

Homework5 Solution

November 13, 2022

1 Problem 1

1.1 a

To find the max output swing, we have
M2:

$$\begin{aligned} V_b - V_{TH} &< V_{OUT} \\ V_b &> V_x + V_{TH} \end{aligned}$$

M1:

$$\begin{aligned} V_{in} - V_{TH} &< V_x \\ V_{in} &> V_{TH} \end{aligned}$$

$\Rightarrow V_{max} = V_{DD}$ AND $V_{min} = V_{OD1} + V_{OD2}$

Assume the V_{OUT} is in the middle of the swing.

$$V_{OUT} = \frac{V_{DD}}{2} + \frac{V_{OD1}}{2} + \frac{V_{OD2}}{2}$$

That means to maximize the output swing, we should find $\frac{V_{OD1}}{2} + \frac{V_{OD2}}{2} \rightarrow \min$

$$A_v = g_m 1 g_m 2 (r_o)^2 = (r_o)^2 \frac{(I_D)^2 * 4}{V_{OD1} V_{OD2}}$$

And

$$r_0 = \frac{1}{\lambda I_D} = \frac{1}{0.2 * 1 \times 10^{-3}} = 5000\Omega$$

We can get the product of V_{OD1} and V_{OD2} , which is 0.0625, also, $x + y \geq 2\sqrt{xy} = 0.5$
Hence, we can choose the $V_{GS} - V_{TH} = 0.25V$ for each transistor.

1.2 b

If $V_{OD1} = 0.25V$ and $V_{OD2} = 0.25V$

$$g_m = \frac{2I_d}{V_{OD}} = \frac{2 * 1 * 10^{-3}}{0.25V} = 0.008$$

Also

$$g_m = \mu_n C_{ox} (W/L) (V_{GS} - V_{TH}) (1 + \lambda V_{DS})$$

and as section A shows, $V_x = 0.375$

We can get $\frac{W}{L} \approx 306$

1.3 c

For M1:

$$V_{OD1} = V_{GS} - V_{TH}$$

$$\Rightarrow V_{GS} = V_{IN} = 0.55V$$

For M2:

$$V_{OD2} = V_{GS} - V_{TH}$$

$$V_{OD2} = V_b - V_x - V_{TH}$$

and as section A shows, $V_x = 0.375$, we can get $V_b = 0.925V$ And the maximum swing is from 0.5V to 1V

1.4 d

$$V_{out, \min} = 1 - 0.3 - 0.25 + 0.25 = 0.7 \text{ V}$$

Swing: $\frac{1-0.7}{2} = 0.15 \text{ V}$

1.5 e

The bias current remains at 1mA, for this PMOS $gm_p = \frac{2I_D}{V_{OD}} = 0.02$

$$g_m = \mu_p C_{ox} \frac{W}{L} V_{OD}$$

We can know $\frac{W}{L} = 4000$

For NMOS:

$$gm_n = \frac{2I_D}{V_{OD}} = 0.008$$

Also,

$$|A_v| = gm_n [gm_n(r_o)^2 || r_o] = 39$$

1.6 f

Because $\lambda \propto 1/L$, length of PMOS double, λ is half $\Rightarrow \lambda = 0.1$
Hence,

$$r_p = \frac{1}{\lambda I_D} = 10000\Omega$$

$\Rightarrow R_{out}$ does not change much, Hence A_v almost unchanged.

Also, $\frac{W}{L} = 2000$

1.7 e

It will increase parasitic capacitance, and large width gives large capacitance, which limit the speed.

Problem 1

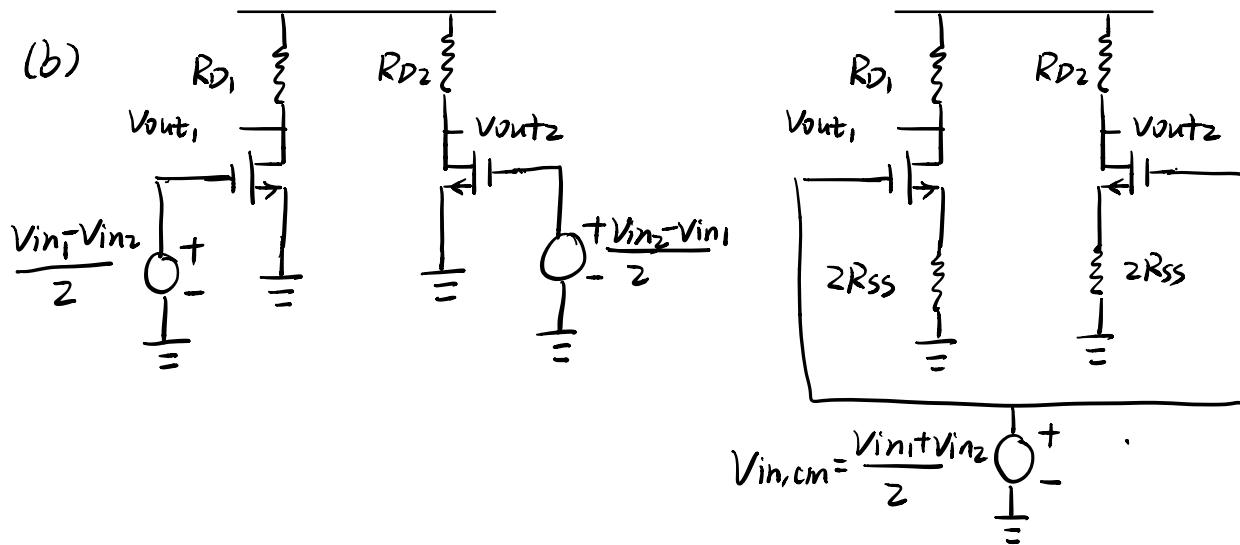
(a) Consider left half

$$P = I_{SS}V_{DD} = 2mW \Rightarrow I_{SS} = 2mA$$

The differential peak-to-peak swing is

$$2I_{SS}R_D = 2 \times 2 \times 10^{-3}A \cdot R_D = 1V$$

$$\Rightarrow R_D = 0.25k\Omega$$



differential half-circuit

common half-circuit.

$$(c) A_v = -g_m R_D = -5$$

$$g_m = \frac{5}{R_D} = \frac{5}{250} = 0.02 \text{ } \Omega^{-1}$$

$$g_m = \frac{2I_D}{V_{OD}} \Rightarrow V_{OD} = \frac{2I_D}{g_m} = \frac{2 \times 10^{-3}}{0.02} = 0.1V$$

$$\frac{W}{L} = \frac{g_m^2}{2 I_D M_{nCox}} = \frac{4 \times 10^{-4}}{2 \times 10^{-3} \times 200 \times 10^{-6}} = \frac{4}{2 \times 10^{-3}}$$

= 1000

(d) According to Eq. 4.14

$$\begin{aligned}\Delta V_{in1} &= \sqrt{\frac{2I_{ss}}{M_{nCox} \frac{W}{L}}} = \sqrt{\frac{2 \times 2 \times 10^{-3}}{200 \times 10^{-6} \times 2000}} \\ &= \sqrt{\frac{4 \times 10^{-3}}{4 \times 10^5 \times 10^{-6} \times 10^{-1}}} \\ &= \sqrt{10^{-2}} = 0.1 \text{ V}\end{aligned}$$

$$(e) Av = \frac{R_D}{\frac{1}{g_m} + 2R_{SS}} = \frac{250}{50 + 2R_{SS}} = 0.05$$

$$50 \times 0.05 + 0.05 \times 2R_{SS} = 250$$

$$R_{SS} = 4.95 \text{ k}\Omega \approx 5 \text{ k}\Omega$$

$$(f) r_o = \frac{1}{g_m I_D} = 5 \text{ k}\Omega$$

$$\lambda = \frac{1}{5 \text{ k}\Omega \times 2 \text{ mA}} = 0.1 \text{ V}^{-1} \Rightarrow L = 2L_0 = 130 \text{ nm}$$

$$(g) I_D = \frac{1}{2} M_{nCox} \left(\frac{W}{L} \right) V_{DD}^2$$

$$W/L = 2I_D / (M_{nCox} V_{DD}^2)$$

$$= 2 \times 2 \times 10^{-3} / (2 \times 10^{-4} \times 0.2^2)$$

$$= 4 \times 10^{-3} / (0.08 \times 10^{-4}) = 500.$$

$$\Rightarrow W = 500 \times 130 \text{ nm} = 65 \mu\text{m}$$

(h) $V_{in,cm} \geq V_{OD\text{current source}} + V_{GS1} = 0.2 + 0.2 + 0.3 = 0.7 \text{ V}$

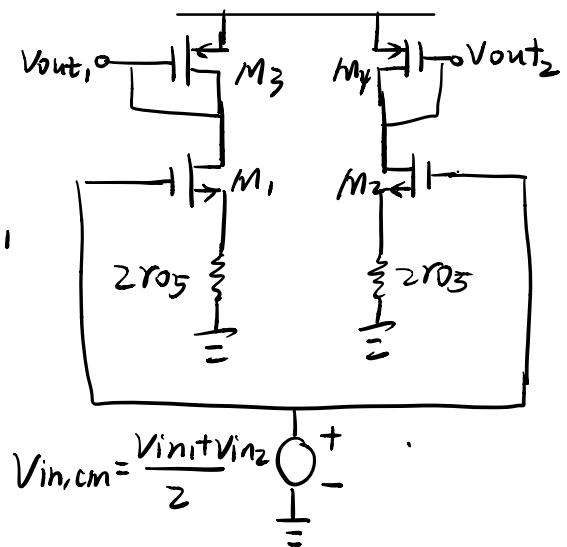
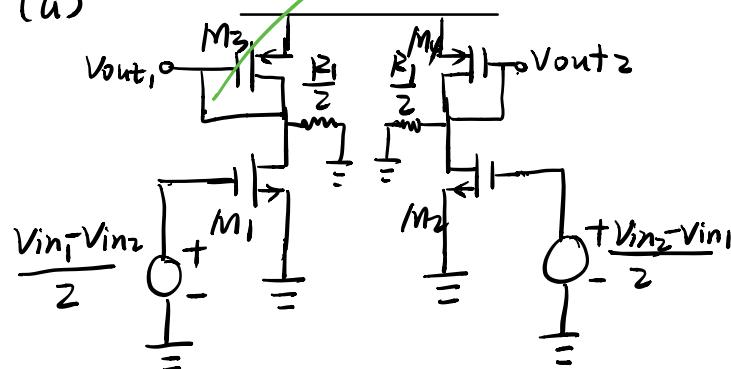
$$V_{in,cm} \leq \min \left[\underbrace{V_{DD} - R_D \frac{I_{SS}}{2} + V_{Th}}_{0.8 \text{ V}}, V_{DD} \right]$$

$$\therefore 0.7 \text{ V} \leq V_{in,cm} \leq 0.8 \text{ V}$$

Problem 2.

always in saturation

(a)



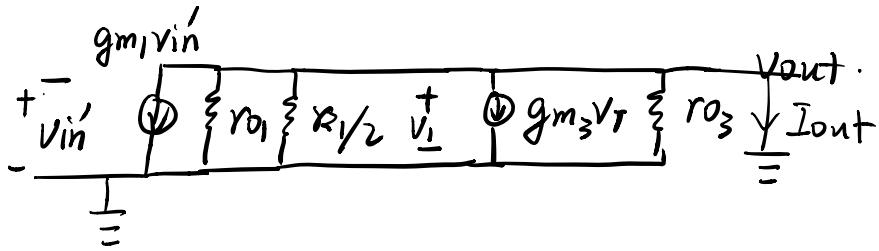
differential half-circuit

common half-circuit.

(b) Only consider the left side now and denote

$$\frac{V_{in_1} - V_{in_2}}{2} \text{ as } V_{in'}$$

small signal model.



Determine G_m : $G_m = \frac{I_{out}}{V_{in}}$

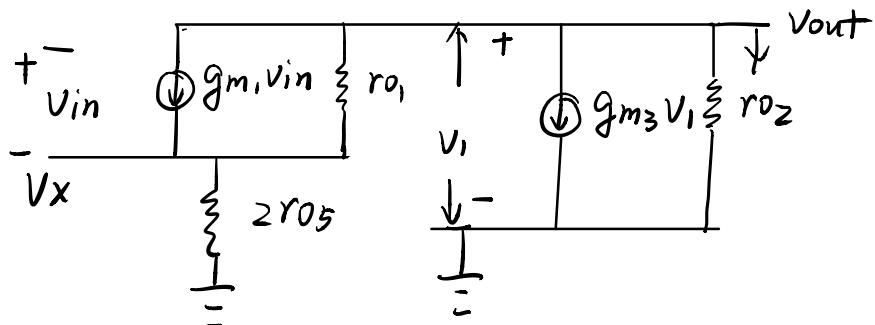
$$I_{out} = -g_m V_{in} \therefore G_m = -g_m$$

Determine R_{out} :

$$V_{out} \left(\frac{1}{r_{o1}} + \frac{1}{r_{o3}} + \frac{2}{R_1} + g_{m3} \right) = I_{out}$$

$$R_{out} = \frac{1}{\frac{1}{r_{o1}} + \frac{1}{r_{o3}} + \frac{2}{R_1} + g_{m3}}$$

$$\therefore A_{v,DM} = \frac{\frac{1}{g_m}}{\frac{1}{r_{o1}} + \frac{1}{r_{o3}} + \frac{2}{R_1} + g_{m3}}$$



Determine G_m : $\frac{V_{in}}{(2r_{o5})/r_{o1}} - g_m V_{in} = I_{out}$

$$\Rightarrow G_m = -\frac{1}{(2r_{o5})/r_{o1}} - g_m,$$

Determine R_{out}

$$R_{out} = (r_{o1} + 2r_{o5}) // r_{o2} // (1/gm_3)$$

$$A_{v,cm} = - \left(gm_1 + \frac{1}{(2r_{o5})//r_{o1}} \right) (r_{o1} + 2r_{o5}) // r_{o2} // (1/gm_3)$$

(c) $V_{DD} + V_{OD5} \leq V_{out, \text{single}} \leq V_{DD} - |V_{Th3}|$

Note the common mode level will be source.

$V_{DD} - V_{SG3}$ where V_{SG3} is set by current I_{M5}

single-end swing: $V_{DD} - |V_{Th3}| - (V_{DD} - V_{SG3}) = |V_{OD3}|$

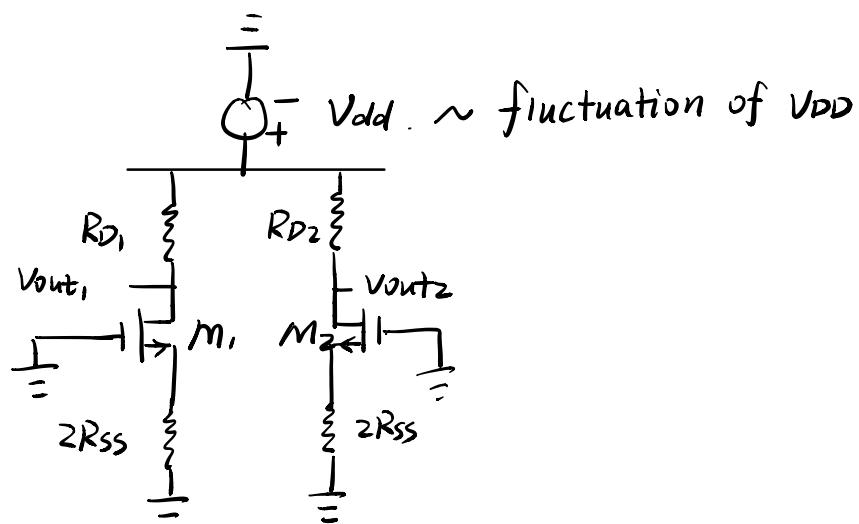
Differential swing: $2|V_{OD3}|$

(d) $V_{OD5} + V_{GS1} \leq V_{in, \text{common.}} \leq V_{DD} - V_{OD3} + V_{Th1}$

Problem 3.

(a) No change in differential mode,
have change in common mode.

(b)



common mode half-circuit.

(c) Note although the gate is grounded in the small signal model, there is current ID flow through $M_{1,2}$. (ID is DC operating point)

Look at the left branch.

According to Fig. 3.56

The output impedance seeing through the drain of M_1 is $(1 + g_m r_o) \cdot 2R_{SS} + r_o \approx 2R_{SS} g_m r_o + r_o$.

The it's in parallel with R_{D1} ,

So the total output impedance is

$$(2R_{SS} g_m r_o + r_o) // R_{D1}$$

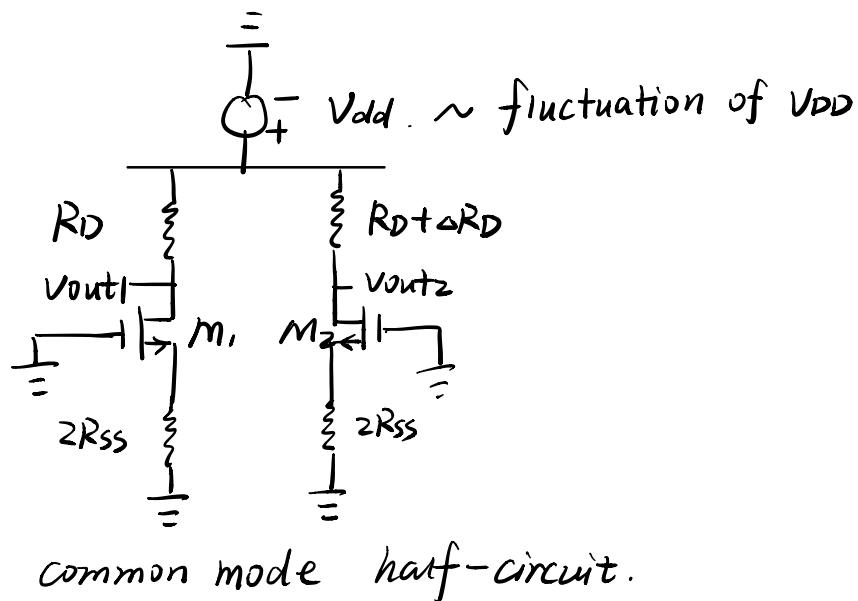
Then calculate G_m : Once v_{out} is grounded,

$$G_m = -1/R_D,$$

$$\therefore A_v = -G_m R_{out} = \frac{1}{R_D} \cdot [(2R_{SS} g_m r_o + r_o) // R_D] \approx 1$$

So the resultant V_{out} fluctuation is the same as the fluctuation of V_{DD} , i.e., v_{dd} .

(d) Here we use a small signal method to solve it. Though the circuit is not fully symmetric, it's still valid to use the Lemma on page 113, thus the half-circuit:



From (3c)

$$|A_{v_i}| = \frac{R_D // [2R_{SS} g_m r_o + r_o]}{R_{D_i}}$$

$$\Delta V_{out} = (A_{v1} - A_{v2}) v_{dd} = \left\{ \frac{R_D // [2R_{SS} g_m r_o + r_o]}{R_D} - \frac{(R_D + \Delta R_D) // [2R_{SS} g_m r_o + r_o]}{R_D + \Delta R_D} \right\} v_{dd}$$

when R_{D_i} is small compared to $r_o + 2R_{SS} g_m r_o$, $\Delta V_{out} = 0$

problem 4

(a) The differential output swing is
 $I_{SS} \cdot R_D$

Single ended swing is
 $I_{SS} R_D / 2$

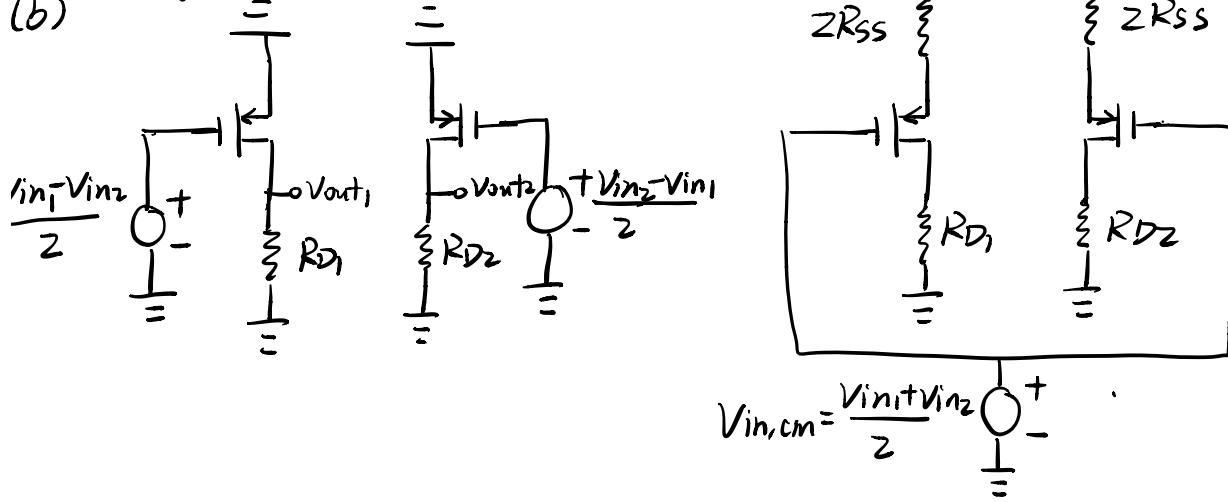
Also note: the output swing is also related to the DC
 $V_{in,cm} - |V_{thp}| < -V_{out}$, thus $V_{out} < V_{in} + |V_{thp}|$
 As we'll discuss in part d,

$$V_{in,cm} \leq V_{DD} - V_{OD,C} - V_{SG1}$$

$$\therefore V_{out} < V_{DD} - V_{OD,C} - V_{OD1}$$

Thus the maximum single end p-p swing
 is $V_{DD} - V_{OD,C} - V_{OD1}$, this swing is limited
 by V_{OD} . This means one can't increase voltage
 swing infinitely by increasing R_D .

(b)



differential half-circuit

common half-circuit.

(c) DM: single end common source amplifier.

$$A_{v,DM} = -g_m R_D$$

CM: degenerated common source amplifier.

$$A_{v,CM} = -\frac{R_D}{1/g_m + 2R_S}$$

(d) When $V_{in} = V_{DD}$, $V_{SG} < V_{Th}$.

As V_{in} continues to decrease, when

$$V_{SG} - |V_{ThP}| = 0 \text{ The transistors are on.}$$

If the current source requires $V_{OD,C}$ overdrive voltage,

$$V_{DD} - V_{OD,C} - V_{in,CM} \geq |V_{ThP}|$$

$$V_{in,CM} \leq V_{DD} - V_{OD,C} - |V_{ThP}|$$

However, the current flows through the transistors requires certain overdrive voltage $V_{OD} = \sqrt{\frac{I_{SS}}{\mu_n C_{ox} \frac{W}{L}}} V_{SD}$

$$\text{So } V_{DD} - V_{OD,C} - V_{in,CM} \geq |V_{ThP}| + V_{OD} V_{SD}$$

$$\Rightarrow V_{in,CM} \leq V_{DD} - V_{OD,C} - V_{SG}.$$

As $V_{in,CM}$ continue to decrease, when

$$V_{SG} - |V_{ThP}| \geq V_{SD}$$

$$\text{i.e., } V_{DD} - V_{OD,C} - V_{in,CM} - |V_{ThP}| \geq V_{DD} - V_{OD,C} - V_{out}$$

The transistors are in triode region.

$$\Rightarrow V_{in,cm} \leq V_{out} - |V_{ThP}|$$

Note V_{out} is $\frac{1}{2}I_{SS}R_D$ in common mode,
to maintain in saturation region

$$V_{in,cm} > \frac{1}{2}I_{SS}R_D - |V_{ThP}|$$

$$\text{if } \frac{1}{2}I_{SS}R_D - |V_{ThP}| < 0, \text{ then}$$

(this is easy to satisfy by design)

For $V_{in,cm} > 0$, condition is always satisfied.

In that case $0 \leq V_{in,cm} \leq V_{DD} - V_{OD,c} - V_{SG}$.

$$(e) V_{OD,c} + V_{GS} \leq V_{in,NMOS} \leq \min \left[V_{DD} - R_D \frac{I_{SS}}{2} + V_{ThN}, V_{DD} \right]$$

Note that when $V_{DD} - R_D \frac{I_{SS}}{2} + V_{ThN} > V_{DD}$
the upper limit of V_{DD} is always satisfied, so

$$V_{OD,c} + V_{GS} \leq V_{in,NMOS} \leq V_{DD}$$

For NMOS we only have a lower bound,
while for PMOS we only have an upper bound.