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# **Project Design Data and Summary**

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## **Project Data**

Job: 2024-09-14-06-15 Date of Calcs: 17-Sep-2024

Mfg. or Insp. Date : Designer : Melior

Project:

Tag ID: Q9027 API

Plant:

Plant Location:

Site:

Design Basis: API-650 13th Edition Errata 1, 2021

Annexes Used: E, F, J, M, S

# Design Parameters and Operating Conditions Design Parameters

Design Internal Pressure = 2.5 psi or 69.2017 inh2o Design External Pressure = -0 psi or -0 inh2o

D of Tank = 10 ftOD of Tank = 10 ft ID of Tank = 9.9688 ft CL of Tank = 9.9844 ft Shell Height = 16 ft S.G of Contents = 1.05S.G of Hydrotest = 1Hydrotest Liquid Level = 15 ft Max Design Liq. Level = 15 ft Max Operating Liq. Level = 15 ft Min Liq. Level = 1 ft Design Temperature = 120 °F MDMT (Minimum Design Metal Temperature) = -20 °F Tank Joint Efficiency = 0.7 Ground Snow Load = 0 psf Roof Live Load = 20 psf Additional Roof Dead Load = 0 psf

#### Appendix F Data

Failure pressure (Pf) = 4.7882 psi Maximum design pressure (P\_max) = 2.5 psi

Wind Load Basis: ASCE 7-05

3 Second Gust Wind Speed (entered), Vg = 110 mph

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Wind Importance Factor, Iw = 1 Design Wind Speed, V = Vg \* SQRT(Iw) = 110 mph

Seismic Method: API-650 - ASCE7 Mapped(Ss & S1)

Seismic Use Group = I

Site Class = D

 $T_L (sec) = 12$ 

Ss(g) = 0.223

S1 (g) = 0.084Av (g) = 0.111

Q = 0.6667

Importance Factor = 1

## Design Remarks

# **Summary Results**

## Shell

Shell #	Width (in)	Material	CA (in)	JE	Min Yield Strength (psi)	Tensile Strength (psi)	Reduction Factor	Sd (psi)	St (psi)
1	48	A240- 304	0	0.7000	29,000	75,000	1	22,500	27,000
2	48	A240- 304	0	0.7000	29,000	75,000	1	22,500	27,000
3	48	A240- 304	0	0.7000	29,000	75,000	1	22,500	27,000
4	48	A240- 304	0	0.7000	29,000	75,000	1	22,500	27,000

#### (continued)

Shell #	Weight (lbf)	Weight CA (lbf)	t-min Erection (in)	t-Des (in)	t-Test (in)	t-min Seismic (in)	t-min Ext- Pe (in)	t-min (in)	t-Actual (in)
1	982	982	0.1875	0.0338	0.0292	0.0321	NA	0.1875	0.1875
2	982	982	0.1875	0.0269	0.0237	0.0258	NA	0.1875	0.1875
3	982	982	0.1875	0.0199	0.0182	0.0196	NA	0.1875	0.1875
4	982	982	0.1875	0.013	0.0127	0.0134	NA	0.1875	0.1875

#### (continued)

Shell #	Status
1	ОК
2	OK
3	ОК
4	ОК

Total Weight of Shell = 3,929.6376 lbf

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#### Roof

Type = Self Supported Conical Roof Plates Material = A240-304 t.required = 0.1875 in t.actual = 0.1875 in Roof corrosion allowance = 0 in Roof Joint Efficiency = 0.7 Plates Overlap Weight = 0 lbf Plates Weight = 635.6869 lbf

#### **Bottom**

Type: Flat Bottom Non Annular
Bottom Material = A240-304
t.required = 0.1875 in
t.actual = 0.1875 in
Bottom corrosion allowance = 0 in
Bottom Joint Efficiency = 0.7
Total Weight of Bottom = 635.6364 lbf

#### **Top Member**

Type = Detail B Size = L2x2x1/4 Material = A240-304 Weight = 100.0838 lbf

#### Anchors

Quantity = 4 Size = 1 in Material = A36 Bolt Hole Circle Radius = 5.1458 ft

# Nameplate Information

Pressure Combination Factor	0.4
Design Standard	API-650 13th Edition Errata 1, 2021
Appendices Used	E, F, J, M, S
Roof	A240-304 : 0.1875 in
Shell (1)	A240-304 : 0.1875 in
Shell (2)	A240-304 : 0.1875 in
Shell (3)	A240-304 : 0.1875 in
Shell (4)	A240-304 : 0.1875 in
Bottom	A240-304 : 0.1875 in

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# Anchor Chair Design Back

#### Anchor Chair Design per AISI T-192 Part V

a = Top Plate Width Along Shell (in) b = Top Plate Length (in) bmin = Top Plate Minimum Length (in) c = Top Plate Thickness (in)CA = Chair Corrosion Allowance (in) c\_corr = Top Plate Corroded Thickness (in) D = Tank Nominal Diameter (ft) d = Anchor Bolt Diameter (in) e = Anchor Bolt Eccentricity (in) Earthquakes-Considered = Earthquakes Considered emin = Minimum Calculated Eccentricity (in) emin-btm = Minimum Eccentricity Based on Bolt Clearance From Bottom Plates per API-650 5.12.4 (in) emin-req = Minimum Required Eccentricity (in) Et = Bottom Plates Thermal Expansion Coefficient per API-650 Table P.1b (in/in.fdeg) f = Top Plate Outside To Hole Edge Distance (in) f\_min = Distance from Outside of Top Plate to Edge of Hole per AISI T-192 Part V, Notation g = Vertical Plates Distance (in) g min = Minimum Distance Between Vertical Plates per AISI T-192, PartV, Notation (in) h = Chair Height (in) h-eff = Effective Chair Height (in) hmax = Chair Maximum Height (in) j = Vertical Plate Thickness (in) i corr = Vertical Plate Corroded Thickness (in) i\_min = Vertical Plate Minimum Thickness per AISI T-192 Part V, Vertical Side Plates (in) k = Vertical Plates Average Width (in) m = Base or Bottom Plate Thickness (in) Ma-chair = Chair Material outside-projection = Bottom Outside Projection (in) R = Nominal Shell Radius (in) Ssw-chair = Chair Allowable Stress for Seismic or Wind Design per API-650 5.12.9 (psi) T = Difference between ambient and design temperature per API 650 5.12.4 (°F) t = Shell Thickness (in)T ambient = Ambient Temperature ( $^{\circ}$ F) T\_design = Design Temperature (°F) V = Wind Velocity (mph) Y-bolt = Anchor Bolt Yield Load (lbf) a = 8 inb = 8 in

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c = 0.5 in

```
CA = 0 in
d = 1 in
D = 10.0 \text{ ft}
e = 1.75 in
Earthquakes-Considered = ASCE7-MAPPED-SS-AND-S1
Et = 6.67E-6 \text{ in/in.fdeg}
f = 4.25 in
g = 4.25 \text{ in}
h = 12 in
j = 0.5 \text{ in}
k = 4.4417 in
m = 0.1875 in
Ma-chair = A240-304
outside-projection = 1 in
R = 60.0 \text{ in}
t = 0.1875 in
T ambient = 70 \, ^{\circ}F
T_design = 120 \, ^{\circ}F
V = 110.0 \text{ mph}
Y-bolt = 19,831.7945 lbf
```

#### **Anchor Chair Material Properties**

Material = A240-304
Minimum Tensile Strength (Sut-chair) = 75,000 psi
As per API-650 S.5.b, Minimum Yield Strength (Sy-chair) = 29,000 psi
As per API-650 S.2b, Allowable Design Stress (Sd-chair) = 22,500 psi
As per API-650 S.2b, Allowable Hydrostatic Test Stress (St-chair) = 27,000 psi

Ssw-chair = 1.33 \* Sd-chair Ssw-chair = 1.33 \* 22,500 Ssw-chair = 29,925 psi

#### **Size Requirements**

c\_corr = c - (2 \* CA) c\_corr = 0.5 - (2 \* 0) c\_corr = 0.5 in

j\_corr = j - (2 \* CA) j\_corr = 0.5 - (2 \* 0) j\_corr = 0.5 in

Chair Minimum Height (hmin) = 12 in

h >= hmin ==> PASS

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# Appurtenances Design Back

# Plan View

LABEL	MARK	CUST. MARK	DESCRIPTION	OUTSIDE PROJ (in)	INSIDE PROJ (in)	ORIENT	RADIUS (in)	REMARKS	REF DWG
Circular- Manway- 0001	RM01A	M1	24" ROOF MANWAY	8"	1"	270 '	2'-9"		
Nozzle- 0001	RN01A	А	8" ROOF NOZZLE	6"	1"	20 '	3'-4"		
Nozzle- 0002	RN02A	В	2" ROOF NOZZLE	6"	1"	90 '	3'-4"	W/ BLIND	
Nozzle- 0004	RN03A	VENT	4" ROOF NOZZLE	6"	1"	0 '	0"		
Nozzle- 0005	RN04A		3" ROOF NOZZLE	6"	0"	0 '	0"		
Nozzle- 0006	RN02A	В	2" ROOF NOZZLE	6"	1"	180 '	3'-4"	W/ BLIND	

# **Elevation View**

LABEL	MARK	CUST. MARK	DESCRIPTION	OUTSIDE PROJ (in)	INSIDE PROJ (in)	ORIENT	ELEVATION (in)	REMARKS	REF DWG
Anchor- Chair- Bolts	AC01A		ANCHOR CHAIRS			SEE TABLE			
Name- Plate	NP01A		STD API			0 '	3'-4"		
Nozzle- 0001	SN01A	FILL	6" SHELL NOZZLE	8"	0"	0 '	1'-0 1/8"		
Nozzle- 0002	SN02A	OUTLET	3" SHELL NOZZLE	7"	0"	90 '	9 1/2"		
Nozzle- 0003	SN03A	T1	2" SHELL NOZZLE	6"	0"	20 '	7"		Ì
Nozzlo	SNI03 V	T2	2" SHELL NOZZLE	6"	0"	70 '	7"		Ì
Nozzle- 0005	SN03A	ТЗ	2" SHELL NOZZLE	6"	0"	110 '	7"		

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Nozzle- 0006 SN04A SAMPLE	1" SHELL NOZZLE	6"	0"	300 '	6"		ĺ
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## Shell Nozzle: Nozzle-0001

## Repad Design

NOZZLE Description: 6 in SCH 40 TYPE RFSO Material: A312-TP304 t rpr = (Repad Required Thickness) t\_n = (Thickness of Neck) Sd\_n = (Stress of Neck Material) Sd\_s = (Stress of Shell Course Material) CA = (Corrosion Allowance of Neck) MOUNTED ON SHELL 1: Elevation = 1.0104 ft **COURSE PARAMETERS:** t-calc = 0.0338 in t\_cr = 0.0338 in (Course t-calc less C.A)  $t_c = 0.1875$  in (Course t less C.A.) t Basis = 0.0338 in (SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7) Required Area = t\_Basis \* D Required Area = 0.0338 \* 6.625 Required Area = 0.2238 in2 Available Shell Area = (t\_c - t\_Basis) \* D Available Shell Area = (0.1875 - 0.0338) \* 6.625 Available Shell Area = 1.0184 in 2 Available Nozzle Neck Area = 2 \* [(4 \* (t\_n - CA)) + t\_c] \* (t\_n - CA) \* MIN((Sd\_n/Sd\_s) 1) Available Nozzle Neck Area = 2 \* [(4 \* (0.28 - 0)) + 0.1875] \* (0.28 - 0) \* MIN((22,500/22,500) 1)Available Nozzle Neck Area = 0.7322 in2 A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area) A-rpr = 0.2238 - 1.0184 - 0.7322A-rpr = 0 in2 Since A-rpr  $\leq 0$ ,  $t_rpr = 0$ 

#### **Nozzle Neck Material Properties**

No Reinforcement Pad required.

Material = A312-TP304

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## Shell Nozzle: Nozzle-0002

#### Repad Design

```
NOZZLE Description: 3 in SCH 40S TYPE RFSO
Material: A312-TP304
t_rpr = (Repad Required Thickness)
t n = (Thickness of Neck)
Sd n = (Stress of Neck Material)
Sd_s = (Stress of Shell Course Material)
CA = (Corrosion Allowance of Neck)
MOUNTED ON SHELL 1: Elevation = 0.7917 ft
COURSE PARAMETERS:
t-calc = 0.0338 in
t cr = 0.0338 in (Course t-calc less C.A)
t c = 0.1875 in (Course t less C.A.)
t_Basis = 0.0338 in
(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)
Required Area = t_Basis * D
Required Area = 0.0338 * 3.5
Required Area = 0.1183 in2
Available Shell Area = (t c - t Basis) * D
Available Shell Area = (0.1875 - 0.0338) * 3.5
Available Shell Area = 0.538 in2
Available Nozzle Neck Area = 2 * [(4 * (t_n - CA)) + t_c] * (t_n - CA) * MIN((Sd_n/Sd_s) 1)
Available Nozzle Neck Area = 2 * [(4 * (0.216 - 0)) + 0.1875] * (0.216 - 0) * MIN((22,500/22,500) 1)
Available Nozzle Neck Area = 0.4542 in2
A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area)
A-rpr = 0.1183 - 0.538 - 0.4542
A-rpr = 0 in2
Since A-rpr \leq 0, t rpr = 0
No Reinforcement Pad required.
Nozzle Neck Material Properties
```

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Material = A312-TP304

As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22,500 psi

## Shell Nozzle: Nozzle-0003

NOZZLE Description: 2 in SCH 80S TYPE RFSO

#### Repad Design

Material: A312-TP304 t rpr = (Repad Required Thickness) t\_n = (Thickness of Neck) Sd\_n = (Stress of Neck Material) Sd s = (Stress of Shell Course Material) CA = (Corrosion Allowance of Neck) MOUNTED ON SHELL 1: Elevation = 0.5833 ft COURSE PARAMETERS: t-calc = 0.0338 in  $t_cr = 0.0338$  in (Course t-calc less C.A)  $t_c = 0.1875$  in (Course t less C.A.) t Basis = 0.0338 in (SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7) Required Area = t\_Basis \* D Required Area = 0.0338 \* 2.375 Required Area = 0.0802 in2 Available Shell Area = (t\_c - t\_Basis) \* D Available Shell Area = (0.1875 - 0.0338) \* 2.375 Available Shell Area = 0.3651 in2 Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - CA) * MIN((Sd_n/Sd_s) 1)$ Available Nozzle Neck Area = 2 \* [(4 \* (0.218 - 0)) + 0.1875] \* (0.218 - 0) \* MIN((22,500/22,500) 1)Available Nozzle Neck Area = 0.4619 in2 A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area) A-rpr = 0.0802 - 0.3651 - 0.4619A-rpr = 0 in2 Since Nozzle size <= NPS 2 (per API-650 Table 5.6 Note f), t rpr = 0 No Reinforcement Pad required.

## Nozzle Neck Material Properties Material = A312-TP304

Material = A312-TP304 As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22,500 psi

Shell Nozzle: Nozzle-0004

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#### Repad Design

NOZZLE Description: 2 in SCH 80S TYPE RFSO

```
Material: A312-TP304
t_rpr = (Repad Required Thickness)
t_n = (Thickness of Neck)
Sd n = (Stress of Neck Material)
Sd_s = (Stress of Shell Course Material)
CA = (Corrosion Allowance of Neck)
MOUNTED ON SHELL 1: Elevation = 0.5833 ft
COURSE PARAMETERS:
t-calc = 0.0338 in
t_cr = 0.0338 in (Course t-calc less C.A)
t c = 0.1875 in (Course t less C.A.)
t Basis = 0.0338 in
(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)
Required Area = t_Basis * D
Required Area = 0.0338 * 2.375
Required Area = 0.0802 in2
Available Shell Area = (t_c - t_Basis) * D
Available Shell Area = (0.1875 - 0.0338) * 2.375
Available Shell Area = 0.3651 in 2
Available Nozzle Neck Area = 2 * [(4 * (t_n - CA)) + t_c] * (t_n - CA) * MIN((Sd_n/Sd_s) 1)
Available Nozzle Neck Area = 2 * [(4 * (0.218 - 0)) + 0.1875] * (0.218 - 0) * MIN((22,500/22,500) 1)
Available Nozzle Neck Area = 0.4619 in2
A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area)
A-rpr = 0.0802 - 0.3651 - 0.4619
A-rpr = 0 in2
Since Nozzle size <= NPS 2 (per API-650 Table 5.6 Note f), t_rpr = 0
No Reinforcement Pad required.
Nozzle Neck Material Properties
Material = A312-TP304
```

Shell Nozzle: Nozzle-0005

As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22,500 psi

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#### Repad Design

NOZZLE Description: 2 in SCH 80S TYPE RFSO Material: A312-TP304 t\_rpr = (Repad Required Thickness) t n = (Thickness of Neck) Sd\_n = (Stress of Neck Material) Sd\_s = (Stress of Shell Course Material) CA = (Corrosion Allowance of Neck) MOUNTED ON SHELL 1: Elevation = 0.5833 ft COURSE PARAMETERS: t-calc = 0.0338 in t cr = 0.0338 in (Course t-calc less C.A) $t_c = 0.1875$  in (Course t less C.A.)  $t_Basis = 0.0338 in$ (SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7) Required Area = t Basis \* D Required Area = 0.0338 \* 2.375Required Area = 0.0802 in2 Available Shell Area = (t\_c - t\_Basis) \* D Available Shell Area = (0.1875 - 0.0338) \* 2.375 Available Shell Area = 0.3651 in2 Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - CA) * MIN((Sd_n/Sd_s) 1)$ Available Nozzle Neck Area = 2 \* [(4 \* (0.218 - 0)) + 0.1875] \* (0.218 - 0) \* MIN((22,500/22,500) 1)Available Nozzle Neck Area = 0.4619 in 2 A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area) A-rpr = 0.0802 - 0.3651 - 0.4619A-rpr = 0 in2 Since Nozzle size <= NPS 2 (per API-650 Table 5.6 Note f), t\_rpr = 0 No Reinforcement Pad required. **Nozzle Neck Material Properties** Material = A312-TP304

## Shell Nozzle: Nozzle-0006

As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22,500 psi

### Repad Design

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```
NOZZLE Description: 1 in SCH 80S TYPE RFSO
```

Material: A312-TP304

t\_rpr = (Repad Required Thickness)

t\_n = (Thickness of Neck)

Sd\_n = (Stress of Neck Material)

Sd\_s = (Stress of Shell Course Material)

CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 1: Elevation = 0.5 ft

#### **COURSE PARAMETERS:**

t-calc = 0.0338 in

t\_cr = 0.0338 in (Course t-calc less C.A)

 $t_c = 0.1875$  in (Course t less C.A.)

t Basis = 0.0338 in

(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)

Required Area = t\_Basis \* D

Required Area = 0.0338 \* 1.315

Required Area = 0.0444 in2

Available Shell Area = (t\_c - t\_Basis) \* D

Available Shell Area = (0.1875 - 0.0338) \* 1.315

Available Shell Area = 0.2021 in2

Available Nozzle Neck Area = 2 \* [(4 \* (t\_n - CA)) + t\_c] \* (t\_n - CA) \* MIN((Sd\_n/Sd\_s) 1)

Available Nozzle Neck Area = 2 \* [(4 \* (0.179 - 0)) + 0.1875] \* (0.179 - 0) \* MIN((22,500/22,500) 1)

Available Nozzle Neck Area = 0.3235 in2

A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area)

A-rpr = 0.0444 - 0.2021 - 0.3235

A-rpr = 0 in2

Since Nozzle size <= NPS 2 (per API-650 Table 5.6 Note f), t\_rpr = 0

No Reinforcement Pad required.

#### **Nozzle Neck Material Properties**

Material = A312-TP304

As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22,500 psi

Roof Nozzle: Nozzle-0001

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#### Repad Design

(Per API-650 and other references below) NOZZLE Description: 8 in SCH 40S TYPE RFSO Material: A312-TP304 t rpr = (Repad Required Thickness) t\_n = (Thickness of Neck) Sd n = (Stress of Neck Material) Sd s = (Stress of Roof Material) CA = (Corrosion Allowance of Neck) MOUNTED ON ROOF: Elevation = 16.3174 ft **ROOF PARAMETERS:** t-calc = 0.1875 in  $t_cr = 0.1875$  in (Roof t-act less C.A) t c = 0.1875 int Basis = 0.1875 in Repad Type: Circular Repad Size (Do): = 12.75 in (FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15, API-650 F.2.4) Required Area = t Basis \* D Required Area = 0.1875 \* 8.625 Required Area = 1.6172 in2 Available Roof Area = (t c - t Basis) \* D Available Roof Area = (0.1875 - 0.1875) \* 8.625 Available Roof Area = 0 in2 Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)$ Available Nozzle Neck Area = 2 \* [(4 \* (0.322 - 0)) + 0.1875] \* (0.322 - 0) \* MIN((22,500/22,500) 1)Available Nozzle Neck Area = 0.9502 in2 A\_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)  $A_{rpr} = 1.6172 - 0 - 0.9502$  $A_{rpr} = 0.667 \text{ in } 2$ t\_rpr = (A\_rpr / (repad-min-OD - D)) + repad\_CA t rpr = (0.667 / (12.75 - 8.625)) + 0 $t_{rpr} = 0.1617 in$ As per API-650 J.3.6.3, reinforcement pad is required since roof loads exceed 25 psf. Reinforcement Pad is required. Based on Roof Nozzle Size of 8" Repad Size (OD) Must be = 18 in

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## Roof Nozzle: Nozzle-0002

#### Repad Design

```
(Per API-650 and other references below)
NOZZLE Description: 2 in SCH 80 TYPE RFSO
Material: A312-TP304
t_rpr = (Repad Required Thickness)
t n = (Thickness of Neck)
Sd n = (Stress of Neck Material)
Sd_s = (Stress of Roof Material)
CA = (Corrosion Allowance of Neck)
MOUNTED ON ROOF: Elevation = 16.3174 ft
ROOF PARAMETERS:
t-calc = 0.1875 in
t cr = 0.1875 in (Roof t-act less C.A)
t c = 0.1875 in
t Basis = 0.1875 in
Repad Type: Circular
Repad Size (Do): = 6.5 in
(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or
API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15, API-650 F.2.4)
Required Area = t_Basis * D
Required Area = 0.1875 * 2.375
Required Area = 0.4453 in2
Available Roof Area = (t c - t Basis) * D
Available Roof Area = (0.1875 - 0.1875) * 2.375
Available Roof Area = 0 in2
Available Nozzle Neck Area = 2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)
Available Nozzle Neck Area = 2 * [(4 * (0.218 - 0)) + 0.1875] * (0.218 - 0) * MIN((22,500/22,500) 1)
Available Nozzle Neck Area = 0.4619 in2
A_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)
A rpr = 0.4453 - 0 - 0.4619
Required A_rpr calculated value = -0.0166 in^2 is less than zero. A_rpr will be set to zero.
A_rpr = 0 in 2
t_rpr = (A_rpr / (repad-min-OD - D)) + repad_CA
t_rpr = (0 / (6.5 - 2.375)) + 0
t rpr = 0 in
```

As per API-650 J.3.6.3, reinforcement pad is required since roof loads exceed 25 psf.

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## Roof Nozzle: Nozzle-0004

### Repad Design

(Per API-650 and other references below)

NOZZLE Description: 4 in SCH 80 TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)

t\_n = (Thickness of Neck)

Sd\_n = (Stress of Neck Material)

Sd\_s = (Stress of Roof Material)

CA = (Corrosion Allowance of Neck)

MOUNTED ON ROOF: Elevation = 16.8886 ft

#### **ROOF PARAMETERS:**

t-calc = 0.1875 in

t\_cr = 0.1875 in (Roof t-act less C.A)

 $t_c = 0.1875$  in

t Basis = 0.1875 in

Repad Type: Circular

Repad Size (Do): = 8.5 in

(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15, API-650 F.2.4)

Required Area = t\_Basis \* D

Required Area = 0.1875 \* 4.5

Required Area = 0.8438 in2

Available Roof Area = (t\_c - t\_Basis) \* D

Available Roof Area = (0.1875 - 0.1875) \* 4.5

Available Roof Area = 0 in2

Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)$ 

Available Nozzle Neck Area = 2 \* [(4 \* (0.337 - 0)) + 0.1875] \* (0.337 - 0) \* MIN((22,500/22,500) 1)

Available Nozzle Neck Area = 1.0349 in2

A\_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)

 $A_rpr = 0.8438 - 0 - 1.0349$ 

Required A\_rpr calculated value = -0.1912 in^2 is less than zero. A\_rpr will be set to zero.

 $A_rpr = 0 in2$ 

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```
t_rpr = (A_rpr / (repad-min-OD - D)) + repad_CA
t_rpr = (0 / (8.5 - 4.5)) + 0
t rpr = 0 in
```

As per API-650 J.3.6.3, reinforcement pad is required since roof loads exceed 25 psf.

Reinforcement Pad is required. Based on Roof Nozzle Size of 4" Repad Size (OD) Must be = 11 in

## Roof Nozzle: Nozzle-0005

### Repad Design

(Per API-650 and other references below)

NOZZLE Description: 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)
t\_n = (Thickness of Neck)
Sd\_n = (Stress of Neck Material)
Sd\_s = (Stress of Roof Material)
CA = (Corrosion Allowance of Neck)

MOUNTED ON ROOF: Elevation = 16.8886 ft

**ROOF PARAMETERS:** 

t-calc = 0.1875 in t\_cr = 0.1875 in (Roof t-act less C.A) t\_c = 0.1875 in t\_Basis = 0.1875 in Repad Type: Circular Repad Size (Do): = 7.5 in

(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15, API-650 F.2.4)

Required Area = t\_Basis \* D Required Area = 0.1875 \* 3.5 Required Area = 0.6563 in2 Available Roof Area = (t\_c - t\_Basis) \* D Available Roof Area = (0.1875 - 0.1875) \* 3.5 Available Roof Area = 0 in2

Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)$ Available Nozzle Neck Area = 2 \* [(4 \* (0.216 - 0)) + 0.1875] \* (0.216 - 0) \* MIN((22,500/22,500) 1)Available Nozzle Neck Area = 0.4542 in2

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```
A_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)
A_rpr = 0.6563 - 0 - 0.4542
A_rpr = 0.202 in2

t_rpr = (A_rpr / (repad-min-OD - D)) + repad_CA
t_rpr = (0.202 / (7.5 - 3.5)) + 0
t_rpr = 0.0505 in
```

As per API-650 J.3.6.3, reinforcement pad is required since roof loads exceed 25 psf.

Reinforcement Pad is required. Based on Roof Nozzle Size of 3" Repad Size (OD) Must be = 9 in

## Roof Nozzle: Nozzle-0006

### Repad Design

(Per API-650 and other references below)

NOZZLE Description: 2 in SCH 80 TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)
t\_n = (Thickness of Neck)
Sd\_n = (Stress of Neck Material)
Sd\_s = (Stress of Roof Material)
CA = (Corrosion Allowance of Neck)

MOUNTED ON ROOF: Elevation = 16.3174 ft

ROOF PARAMETERS: t-calc = 0.1875 in t\_cr = 0.1875 in (Roof t-act less C.A) t\_c = 0.1875 in t\_Basis = 0.1875 in Repad Type: Circular Repad Size (Do): = 6.5 in

(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15, API-650 F.2.4)

Required Area = t\_Basis \* D Required Area = 0.1875 \* 2.375 Required Area = 0.4453 in2 Available Roof Area = (t\_c - t\_Basis) \* D Available Roof Area = (0.1875 - 0.1875) \* 2.375

Available Roof Area = 0 in2

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```
Available Nozzle Neck Area = 2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)

Available Nozzle Neck Area = 2 * [(4 * (0.218 - 0)) + 0.1875] * (0.218 - 0) * MIN((22,500/22,500) 1)

Available Nozzle Neck Area = 0.4619 in2

A_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)

A_rpr = 0.4453 - 0 - 0.4619

Required A_rpr calculated value = -0.0166 in^2 is less than zero. A_rpr will be set to zero.

A_rpr = 0 in2

t_rpr = (A_rpr / (repad-min-OD - D)) + repad_CA

t_rpr = (0 / (6.5 - 2.375)) + 0

t_rpr = 0 in

As per API-650 J.3.6.3, reinforcement pad is required since roof loads exceed 25 psf.

Reinforcement Pad is required.

Based on Roof Nozzle Size of 2"

Repad Size (OD) Must be = 7 in
```

#### Repad Design

```
(Per API-650 Section 5.8.4 and other references below)
MANWAY Description: 24 in Neck Thickness 0.25
Material: A240-304
t_rpr = (Repad Required Thickness)
MOUNTED ON ROOF: Elevation = 16.4146 ft
ROOF PARAMETERS:
t-calc = 0.1875 in
t cr = 0.1875 in (Roof t-act less C.A)
t c = 0.1875 in
t Basis = 0.1875 in
Repad Type: Circular
Repad Size (Do): = 40 in
(FOR ROOF MANWAY, REF. API-650 FIG 5-16, TABLE 5-13)
Required Area = t Basis * D
Required Area = 0.1875 * 24
Required Area = 4.5 in2
Available Roof Area = (t_c - t_Basis) * D
Available Roof Area = (0.1875 - 0.1875) * 24
Available Roof Area = 0 in2
Available Manway Neck Area = 2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * MIN((Sd_n/Sd_s) 1)
```

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```
Available Manway Neck Area = 2 * [(4 * (0.25 - 0)) + 0.1875] * (0.25 - 0) * MIN((22,500/22,500) 1)
Available Manway Neck Area = 0.5938 \text{ in} 2
```

A-rpr = (Required Area - Available Roof Area - Available Manway Neck Area) A-rpr = 4.5 - 0 - 0.5938

A-rpr = 3.9063 in 2

t\_rpr = (A\_rpr / (repad-min-OD - D)) + repad\_CA

 $t_rpr = (3.9063 / (40 - 24)) + 0$ 

 $t_{rpr} = 0.2441 \text{ in}$ 

Reinforcement Pad is required. Based on Roof Manway Size of 24" Repad Size (OD) Must be = 46 in

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# Capacities and Weights Back

Capacity to Top of Shell (to Tank Height): 9,341 gal

Capacity to Design Liquid Level: 8,757 gal Capacity to Maximum Liquid Level: 8,757 gal

Working Capacity (to Normal Working Level): 8,757 gal

Net working Capacity (Working Capacity - Min Capacity): 8,173 gal

Minimum Capacity (to Min Liq Level): 583 gal

Component	New Condition (lbf)	Corroded (lbf)
SHELL	3,930	3,930
ROOF	602	602
RAFTERS	0	0
GIRDERS	0	0
FRAMING	0	0
COLUMNS	0	0
TRUSS	0	0
STRUCTURE COMPONENTS	0	0
воттом	635	635
STAIRWAYS	0	0
ACCESS	0	0
STIFFENERS	101	101
WIND GIRDERS	0	0
ANCHOR CHAIRS	62	62
SHELL APPURTENANCES	70	70
ROOF APPURTENANCES	457	457
BOTTOM APPURTENANCES	0	0
INSULATION	0	0
FLOATING ROOF	0	0
TOTAL	5,858.1886	5,858.1886

Weight of Tank, Empty: 5,858.1886 lbf

Weight of Tank, Full of Product (Design SG = 1.05): 83,081.1886 lbf

Weight of Tank, Full of Water: 79,404.3257 lbf

Net Working Weight, Full of Product (Design SG = 1.05): 77,933.4029 lbf

Net Working Weight Full of Water: 74,501.2499 lbf

Foundation Area Req'd: 81.1796 ft2

Foundation Loading, Empty: 72.1632 lbf/ft2

Foundation Loading, Full of Product Design: 1,023.4241 lbf/ft2

Foundation Loading, Full of Water: 978.1311 lbf/ft2

SURFACE AREAS Roof: 81.186 ft2 Shell: 501.084 ft2 Bottom: 81.1796 ft2

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