Circuits

- Bandwidth Modification:



- The closed-loop gain at low frequencies is reduced by a factor of $1 + \beta A_0$, and the 3-dB bandwidth is increased by the same factor, revealing a pole at $(1 + \beta A_0)\omega_0$.
- If A is large enough, closed-loop gain remains approximately equal to $1/\beta$
- At high frequencies, A drops so that βA is comparable to unity and closed-loop gain falls below $1/\beta$

Properties of Feedback Circuits

- Bandwidth Modification:

