

An arbitrary rotation without matrices

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February 1, 2018

NOTE: This paper uses the nomenclature that \mathbf{w} is a vector and $\hat{\mathbf{w}}$ is a unit vector.

A right-handed (RH) rotation, by some angle ψ about some axis $\hat{\mathbf{x}}$, can be defined without matrices. The victim vector \mathbf{w} is projected into three pieces: (\mathbf{w}_{\parallel}) the piece parallel to the axis, (\mathbf{w}_{\perp}) the piece perpendicular to the axis, and (\mathbf{w}'_{\perp}) , the perpendicular \mathbf{w}_{\perp} rotated by 90° . The parallel piece is unaltered by the rotation, and the two \mathbf{w}_{\perp} form a basis for the rotation;

$$\mathbf{w}' = R(\mathbf{w}) = \underbrace{(\mathbf{w} \cdot \hat{\mathbf{x}})\hat{\mathbf{x}}}_{\mathbf{w}_{\parallel}} + \underbrace{\cos \psi (\mathbf{w} - \mathbf{w}_{\parallel})}_{\mathbf{w}_{\perp}} + \underbrace{\sin \psi (\hat{\mathbf{x}} \times \mathbf{w})}_{\mathbf{w}'_{\perp}}. \quad (1)$$

We can validate this scheme by showing it preserves the defining properties of rotations. First, the angle to the axis is unaltered;

$$\begin{aligned} \mathbf{w}' \cdot \hat{\mathbf{x}} &= (\mathbf{w} \cdot \hat{\mathbf{x}}) \cancel{\hat{\mathbf{x}} \cdot \hat{\mathbf{x}}^1} + \cos \psi (\mathbf{w} \cdot \hat{\mathbf{x}} - (\mathbf{w} \cdot \hat{\mathbf{x}}) \cancel{\hat{\mathbf{x}} \cdot \hat{\mathbf{x}}^1}) + \sin \psi ((\hat{\mathbf{x}} \times \mathbf{w}) \cdot \hat{\mathbf{x}})^0 \\ &= \mathbf{w} \cdot \hat{\mathbf{x}} \end{aligned} \quad (2)$$

(which uses $\mathbf{a} \cdot (\mathbf{b} \times \mathbf{c}) = \mathbf{b} \cdot (\mathbf{c} \times \mathbf{a}) = \mathbf{c} \cdot (\mathbf{a} \times \mathbf{b})$). Second, the vector's length is unaltered;

$$\begin{aligned} |\mathbf{w}'|^2 &= (\mathbf{w} \cdot \hat{\mathbf{x}})^2 \cancel{\hat{\mathbf{x}} \cdot \hat{\mathbf{x}}^1} + \cos^2 \psi (|\mathbf{w}|^2 - 2(\mathbf{w} \cdot \hat{\mathbf{x}})^2 + (\mathbf{w} \cdot \hat{\mathbf{x}})^2) + \sin^2 \psi |\mathbf{w}|^2 (|\mathbf{w}|^2 - (\mathbf{w} \cdot \hat{\mathbf{x}})^2) \\ &= (\mathbf{w} \cdot \hat{\mathbf{x}})^2 + (\sin^2 \psi + \cos^2 \psi) (|\mathbf{w}|^2 - (\mathbf{w} \cdot \hat{\mathbf{x}})^2) \\ &= |\mathbf{w}|^2 \end{aligned} \quad (3)$$

Here, we have used the identity $|\mathbf{u} \times \mathbf{v}|^2 = |\mathbf{u}|^2 |\mathbf{v}|^2 - (\mathbf{u} \cdot \mathbf{v})^2$ (from $\epsilon_{ijk} \epsilon_{ilm} = \delta_{jl} \delta_{km} - \delta_{jm} \delta_{kl}$), and implicitly used the orthogonality of the each component vector

$$\mathbf{w}_{\parallel} \cdot \mathbf{w}_{\perp} = (\mathbf{w} \cdot \hat{\mathbf{x}})^2 - (\mathbf{w} \cdot \hat{\mathbf{x}})^2 = 0, \quad (4)$$

$$\mathbf{w}_{\perp} \cdot \mathbf{w}'_{\perp} = \mathbf{w} \cdot (\hat{\mathbf{x}} \times \mathbf{w})^0 - (\mathbf{w} \cdot \hat{\mathbf{x}}) \hat{\mathbf{x}} \cdot (\hat{\mathbf{x}} \times \mathbf{w})^0 = 0. \quad (5)$$

Instead of an axis $\hat{\mathbf{x}}$ and angle ψ as our input degrees of freedom, we may want the rotation that takes vector $\mathbf{u} \rightarrow \mathbf{v}$. We can reuse Eq. 1, and define:

$$\cos \psi = \hat{\mathbf{u}} \cdot \hat{\mathbf{v}} \quad (6)$$

$$\sin \psi = |\mathbf{u} \times \mathbf{v}| \quad (7)$$

$$\hat{\mathbf{x}}_1 = \frac{\hat{\mathbf{u}} \times \hat{\mathbf{v}}}{|\hat{\mathbf{u}} \times \hat{\mathbf{v}}|} = \frac{\hat{\mathbf{u}} \times \hat{\mathbf{v}}}{\sin \psi} \quad (8)$$

However, $\hat{\mathbf{x}}_1$ is only one *possible* rotation axis which takes $\mathbf{u} \rightarrow \mathbf{v}$. Consider a rotation of $\psi = \pi$ about the axis bisecting the two normalized vectors

$$\hat{\mathbf{x}}_2 = \frac{\hat{\mathbf{u}} + \hat{\mathbf{v}}}{|\hat{\mathbf{u}} + \hat{\mathbf{v}}|} = \frac{\hat{\mathbf{u}} + \hat{\mathbf{v}}}{\sqrt{2(1 + \hat{\mathbf{u}} \cdot \hat{\mathbf{v}})}}. \quad (9)$$

This rotation also clearly takes $\mathbf{u} \rightarrow \mathbf{v}$. In fact, any axis which satisfies

$$\hat{\mathbf{u}} \cdot \hat{\mathbf{x}} = \hat{\mathbf{v}} \cdot \hat{\mathbf{x}} \quad (10)$$

defines a valid rotation (since \mathbf{u} and \mathbf{v} will have the same latitude relative to $\hat{\mathbf{x}}$, and thus trace out the same circle during the rotation). Thus, “the rotation which takes $\mathbf{u} \rightarrow \mathbf{v}$ ” is ambiguous.

This ambiguity stems from a hidden degree of freedom. We are free to choose (x, y, z) vectors

$$\mathbf{u} = (0, 0, 1) \quad (11)$$

$$\mathbf{v} = (\cos \phi \sin \theta, \sin \phi \sin \theta, \cos \theta) \quad (12)$$

We can get from \mathbf{u} to \mathbf{v} in two steps: (i) A RH rotation about $\hat{\mathbf{z}}$ by angle ϕ . (ii) A RH rotation about $\hat{\mathbf{y}}'$ (the new y -axis, after the first rotation) by angle θ . This procedure uses only two of the three Euler angles required to cover $\text{SO}(3)$, the group of 3-dimensional rotations. To complete the coverage, we need a final RH rotation about $\hat{\mathbf{z}}''$ (the final z -axis, which in our case is the newly minted \mathbf{v}).

By construction, this post-rotation about \mathbf{v} by angle ω cannot alter \mathbf{v} , so it does not spoil the original purpose of this rotation (take $\mathbf{u} \rightarrow \mathbf{v}$). Instead, ω determines what happens to *every other* vector, and does so by selecting *one* axis $\hat{\mathbf{x}}$ from the set which map $\mathbf{u} \rightarrow \mathbf{v}$. If we can find this $\hat{\mathbf{x}}$, we can describe the complete operation as a single rotation (instead of two sequential rotations). We have already found two valid $\hat{\mathbf{x}}$ (Eqs. 8 and 9), and they are fortuitously orthogonal, so we can use them to construct a basis that parameterizes all possible axes of rotation

$$\hat{\mathbf{x}} = a \hat{\mathbf{x}}_1 + b \hat{\mathbf{x}}_2 \quad (13)$$

Our task is now clear; given \mathbf{u} , \mathbf{v} and ω , determine a and b to find $\hat{\mathbf{x}}$.

R_1 is the rotation about $\hat{\mathbf{x}}_1$ by $\theta = \arccos(\hat{\mathbf{u}} \cdot \hat{\mathbf{v}})$ and R_2 is the rotation about $\hat{\mathbf{x}}_2$ by ω . Applying them consecutively produces a composite rotation which cannot alter the axis of rotation;

$$\hat{\mathbf{x}} = R_2(R_1(\hat{\mathbf{x}})) . \quad (14)$$

Since this defining property applies to both of $\hat{\mathbf{x}}$'s component individually (and linearly), we can solve for a and b by using unitarity as one equation (i.e. $a^2 + b^2 = 1$), then obtain the other equation by calculating

$$\begin{aligned} a &= R_2(R_1(a \hat{\mathbf{x}}_1 + b \hat{\mathbf{x}}_2)) \cdot \hat{\mathbf{x}}_1 \\ &= a R_2(R_1(\hat{\mathbf{x}}_1)) \cdot \hat{\mathbf{x}}_1 + b R_2(R_1(\hat{\mathbf{x}}_2)) \cdot \hat{\mathbf{x}}_1 . \end{aligned} \quad (15)$$

Beginning with $\hat{\mathbf{x}}_1$, we are lucky that R_1 does not alter it's own axis, while R_2 creates only one term parallel to $\hat{\mathbf{x}}_1$;

$$R_1(\hat{\mathbf{x}}_1) = \hat{\mathbf{x}}_1 ; \quad (16)$$

$$R_2(R_1(\hat{\mathbf{x}}_1)) \cdot \hat{\mathbf{x}}_1 = ((\hat{\mathbf{x}}_1 \cdot \hat{\mathbf{v}}) \hat{\mathbf{v}} + \cos \omega (\hat{\mathbf{x}}_1 - 0) + \sin \omega \underbrace{(\hat{\mathbf{v}} \times \hat{\mathbf{x}}_1)}_{\perp \text{ to } \hat{\mathbf{x}}_1}) \cdot \hat{\mathbf{x}}_1 = \cos \omega \quad (17)$$

The effect on $\hat{\mathbf{x}}_2$ is slightly more complicated;

$$\begin{aligned} R_1(\hat{\mathbf{x}}_2) &= ((\hat{\mathbf{x}}_2 \cdot \hat{\mathbf{x}}_1) \hat{\mathbf{x}}_1 + \cos \theta (\hat{\mathbf{x}}_2 - 0) + \sin \theta (\hat{\mathbf{x}}_1 \times \hat{\mathbf{x}}_2)) \\ &= \frac{1}{\sqrt{2(1 + \cos(\theta))}} \left(\cos \theta (\hat{\mathbf{u}} + \hat{\mathbf{v}}) + \sin \theta \frac{(\hat{\mathbf{u}} \times \hat{\mathbf{v}})}{\sin \theta} \times (\hat{\mathbf{u}} + \hat{\mathbf{v}}) \right) \\ &= \frac{1}{\sqrt{2(1 + \cos(\theta))}} (\cos \theta (\hat{\mathbf{u}} + \hat{\mathbf{v}}) + \hat{\mathbf{v}} - \hat{\mathbf{u}} \cos \theta + \hat{\mathbf{v}} \cos \theta - \hat{\mathbf{u}}) \\ &= \frac{1}{\sqrt{2(1 + \cos(\theta))}} ((2 \cos \theta + 1) \hat{\mathbf{v}} - \hat{\mathbf{u}}) \end{aligned} \quad (18)$$

(using $(\mathbf{a} \times \mathbf{b}) \times \mathbf{c} = \mathbf{b}(\mathbf{a} \cdot \mathbf{c}) - \mathbf{a}(\mathbf{b} \cdot \mathbf{c})$). Before we put all of Eq. 18 through R_2 , we should recall that the final equation only uses terms parallel to $\hat{\mathbf{x}}_1$. R_2 only returns terms which are (i) parallel to the incoming vector (which in this case is in the uv -plane, and thus orthogonal to $\hat{\mathbf{x}}_1$), (ii) parallel to $\hat{\mathbf{v}}$ (also in the uv plane) and (iii) perpendicular to $\hat{\mathbf{v}}$ (via $\hat{\mathbf{v}} \times \mathbf{w}$). Hence, only the 3rd piece is meaningful, and since $\hat{\mathbf{v}} \times \hat{\mathbf{v}} = 0$, we only need to give it Eq. 18's $\hat{\mathbf{u}}$ term;

$$\begin{aligned} R_2(R_1(\hat{\mathbf{x}}_2)) \cdot \hat{\mathbf{x}}_1 &= \frac{1}{\sqrt{2(1 + \cos(\theta))}} R_2(-\hat{\mathbf{u}}) \cdot \hat{\mathbf{x}}_1 = \frac{1}{\sqrt{2(1 + \cos(\theta))}} (\hat{\mathbf{v}} \times (-\hat{\mathbf{u}})) \cdot \hat{\mathbf{x}}_1 \\ &= \sin \omega \frac{\sin \theta}{\sqrt{2(1 + \cos(\theta))}} \end{aligned} \quad (19)$$

(using $\hat{\mathbf{u}} \times \hat{\mathbf{v}} = \sin \theta \hat{\mathbf{x}}_1$). Combining Eq. 15, 16 and 19 we get

$$a = a \cos \omega + b \sin \omega \frac{\sin \theta}{\sqrt{2(1 + \cos(\theta))}} \quad (20)$$

Having done the hard work, we can plug our system of equations into Mathematica to obtain

$$a = 2 \cos(\omega/2) \frac{\sin(\theta/2)}{c(\theta)} \quad (21)$$

$$b = 2 \sin(\omega/2) \frac{1}{c(\theta)} \quad (22)$$

$$c(\theta) = \sqrt{3 - \cos(\omega) - \cos(\theta)(1 + \cos(\omega))} \quad (23)$$

I then used Mathematica to validate this solution by checking that $\hat{\mathbf{x}}$ matches the eigenvector of the composite rotation $R_2(R_1(\mathbf{w}))$. However, $c(\theta)$ is numerically unstable if used naïvely, due to the cosine cancellations. These terms should be rewritten in a form which *doubles* the precision of the floating point result

$$1 - \cos(t) \mapsto 2 \sin^2(t/2). \quad (24)$$

This gives us

$$c(\theta) \mapsto \sqrt{2 \sin^2(\theta/2) + 2 \sin^2(\omega/2) + (1 - \cos(\theta) \cos(\omega))}. \quad (25)$$

The final cancellation can be corrected using

$$\cos(\theta) \cos(\omega) = \frac{1}{2}(\cos(\theta + \omega) + \cos(\theta - \omega)); \quad (26)$$

$$(1 - \cos(\theta) \cos(\omega)) \mapsto \frac{1}{2}(1 - \cos(\theta + \omega)) + \frac{1}{2}(1 - \cos(\theta - \omega)). \quad (27)$$

Again using Eq. 24, we obtain the final expression

$$c(\theta) \mapsto \sqrt{2 \sin^2(\theta/2) + 2 \sin^2(\omega/2) + \sin^2(\theta + \omega) + \sin^2(\theta - \omega)}. \quad (28)$$

Given \mathbf{u} , \mathbf{v} and ω , we now have the tools to find the axis $\hat{\mathbf{x}}$ about which the composite rotations occur.¹ But what is the angle ψ of rotation? We can determine ψ empirically by projecting $\hat{\mathbf{u}}$ and $\hat{\mathbf{v}}$ into the plane of rotation (e.g. $\hat{\mathbf{u}}_{\perp} = \hat{\mathbf{u}} - (\hat{\mathbf{u}} \cdot \hat{\mathbf{x}})\hat{\mathbf{x}}$). The rotation angle is then defined via

$$\psi = \text{atan2}(\sin \psi, \cos \psi) = \text{atan2}(\text{sign}(a)|\hat{\mathbf{u}}_{\perp} \times \hat{\mathbf{v}}_{\perp}|, \hat{\mathbf{u}}_{\perp} \cdot \hat{\mathbf{v}}_{\perp}). \quad (29)$$

¹There is one class of system where $\hat{\mathbf{x}}$ remains ambiguous; when \mathbf{u} and \mathbf{v} are antiparallel, $\hat{\mathbf{x}}_1$ and $\hat{\mathbf{x}}_2$ are both null. If \mathbf{x} is supplied externally, ω rotates it around the shared uv axis, but \mathbf{x} cannot be determined from ω alone.

It is best to use `atan2` because it is more precise for angles near 0, $\pi/2$ and π . Note that we have to inject the *sign* of a into $\sin(\psi)$, because when $a < 0$, the RH rotation becomes larger than π , so we must instead use a *negative* RH rotation.

I have tested an implementation of this algorithm and it works quite well (it is both length and angle preserving). I have additionally validated that rotating once about $\hat{\mathbf{x}}$ gives the same result as the two-step composite rotation.