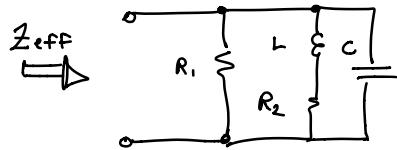


# Homework #3

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## - Problem #1

Calculate  $Z_{\text{eff}}(s)$  of circuit below & put into standard form:



$$Z_{\text{eff}}(s) = \frac{1}{\frac{1}{R_1} + \frac{1}{sL + R_2} + \frac{1}{sC}} \cdot \frac{R_1(sL + R_2)(\frac{1}{sC})}{R_1(sL + R_2)(\frac{1}{sC})}$$

$$= \frac{R_1(sL + R_2)(\frac{1}{sC})}{(sL + R_2)(\frac{1}{sC}) + R_1(\frac{1}{sC}) + R_1(sL + R_2)} \cdot \frac{\frac{sc}{sc}}{\frac{sc}{sc}}$$

$$= \frac{R_1(sL + R_2)}{(sL + R_2) + R_1 + R_1(s^2LC + sR_2C)}$$

\* collect terms by order

$$= \frac{sR_1L + R_1R_2}{s^2R_1LC + s(L + R_1R_2C) + R_2 + R_1} \cdot \frac{\frac{1}{R_2 + R_1}}{\frac{1}{R_2 + R_1}}$$

\* massage into form

$$G = G_0 \frac{\left(1 - \frac{s}{\omega_0}\right)}{1 + \frac{s}{Q\omega_0} + \left(\frac{s}{\omega_0}\right)^2}$$

Observation:

\* - to get 1 term in denominator, must  $\div$  by  $(R_2 + R_1)$

$$= \frac{\frac{1}{R_1+R_2} (R_1 R_2 + S R_1 L)}{1 + S \frac{(L + R_1 R_2 C)}{R_1 + R_2} + S^2 \frac{R_1 L C}{R_1 + R_2}}$$

↙ reshuffled order of terms slightly  
to match targeted form above

\* Next steps  
- Look @  $S^2$  coefficient in denom & try to deduce  $\frac{1}{\omega_0^2}$  factor

$$\Rightarrow \frac{1}{\omega_0} = \sqrt{\frac{R_1 L C}{R_1 + R_2}} \quad (1)$$

- Now look at  $S$  coeff. in denom. It follows that

$$S \frac{L + R_1 R_2 C}{R_1 + R_2} = \frac{1}{Q \omega_0}$$

\* use (1)

$$= \frac{1}{Q} \sqrt{\frac{R_1 L C}{R_1 + R_2}}$$

Now solve for  $Q$

$$\frac{(\ )}{N(C)} = \frac{(\ )'}{(\ )^{1/2}} = ( \ )^{1/2} = \sqrt{C}$$

$$Q = \sqrt{\frac{R_1 L C}{R_1 + R_2}} \cdot \frac{R_1 + R_2}{L + R_1 R_2 C}$$

$$\begin{aligned} &= \frac{\sqrt{(R_1 L C)(R_1 + R_2)}}{L + R_1 R_2 C} \\ &= Q \end{aligned} \quad (2)$$

- denom is basically fully defined in desired form now. Focus on num next!

$$= \frac{\frac{1}{R_1+R_2} (R_1 R_2 + S R_1 L) \cdot \frac{R_1 R_2}{R_1 R_2}}{1 + \frac{S}{Q \omega_0} + \left(\frac{S}{\omega_0}\right)^2} \text{ where } Q \& \omega_0 \text{ are in (1)-(2)}$$

\* Next  
- want num in  $G_o(1 + \frac{S}{\omega_0})$  form. Factor out  $R_1 R_2$  to get "1" term.

$$= \frac{\frac{G_0}{R_1 R_2} \left( 1 + s \frac{\frac{-1}{\omega_Z}}{\cancel{R_1 R_2}} \right)}{1 + \frac{s}{Q \omega_0} + \left( \frac{s}{\omega_0} \right)^2}$$

$$= \frac{G_0 \left( 1 - \frac{s}{\omega_Z} \right)}{1 + \frac{s}{Q \omega_0} + \left( \frac{s}{\omega_0} \right)^2}$$

done!

$$= Z_{ef}(s)$$

# 1

where

$$\begin{aligned} G_0 &= \frac{R_1 R_2}{R_1 + R_2} \\ \omega_Z &= -\frac{R_2}{L} \\ Q &= \frac{\sqrt{(R_1 C)(R_1 + R_2)}}{L + R_1 R_2 C} \\ \omega_0 &= \sqrt{\frac{R_1 + R_2}{R_1 L C}} \end{aligned}$$

- Problem #2

a) Draw  $G_1(j\omega)$  &  $G_2(j\omega)$  asymptote plots

- Look @  $G_1(j\omega)$ . Use material in lecture # 8.

$f = \frac{\omega}{2\pi}$	$\ G_1(j\omega)\ $	$\ G_1(j\omega)\ _{dB}$	$\angle G_1(j\omega)$
0	100	40 dB	$0^\circ$
$f_0 = 1 \text{ kHz}$	$\frac{100}{\sqrt{2}}$	$\approx (40 - 3) \text{ dB}$	$-45^\circ$
$\infty$	drops as $\left(\frac{f}{f_0}\right)^{-1}$	$\rightarrow -20 \text{ dB/decade}$ slope	$-90^\circ$

$$G_1 = \frac{100}{1 + \frac{s}{\omega_0}}$$

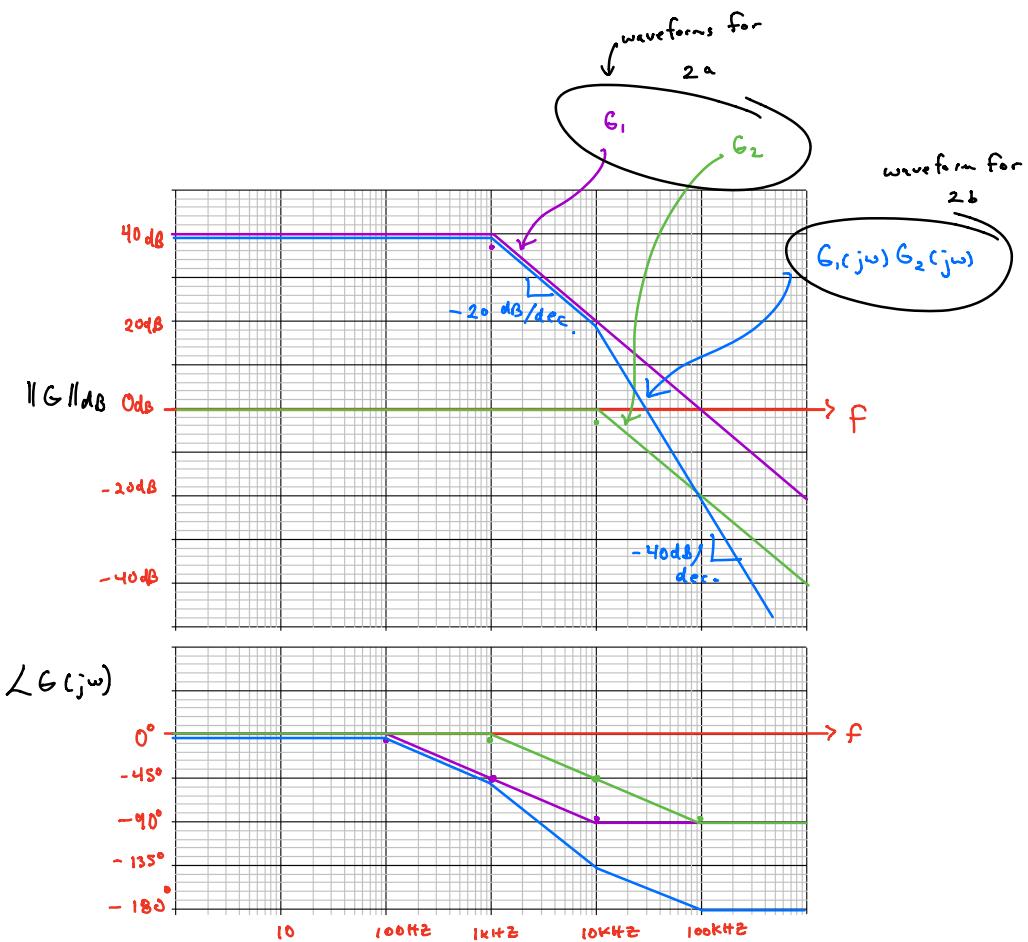
$$\omega_0 = 2\pi 1 \times 10^3 \text{ rad/s}$$

- Look @  $G_2(j\omega)$ :

$f = \frac{\omega}{2\pi}$	$\ G_2(j\omega)\ $	$\ G_2(j\omega)\ _{dB}$	$\angle G_2(j\omega)$
0	1	0 dB	$0^\circ$
$f_0 = 10 \text{ kHz}$	$\frac{1}{\sqrt{2}}$	$\approx -3 \text{ dB}$	$-45^\circ$
$\infty$	drops as $\left(\frac{f}{f_0}\right)^{-1}$	$\rightarrow -20 \text{ dB/decade}$ slope	$-90^\circ$

$$G_2 = \frac{1}{1 + \frac{s}{2\pi 10 \times 10^3}}$$

b) Add breakpoints of asymptotes to approximate product of  $G_1$  &  $G_2$ .



- Problem #3

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a) Find  $K_{A/D}$  given  $V_{A/D} = 0.75 \text{ V}$ :

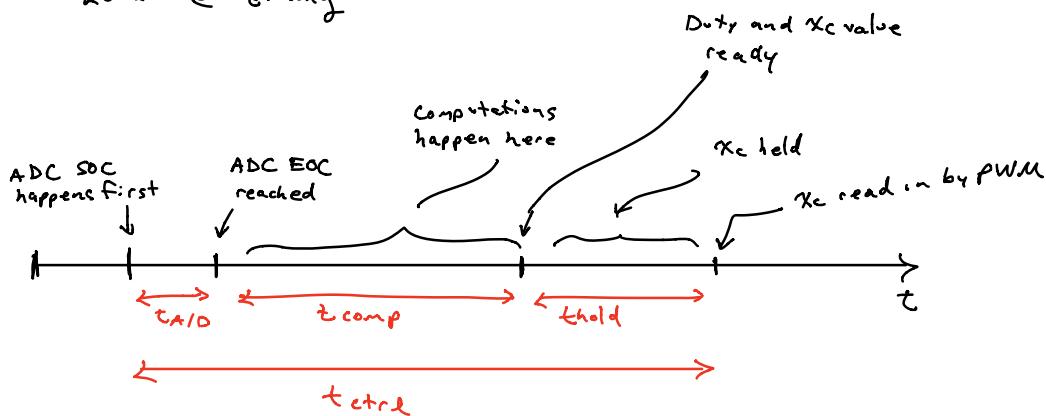
$$\begin{aligned}
 K_{A/D} &= \text{round} \left( (2^{n_{A/D}} - 1) \frac{V_{A/D}}{V_{FS}} \right) \\
 &= \text{round} \left( (2^{12} - 1) \left( \frac{0.75 \text{ V}}{3 \text{ V}} \right) \right) \\
 &= \text{round} (1,023.75) \\
 &= 1,024 \quad \text{when } V_{A/D} = 0.75 \text{ V}
 \end{aligned}
 \boxed{3a}$$

b) ADC voltage resolution

$$q_{A/D} = \frac{V_{FS}}{2^{n_{A/D}}} = \frac{3 \text{ V}}{2^{12}} \approx 732 \mu\text{V} \approx q_{A/D} \boxed{3b}$$

c) Compute  $T_{hold}$  &  $T_{ctrl}$ .

Look @ timing



Waveform diagram below gives more explanation of timing illustrated above. From above, it is clear that

$$t_{ctrl} = t_{A/D} + t_{comp} + t_{hold}$$

Since the PWM is configured to read  $X_C$  only @ counter reset, it follows that  $t_{ctrl}$  is fixed at

$$\underbrace{t_{ctrl}}_{\text{fixed}} = T_s$$

$\hookrightarrow$  PWM reads  $X_C$  once per sw. cycle.

Calculations below are easier if  $t_{ctrl}$  written in terms of  $T_{clk}$ .

$$\Rightarrow t_{ctrl} - T_s = (100\text{kHz})^{-1} = \left(\frac{100\mu\text{Hz}}{10^3}\right)^{-1} \\ = \left(\frac{f_{clk}}{10}\right)^{-1} = \frac{10^3}{f_{clk}} = 10^3 T_{clk}$$

Now solve for  $t_{hold}$ :

$$\Rightarrow t_{hold} = t_{ctrl} - t_{A/D} - t_{comp}$$

$$* \text{ where } t_{A/D} = 50 T_{clk}$$

$$t_{comp} = 500 T_{clk}$$

$$t_{ctrl} = 1000 T_{clk}$$

$$= 1000 T_{clk} - 50 T_{clk} - 500 T_{clk}$$

$$\boxed{\begin{aligned} &= 450 T_{clk} = 4\mu\text{s} \\ &\quad \boxed{3C} \\ &\quad \boxed{t_{hold}} \end{aligned}}$$

and

$$\boxed{\frac{t_{hold}}{t_{ctrl}} = \frac{450 T_{clk}}{1000 T_{clk}} = 0.45 = 45\%} \quad \boxed{3C}$$

$\hookrightarrow$  This tells us that 45% of the time interval between ADC soc & when  $X_C$  is read by PWM is unused.  
Hence, we have a 45% margin to do extra computations if necessary.

a) Get  $t_{ctrl}$ ,  $t_{mod}$ , &  $t_d$ .

- From part c, we know  $t_{ctrl} = T_s = 1000 \text{ TcIK}$ .

- For asymmetric leading edge carrier,

$$t_{mod} = D' T_s = 1000 D' \text{ TcIK}$$

- Sum up

$$\begin{aligned} t_d &= t_{ctrl} + t_{mod} = 1000 \text{ TcIK} + 1000 D' \text{ TcIK} \\ &= 1000 \text{ TcIK} \underbrace{(1 + D')}_{1+1-D} \\ &= 1000 \text{ TcIK} (2 - D) \quad | \quad 3d \end{aligned}$$

(e) & (f): See next page.

$$\begin{aligned} \text{Note } N_r &= \frac{T_{cIK}}{T_s} - 1 = \frac{100 \text{ MHz}}{100 \text{ kHz}} - 1 \\ &= \frac{\cancel{100} \times \cancel{10^6}^3}{\cancel{100} \times \cancel{10^3}^2} - 1 = 1000 - 1 \\ &= 999 \end{aligned}$$

Answer the questions below:

- If the voltage on the ADC pin,  $v_{A/D}$ , is 0.75 V, what digital integer value,  $x_{A/D}$ , will the ADC produce?
- What is the voltage resolution,  $q_{A/D}$ , of the ADC analog input?
- Compute  $T_{\text{hold}}$  and the ratio  $T_{\text{hold}}/T_{\text{ctrl}}$ . What does the value of  $T_{\text{hold}}/T_{\text{ctrl}}$  tell us about the computational burden on the processor? What happens to the ratio  $T_{\text{hold}}/T_{\text{ctrl}}$  as the controller requires more computations?
- Compute  $T_{\text{ctrl}}$ ,  $T_{\text{mod}}$ , and  $T_d$ . Express your results in terms of  $T_{\text{clk}}$  and  $D$ .
- Sketch the binary PWM output  $c(t)$  and sampled ADC value  $x_{A/D}$  waveforms onto Figure 2. Overlay  $x_{A/D}$  on the same plot as  $v_{A/D}$ .
- Add the following items onto Figure 2: Label the maximum feasible integer value of  $x_{A/D}$  vertical axis, specify the DPWM counter maximum  $N_r$ , label the duty  $D$ , and the delays  $T_{\text{ctrl}}$  and  $T_{\text{mod}}$ . Also draw the delays  $T_{A/D}$ ,  $T_{\text{comp}}$ , and  $T_{\text{hold}}$  within  $T_{\text{ctrl}}$  and try to draw them to scale.

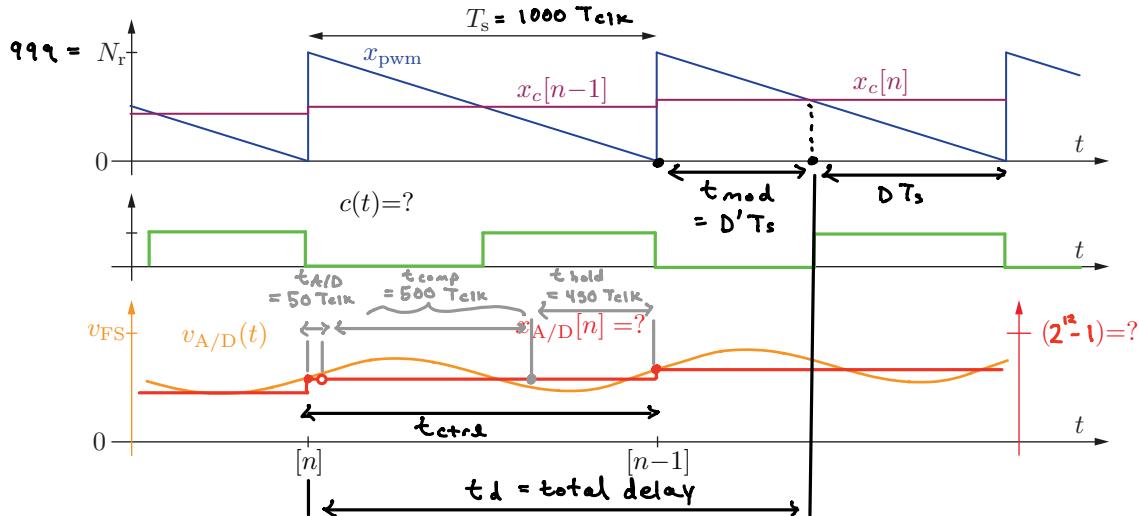


Figure 2: Digital system waveforms for Problem 3.