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#### Warnings!!

#### **Shell Nozzles**

#### SUCTION

1.- Start Elevation is less than min elevation per table 5.6.

## **Project Design Data and Summary**

#### Back

### **Project Data**

Job : 2024-08-23-00-09 Date of Calcs. : 26-Aug-2024

Mfg. or Insp. Date : Designer : Melior

Project:

Tag ID: Q9003

Plant:

Plant Location:

Site:

Design Basis: API-650 13th Edition Errata 1, 2021

Annexes Used: E, J, S

# Design Parameters and Operating Conditions Design Parameters

Design Internal Pressure = 0 psi or 0 inh2o Design External Pressure = -0 psi or -0 inh2o

D of Tank = 10 ft

OD of Tank = 10.0313 ft

ID of Tank = 10 ft

 $CL ext{ of } Tank = 10.0156 ext{ ft}$ 

Shell Height = 17 ft

S.G of Contents = 1

S.G of Hydrotest = 1

Hydrotest Liquid Level = 17 ft

Max Design Liq. Level = 17 ft

Max Operating Liq. Level = 17 ft

Min Liq. Level = 1 ft

Design Temperature = 100 °F

MDMT (Minimum Design Metal Temperature) = -20 °F

Tank Joint Efficiency = 0.7

Ground Snow Load = 0 psf

Roof Live Load = 20 psf

Additional Roof Dead Load = 0 psf

Wind Load Basis: ASCE 7-05

3 Second Gust Wind Speed (entered), Vg = 109 mph

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Wind Importance Factor, Iw = 1
Design Wind Speed, V = Vg \* SQRT(Iw) = 109 mph

Seismic Method: API-650 - ASCE7 Mapped(Ss & S1)

Seismic Use Group = II

Site Class = C

 $T_L (sec) = 12$ 

Ss(g) = 0.121

S1(g) = 0.049

Av(g) = 0.0452

Q = 0.6667

Importance Factor = 1.25

### **Design Remarks**

## **Summary Results**

### Shell

Shell #	Width (in)	Material	CA (in)	JE	Min Yield Strength (psi)	Tensile Strength (psi)	Sd (psi)	St (psi)	Weight (lbf)
1	60	A240- 304	0	0.7000	30,000	75,000	22,500	27,000	1,228
2	48	A240- 304	0	0.7000	30,000	75,000	22,500	27,000	982
3	48	A240- 304	0	0.7000	30,000	75,000	22,500	27,000	982
4	48	A240- 304	0	0.7000	30,000	75,000	22,500	27,000	982

#### (continued)

Shell #	Weight CA (lbf)	t-min Erection (in)	t-Des (in)	t-Test (in)	t-min Seismic (in)	t-min Ext- Pe (in)	t-min (in)	t-Actual (in)	Status
1	1,228	0.1875	0.0264	0.022	0.0239	NA	0.1875	0.1875	OK
2	982	0.1875	0.0182	0.0151	0.0169	NA	0.1875	0.1875	OK
3	982	0.1875	0.0116	0.0096	0.0113	NA	0.1875	0.1875	OK
4	982	0.1875	0.005	0.0041	0.0057	NA	0.1875	0.1875	OK

Total Weight of Shell = 4,188.308 lbf

### Roof

Type = Self Supported Conical Roof Plates Material = A240-304 t.required = 0.1875 in t.actual = 0.1875 in Roof corrosion allowance = 0 in Roof Joint Efficiency = 0.7 Plates Overlap Weight = 7.1487 lbf

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### **Bottom**

Type: Flat Bottom Non Annular
Bottom Material = A240-304
t.required = 0.1875 in
t.actual = 0.1875 in
Bottom corrosion allowance = 0 in
Bottom Joint Efficiency = 0.7
Total Weight of Bottom = 639.55 lbf

### Top Member

Type = Detail B Size = L2x2x1/4 Material = A240-304 Weight = 100.397 lbf

### **Anchors**

Quantity = 4 Size = 1 in Material = A36 Bolt Hole Circle Radius = 5.1822 ft

## Nameplate Information

Pressure Combination Factor	0.4
Design Standard	API-650 13th Edition Errata 1, 2021
Appendices Used	E, J, S
Roof	A240-304 : 0.1875 in
Shell (1)	A240-304 : 0.1875 in
Shell (2)	A240-304 : 0.1875 in
Shell (3)	A240-304 : 0.1875 in
Shell (4)	A240-304 : 0.1875 in
Bottom	A240-304 : 0.1875 in

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## Anchor Chair Design Back

### Anchor Chair Design per AISI T-192 Part V

a = Top Plate Width Along Shell (in) b = Top Plate Length (in) bmin = Top Plate Minimum Length (in) c = Top Plate Thickness (in)CA = Chair Corrosion Allowance (in) c\_corr = Top Plate Corroded Thickness (in) D = Tank Nominal Diameter (ft) d = Anchor Bolt Diameter (in) e = Anchor Bolt Eccentricity (in) Earthquakes-Considered = Earthquakes Considered emin = Minimum Calculated Eccentricity (in) emin-btm = Minimum Eccentricity Based on Bolt Clearance From Bottom Plates per API-650 5.12.4 (in) emin-req = Minimum Required Eccentricity (in) Et = Bottom Plates Thermal Expansion Coefficient per API-650 Table P.1b (in/in.fdeg) f = Top Plate Outside To Hole Edge Distance (in) f min = Distance from Outside of Top Plate to Edge of Hole per AISI T-192 Part V, Notation g = Vertical Plates Distance (in) g min = Minimum Distance Between Vertical Plates per AISI T-192, PartV, Notation (in) h = Chair Height (in) h-eff = Effective Chair Height (in) hmax = Chair Maximum Height (in) j = Vertical Plate Thickness (in) i corr = Vertical Plate Corroded Thickness (in) i\_min = Vertical Plate Minimum Thickness per AISI T-192 Part V, Vertical Side Plates (in) k = Vertical Plates Average Width (in) m = Base or Bottom Plate Thickness (in) Ma-chair = Chair Material outside-projection = Bottom Outside Projection (in) R = Nominal Shell Radius (in) Ssw-chair = Chair Allowable Stress for Seismic or Wind Design per API-650 5.12.9 (psi) T = Difference between ambient and design temperature per API 650 5.12.4 (°F) t = Shell Thickness (in)T ambient = Ambient Temperature ( $^{\circ}$ F) T\_design = Design Temperature (°F) V = Wind Velocity (mph) Y-bolt = Anchor Bolt Yield Load (lbf) a = 6 inb = 8 in

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c = 0.375 in

```
CA = 0 in
d = 1 in
D = 10 \text{ ft}
e = 2 in
Earthquakes-Considered = ASCE7-MAPPED-SS-AND-S1
Et = 6.67E-6 \text{ in/in.fdeg}
f = 4.0 in
g = 3 in
h = 12 in
j = 0.5 \text{ in}
k = 4.4124 \text{ in}
m = 0.1875 in
Ma-chair = A240-304
outside-projection = 1 in
R = 60.0 \text{ in}
t = 0.1875 in
T ambient = 0 \, ^{\circ}F
T_design = 100 \, ^{\circ}F
V = 109.0 \text{ mph}
Y-bolt = 19,831.7945 lbf
```

#### **Anchor Chair Material Properties**

Material = A240-304 Minimum Tensile Strength (Sut-chair) = 75,000 psi As per API-650 S.5.b, Minimum Yield Strength (Sy-chair) = 30,000 psi As per API-650 S.2b, Allowable Design Stress (Sd-chair) = 22,500 psi As per API-650 S.2b, Allowable Hydrostatic Test Stress (St-chair) = 27,000 psi

Ssw-chair = 1.33 \* Sd-chair Ssw-chair = 1.33 \* 22,500 Ssw-chair = 29,925 psi

#### **Size Requirements**

c\_corr = c - (2 \* CA) c\_corr = 0.375 - (2 \* 0) c\_corr = 0.375 in

j\_corr = j - (2 \* CA) j\_corr = 0.5 - (2 \* 0) j\_corr = 0.5 in

Chair Minimum Height (hmin) = 12 in

h >= hmin ==> PASS

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## Appurtenances Design Back

## Plan View

LABEL	MARK	CUST. MARK	DESCRIPTION	OUTSIDE PROJ (in)	INSIDE PROJ (in)	ORIENT	RADIUS (in)	REMARKS	REF DWG
Circular- Manway- 0001	RM01A	N11	24" ROOF MANWAY	8"	1"	60 '	2'-11"		Ì
FILL	RN02A	N5	3" ROOF NOZZLE	6"	1"	0 '	3'-9"		
LEVEL	RN02A	N8	3" ROOF NOZZLE	6"	1"	240 '	3'-9"		
LEVEL	RN02A	N12	3" ROOF NOZZLE	6"	1"	180 '	3'-9"		
PRESSURE	RN02A	N6	3" ROOF NOZZLE	6"	1"	120 '	3'-9"		
SPARE	RN01A	N4	3" ROOF NOZZLE	6"	1"	270 '	3'-9"	W/ BLIND	
VALVE	RN03A	N7	6" ROOF NOZZLE	6"	1"	0 '	0"		
VAPOR	RN02A	N10	3" ROOF NOZZLE	6"	1"	300 '	3'-9"		

## **Elevation View**

LABEL	MARK	CUST. MARK	DESCRIPTION	OUTSIDE PROJ (in)		ORIENT	ELEVATION (in)	REMARKS	REF DWG
Anchor- Chair- Bolts	AC01A		ANCHOR CHAIRS			SEE TABLE			
Circular- Manway- 0001		N2	24" SHELL MANWAY	11"	0"	135 '	2'-6"	W/ DAVIT	
LEVEL	SN01A	N3	3" SHELL NOZZLE	7"	0"	180 '	1'-9 1/2"		
Name- Plate	NP01A		STD API			0 '	3'-4"		

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SPARE	SN02A	N14	3" SHELL NOZZLE	7"	0"	180 '	8"	W/ BLIND	
SPARE	SN02A	N9	3" SHELL NOZZLE	7"	0"	270 '	8"	W/ BLIND	
SUCTION	SN01A	N1	3" SHELL NOZZLE	7"	0"	0 '	1 9/16"		
TEMP	SN03A	N13	3" SHELL NOZZLE	7"	0"	342 '	8"		

#### Warnings!!

#### **Shell Nozzles**

#### **SUCTION**

1.- Start Elevation is less than min elevation per table 5.6.

### Shell Nozzle: SUCTION

### Repad Design

NOZZLE Description: 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)

t\_n = (Thickness of Neck)

Sd\_n = (Stress of Neck Material)

Sd\_s = (Stress of Shell Course Material)

CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 1: Elevation = 0.1302 ft

#### **COURSE PARAMETERS:**

t-calc = 0.0264 in

t\_cr = 0.0264 in (Course t-calc less C.A)

c = 0.1875 in (Course t less C.A.)

t Basis = 0.0264 in

(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)

Required Area = t\_Basis \* D

Required Area = 0.0264 \* 3.5

Required Area = 0.0924 in2

Available Shell Area = (t\_c - t\_Basis) \* D

Available Shell Area = (0.1875 - 0.0264) \* 3.5

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Available Shell Area = 0.5638 in2

Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - CA) * MIN((Sd_n/Sd_s) 1)$ Available Nozzle Neck Area = 2 \* [(4 \* (0.216 - 0)) + 0.1875] \* (0.216 - 0) \* MIN((22,500/22,500) 1)Available Nozzle Neck Area = 0.4542 in2

A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area) A-rpr = 0.0924 - 0.5638 - 0.4542 A-rpr = 0 in2

Since A-rpr  $\leq 0$ ,  $t_rpr = 0$ 

No Reinforcement Pad required.

#### Notes:

- As per API-650 J.3.6.6, the provisions for stress relief specified in API-650 5.7.4 and 5.7.8.3 are not required

#### **Nozzle Neck Material Properties**

Material = A312-TP304

As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22,500 psi

### Shell Nozzle: LEVEL

### Repad Design

NOZZLE Description: 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)

t\_n = (Thickness of Neck)

Sd\_n = (Stress of Neck Material)

Sd\_s = (Stress of Shell Course Material)

CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 1: Elevation = 1.7917 ft

#### **COURSE PARAMETERS:**

t-calc = 0.0264 in

t\_cr = 0.0264 in (Course t-calc less C.A)

 $t_c = 0.1875$  in (Course t less C.A.)

t Basis = 0.0264 in

(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)

Required Area = t\_Basis \* D Required Area = 0.0264 \* 3.5 Required Area = 0.0924 in2

Available Shell Area = (t\_c - t\_Basis) \* D

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```
Available Shell Area = (0.1875 - 0.0264) * 3.5

Available Shell Area = 0.5638 in2

Available Nozzle Neck Area = 2 * [(4 * (t_n - CA)) + t_c] * (t_n - CA) * MIN((Sd_n/Sd_s) 1)

Available Nozzle Neck Area = 2 * [(4 * (0.216 - 0)) + 0.1875] * (0.216 - 0) * MIN((22,500/22,500) 1)

Available Nozzle Neck Area = 0.4542 in2

A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area)

A-rpr = 0.0924 - 0.5638 - 0.4542

A-rpr = 0 in2

Since A-rpr <= 0, t_rpr = 0
```

No Reinforcement Pad required.

#### **Nozzle Neck Material Properties**

Material = A312-TP304 As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22,500 psi

### Shell Nozzle: SPARE

### Repad Design

NOZZLE Description: 3 in SCH 40S TYPE RFSO Material: A312-TP304

t\_rpr = (Repad Required Thickness)
t\_n = (Thickness of Neck)
Sd\_n = (Stress of Neck Material)
Sd\_s = (Stress of Shell Course Material)
CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 1 : Elevation = 0.6667 ft

#### **COURSE PARAMETERS:**

t-calc = 0.0264 in t\_cr = 0.0264 in (Course t-calc less C.A) t\_c = 0.1875 in (Course t less C.A.) t\_Basis = 0.0264 in Repad Type: Dog House Repad Size (Do): = 10.5 in

(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)

Required Area = t\_Basis \* D Required Area = 0.0264 \* 3.5 Required Area = 0.0924 in2

Available Shell Area = (t\_c - t\_Basis) \* D Available Shell Area = (0.1875 - 0.0264) \* 3.5

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Available Shell Area = 0.5638 in2

Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - CA) * MIN((Sd_n/Sd_s) 1)$ Available Nozzle Neck Area = 2 \* [(4 \* (0.216 - 0)) + 0.1875] \* (0.216 - 0) \* MIN((22,500/22,500) 1)Available Nozzle Neck Area = 0.4542 in2

A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area) A-rpr = 0.0924 - 0.5638 - 0.4542 A-rpr = 0 in2

Since A-rpr  $\leq 0$ , t rpr = 0

No Reinforcement Pad required.

#### **Nozzle Neck Material Properties**

Material = A312-TP304 As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22,500 psi

#### **Nozzle Repad Material Properties**

Material = A240-304

### Shell Nozzle: TEMP

### Repad Design

NOZZLE Description: 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)

t n = (Thickness of Neck)

Sd\_n = (Stress of Neck Material)

Sd\_s = (Stress of Shell Course Material)

CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 1: Elevation = 0.6667 ft

#### COURSE PARAMETERS:

t-calc = 0.0264 in

t cr = 0.0264 in (Course t-calc less C.A)

t = 0.1875 in (Course t less C.A.)

t Basis = 0.0264 in

Repad Type: Dog House

Repad Size (Do): = 10.5 in

(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)

Required Area = t\_Basis \* D Required Area = 0.0264 \* 3.5

Required Area = 0.0924 in2

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```
Available Shell Area = (t_c - t_basis) * D

Available Shell Area = (0.1875 - 0.0264) * 3.5

Available Nozzle Neck Area = 2 * [(4 * (t_n - CA)) + t_c] * (t_n - CA) * MIN((Sd_n/Sd_s) 1)

Available Nozzle Neck Area = 2 * [(4 * (0.216 - 0)) + 0.1875] * (0.216 - 0) * MIN((22,500/22,500) 1)

Available Nozzle Neck Area = 0.4542 in2

A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area)

A-rpr = 0.0924 - 0.5638 - 0.4542

A-rpr = 0.0924 - 0.5638 - 0.4542

Since A-rpr <= 0, t_rpr = 0
```

No Reinforcement Pad required.

#### **Nozzle Neck Material Properties**

Material = A312-TP304 As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22,500 psi

#### **Nozzle Repad Material Properties**

Material = A240-304

### Shell Nozzle: SPARE

### Repad Design

NOZZLE Description: 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)
t\_n = (Thickness of Neck)
Sd\_n = (Stress of Neck Material)
Sd\_s = (Stress of Shell Course Material)
CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 1: Elevation = 0.6667 ft

#### COURSE PARAMETERS:

t-calc = 0.0264 in t\_cr = 0.0264 in (Course t-calc less C.A) t\_c = 0.1875 in (Course t less C.A.) t\_Basis = 0.0264 in Repad Type: Dog House Repad Size (Do): = 10.5 in

(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)

Required Area = t\_Basis \* D Required Area = 0.0264 \* 3.5

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```
Required Area = 0.0924 in2
```

Available Shell Area = (t\_c - t\_Basis) \* D Available Shell Area = (0.1875 - 0.0264) \* 3.5 Available Shell Area = 0.5638 in2

Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - CA) * MIN((Sd_n/Sd_s) 1)$ Available Nozzle Neck Area = 2 \* [(4 \* (0.216 - 0)) + 0.1875] \* (0.216 - 0) \* MIN((22,500/22,500) 1)Available Nozzle Neck Area = 0.4542 in2

A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area) A-rpr = 0.0924 - 0.5638 - 0.4542 A-rpr = 0 in2

Since A-rpr  $\leq 0$ ,  $t_rpr = 0$ 

No Reinforcement Pad required.

#### **Nozzle Neck Material Properties**

Material = A312-TP304 As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22,500 psi

#### **Nozzle Repad Material Properties**

Material = A240-304

### Shell Manway: Circular-Manway-0001

### Repad Design

MANWAY Description: 24 in Neck Thickness 0.25

Material: A240-304

t\_rpr = (Repad Required Thickness)

t\_n = (Thickness of Neck)

Sd n = (Stress of Neck Material)

Sd\_s = (Stress of Shell Course Material)

CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 1: Elevation = 2.5 ft

#### **COURSE PARAMETERS:**

t-calc = 0.0264 in

t\_cr = 0.0264 in (Course t-calc less C.A)

t = 0.1875 in (Course t less C.A.)

t Basis = 0.0264 in

(SHELL MANWAY REF. API-650 TABLE 5-6, AND FOOTNOTE A OF TABLE 5-7)

Required Area = t\_Basis \* D

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```
Required Area = 0.0264 * 24
Required Area = 0.6339 in 2
Available Shell Area = (t_c - t_Basis) * D
Available Shell Area = (0.1875 - 0.0264) * 24
Available Shell Area = 3.8661 in 2
Available Manway Neck Area = 2 * [(4 * (t_n - CA)) + t_c] * (t_n - CA) * MIN((Sd_n/Sd_s) 1)
Available Manway Neck Area = 2 * [(4 * (0.25 - 0)) + 0.1875] * (0.25 - 0) * MIN((22,500/22,500) 1)
Available Manway Neck Area = 0.5938 in2
A-rpr = (Required Area - Available Shell Area - Available Manway Neck Area)
A-rpr = 0.6339 - 3.8661 - 0.5938
A-rpr = 0 in2
Since A rpr \leq 0, t rpr = 0
No Reinforcement Pad required.
Manway Neck Material Properties
Material = A240-304
As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22,500 psi
Cover Plate and Bolting Flange Design
CA-cover = Cover Plate and Bolting Flange Corrosion Allowance (in)
Db = Bolt Circle Diameter (in)
H = Design Liquid Level (ft)
M = Bolting Flange Thickness Multiplication Factor per API-650 S.3.3.3
M = Cover Plate Thickness Multiplication Factor per API-650 S.3.3.3
Ma-cover = Cover Plate Material
Ma-flange = Bolting Flange Material
Sd = Allowable Stress per API-650 5.7.5.6 (psi)
SG = Product Specific Gravity
tc = Cover Plate Thickness (in)
tc-design = Cover Plate Required Thickness per API-650 5.7.5.6 (in)
tc-reg = Cover Plate Minimum Required Thickness (in)
tf = Bolting Flange Thickness (in)
tf-design = Cover Plate Required Thickness per API-650 5.7.5.6 (in)
tf-req = Bolting Flange Minimum Required Thickness (in)
CA-cover = 0 in
Db = 30.25 in
H = 17.0 \text{ ft}
Ma-cover = A240-304
Ma-flange = A240-304
SG = 1
tc = 0.625 in
tf = 0.625 in
Water Density (Y) = 0.433 \text{ psi/ft}
As per API-650 5.7.5.6, Coefficient For Circular Plate (C) = 0.3
```

Material = A240-304

**Cover Plate Material Properties and Required Thickness** 

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```
As per API-650 S.5.b, Minimum Yield Strength at Ambient Temperature (Sy-ambient-cover) = 30,000 psi
As per API-650 S.5.b, Minimum Yield Strength (Sy-cover) = 30,000 psi
Sd = MIN(Sy-ambient-cover, 30000) / 2 = 15,000 psi
M = MAX(SQRT((Sy-ambient-cover / Sy-cover)), SQRT((30000 / Sy-cover)), 1) = 1.0
As per API-650 5.7.5.6, Cover Plate Erection Thickness (tc-erec) = 0.3125 in
tc-design = ((Db * SQRT(((C * Y * H * MAX(SG , 1)) / Sd))) + CA-cover) * M
tc-design = ((30.25 * SQRT(((0.3 * 0.433 * 17.0 * MAX(1, 1)) / 15,000))) + 0) * 1.0)
tc-design = 0.367 in
tc-req = MAX(tc-erec, tc-design)
tc\text{-req} = MAX(0.3125, 0.367)
tc\text{-req} = 0.367 in
t-cover >= tc-req ==> PASS
Bolting Flange Material Properties and Required Thickness
Material = A240-304
As per API-650 S.5.b, Minimum Yield Strength at Ambient Temperature (Sy-ambient-flange) = 30,000 psi
As per API-650 S.5.b, Minimum Yield Strength (Sy-flange) = 30,000 psi
M = MAX(SQRT((Sy-ambient-flange / Sy-flange)), SQRT((30000 / Sy-flange)), 1) = 1.0
As per API-650 5.7.5.6, Bolting Flange Erection Thickness (tf-erec) = 0.25 in
tf-design = tc-design - 0.125
tf-design = 0.367 - 0.125
tf-design = 0.242 in
tf-reg = MAX(tf-erec, tf-design)
tf\text{-req} = MAX(0.25, 0.242)
tf-req = 0.25 in
```

### Roof Nozzle: SPARE

### Repad Design

t-flange >= tf-req ==> PASS

(Per API-650 and other references below)

NOZZLE Description: 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)

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t\_n = (Thickness of Neck)
Sd\_n = (Stress of Neck Material)
Sd\_s = (Stress of Roof Material)
CA = (Corrosion Allowance of Neck)

MOUNTED ON ROOF: Elevation = 17.2505 ft

#### **ROOF PARAMETERS:**

t-calc = 0.1875 in t\_cr = 0.1875 in (Roof t-act less C.A) t\_c = 0.1875 in t\_Basis = 0.1875 in

(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15)

Required Area = t\_Basis \* D Required Area = 0.1875 \* 3.5 Required Area = 0.6563 in2

Available Roof Area = (t\_c - t\_Basis) \* D Available Roof Area = (0.1875 - 0.1875) \* 3.5 Available Roof Area = 0 in2

Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)$ Available Nozzle Neck Area = 2 \* [(4 \* (0.216 - 0)) + 0.1875] \* (0.216 - 0) \* MIN((22,500/22,500) 1)Available Nozzle Neck Area = 0.4542 in2

A\_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area) A\_rpr = 0.6563 - 0 - 0.4542 A\_rpr = 0.202 in2

As per API-650 J.3.6.3, reinforcement pad is not required since roof loads do not exceed 25 psf.

No Reinforcement Pad required.

### Roof Nozzle: FILL

### Repad Design

(Per API-650 and other references below)

NOZZLE Description: 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)

t\_n = (Thickness of Neck)

Sd n = (Stress of Neck Material)

Sd s = (Stress of Roof Material)

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CA = (Corrosion Allowance of Neck)

MOUNTED ON ROOF: Elevation = 17.2505 ft

**ROOF PARAMETERS:** 

t-calc = 0.1875 in

 $t_cr = 0.1875$  in (Roof t-act less C.A)

 $t_c = 0.1875$  in

 $t_Basis = 0.1875 in$ 

(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15)

Required Area = t\_Basis \* D

Required Area = 0.1875 \* 3.5

Required Area = 0.6563 in2

Available Roof Area = (t\_c - t\_Basis) \* D

Available Roof Area = (0.1875 - 0.1875) \* 3.5

Available Roof Area = 0 in2

Available Nozzle Neck Area = 2 \* [(4 \* (t\_n - CA)) + t\_c] \* (t\_n - ca) \* MIN((Sd\_n/Sd\_s) 1)

Available Nozzle Neck Area = 2 \* [(4 \* (0.216 - 0)) + 0.1875] \* (0.216 - 0) \* MIN((22,500/22,500) 1)

Available Nozzle Neck Area = 0.4542 in2

A\_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)

A rpr = 0.6563 - 0 - 0.4542

 $A_{rpr} = 0.202 \text{ in } 2$ 

As per API-650 J.3.6.3, reinforcement pad is not required since roof loads do not exceed 25 psf.

No Reinforcement Pad required.

### Roof Nozzle: PRESSURE

### Repad Design

(Per API-650 and other references below)

NOZZLE Description: 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)

t n = (Thickness of Neck)

Sd n = (Stress of Neck Material)

Sd\_s = (Stress of Roof Material)

CA = (Corrosion Allowance of Neck)

MOUNTED ON ROOF: Elevation = 17.2505 ft

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### ROOF PARAMETERS:

t-calc = 0.1875 in t\_cr = 0.1875 in (Roof t-act less C.A) t\_c = 0.1875 in t\_Basis = 0.1875 in

(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15)

Required Area = t\_Basis \* D Required Area = 0.1875 \* 3.5 Required Area = 0.6563 in2

Available Roof Area = (t\_c - t\_Basis) \* D Available Roof Area = (0.1875 - 0.1875) \* 3.5 Available Roof Area = 0 in2

Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)$ Available Nozzle Neck Area = 2 \* [(4 \* (0.216 - 0)) + 0.1875] \* (0.216 - 0) \* MIN((22,500/22,500) 1)Available Nozzle Neck Area = 0.4542 in2

A\_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area) 
A\_rpr = 0.6563 - 0 - 0.4542 
A\_rpr = 0.202 in2

As per API-650 J.3.6.3, reinforcement pad is not required since roof loads do not exceed 25 psf.

No Reinforcement Pad required.

### Roof Nozzle: VALVE

### Repad Design

(Per API-650 and other references below)

NOZZLE Description: 6 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)
t\_n = (Thickness of Neck)
Sd\_n = (Stress of Neck Material)
Sd\_s = (Stress of Roof Material)
CA = (Corrosion Allowance of Neck)

MOUNTED ON ROOF: Elevation = 17.8753 ft

**ROOF PARAMETERS:** 

t-calc = 0.1875 in

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```
t_cr = 0.1875 in (Roof t-act less C.A)
t_c = 0.1875 in
t Basis = 0.1875 in
```

(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15)

```
Required Area = t_Basis * D
Required Area = 0.1875 * 6.625
Required Area = 1.2422 in2

Available Roof Area = (t_c - t_Basis) * D
Available Roof Area = (0.1875 - 0.1875) * 6.625
Available Roof Area = 0 in2

Available Nozzle Neck Area = 2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)
Available Nozzle Neck Area = 2 * [(4 * (0.28 - 0)) + 0.1875] * (0.28 - 0) * MIN((22,500/22,500) 1)
Available Nozzle Neck Area = 0.7322 in2

A_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)
```

As per API-650 J.3.6.3, reinforcement pad is not required since roof loads do not exceed 25 psf.

No Reinforcement Pad required.

 $A_rpr = 1.2422 - 0 - 0.7322$ 

A rpr = 0.51 in 2

### Roof Nozzle: LEVEL

### Repad Design

(Per API-650 and other references below)

NOZZLE Description: 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)
t\_n = (Thickness of Neck)
Sd\_n = (Stress of Neck Material)
Sd\_s = (Stress of Roof Material)
CA = (Corrosion Allowance of Neck)

MOUNTED ON ROOF: Elevation = 17.2505 ft

**ROOF PARAMETERS:** 

t-calc = 0.1875 in t\_cr = 0.1875 in (Roof t-act less C.A) t\_c = 0.1875 in t\_Basis = 0.1875 in

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(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15)

Required Area = t\_Basis \* D
Required Area = 0.1875 \* 3.5
Required Area = 0.6563 in2

Available Roof Area = (t\_c - t\_Basis) \* D
Available Roof Area = (0.1875 - 0.1875) \* 3.5
Available Roof Area = 0 in2

Available Nozzle Neck Area = 2 \* [(4 \* (t\_n - CA)) + t\_c] \* (t\_n - ca) \* MIN((Sd\_n/Sd\_s) 1)
Available Nozzle Neck Area = 2 \* [(4 \* (0.216 - 0)) + 0.1875] \* (0.216 - 0) \* MIN((22,500/22,500) 1)
Available Nozzle Neck Area = 0.4542 in2

A\_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)
A\_rpr = 0.6563 - 0 - 0.4542
A\_rpr = 0.202 in2

As per API-650 J.3.6.3, reinforcement pad is not required since roof loads do not exceed 25 psf.

No Reinforcement Pad required.

### Roof Nozzle: VAPOR

### Repad Design

(Per API-650 and other references below)

NOZZLE Description: 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)
t\_n = (Thickness of Neck)
Sd\_n = (Stress of Neck Material)
Sd\_s = (Stress of Roof Material)
CA = (Corrosion Allowance of Neck)

MOUNTED ON ROOF: Elevation = 17.2505 ft

ROOF PARAMETERS: t-calc = 0.1875 in  $t\text{\_cr} = 0.1875$  in (Roof t-act less C.A)  $t\text{\_c} = 0.1875$  in  $t\text{\_Basis} = 0.1875$  in

(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15)

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```
Required Area = t_Basis * D
Required Area = 0.1875 * 3.5
Required Area = 0.6563 in2

Available Roof Area = (t_c - t_Basis) * D
Available Roof Area = (0.1875 - 0.1875) * 3.5
Available Roof Area = 0 in2

Available Nozzle Neck Area = 2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)
Available Nozzle Neck Area = 2 * [(4 * (0.216 - 0)) + 0.1875] * (0.216 - 0) * MIN((22,500/22,500) 1)
Available Nozzle Neck Area = 0.4542 in2

A_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)
A_rpr = 0.6563 - 0 - 0.4542
A_rpr = 0.202 in2
```

As per API-650 J.3.6.3, reinforcement pad is not required since roof loads do not exceed 25 psf.

No Reinforcement Pad required.

### Roof Nozzle: LEVEL

### Repad Design

(Per API-650 and other references below)

NOZZLE Description: 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)
t\_n = (Thickness of Neck)
Sd\_n = (Stress of Neck Material)
Sd\_s = (Stress of Roof Material)
CA = (Corrosion Allowance of Neck)

MOUNTED ON ROOF: Elevation = 17.2505 ft

ROOF PARAMETERS: t-calc = 0.1875 in

t\_cr = 0.1875 in (Roof t-act less C.A) t c = 0.1875 in

 $t_{Basis} = 0.1875 \text{ in}$ 

(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15)

Required Area = t\_Basis \* D Required Area = 0.1875 \* 3.5

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```
Required Area = 0.6563 in2
Available Roof Area = (t_c - t_Basis) * D
Available Roof Area = (0.1875 - 0.1875) * 3.5
Available Roof Area = 0 in2
Available Nozzle Neck Area = 2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)
Available Nozzle Neck Area = 2 * [(4 * (0.216 - 0)) + 0.1875] * (0.216 - 0) * MIN((22,500/22,500) 1)
Available Nozzle Neck Area = 0.4542 in2
A rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)
A rpr = 0.6563 - 0 - 0.4542
A_{rpr} = 0.202 \text{ in } 2
As per API-650 J.3.6.3, reinforcement pad is not required since roof loads do not exceed 25 psf.
No Reinforcement Pad required.
Roof Manway: Circular-Manway-0001
Repad Design
(Per API-650 Section 5.8.4 and other references below)
MANWAY Description: 24 in Neck Thickness 0.25
Material: A240-304
t_rpr = (Repad Required Thickness)
MOUNTED ON ROOF: Elevation = 17.3894 ft
ROOF PARAMETERS:
t-calc = 0.1875 in
t_cr = 0.1875 in (Roof t-act less C.A)
t_c = 0.1875 in
t Basis = 0.1875 in
(FOR ROOF MANWAY, REF. API-650 FIG 5-16, TABLE 5-13)
Required Area = t Basis * D
Required Area = 0.1875 * 24
Required Area = 4.5 \text{ in } 2
Available Roof Area = (t c - t Basis) * D
Available Roof Area = (0.1875 - 0.1875) * 24
Available Roof Area = 0 in2
```

Available Manway Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)$ Available Manway Neck Area = 2 \* [(4 \* (0.25 - 0)) + 0.1875] \* (0.25 - 0) \* MIN((22,500/22,500) 1)

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Available Manway Neck Area = 0.5938 in2

A-rpr = (Required Area - Available Roof Area - Available Manway Neck Area) A-rpr = 4.5 - 0 - 0.5938 A-rpr = 3.9063 in 2

As per API-650 J.3.6.3, since roof loads does not exceed 25 psf, t\_rpr = 0

No Reinforcement Pad required.

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## Capacities and Weights Back

Capacity to Top of Shell (to Tank Height): 9,987 gal

Capacity to Design Liquid Level: 9,987 gal Capacity to Maximum Liquid Level: 9,987 gal

Working Capacity (to Normal Working Level): 9,987 gal

Net working Capacity (Working Capacity - Min Capacity): 9,400 gal

Minimum Capacity (to Min Liq Level): 587 gal

Component	New Condition (lbf)	Corroded (lbf)
SHELL	4,189	4,189
ROOF	647	647
RAFTERS	0	0
GIRDERS	0	0
FRAMING	0	0
COLUMNS	0	0
TRUSS	0	0
STRUCTURE COMPONENTS	0	0
воттом	639	639
STAIRWAYS	0	0
ACCESS	0	0
STIFFENERS	101	101
WIND GIRDERS	0	0
ANCHOR CHAIRS	59	59
SHELL APPURTENANCES	439	439
ROOF APPURTENANCES	262	262
BOTTOM APPURTENANCES	0	0
INSULATION	0	0
FLOATING ROOF	0	0
TOTAL	6,336.5188	6,336.5188

Weight of Tank, Empty: 6,336.5188 lbf

Weight of Tank, Full of Product (Design SG = 1): 89,688.5188 lbf

Weight of Tank, Full of Water: 89,688.8074 lbf

Net Working Weight, Full of Product (Design SG = 1): 84,785.7316 lbf

Net Working Weight Full of Water: 84,785.7316 lbf

Foundation Area Req'd: 81.6794 ft2

Foundation Loading, Empty: 77.5778 lbf/ft2

Foundation Loading, Full of Product Design: 1,098.0548 lbf/ft2

Foundation Loading, Full of Water: 1,098.0584 lbf/ft2

SURFACE AREAS Roof: 81.6893 ft2 Shell: 534.0707 ft2 Bottom: 81.6794 ft2

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