

Introduction to AC Induction Machines:

M2VA - Totally enclosed squirrel cage three phase motors

ABB Automation Cell BS/M2VA 08 00-06

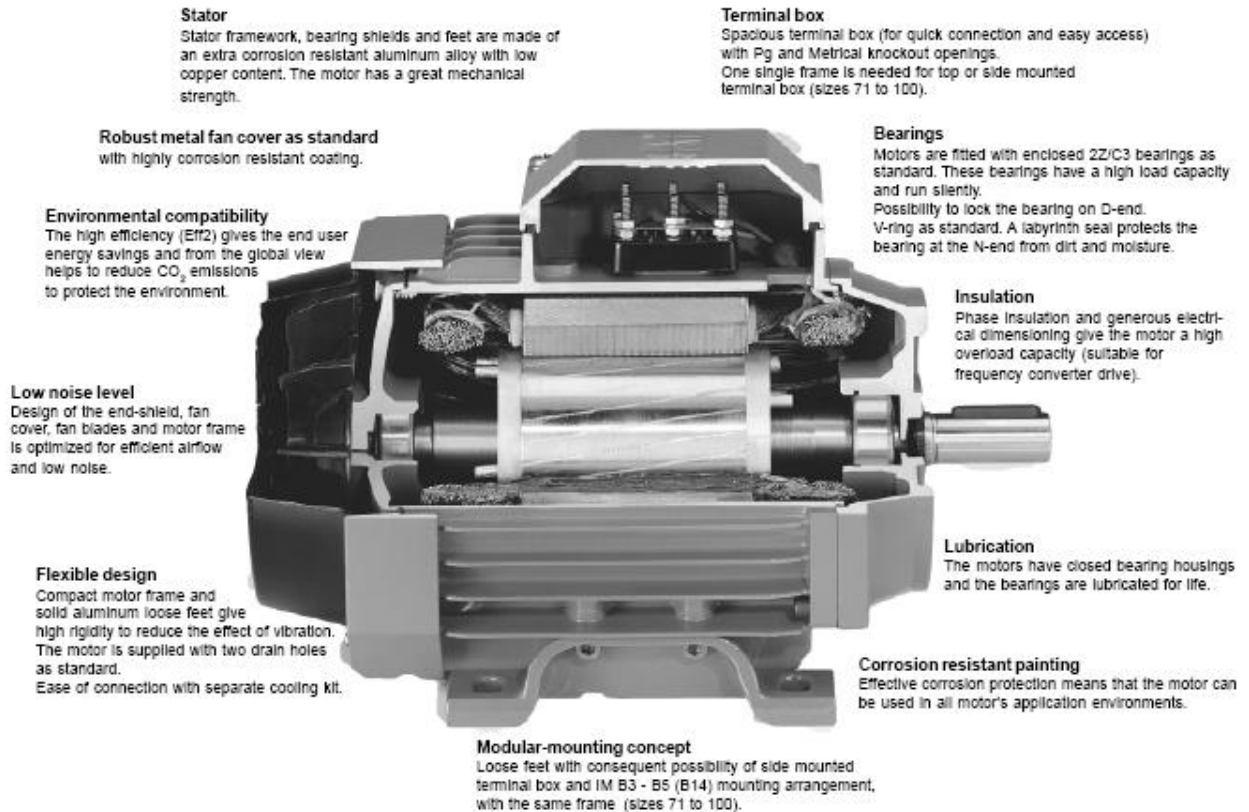
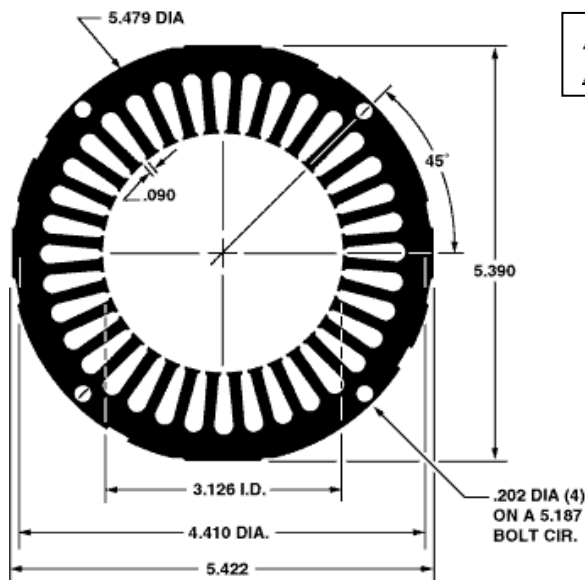
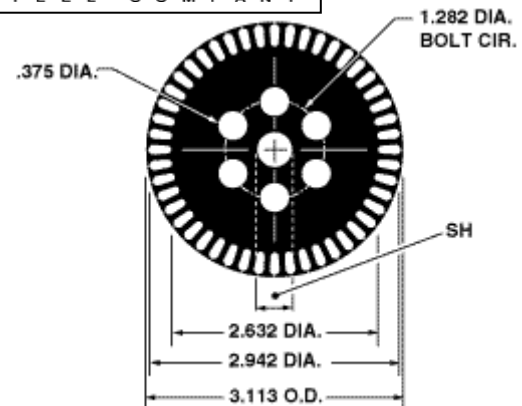


ABB Induction Motor



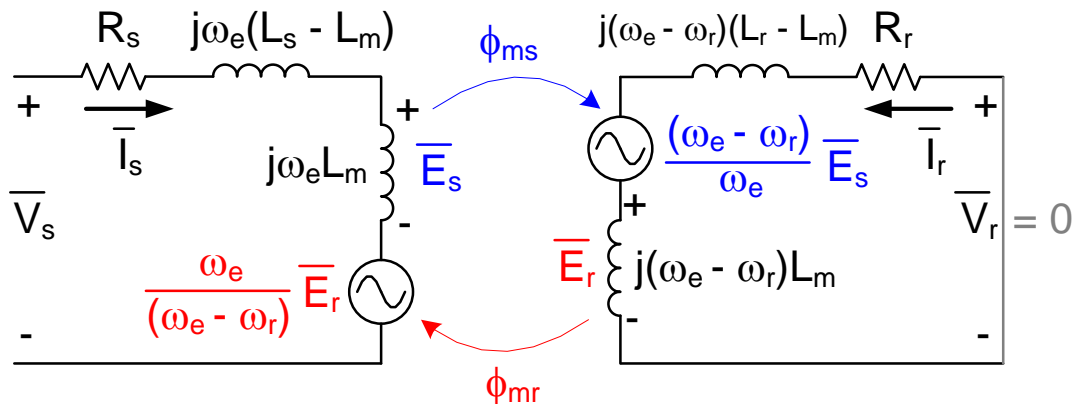
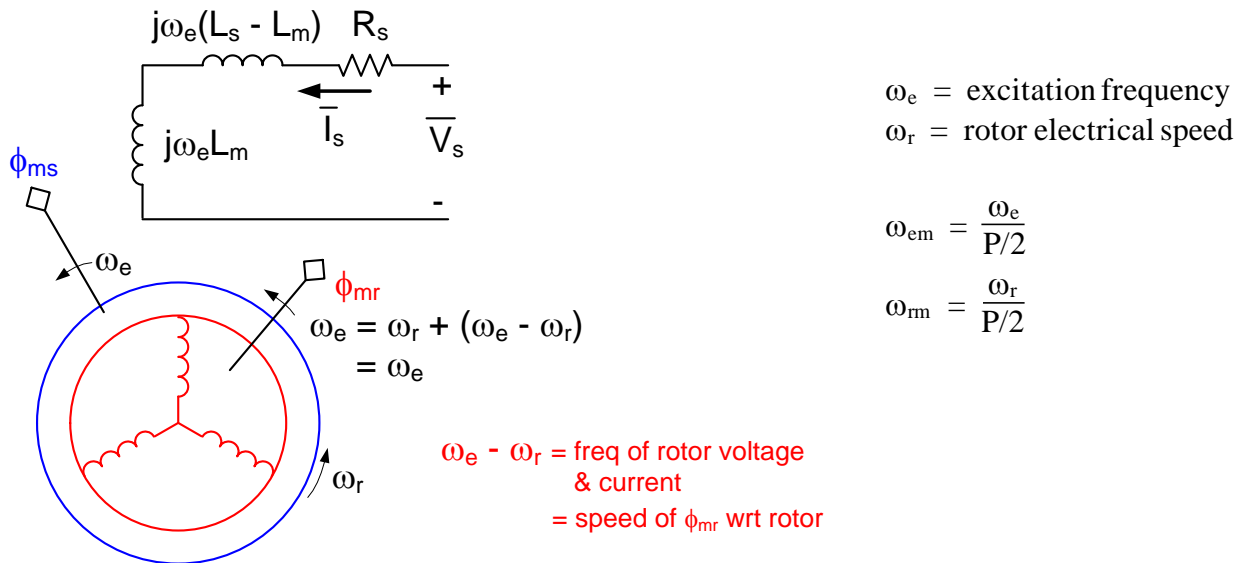
Induction Motor Stator



Induction Motor Rotor

Stator and Rotor Laminations from Tempel Steel Company

Basic Theory of Squirrel Cage Induction Machines:



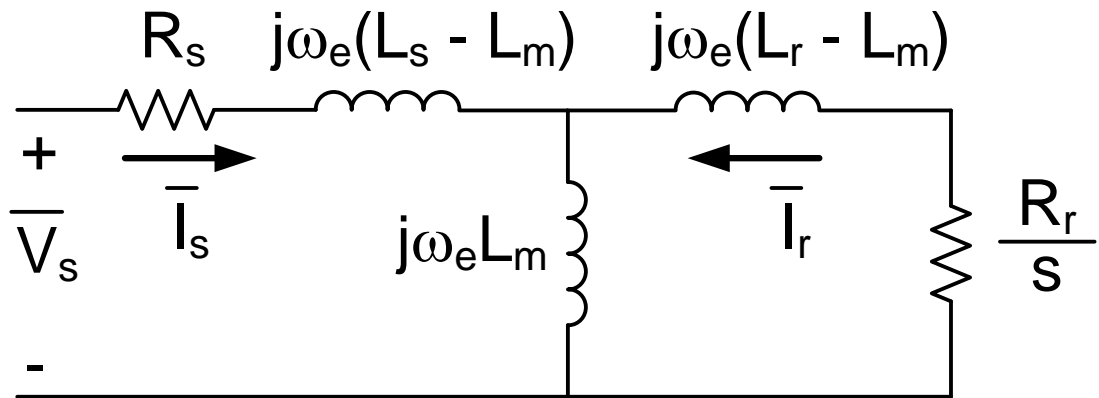
Per Phase Equivalent Schematic of Induction Motor

Circuit Model of Induction Motor

stator: $\bar{V}_s =$

rotor: $0 =$

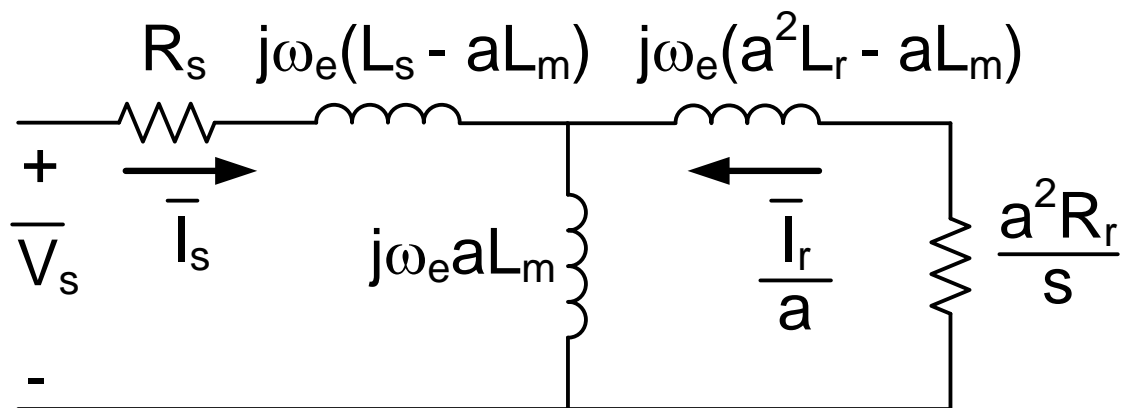
multiply rotor equation by



Per Phase Equivalent Schematic of Induction Motor Reflected to Stator

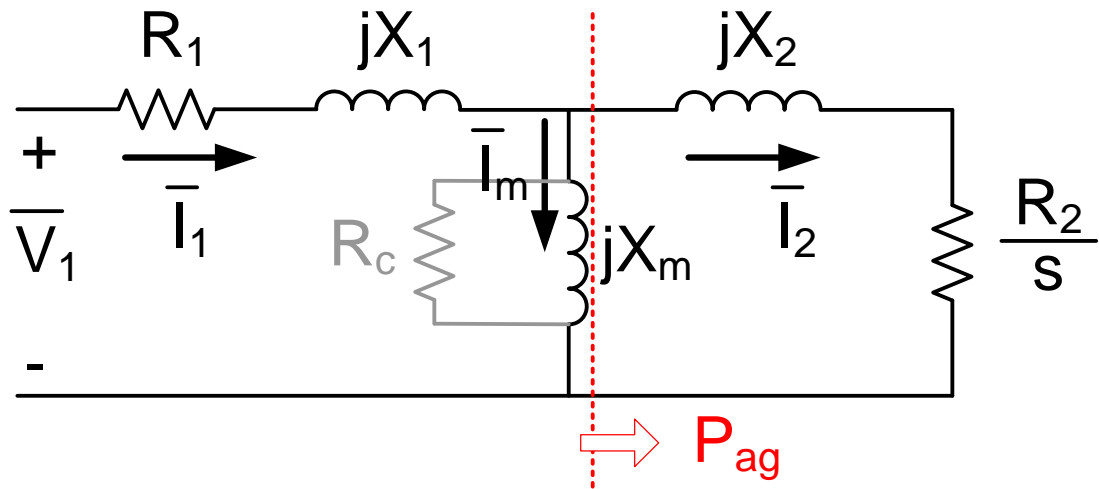
multiply rotor equation by $a \neq 0$ and introduce a new rotor current $= \frac{\bar{I}_r}{a}$

$0 =$



Per Phase Equivalent Schematic of Induction Motor Reflected to Stator

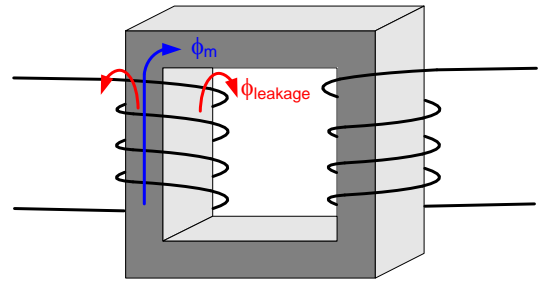
Conventional Per Phase Equivalent Circuit:



Per Phase Equivalent Schematic of Induction Motor Reflected to Stator

$$a = \quad R_2 =$$

X_1 & X_2 are called “Leakage” Inductances



$$X_1 = \quad X_2 =$$

$$X_m = \omega_e \frac{N_s}{N_r} L_m$$

Airgap Power:

$$P_{ag} = \frac{3I_2^2 R_2}{s} \rightarrow 3I_2^2 R_2 = sP_{ag}$$

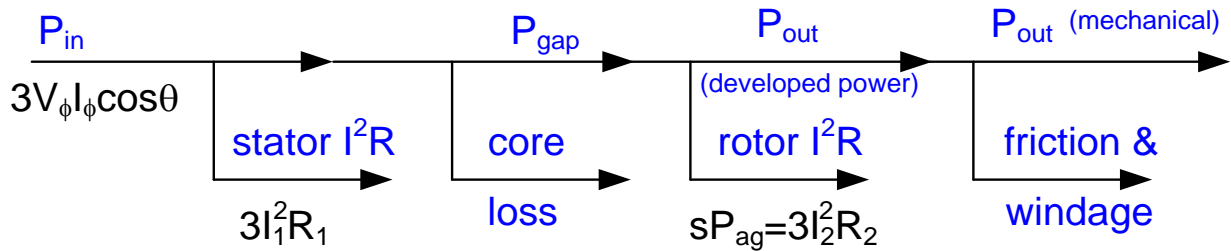
$$\text{Rotor Loss} = sP_{ag}$$

$$P_{out} = \frac{3I_2^2 R_2}{s} (1 - s) = P_{ag} (1 - s)$$

A good (efficient) induction motor must run with low slip.

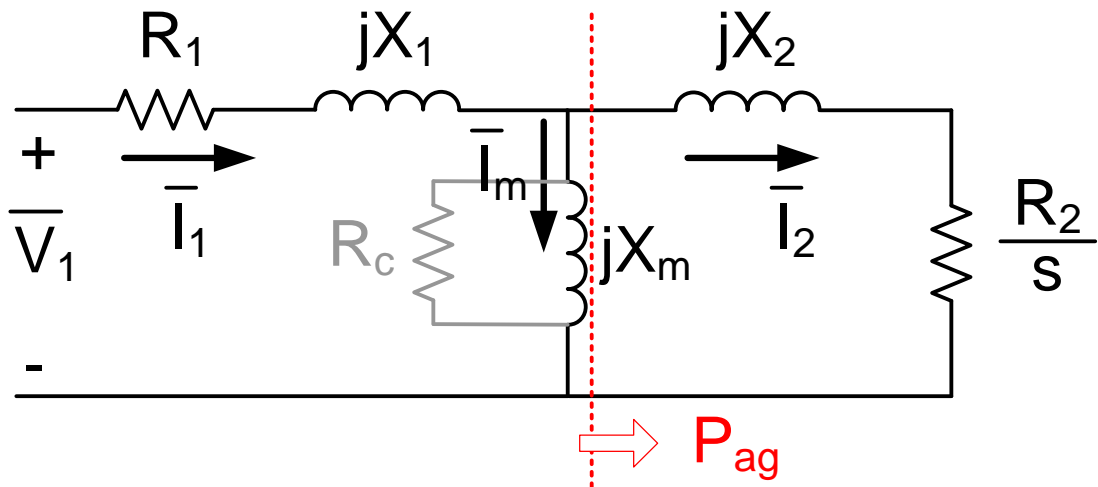
Electromagnetic Torque:

$$T_{em} = \frac{P_{out}}{\omega_{rm}} = \frac{P}{2} \frac{P_{out}}{\omega_r} = \frac{P}{2} \frac{P_{ag}(1-s)}{\omega_r} = \frac{P}{2} \frac{P_{ag}(1-s)}{\omega_e(1-s)} = \frac{P}{2} \frac{P_{ag}}{\omega_e}$$



Power Flow in an Induction Motor

Conventional Per Phase Equivalent Circuit:



Per Phase Equivalent Schematic of Induction Motor Reflected to Stator

$$T_{em} = \frac{P}{2} \frac{P_{ag}}{\omega_e} \qquad P_{ag} = \frac{3I_2^2 R_2}{s}$$

$$T_{em} = \frac{3P}{2} \frac{I_2^2 R_2}{s \omega_e}$$

For a “good” motor

for sure:

$R_1 \rightarrow 0$ economics only (amount of wire)
 $X_m \rightarrow \infty$ economics only (small air gap, good magnetic steel)

probably:

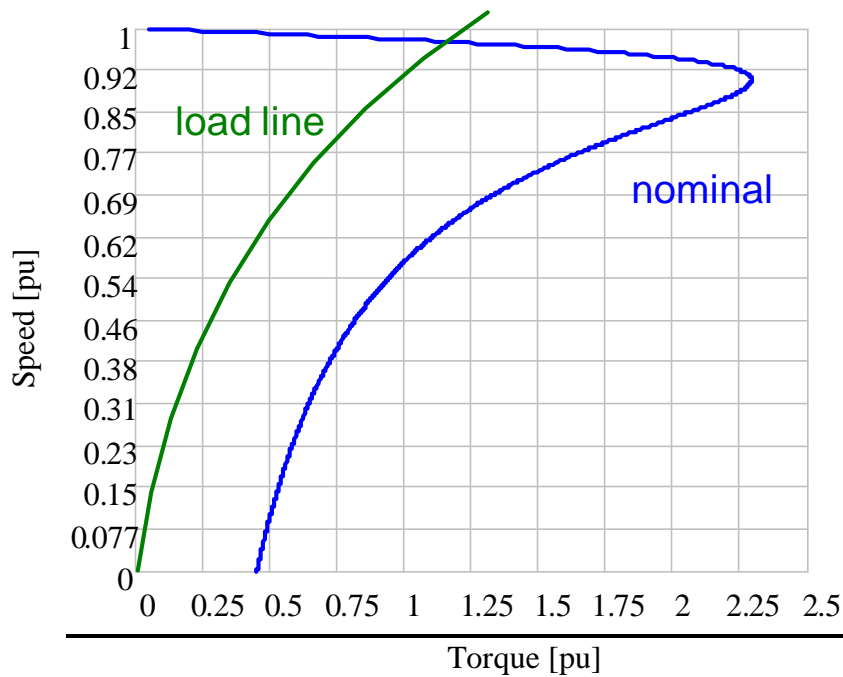
$R_2 \rightarrow 0$
 $X_1, X_2 \rightarrow 0$

{ Large T_{\max} (good)
Large Current at T_{\max} (bad)
Large Starting Currents (bad)

Controlling the speed of an induction motor:

Reduced Voltage Operation:

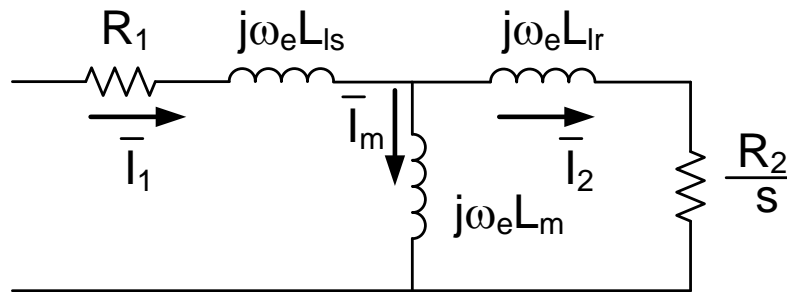
$$T_{em} \propto V^2$$



Reduced Voltage Operation of Induction Motor

Constant Volts/Hz operation:

$$Z_{in} = R_1 + j\omega_e L_{ls} + j\omega_e L_m \parallel \left(\frac{R_2}{s} + j\omega_e L_{lr} \right)$$



Induction Motor Per Phase Equivalent Circuit

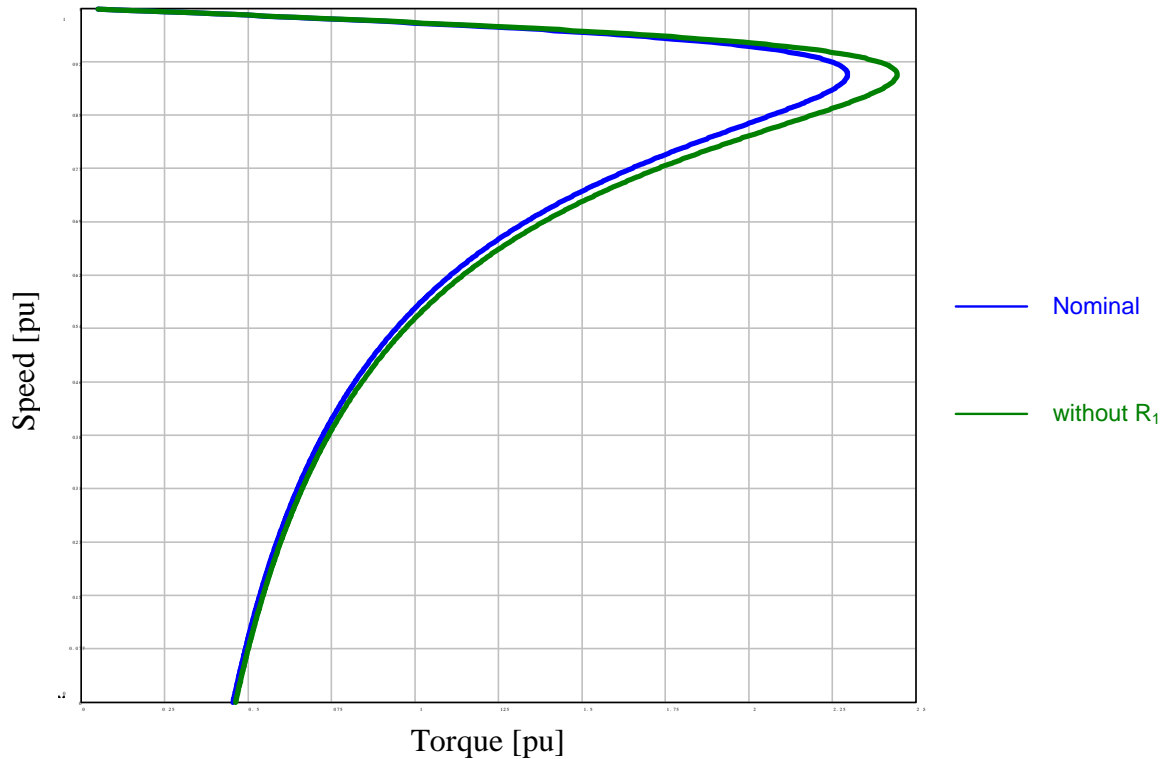
Neglecting R_1 :

$$Z_{in}(\omega_e) = j\omega_e L_{ls} + j\omega_e L_m \parallel \left(\frac{R_2}{s\omega_e} + j\omega_e L_{lr} \right)$$

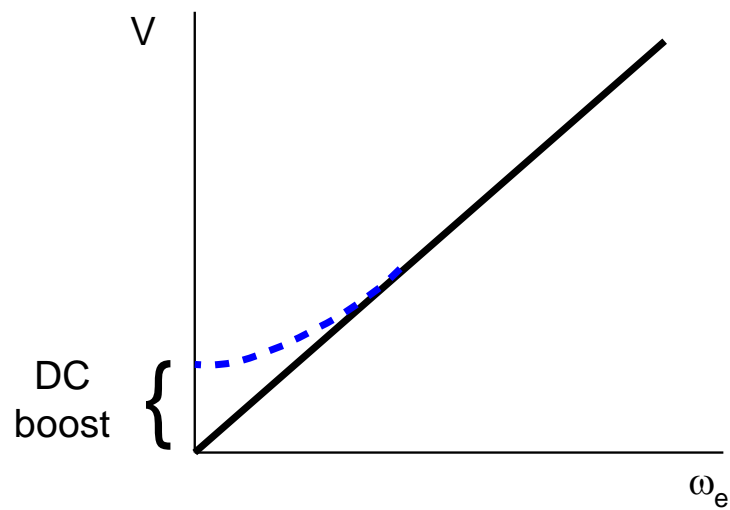
$$T_{em} = \frac{3P}{2} \frac{I_2^2 R_2}{s\omega_e}$$

Maintain constant V/f:

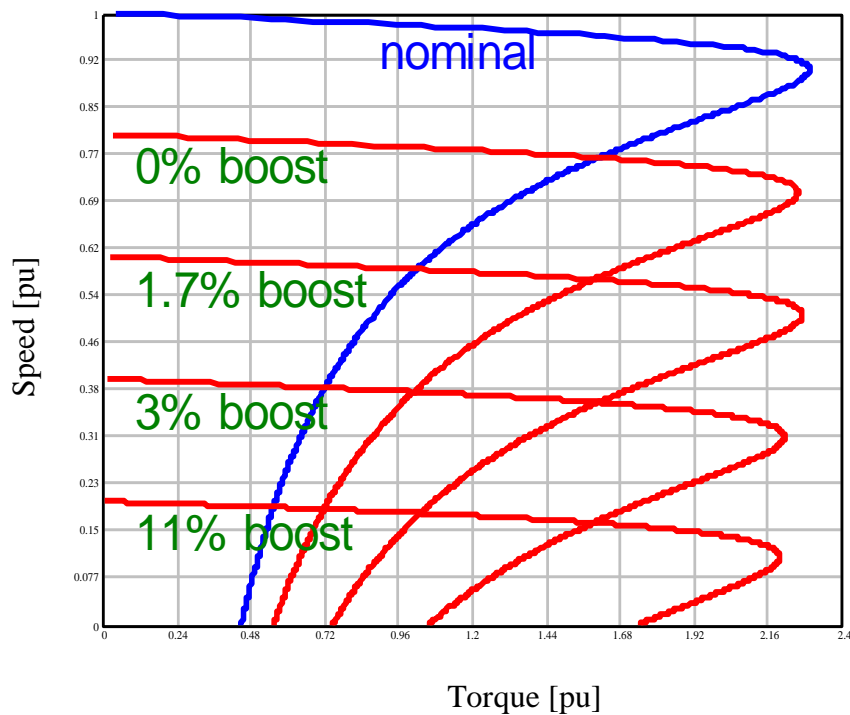
- Maintains circuit (machine) impedance
- Maintains stator current
- Maintains rotor current (and thus torque)
- Maintains magnetizing current (and thus flux)



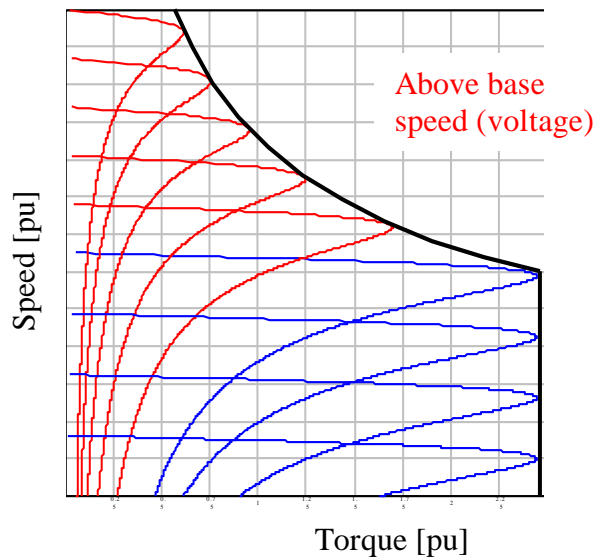
Stator resistance causes deviation from ideal \rightarrow use **voltage boost** to (partially) compensate



Typical Voltage Boost Strategy for V/Hz Drives



Induction Motor Speed Torque Curves with Constant V/Hz with Boost



Induction Motor Capability Curves

Recap – Constant Volts/Hz operation:

$$Z_{in} = R_1 + j\omega_e L_{ls} + j\omega_e L_m \parallel \left(\frac{R_2}{s} + j\omega_e L_{lr} \right)$$

Neglecting R_1

$$Z_{in}(\omega_e) = j\omega_e L_{ls} + j\omega_e L_m \parallel \left(\frac{R_2}{s\omega_e} + j\omega_e L_{lr} \right)$$

$$T_{em} = \frac{3P}{2} \frac{I_2^2 R_2}{s\omega_e} \quad s\omega_e = \omega_e - \omega_r = \text{constant}$$

