

Lecture 3 (11th January 2022)

Linear operator

input: x

output: y



$$y = L(x)$$

Q: When is 'L' a linear operator.

A: L is a linear operator iff it satisfies the following property:

- ① Scaling: If input is scaled by α (α is a scalar) the o/p is also scaled by α .

$$x \rightarrow [L(\cdot)] \rightarrow y \Rightarrow L(x) = y$$

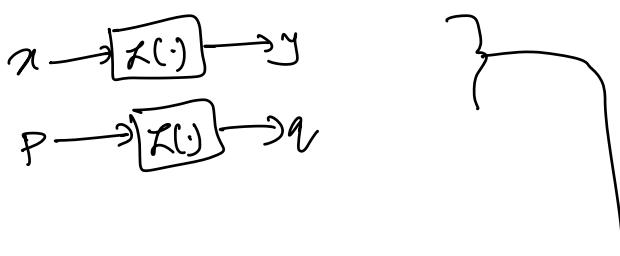
$$\alpha x \rightarrow [L(\cdot)] \rightarrow \alpha y$$

$$\Rightarrow L(\underline{\alpha x}) = \underline{\alpha \cdot y}$$

But we know $L(x) = y$

$\therefore L(\alpha x) = \alpha L(x)$

- ② Superposition



$$x+p \xrightarrow{L(\cdot)} y+q$$

$L(x+p) = y+q$

$\therefore y = L(x) \quad q = L(p)$

$\therefore L(x+p) = L(x) + L(p)$

Q: What is linear system?

A: Any system in which input x and output y are related by:

$L_1(x) = L_2(y)$; where L_1 & L_2 are linear operators. Then we call the sys to be linear.

Linear operators:-

(1) R = gain

(2) $\frac{d}{dt}, \frac{d^2}{dt^2}, \dots$

(3) $\int(\) dt$

Linear sys

(1) $y = k \cdot x$

(2) $\frac{dy}{dt} = kx$

(3) $\frac{d^2y}{dt^2} + \frac{dy}{dt} + y = \frac{du}{dt} + u$

$$\textcircled{4} \quad t^2 \frac{d}{dt} y = x \quad \leftarrow \text{linear s/s.}$$

$$\Leftrightarrow 2x \quad x \frac{dx}{dt} + y = 2 \quad \rightarrow \text{linear?}$$

$$\left[\begin{array}{c} \frac{d}{dt}(x) \\ \frac{d}{dt}(y) \end{array} \right] + \begin{bmatrix} 0 \\ 2 \end{bmatrix}$$

linear

$$x \cdot \underbrace{\frac{d}{dt} x}_{\text{non-linear.}}$$

$$\textcircled{5} \quad L \frac{di_L}{dt} = v_L \quad \begin{array}{c} i_L \\ \overrightarrow{m} \\ + v_L - \end{array}$$

linear

$$L(i_L) \frac{di_L}{dt} = v_L$$

non-linear.

$$\textcircled{6} \quad \overset{\circ}{n} = ax + bu \quad \overset{\circ}{n} = \frac{dx}{dt}$$

linear s/s

$$\overset{\circ}{x} = A \overset{\circ}{x} + B \overset{\circ}{u} \quad \begin{array}{c} \overset{\circ}{x} \rightarrow \text{vector} \\ \downarrow \text{vector} \\ \downarrow \text{Matrices} \end{array} \quad \left. \begin{array}{c} \text{vector} \\ \text{Matrices} \end{array} \right\} \text{linear s/s}$$

Differential Equations

State variables : Any variable that has a time derivative.

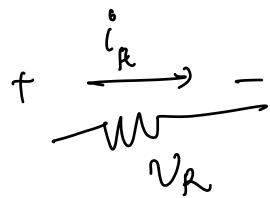
$$v_L = L \frac{di_L}{dt}$$

i_L, v_C are state variables

$$i_C = C \frac{dv_C}{dt}$$

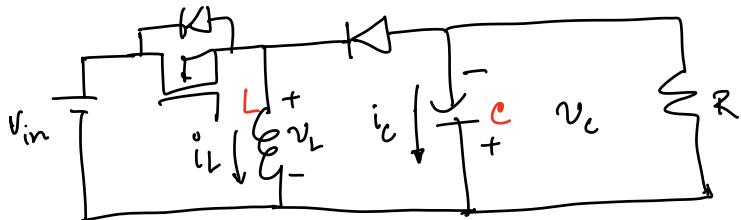
$$i_L \left\{ \begin{array}{l} \\ \end{array} \right.$$

$$\int_{T_1}^T v_C$$



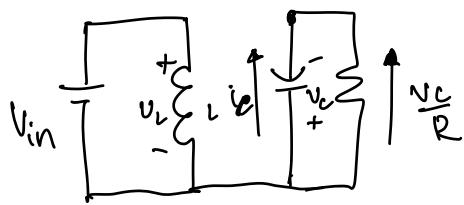
v_L, i_C are not state variables

v_R, i_R are not state " .



Buck Boost converter

mode 1



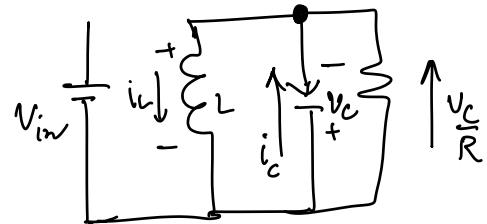
$$N_L = L \frac{di_L}{dt} = V_{in} \quad \checkmark$$

$$i_C + \frac{V_c}{R} = 0$$

$$L \frac{dV_c}{dt} + \frac{V_c}{R} = 0$$

$$\therefore C \frac{dV_c}{dt} = -\frac{V_c}{R}$$

Mode 2



$$v_L = -v_c = L \frac{di}{dt}$$

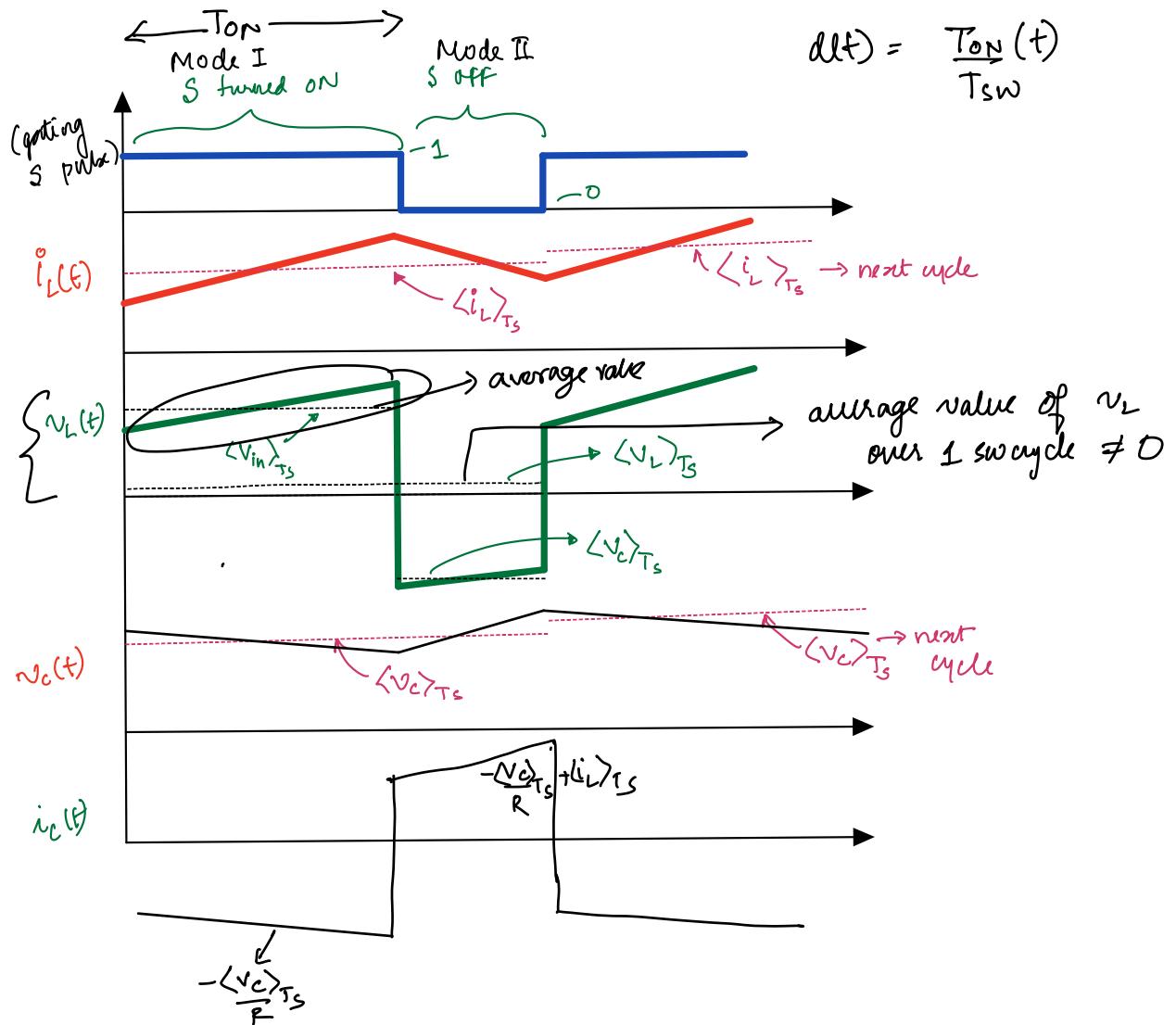
$$i_C + \frac{V_c}{R} = i_L$$

$$C \frac{dV_c}{dt} = -\frac{V_c}{R} + i_L$$

EE 452 : $(V_{in})D + (-V_c)D' = 0$

$$\langle x(t) \rangle_{T_s} = \int_t^{t+T_s} x(t) dt$$

EE 452 : $\left(-\frac{V_c}{R}\right)D + \left(-\frac{V_c}{R} + I_L\right)D' = 0$



$$\langle v_L(t) \rangle_{T_S} = [v_L \text{ during mode ①}] d(t) + [v_L \text{ during mode ②}] \cdot d'(t)$$

$$= \langle v_{in}(t) \rangle_{T_S} d(t) + \langle -v_C(t) \rangle_{T_S} d'(t)$$

$$= \langle v_{in}(t) \rangle_{T_S} d(t) - \langle v_C(t) \rangle_{T_S} d'(t)$$

$$\langle i_C(t) \rangle_{T_S} = [i_C \text{ during mode ①}] d(t) + [i_C \text{ during mode ②}] d'(t)$$

$$= \frac{\langle v_c(t) \rangle_{T_S}}{R} \cdot d(t) + \left(\frac{\langle v_c(t) \rangle_{T_S}}{R} + \langle i_c(t) \rangle_{T_S} \right) d'(t)$$

$$\langle v_L(t) \rangle_{T_S} = \langle \frac{d i_L(t)}{dt} \rangle_{T_S} = \langle v_{in}(t) \rangle_{T_S} dt - \langle v_c(t) \rangle_{T_S} d'(t)$$

$$\langle i_c(t) \rangle_{T_S} = C \frac{d}{dt} \langle v_c(t) \rangle_{T_S} = \frac{\langle v_c(t) \rangle_{T_S}}{R} \cdot d(t) + \left(\frac{\langle v_c(t) \rangle_{T_S}}{R} + \langle i_c(t) \rangle_{T_S} \right) d'(t)$$

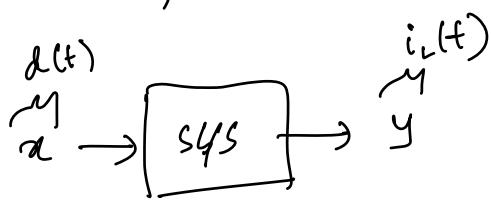
Q: Is this a linear sys?

States := $\langle i_L(t) \rangle_{T_S}, \langle v_c(t) \rangle_{T_S}$ } which have derivative.

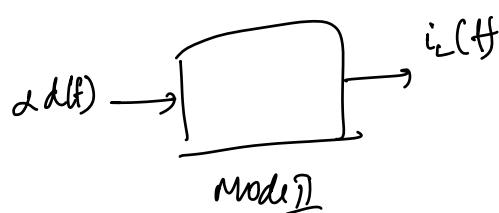
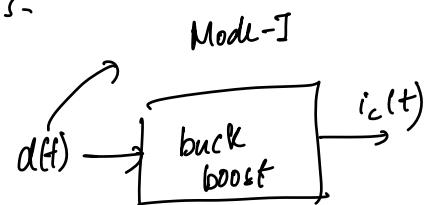
$$\frac{d}{dt} x$$

inputs : $d(t), \langle v_{in}(t) \rangle_{T_S}$
things you can control.

No, it's not a linear sys



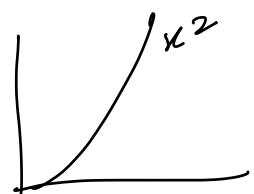
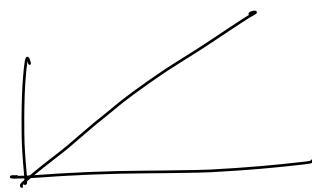
$$dx \rightarrow \rightarrow dy$$



$$\frac{dx}{dt} = y \rightarrow L$$

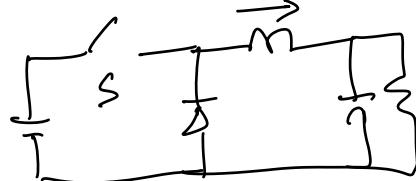
$$x \frac{dx}{dt} = y \rightarrow NL$$

$$\frac{dx}{dt} = \underbrace{x \cdot y}_{\sim} \rightarrow NL$$



D: constant

$d(t)$: time varying signal.

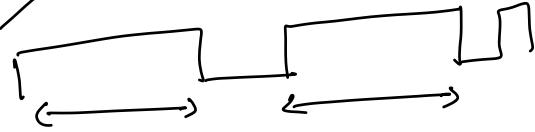
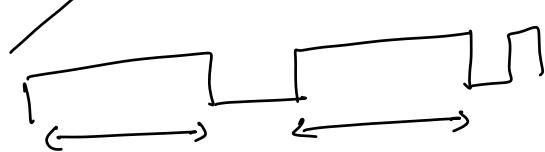


$$i_L(t=0) = 0A .$$

$$i_L = 5A \leftarrow \text{desired value}$$

turn on S

$d(t)$



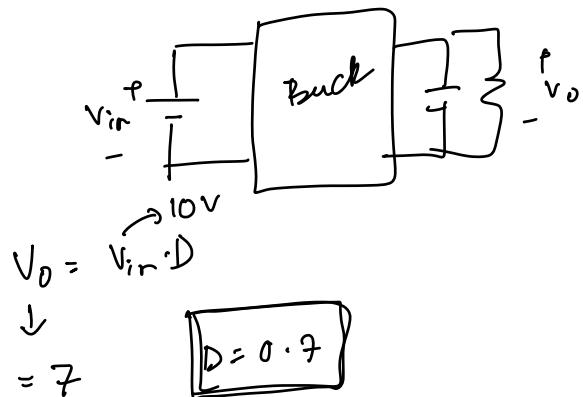
Q $\langle i_L(t) \rangle_{T_S}$ can be influenced by $d(t)$.

Can you exactly tell how?

$\langle v_C(t) \rangle_{T_S}$ $d(t)$.
?

$$V_o = \frac{V_{in} \cdot D}{D}$$

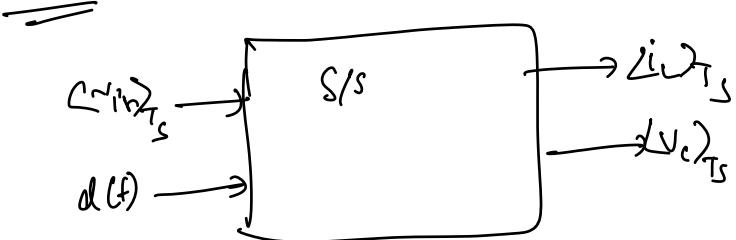
Buck converter

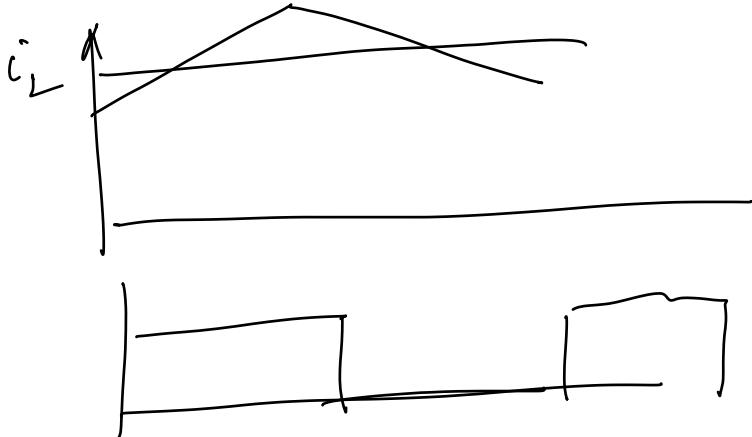


I want a relationship between

$\langle v_C(t) \rangle_{T_S}$, $\langle i_L(t) \rangle_{T_S}$ & $d(t)$

Q $\langle v_C(t) \rangle_{T_S}$? & not $\langle d(t) \rangle_{T_S}$





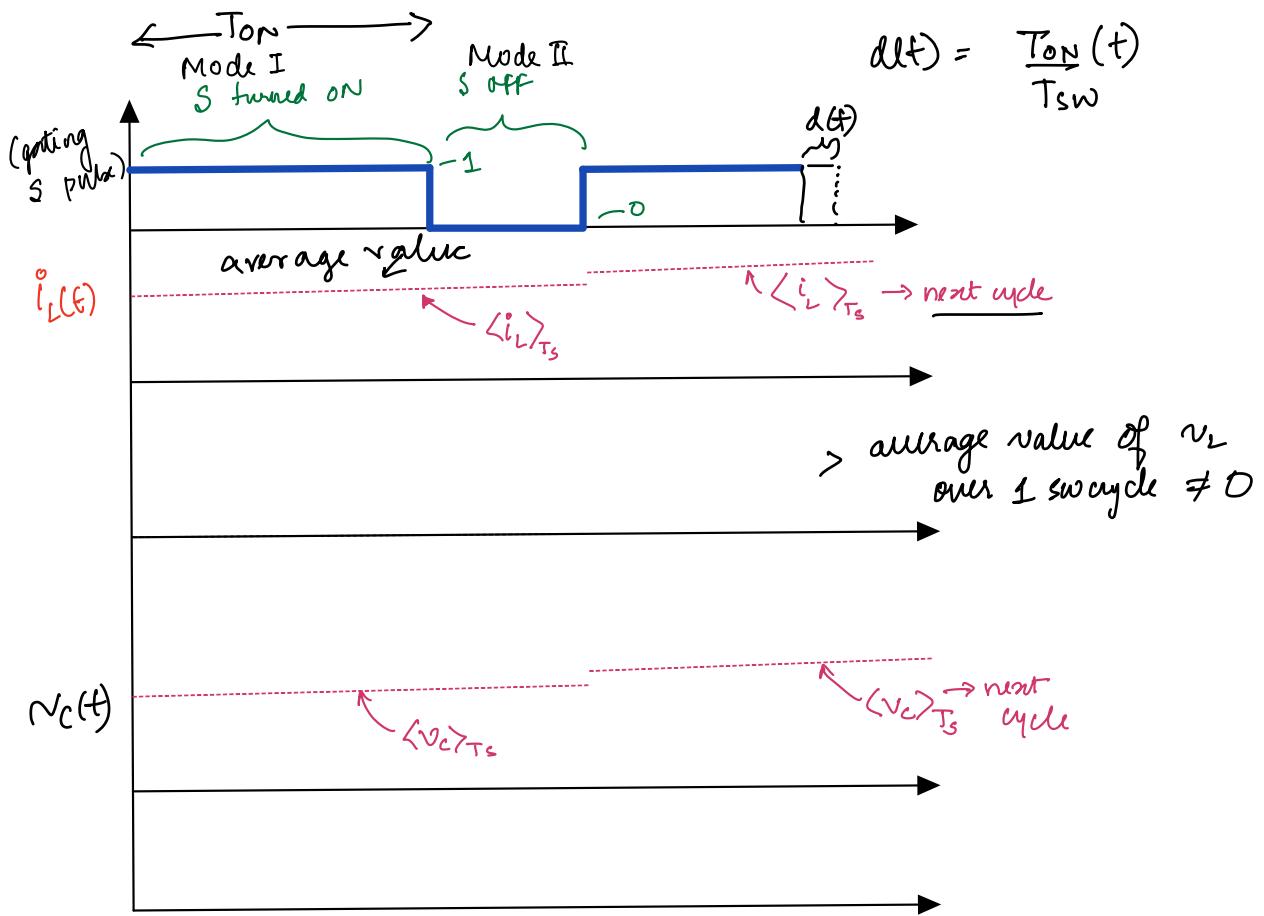
$\alpha(t)$ has no variation in 1 sw. cycle hence,

$$\alpha(t) = \langle \alpha(\theta) \rangle_{IS}$$

$$D ; \alpha(t)$$

$$\langle v_L(t) \rangle_{T_S} = \left\langle \frac{d i_L(t)}{dt} \right\rangle_{T_S} = \langle v_{in}(t) \rangle_{T_S} dt - \langle v_e(t) \rangle_{T_S} d'(t)$$

$$\begin{aligned} \langle i_L(t) \rangle_{T_S} &= C \frac{d}{dt} \langle v_c(t) \rangle_{T_S} = \\ &\quad \frac{\langle v_c(t) \rangle_{T_S}}{R} \cdot d(t) + \left(-\frac{\langle v_c(t) \rangle_{T_S}}{R} + \langle i_L(t) \rangle_{T_S} \right) d'(t) \end{aligned}$$



Q If I slightly change my $d(t)$, how is it going to affect my $\langle i_c(t) \rangle_{T_S}$ & $\langle v_c(t) \rangle_{T_S}$?

A To get to that, we will consider every signal to have a steady state + perturbation.

$$x(t) = X + \tilde{x}$$

e.g. Buck conv.

$$v_o = v_{in} \cdot D$$

$$v_{in} = 10V, D = 0.7, v_o = 7V$$

$$D = 0.71$$

$$D + \tilde{D} = 0.71$$

\downarrow \uparrow

0.7 0.01

$$v_o = \frac{v_o + \tilde{v}_o}{\downarrow \quad \downarrow}$$

$v_o = 7.1V$

$7V \quad 0.1V$

Step 1

Introduce perturbation

$$\langle i_c(t) \rangle_{T_S} = I_c + \tilde{i}_c(t)$$

$$\tilde{i}_c(t) \ll I_c$$

$$\langle v_c(t) \rangle_{T_S} = v_c + \tilde{v}_c(t)$$

$$\tilde{v}_c(t) \ll v_c$$

$$d(t) = D + \tilde{d}(t)$$

$$\tilde{d}(t) \ll D$$

$$\langle v_{in}(t) \rangle_{T_S} = v_{in} + \underbrace{\tilde{v}_{in}(t)}_{\text{large signal (or DC)}}$$

small signal (or perturbation)

$$\langle v_L(t) \rangle_{T_S} = L \frac{d \langle i_L(t) \rangle_{T_S}}{dt} = \langle v_{in}(t) \rangle_{T_S} d(t) - \langle v_c(t) \rangle_{T_S} d'(t)$$

$$L \frac{d}{dt} (i_L + \tilde{i}_L(t)) = (V_{in} + \tilde{v}_{in}(t)) (D + \tilde{d}(t)) - (V_c + \tilde{v}_c(t)) (D' - \tilde{d}'(t))$$

$$\begin{aligned} d'(t) &\Rightarrow 1 - d(t) \xrightarrow{\text{By definition}} \\ &= 1 - (D + \tilde{d}(t)) \\ &= 1 - D - \tilde{d}(t) \\ \xleftarrow{\text{from 4.52}} &= D' - \tilde{d}'(t) \end{aligned}$$

①

$$L \frac{d}{dt} i_L + L \frac{d \tilde{i}_L(t)}{dt} = V_{in} D + V_{in} \tilde{d}(t) + D \tilde{v}_{in}(t) + \tilde{v}_{in}(t) \tilde{d}(t) - V_c D' + V_c \tilde{d}(t) - \tilde{v}_c(t) D' + \tilde{v}_c(t) \tilde{d}'(t)$$

Collect similar terms

① Large signal terms / DC terms

$$L \frac{d i_L}{dt} = V_{in} D - V_c D' = 0 \Rightarrow V_{in} D = V_c D' \quad \therefore V_c = \frac{V_{in} D}{D'}$$

② Linear small signal.

$$L \frac{d \tilde{i}_L(t)}{dt} = V_{in} \tilde{d}(t) + D \tilde{v}_{in}(t) + V_c \tilde{d}'(t) - D' \tilde{v}_c(t)$$

②

$$\text{①} \rightarrow V_o = \frac{V_{in} D}{D'}$$

Cap. Voltage.

$$\langle i_c(t) \rangle_{T_S} = C \frac{d}{dt} \langle v_c(t) \rangle_{T_S} = \underbrace{\frac{\langle v_c(t) \rangle_{T_S}}{R} \cdot d(t)} + \left(\frac{\langle v_c(t) \rangle_{T_S}}{R} + \langle i_L(t) \rangle_{T_S} \right) d'(t)$$

$$C \frac{d}{dt} \langle v_c(t) \rangle_{T_S} = - \underbrace{\frac{\langle v_c(t) \rangle_{T_S}}{R} (d(t) + d'(t))}_{=1} + \langle i_L(t) \rangle_{T_S} d'(t)$$

$$= - \frac{\langle v_c(t) \rangle_{T_S}}{R} + \langle i_L(t) \rangle_{T_S} d'(t)$$

$$\therefore C \frac{d}{dt} (V_c + \tilde{v}_c(t)) = - \left(\frac{V_c + \tilde{v}_c(t)}{R} \right) + (I_L + \tilde{i}_L(t)) (D' - \tilde{d}(t))$$

① DC / Large signal term.

$$C \frac{d V_c}{dt} = - \frac{V_c}{R} + I_L D' = 0 \Rightarrow I_L = + \frac{V_c}{R D'}$$

$$I_L = \frac{V_0}{R D'} = \frac{I_0}{D'}$$

② Small signal linear term.

$$C \frac{d}{dt} \tilde{v}_c(t) = - \frac{\tilde{v}_c(t)}{R} + D' \tilde{i}_L(t) - I_L \tilde{d}(t)$$

④

$$\textcircled{1} \rightarrow V_0 = V_c = \frac{V_{in} D'}{D'}$$

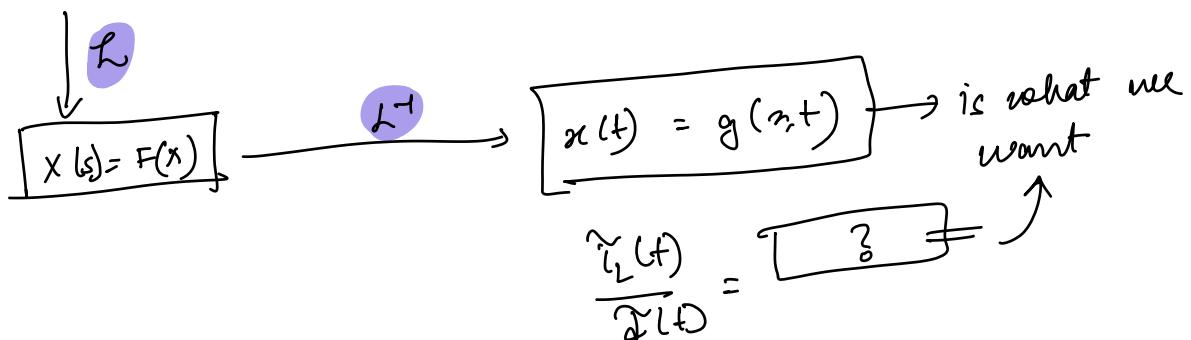
$$\textcircled{3} \rightarrow I_L = \frac{I_0}{D'}$$

$$L \frac{d \tilde{i}_L(t)}{dt} = v_{in} \tilde{d}(t) + D \tilde{v}_{in}(t) + V_c \tilde{d}(t) - D' \tilde{v}_c(t)$$

$$C \frac{d}{dt} \tilde{v}_c(t) = - \frac{\tilde{v}_c(t)}{R} + D' \tilde{i}_L(t) - I_L \tilde{d}(t)$$

Q: How $\tilde{d}, \tilde{v}_{in}$ affects \tilde{i}_L, \tilde{v}_c

$$\dot{x} = f(x, t) \xrightarrow{\text{some PDE/ODE}} n(t) = g(x, t)$$

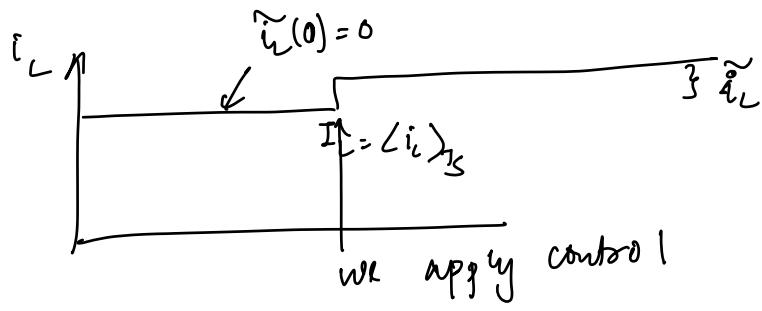


$$\begin{aligned} x(t) &\xrightarrow{L} \frac{1}{s} \\ \frac{d(x(t))}{dt} &\xrightarrow{L} sX(s) - x(0) \xrightarrow{\text{initial value}} \boxed{x(t) \xrightarrow{L} X(s)} \\ \int_0^t x(\tau) d\tau &\xrightarrow{L} \frac{X(s)}{s} \end{aligned}$$

$$L \frac{d \tilde{i}_L(t)}{dt} = v_{in} \tilde{d}(t) + D \tilde{v}_{in}(t) + V_c \tilde{d}(t) - D' \tilde{v}_c(t)$$

$$L \left[s \tilde{i}_L(s) - \tilde{i}_L(0) \right] = V_{in} \tilde{d}(s) + D \tilde{v}_{in}(s) + V_c \tilde{d}(s) - D' \tilde{v}_c(s)$$

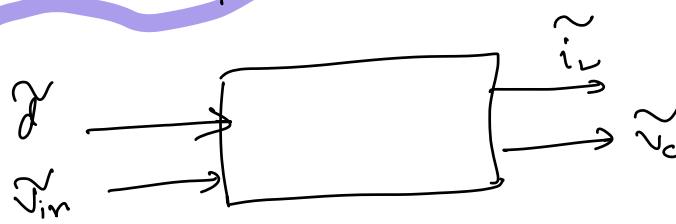
$= ?$



$$sL \tilde{i}_L(s) = V_{in} \tilde{x}(s) + D \tilde{v}_{in}(s) + V_c \tilde{d}(s) - D' \tilde{v}_c(s) \quad (5)$$

$$C \frac{d}{dt} \tilde{v}_c(t) = - \frac{\tilde{v}_c(t)}{R} + D' \tilde{i}_L(t) - I_L \tilde{x}(t)$$

$$sC \tilde{v}_c(s) = - \frac{\tilde{v}_c(s)}{R} + D' \tilde{i}_L(s) - I_L \tilde{x}(s) \quad (6)$$



① I want to find $\frac{\tilde{i}_L}{\tilde{x}(s)}$, $\frac{\tilde{v}_c}{\tilde{x}(s)}$.

$$\tilde{v}_{in} = 0$$

$$sL \tilde{i}_L(s) = V_{in} \tilde{x}(s) + V_c \tilde{d}(s) - D' \tilde{v}_c(s)$$

$$(sC + \frac{1}{R}) \tilde{v}_c(s) = D' \tilde{i}_L(s) - I_L \tilde{x}(s)$$

② Let's find $\frac{\tilde{i}_L(s)}{\tilde{x}(s)}$

remove $\tilde{v}_c(s)$

$$\tilde{v}_c(s) = \frac{D' \tilde{i}_L(s) - I_L \tilde{x}(s)}{(sC + \frac{1}{R})}$$

$$sL \tilde{i}_L(s) = (V_{in} + V_c) \tilde{d}(s) - D' \cdot \frac{D' \tilde{i}_L(s) - I_L \tilde{d}(s)}{\left(sc + \frac{1}{R} \right)}$$

or, $sL \tilde{i}_L(s) = (V_{in} + V_c) \tilde{d}(s) - \frac{D'^2 \tilde{i}_L(s)}{\left(sc + \frac{1}{R} \right)} + \frac{D' I_L \tilde{d}(s)}{sc + \frac{1}{R}}$

or, $\left(scL + \frac{D'^2}{sc + \frac{1}{R}} \right) \tilde{i}_L(s) = \left[(V_{in} + V_c) + \frac{D' I_L}{sc + \frac{1}{R}} \right] \tilde{d}(s)$

$\therefore \frac{\tilde{i}_L(s)}{\tilde{d}(s)} = \frac{\left[(V_{in} + V_c) + \frac{D' I_L}{sc + \frac{1}{R}} \right]}{\left(sc^2 L C + scL + D'^2 \right)}$

$$\boxed{\frac{\tilde{i}_L(s)}{\tilde{d}(s)} = \frac{(V_{in} + V_c)(sc + \frac{1}{R}) + D' I_L}{s^2 L C + \frac{scL}{R} + D'^2}}$$

Similarly you could find

$$\frac{\tilde{v}_c(s)}{\tilde{d}(s)} = \dots \quad \dots \quad \dots$$

① Two other alternative methods to do the same derivation

② Why did we do this at all?

→ Basis of closed loop control, bode, lot 2
controller design.