

• HW 7 due Friday

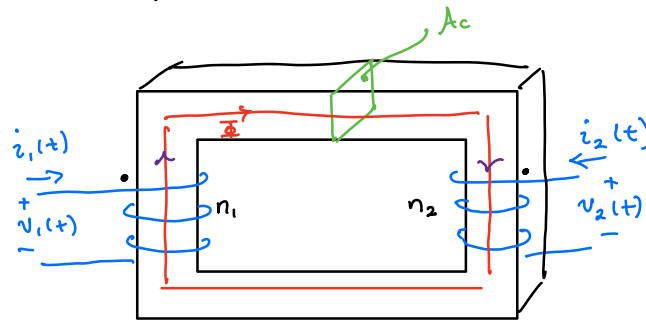
- Today

- ↳ Finish magnetics chapter (finish eddy currents, transformer)
- ↳ Next time: Chapter on "Converter Structures"

- Transformers

Ch 6 in 2nd Ed
Ch 7 in 3rd Ed.

ex: 2 windings & no air gap



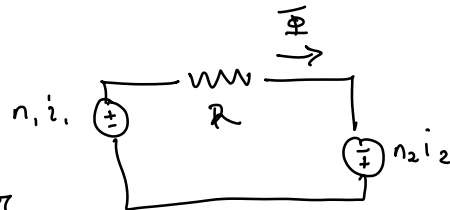
Core reluctance

$$R = \frac{l_m}{\mu A_c}$$

$$\oint \vec{H} = n_1 i_1 + n_2 i_2$$

$\underbrace{\quad}_{\text{MMF}}$

$$\underbrace{n_1 i_1 + n_2 i_2}_{\text{sources}} = \underbrace{\Phi R}_{\text{drop}} \quad (1)$$



- If $R = 0 \rightarrow$ Recover ideal xfmr eqns.

Look @ (1)

$$\boxed{n_1 i_1 + n_2 i_2 = 0} \quad (1') \quad \text{Ampere's Law}$$

And Faraday's Law gives

$$v_1 = n_1 \frac{d\Phi}{dt} \quad \& \quad v_2 = n_2 \frac{d\Phi}{dt}$$

$$\Rightarrow \frac{d\Phi}{dt} = \left\{ \frac{v_1}{n_1} = \frac{v_2}{n_2} \right\} \quad \leftarrow \text{look familiar?} \quad (2)$$

(2) & (1') imply perfect $\eta = 100\%$ power transfer

- Look at realistic case where $R \neq 0$

Apply Faraday again

$$v_1 = n_1 \frac{d\Phi}{dt} \quad \& \quad v_2 = \dots$$

need to solve for Φ from (1)

(1) gives

$$\Phi = \frac{n_1 i_1 + n_2 i_2}{R} \quad (3)$$

Substitute & get

$$v_1 = n_1 \frac{d}{dt} \left(\frac{n_1 i_1 + n_2 i_2}{R} \right)$$

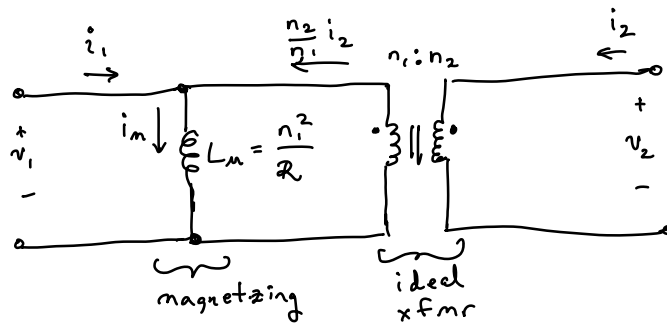
$$= \frac{n_1^2}{R} \frac{d}{dt} \left(i_1 + \frac{n_2}{n_1} i_2 \right) \quad (4)$$

$L_M =$ "magnetizing inductance"

$$v_2 = n_2 \frac{d}{dt} \left(\frac{n_1 i_1 + n_2 i_2}{R} \right)$$

\vdots
similar story.

Eq (4) implies the ckt:



apply KCL to get i_m .

$$i_m = i_1 + \frac{n_2}{n_1} i_2$$

Observations:

- Remove coil #2 \rightarrow recover "regular ol'" inductor w/ value L_m .

- L_m causes departure from idealized ^{xfmr} eqns.

~~$$n_1 i_1 + n_2 i_2 = 0$$~~ not true

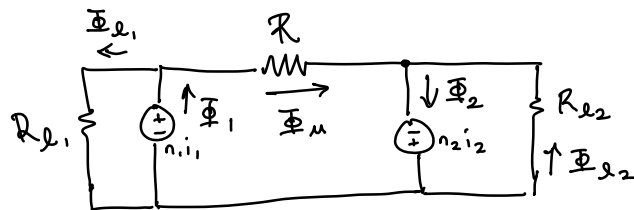
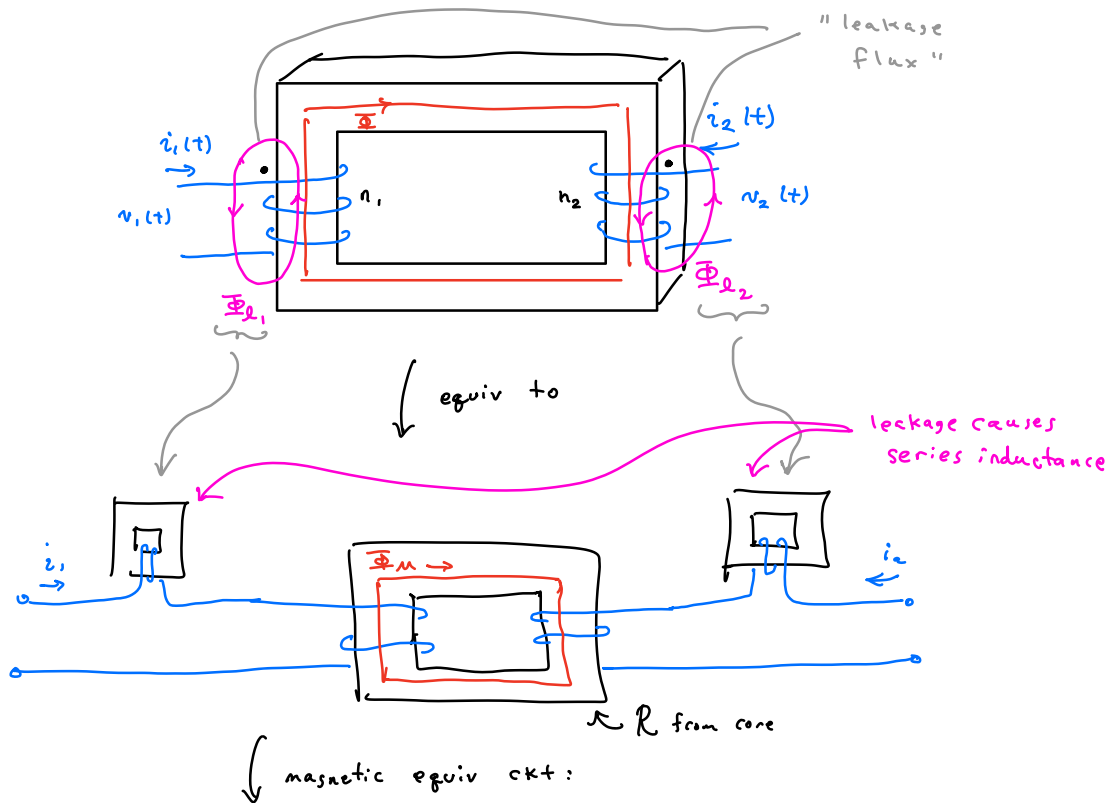
- What about saturation?

$$i_m(t) = \frac{1}{L_m} \int_0^t v_1(t) dt$$

$$\nabla v_1 = n_1 \frac{d\Phi}{dt} = n A_c \frac{dB(t)}{dt}$$

$$\rightarrow B(t) = \frac{1}{n_1 A_c} \int_0^t v_1(t) dt$$

B reaching B_{sat} is
caused by too many
"volt-seconds"



Solve for Φ_1 & Φ_2 & Apply Faraday's Law

$$v_1 = n_1 \frac{d\Phi_1}{dt} \quad \& \quad v_2 = n_2 \frac{d\Phi_2}{dt}$$

↓ after some algebra

$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} L_{11} & L_{12} \\ L_{12} & L_{22} \end{bmatrix} \frac{d}{dt} \begin{bmatrix} i_1 \\ i_2 \end{bmatrix}$$

relate to L_M & leakages?

$$L_{12} = \frac{n_1 n_2}{\mathcal{R}} = \frac{n_2}{n_1} \frac{1}{L_M}$$

$$L_{11} = L_{e1} + \frac{n_1}{n_2} L_{12}$$

$$L_{22} = L_{e2} + \frac{n_2}{n_1} L_{12}$$

$$n_e = \text{"effective turns ratio"} = \sqrt{\frac{L_{22}}{L_{11}}}$$

$$n_e \text{ in ideal case} = \frac{n_2}{n_1}$$

$$K = \text{"coupling coefficient"} = \frac{L_{12}}{\sqrt{L_{11} L_{22}}}$$

$$0 \leq K \leq 1$$

as $K \rightarrow 1$, approach ideal xfrmr where $n_e \rightarrow \frac{n_2}{n_1}$

looks like

