

**No Warnings!!**

# Project Design Data and Summary

[Back](#)

## Project Data

Job : 2025-07-22-06-17

Date of Calcs. : 06-Aug-2025

Mfg. or Insp. Date :

Designer : Melior

Project :

Tag ID : Q9294 API

Plant :

Plant Location :

Site :

Design Basis : API-650 13th Edition Errata 1, 2021

Annexes Used : E, J, M, S

## Design Parameters and Operating Conditions

### Design Parameters

Design Internal Pressure = 0 psi or 0 inhh<sub>2</sub>o

Design External Pressure = -0 psi or -0 inhh<sub>2</sub>o

D of Tank = 13.2217 ft

OD of Tank = 13.2842 ft

ID of Tank = 13.2217 ft

CL of Tank = 13.2529 ft

Shell Height = 60.4167 ft

S.G of Contents = 1

S.G of Hydrotest = 1

Hydrotest Liquid Level = 60.4167 ft

Max Design Liq. Level = 60.4167 ft

Max Operating Liq. Level = 60.4167 ft

Min Liq. Level = 1 ft

Design Temperature = 122 °F

MDMT (Minimum Design Metal Temperature) = -20 °F

Tank Joint Efficiency = 0.7

Ground Snow Load = 0 psf

Roof Live Load = 20 psf

Additional Roof Dead Load = 0 psf

Wind Load Basis: ASCE 7-16

3 Second Gust Wind Speed (entered), V<sub>g</sub> = 105 mph

Design Wind Speed, V = V<sub>g</sub> = 105 mph

Seismic Method: API-650 - ASCE7 Mapped(Ss & S1)

Seismic Use Group = II

Site Class = C

$T_L$  (sec) = 12  
 $S_s$  (g) = 0.27  
 $S_1$  (g) = 0.094  
 $A_v$  (g) = 0.1008  
 $Q$  = 0.6667  
 Importance Factor = 1.25

## Design Remarks

## Summary Results

### Shell

Shell #	Width (in)	Material	CA (in)	JE	Min Yield Strength (psi)	Tensile Strength (psi)	Reduction Factor	Sd (psi)	St (psi)
1	60	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
2	60	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
3	60	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
4	60	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
5	60	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
6	60	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
7	60	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
8	60	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
9	60	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
10	48	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
11	48	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
12	48	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000
13	39.5	A240-304	0	0.7000	28,900	75,000	1	22,500	27,000

(continued)

Shell #	Weight (lbf)	Weight CA (lbf)	t-min Erection (in)	t-Des (in)	t-Test (in)	t-min Seismic (in)	t-min Ext-Pe (in)	t-min (in)	t-Actual (in)
1	3,244	3,244	0.1875	0.1297	0.1081	0.1188	NA	0.1875	0.375
2	1,624	1,624	0.1875	0.1188	0.099	0.1089	NA	0.1875	0.1875

3	1,624	1,624	0.1875	0.1079	0.0899	0.0991	NA	0.1875	0.1875
4	1,624	1,624	0.1875	0.0969	0.0808	0.0893	NA	0.1875	0.1875
5	1,624	1,624	0.1875	0.086	0.0717	0.0795	NA	0.1875	0.1875
6	1,624	1,624	0.1875	0.0751	0.0626	0.0697	NA	0.1875	0.1875
7	1,624	1,624	0.1875	0.0642	0.0535	0.0599	NA	0.1875	0.1875
8	1,624	1,624	0.1875	0.0533	0.0444	0.0501	NA	0.1875	0.1875
9	1,624	1,624	0.1875	0.0424	0.0353	0.0403	NA	0.1875	0.1875
10	1,299	1,299	0.1875	0.0315	0.0262	0.0306	NA	0.1875	0.1875
11	1,299	1,299	0.1875	0.0227	0.0189	0.0228	NA	0.1875	0.1875
12	1,299	1,299	0.1875	0.014	0.0117	0.015	NA	0.1875	0.1875
13	1,069	1,069	0.1875	0.0053	0.0044	0.0071	NA	0.1875	0.1875

(continued)

Shell #	Status
1	OK
2	OK
3	OK
4	OK
5	OK
6	OK
7	OK
8	OK
9	OK
10	OK
11	OK
12	OK
13	OK

Total Weight of Shell = 21,264.1013 lbf

## Roof

Type = Self Supported Conical Roof

Plates Material = A240-304

t.required = 0.1875 in

t.actual = 0.1875 in

Roof corrosion allowance = 0 in

Roof Joint Efficiency = 0.7

Plates Overlap Weight = 0 lbf

Plates Weight = 1,111.2243 lbf

## Bottom

Type : Flat Bottom Non Annular

Bottom Material = A240-304

t.required = 0.1875 in

t.actual = 0.1875 in

Bottom corrosion allowance = 0 in  
Bottom Joint Efficiency = 0.7  
Total Weight of Bottom = 1,112.6281 lbf

## Top Member

Type = Detail B  
Size = L2x2x1/4  
Material = A240-304  
Weight = 132.6171 lbf

## Anchors

Quantity = 8  
Size = 1.625 in  
Material = A36  
Bolt Hole Circle Radius = 6.8191 ft

## Nameplate Information

Pressure Combination Factor	0.4
Design Standard	API-650 13th Edition Errata 1, 2021
Appendices Used	E, J, M, S
Roof	A240-304 : 0.1875 in
Shell (1)	A240-304 : 0.375 in
Shell (2)	A240-304 : 0.1875 in
Shell (3)	A240-304 : 0.1875 in
Shell (4)	A240-304 : 0.1875 in
Shell (5)	A240-304 : 0.1875 in
Shell (6)	A240-304 : 0.1875 in
Shell (7)	A240-304 : 0.1875 in
Shell (8)	A240-304 : 0.1875 in
Shell (9)	A240-304 : 0.1875 in
Shell (10)	A240-304 : 0.1875 in
Shell (11)	A240-304 : 0.1875 in
Shell (12)	A240-304 : 0.1875 in
Shell (13)	A240-304 : 0.1875 in
Bottom	A240-304 : 0.1875 in

# Anchor Chair Design [Back](#)

## Anchor Chair Design per AISI T-192 Part V

a = Top Plate Width Along Shell (in)

b = Top Plate Length (in)

bmin = Top Plate Minimum Length (in)

c = Top Plate Thickness (in)

CA = Chair Corrosion Allowance (in)

c\_corr = Top Plate Corroded Thickness (in)

D = Tank Nominal Diameter (ft)

d = Anchor Bolt Diameter (in)

e = Anchor Bolt Eccentricity (in)

Earthquakes-Considered = Earthquakes Considered

emin = Minimum Calculated Eccentricity (in)

emin-btm = Minimum Eccentricity Based on Bolt Clearance From Bottom Plates per *API-650 5.12.4* (in)

emin-req = Minimum Required Eccentricity (in)

Et = Bottom Plates Thermal Expansion Coefficient per *API-650 Table P.1b* (in/in.fdeg)

f = Top Plate Outside To Hole Edge Distance (in)

f\_min = Distance from Outside of Top Plate to Edge of Hole per *AISI T-192 Part V, Notation* (in)

g = Vertical Plates Distance (in)

g\_min = Minimum Distance Between Vertical Plates per *AISI T-192, PartV, Notation* (in)

h = Chair Height (in)

h-eff = Effective Chair Height (in)

hmax = Chair Maximum Height (in)

j = Vertical Plate Thickness (in)

j\_corr = Vertical Plate Corroded Thickness (in)

j\_min = Vertical Plate Minimum Thickness per *AISI T-192 Part V, Vertical Side Plates* (in)

k = Vertical Plates Average Width (in)

m = Base or Bottom Plate Thickness (in)

Ma-chair = Chair Material

outside-projection = Bottom Outside Projection (in)

R = Nominal Shell Radius (in)

Ssw-chair = Chair Allowable Stress for Seismic or Wind Design per *API-650 5.12.9* (psi)

T = Difference between ambient and design temperature per *API 650 5.12.4* (°F)

t = Shell Thickness (in)

T\_ambient = Ambient Temperature (°F)

T\_design = Design Temperature (°F)

V = Wind Velocity (mph)

Y-bolt = Anchor Bolt Yield Load (lbf)

a = 8.0 in

b = 8.0 in

c = 0.750 in

CA = 0.0 in  
d = 1.6250 in  
D = 13.2217 ft  
e = 2.1250 in  
Earthquakes-Considered = ASCE7-MAPPED-SS-AND-S1  
Et = 6.670e-6 in/in/fdeg  
f = 4.81250 in  
g = 4.250 in  
h = 12.0 in  
j = 0.6250 in  
k = 4.55022 in  
m = 0.18750 in  
Ma-chair = A240-304  
outside-projection = 1.0 in  
R = 79.330 in  
t = 0.3750 in  
T\_ambient = 70.0 °F  
T\_design = 122.0 °F  
V = 81.90 mph  
Y-bolt = 60.4761e3 lbf



### Anchor Chair Material Properties

Material = A240-304

Minimum Tensile Strength (Sut-chair) = 75.0e3 psi

As per API-650 S.5.b, Minimum Yield Strength (Sy-chair) = 28.90e3 psi

As per API-650 S.2b, Allowable Design Stress (Sd-chair) = 22.50e3 psi

As per API-650 S.2b, Allowable Hydrostatic Test Stress (St-chair) = 27.0e3 psi

Ssw-chair = 1.33 \* Sd-chair

Ssw-chair = 1.33 \* 22.50e3

Ssw-chair = 29.9250e3 psi

### Size Requirements

c\_corr = c - (2 \* CA)

c\_corr = 0.750 - (2 \* 0.0)

c\_corr = 0.750 in

j\_corr = j - (2 \* CA)

j\_corr = 0.6250 - (2 \* 0.0)

j\_corr = 0.6250 in

Chair Minimum Height (hmin) = 12.0 in

h >= hmin ==> PASS

# Appurtenances Design [Back](#)

## Plan View

LABEL	MARK	CUST. MARK	DESCRIPTION	OUTSIDE PROJ (in)	INSIDE PROJ (in)	ORIENT	RADIUS (in)	REMARKS	REF DWG
N1	RN02A		4" ROOF NOZZLE	6"	1"	0 '	5'-6"		
N2	RN01A		6" ROOF NOZZLE	6"	0"	0 '	0"		
N7	BD01		2" FLUSH DRAIN	3 1/2"	8"	270 '	0"	RADIAL	

## Elevation View

LABEL	MARK	CUST. MARK	DESCRIPTION	OUTSIDE PROJ (in)	INSIDE PROJ (in)	ORIENT	ELEVATION (in)	REMARKS	REF DWG
Anchor-Chair-Bolts	AC01A		ANCHOR CHAIRS	--	--	SEE TABLE	--		
N3	SN02A		3" SHELL NOZZLE	7"	1"	0 '	49'-8"		
N4	SN01A		3" SHELL NOZZLE	7"	1"	0 '	9 1/2"		
N5	SM01A		20" SHELL MANWAY	10"	1"	90 '	2'-6"	W/ DAVIT	
N6	SN03A		4" SHELL NOZZLE	7"	0"	180 '	10 1/4"		
Name-Plate	NP01A		STD API	--	--	0 '	3'-4"		

## Shell Nozzle: N4

### Repad Design

NOZZLE Description : 3 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)

t\_n = (Thickness of Neck)

Sd\_n = (Stress of Neck Material)

Sd\_s = (Stress of Shell Course Material)

CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 1 : Elevation = 0.7917 ft

COURSE PARAMETERS:

t\_calc = 0.1297 in

t\_cr = 0.1297 in (Course t\_calc less C.A.)

t\_c = 0.375 in (Course t less C.A.)

t\_Basis = 0.1297 in

(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)

Required Area = t\_Basis \* D

Required Area = 0.1297 \* 3.5

Required Area = 0.4539 in<sup>2</sup>

Available Shell Area = (t\_c - t\_Basis) \* D

Available Shell Area = (0.375 - 0.1297) \* 3.5

Available Shell Area = 0.8586 in<sup>2</sup>

Available Nozzle Neck Area = 2 \* [(4 \* (t\_n - CA)) + t\_c] \* (t\_n - CA) \* MIN((Sd\_n/Sd\_s) 1)

Available Nozzle Neck Area = 2 \* [(4 \* (0.216 - 0)) + 0.375] \* (0.216 - 0) \* MIN((22,500/22,500) 1)

Available Nozzle Neck Area = 0.5352 in<sup>2</sup>

A\_rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area)

A\_rpr = 0.4539 - 0.8586 - 0.5352

A\_rpr = 0 in<sup>2</sup>

Since A\_rpr <= 0, t\_rpr = 0

No Reinforcement Pad required.

t\_shell\_PWHT = Thickness of the shell plate, insert plate, or thickened insert plate for PWHT (in)

**Nozzle Neck Material Properties**

Material = A312-TP304

As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22.50e3 psi

t\_shell\_PWHT = t\_plate

t\_shell\_PWHT = 0.3750

t\_shell\_PWHT = 0.3750 in

**Thermal Stress Relief (PWHT) Requirements**

D = Nozzle Nominal Diameter (NPS) (in)

Group = Shell Material Group

t\_shell = Shell Plate Thickness (in)

D = 3.0 in

Group = None  
t\_shell = 0.3750 in

Shell material group (None) is not a group specified by API 650, 13th Ed, Section 5.7.4. Requirement for Thermal Stress Relief (PWHT) is unknown.

## Shell Nozzle: N3

### Repad Design

NOZZLE Description : 3 in SCH 40S TYPE RFSO  
Material: A312-TP304

t\_rpr = (Repad Required Thickness)  
t\_n = (Thickness of Neck)  
Sd\_n = (Stress of Neck Material)  
Sd\_s = (Stress of Shell Course Material)  
CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 11 : Elevation = 49.6667 ft

#### COURSE PARAMETERS:

t-calc = 0.0228 in  
t\_cr = 0.0228 in (Course t-calc less C.A.)  
t\_c = 0.1875 in (Course t less C.A.)  
t\_Basis = 0.0228 in

(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)

Required Area = t\_Basis \* D  
Required Area = 0.0228 \* 3.5  
Required Area = 0.0798 in<sup>2</sup>

Available Shell Area = (t\_c - t\_Basis) \* D  
Available Shell Area = (0.1875 - 0.0228) \* 3.5  
Available Shell Area = 0.5764 in<sup>2</sup>

Available Nozzle Neck Area = 2 \* [(4 \* (t\_n - CA)) + t\_c] \* (t\_n - CA) \* MIN((Sd\_n/Sd\_s) 1)  
Available Nozzle Neck Area = 2 \* [(4 \* (0.216 - 0)) + 0.1875] \* (0.216 - 0) \* MIN((22,500/22,500) 1)  
Available Nozzle Neck Area = 0.4542 in<sup>2</sup>

A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area)  
A-rpr = 0.0798 - 0.5764 - 0.4542  
A-rpr = 0 in<sup>2</sup>

Since A-rpr <= 0, t\_rpr = 0

No Reinforcement Pad required.

t\_shell\_PWHT = Thickness of the shell plate, insert plate, or thickened insert plate for PWHT (in)

### Nozzle Neck Material Properties

Material = A312-TP304

As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22.50e3 psi

t\_shell\_PWHT = t-plate

t\_shell\_PWHT = 0.18750

t\_shell\_PWHT = 0.18750 in

### Thermal Stress Relief (PWHT) Requirements

D = Nozzle Nominal Diameter (NPS) (in)

Group = Shell Material Group

t\_shell = Shell Plate Thickness (in)

D = 3.0 in

Group = None

t\_shell = 0.18750 in

Shell material group (None) is not a group specified by API 650, 13th Ed, Section 5.7.4. Requirement for Thermal Stress Relief (PWHT) is unknown.

## Shell Nozzle: N6

### Repad Design

NOZZLE Description : 4 in SCH 40S TYPE RFSO

Material: A312-TP304

t\_rpr = (Repad Required Thickness)

t\_n = (Thickness of Neck)

Sd\_n = (Stress of Neck Material)

Sd\_s = (Stress of Shell Course Material)

CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 1 : Elevation = 0.8542 ft

#### COURSE PARAMETERS:

t\_calc = 0.1297 in

t\_cr = 0.1297 in (Course t\_calc less C.A.)

t\_c = 0.375 in (Course t less C.A.)

t\_Basis = 0.1297 in

(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)

Required Area = t\_Basis \* D

Required Area = 0.1297 \* 4.5

Required Area = 0.5836 in<sup>2</sup>

Available Shell Area = (t\_c - t\_Basis) \* D

Available Shell Area = (0.375 - 0.1297) \* 4.5

Available Shell Area = 1.1039 in<sup>2</sup>

Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - CA) * \text{MIN}((Sd_n/Sd_s) 1)$   
Available Nozzle Neck Area =  $2 * [(4 * (0.237 - 0)) + 0.375] * (0.237 - 0) * \text{MIN}((22,500/22,500) 1)$   
Available Nozzle Neck Area = 0.6271 in<sup>2</sup>

A-rpr = (Required Area - Available Shell Area - Available Nozzle Neck Area)  
A-rpr = 0.5836 - 1.1039 - 0.6271  
A-rpr = 0 in<sup>2</sup>

Since A-rpr <= 0, t\_rpr = 0

No Reinforcement Pad required.

t\_shell\_PWHT = Thickness of the shell plate, insert plate, or thickened insert plate for PWHT (in)

#### Nozzle Neck Material Properties

Material = A312-TP304

As per API-650 S.2b, Allowable Design Stress (Sd-neck) = 22.50e3 psi

t\_shell\_PWHT = t-plate  
t\_shell\_PWHT = 0.3750  
t\_shell\_PWHT = 0.3750 in

#### Thermal Stress Relief (PWHT) Requirements

D = Nozzle Nominal Diameter (NPS) (in)

Group = Shell Material Group

t\_shell = Shell Plate Thickness (in)

D = 4.0 in  
Group = None  
t\_shell = 0.3750 in

Shell material group (None) is not a group specified by API 650, 13th Ed, Section 5.7.4. Requirement for Thermal Stress Relief (PWHT) is unknown.

## Shell Manway: N5

### Repad Design

MANWAY Description : 20 in Neck Thickness 0.25  
Material: A240-304

t\_rpr = (Repad Required Thickness)  
t\_n = (Thickness of Neck)  
Sd\_n = (Stress of Neck Material)  
Sd\_s = (Stress of Shell Course Material)  
CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 1 : Elevation = 2.5 ft

As per API-650 S.5.b, Minimum Yield Strength at Ambient Temperature (Sy-ambient-flange) = 30.0e3 psi  
As per API-650 S.5.b, Minimum Yield Strength (Sy-flange) = 28.90e3 psi  
Thickness for MDMT-permissible-flange (per API-650 Figure 4.3) = 0.250 in

$$M = \text{MAX}(\text{SQRT}((\text{Sy-ambient-flange} / \text{Sy-flange})) , \text{SQRT}((30000 / \text{Sy-flange})) , 1) = 1.01885$$

As per API-650 5.7.5.6, Bolting Flange Erection Thickness (tf-erec) = 0.250 in

$$\text{tf-design} = \text{tc-design} - 0.125$$

$$\text{tf-design} = 0.611756 - 0.125$$

$$\text{tf-design} = 0.486756 \text{ in}$$

$$\text{tf-req} = \text{MAX}(\text{tf-erec} , \text{tf-design})$$

$$\text{tf-req} = \text{MAX}(0.250 , 0.486756)$$

$$\text{tf-req} = 0.486756 \text{ in}$$

$t_{\text{flange}} \geq \text{tf-req} \Rightarrow \text{PASS}$

## Roof Nozzle: N2

### Repad Design

(Per API-650 and other references below)

NOZZLE Description : 6 in SCH 40S TYPE RFSO  
Material: A312-TP304

$$t_{\text{rpr}} = (\text{Repad Required Thickness})$$

$$t_n = (\text{Thickness of Neck})$$

$$Sd_n = (\text{Stress of Neck Material})$$

$$Sd_s = (\text{Stress of Roof Material})$$

$$CA = (\text{Corrosion Allowance of Neck})$$

MOUNTED ON ROOF: Elevation = 61.5605 ft

ROOF PARAMETERS:

$$t_{\text{calc}} = 0.1875 \text{ in}$$

$$t_{\text{cr}} = 0.1875 \text{ in} (\text{Roof t-act less C.A})$$

$$t_c = 0.1875 \text{ in}$$

$$t_{\text{Basis}} = 0.1875 \text{ in}$$

(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15)

$$\text{Required Area} = t_{\text{Basis}} * D$$

$$\text{Required Area} = 0.1875 * 6.625$$

$$\text{Required Area} = 1.2422 \text{ in}^2$$

Available Roof Area =  $(t_c - t_{Basis}) * D$   
Available Roof Area =  $(0.1875 - 0.1875) * 6.625$   
Available Roof Area = 0 in<sup>2</sup>

Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * \text{MIN}((Sd_n/Sd_s) 1)$   
Available Nozzle Neck Area =  $2 * [(4 * (0.28 - 0)) + 0.1875] * (0.28 - 0) * \text{MIN}((22,500/22,500) 1)$   
Available Nozzle Neck Area = 0.7322 in<sup>2</sup>

A\_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)  
A\_rpr = 1.2422 - 0 - 0.7322  
A\_rpr = 0.51 in<sup>2</sup>

As per API-650 J.3.6.3, reinforcement pad is not required since roof loads do not exceed 25 psf.

No Reinforcement Pad required.

## Roof Nozzle: N1

### Repad Design

(Per API-650 and other references below)

NOZZLE Description : 4 in SCH 40S TYPE RFSO  
Material: A312-TP304

t\_rpr = (Repad Required Thickness)  
t\_n = (Thickness of Neck)  
Sd\_n = (Stress of Neck Material)  
Sd\_s = (Stress of Roof Material)  
CA = (Corrosion Allowance of Neck)

MOUNTED ON ROOF: Elevation = 60.644 ft

#### ROOF PARAMETERS:

t\_calc = 0.1875 in  
t\_cr = 0.1875 in (Roof t\_act less C.A)  
t\_c = 0.1875 in  
t\_Basis = 0.1875 in

(FOR ROOF NOZZLES, REF. API-650 FIG 5-19, TABLE 5-14 AND FOOTNOTE A OF TABLE 5-14, or API-650 FIG 5-20, TABLE 5-15 AND FOOTNOTE A OF TABLE 5-15)

Required Area =  $t_{Basis} * D$   
Required Area =  $0.1875 * 4.5$   
Required Area = 0.8438 in<sup>2</sup>

Available Roof Area =  $(t_c - t_{Basis}) * D$   
Available Roof Area =  $(0.1875 - 0.1875) * 4.5$

Available Roof Area = 0 in<sup>2</sup>

Available Nozzle Neck Area =  $2 * [(4 * (t_n - CA)) + t_c] * (t_n - ca) * \text{MIN}((Sd_n/Sd_s) 1)$   
Available Nozzle Neck Area =  $2 * [(4 * (0.237 - 0)) + 0.1875] * (0.237 - 0) * \text{MIN}(22,500/22,500) 1$   
Available Nozzle Neck Area = 0.5382 in<sup>2</sup>

A\_rpr = (Required Area - Available Roof Area - Available Nozzle Neck Area)  
A\_rpr = 0.8438 - 0 - 0.5382  
A\_rpr = 0.3055 in<sup>2</sup>

As per API-650 J.3.6.3, reinforcement pad is not required since roof loads do not exceed 25 psf.

No Reinforcement Pad required.

## Bottom Drain: N7

### Repad Design

NOZZLE Description : 2 in SCH 80S TYPE RFWN  
Material: A312-TP304

t\_rpr = (Repad Required Thickness)  
t\_n = (Thickness of Neck)  
Sd\_n = (Stress of Neck Material)  
Sd\_s = (Stress of Shell Course Material)  
CA = (Corrosion Allowance of Neck)

MOUNTED ON SHELL 1 : Elevation = 0 ft

#### COURSE PARAMETERS:

t\_calc = 0.1297 in  
t\_cr = 0.1297 in (Course t\_calc less C.A.)  
t\_c = 0.375 in (Course t less C.A.)  
t\_Basis = 0.1297 in

(SHELL NOZZLE REF. API-650 S.3.3.1, AND FOOTNOTE A OF TABLE 5-7)

Required Area = t\_Basis \* D  
Required Area = 0.1297 \* 2.375  
Required Area = 0.308 in<sup>2</sup>

Available Shell Area = (t\_c - t\_Basis) \* D

# Capacities and Weights [Back](#)

Capacity to Top of Shell (to Tank Height) : 62,051 gal  
Capacity to Design Liquid Level : 62,051 gal  
Capacity to Maximum Liquid Level : 62,051 gal  
Working Capacity (to Normal Working Level) : 0 gal  
Net working Capacity (Working Capacity - Min Capacity) : 0 gal  
Minimum Capacity (to Min Liq Level) : 1,027 gal

Component	New Condition (lbf)	Corroded (lbf)
SHELL	21,265	21,265
ROOF	1,102	1,102
RAFTERS	0	0
GIRDERS	0	0
FRAMING	0	0
COLUMNS	0	0
TRUSS	0	0
STRUCTURE COMPONENTS	0	0
BOTTOM	1,088	1,088
STAIRWAYS	0	0
ACCESS	0	0
STIFFENERS	133	133
WIND GIRDERS	0	0
ANCHOR CHAIRS	253	253
SHELL APPURTEANCES	362	362
ROOF APPURTEANCES	45	45
BOTTOM APPURTEANCES	0	0
INSULATION	0	0
FLOATING ROOF	0	0
TOTAL	24,249.4654	24,249.4654

Weight of Tank, Empty : 24,249.4654 lbf  
Weight of Tank, Full of Product (Design SG = 1) : 542,092.4654 lbf  
Weight of Tank, Full of Water : 542,092.0668 lbf  
Net Working Weight, Full of Product (Design SG = 1) : 533,520.8789 lbf  
Net Working Weight Full of Water : 533,520.8789 lbf

Foundation Area Req'd : 142.098 ft<sup>2</sup>  
Foundation Loading, Empty : 170.6529 lbf/ft<sup>2</sup>  
Foundation Loading, Full of Product Design : 3,814.9171 lbf/ft<sup>2</sup>  
Foundation Loading, Full of Water : 3,814.9143 lbf/ft<sup>2</sup>

## SURFACE AREAS

Roof : 141.9188 ft<sup>2</sup>  
Shell : 2,509.5325 ft<sup>2</sup>  
Bottom : 142.098 ft<sup>2</sup>