

Model Predictive Control for Object Avoidance with UAVs: Literature Review

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Papers Reviewed:

- Constrained Model-Based Predictive Control For Obstacle Avoidance (*Robotica 2017*)
- Model Predictive Control for Aerial Collision Avoidance in dynamic environments (*MED 2018*)
- Nonlinear MPC for Collision Avoidance and Control of UAVs with Dynamic Obstacles (*R-AL 2020*)
- Nonlinear Model Predictive Control-Based Guidance Algorithm for Quadrotor Trajectory Tracking with Obstacle Avoidance (*JSSC 2021*)

Constrained Model-Based Predictive Control For Obstacle Avoidance (Robotica 2017)

Eric Boivin, Andre Desbiens, Eric Gagnon

- This paper uses a MPC to control a fixed-wing autonomous airplane.
- Obstacle avoidance is achieved through MPC constraints.
 - Obstacles are assumed to be ellipsoidal or fit within ellipsoidal bounds.
 - Shape and location of obstacles are known and fixed.
 - Collision avoidance is achieved with a hard constraint on path intersection.

Constrained Model-Based Predictive Control For Obstacle Avoidance (Robotica 2017)

UAV Modeling (Fixed Wing)

$$\Delta \mathbf{X}(k+1) = A\Delta \mathbf{X}(k) + B\Delta \mathbf{U}(k)$$

$$\Delta \mathbf{Y}(k) = C\Delta \mathbf{X}(k)$$

$$\mathbf{U}(k) = \begin{bmatrix} u_\rho(k) & u_\psi(k) & u_z(k) \end{bmatrix}^T$$

$$\mathbf{Y}(k) = \begin{bmatrix} y_\rho(k) & y_\psi(k) & y_z(k) \end{bmatrix}^T$$

$$\begin{aligned} \mathbf{N}(k) &= \begin{bmatrix} n_x(k) \\ n_y(k) \\ n_z(k) \end{bmatrix} \\ &= \begin{bmatrix} n_x(k-1) + T_s y_\rho(k) \cos[y_\psi(k)] \\ n_y(k-1) + T_s y_\rho(k) \sin[y_\psi(k)] \\ y_z(k) \end{bmatrix} \end{aligned}$$

- \mathbf{X} is the state vector, and \mathbf{k} is the current iteration
- \mathbf{U} is the command vector, where $\mathbf{\Delta U(k)} = \mathbf{U(k)} - \mathbf{U(k-1)}$:
 - $\mathbf{u_rho}$ is the velocity set point,
 - $\mathbf{u_phi}$ is the heading set point,
 - $\mathbf{u_z}$ is the altitude set point,
- The output vector is \mathbf{Y} :
 - $\mathbf{y_rho}$ is the velocity in the flat earth horizontal plane,
 - $\mathbf{y_phi}$ is the heading,
 - $\mathbf{Y_z}$ is the altitude.
- \mathbf{N} is the position vector in an xyz frame, with \mathbf{k} being the current iteration, and $\mathbf{T_s}$ being the sample time
 - This position can be deduced from the output vector, as shown

Constrained Model-Based Predictive Control For Obstacle Avoidance (Robotica 2017)

Scenario Definition

- **P** contains all of the target waypoints, defined by a x,y,z coordinates
- **M** contains all of the x,y,z coordinates of the center of each obstacle
- **W** contains the ellipsoid semi-axis of each obstacle
 - **f_m** (>= 1) is a multiplicative safety factor
 - **f_a** (>= 0) is an additive safety factor
- **delta_j** represents the predicted distance between the vehicle and the jth target
 - **k** is the current time, while **tao** is a future time between 1 and the prediction horizon.

$$P = \begin{bmatrix} P_1 \\ P_2 \\ \vdots \\ P_p \end{bmatrix} = \begin{bmatrix} \begin{bmatrix} p_{x1} & p_{y1} & p_{z1} \end{bmatrix}^T \\ \begin{bmatrix} p_{x2} & p_{y2} & p_{z2} \end{bmatrix}^T \\ \vdots \\ \begin{bmatrix} p_{xp} & p_{yp} & p_{zp} \end{bmatrix}^T \end{bmatrix}$$

$$M(k) = \begin{bmatrix} M_1 & M_2 & \cdots & M_m \end{bmatrix}^T$$

$$W(k) = \begin{bmatrix} W_1 & W_2 & \cdots & W_m \end{bmatrix}^T$$

$$W_i = f_m \begin{bmatrix} w_{xi} & 0 & 0 \\ 0 & w_{yi} & 0 \\ 0 & 0 & w_{zi} \end{bmatrix} + f_a$$

$$\begin{aligned} \delta_j(k + \tau/k) &= \left| \hat{N}(k + \tau/k) - P_j \right| \\ &= \sqrt{\left[\hat{N}(k + \tau/k) - P_j \right]^T \left[\hat{N}(k + \tau/k) - P_j \right]} \end{aligned}$$

Constrained Model-Based Predictive Control For Obstacle Avoidance (Robotica 2017)

MPC Formation : Cost & Non-Linear Inequality Constraints

$$\Phi = [\Delta \mathbf{U}(k : k + h_c - 1)]^T \boldsymbol{\lambda} [\Delta \mathbf{U}(k : k + h_c - 1)] + \sum_{\tau=1}^{h_p} \delta_j(k + \tau/k)$$

$$\Delta \mathbf{U}_{min}(k : k + h_c - 1) \leq \Delta \mathbf{U}(k : k + h_c - 1) \leq \Delta \mathbf{U}_{max}(k : k + h_c - 1)$$

$$\mathbf{U}_{min}(k : k + h_c - 1) \leq \mathbf{U}(k : k + h_c - 1) \leq \mathbf{U}_{max}(k : k + h_c - 1)$$

$$\mathbf{N}_{min}(k + 1 : k + h_p) \leq \hat{\mathbf{N}}(k + 1 : k + h_p/k) \leq \mathbf{N}_{max}(k + 1 : k + h_p)$$

$$0 \leq \left| \mathbf{N}_R(k) - \hat{\mathbf{N}}(k + \tau/k) \right| \leq h_s \quad \text{for } \tau \in [1, h_p]$$

$$\mathbf{y}_{s-min}(k + 1 : k + h_p) \leq \hat{\mathbf{y}}_s(k + 1 : k + h_p/k) \leq \mathbf{y}_{s-max}(k + 1 : k + h_p)$$

- The cost function **Phi** minimizes both the distance to the j th target, while weighing the command input
 - Command inputs and rates are constrained for safe operation of autopilot with **U_min**, **deltaU_min**, **U_max** and **deltaU_max**
- The predicted position **N** is constrained over the prediction horizon
 - Also constrained over the sensor horizon relative to the current measured position
- The predicted velocity **y_s** is bounded over the prediction horizon as well, defined by:

$$\hat{\mathbf{y}}_s(k + \tau/k) = \sqrt{\frac{(\hat{\mathbf{y}}_p(k + \tau/k))^2 + \left(\frac{\hat{\mathbf{y}}_z(k + \tau/k) - \hat{\mathbf{y}}_z(k + \tau - 1/k)}{T_s} \right)^2}{}}$$

Constrained Model-Based Predictive Control For Obstacle Avoidance (Robotica 2017)

MPC Formation : Obstacle Avoidance

- The point $\mathbf{L}(k + \tau/k)$ exists on the line between $\mathbf{N}(k + \tau/k - 1/k)$ and $\mathbf{N}(k + \tau/k)$ if $0 \leq n(k + \tau/k) \leq 1$.
- The surface of the ellipsoid of the obstacle is defined by the equation:

$$[\mathbf{E}_i - \mathbf{M}_i]^T \mathbf{W}_i^{-2} [\mathbf{E}_i - \mathbf{M}_i] = 1$$

- If $\mathbf{E}_i = \mathbf{L}(k + \tau/k)$, then there is an intersection between the path and the obstacle.
 - This can be calculated with \mathbf{n}_1 and \mathbf{n}_2 .
 - If both are complex, then the line does not intersect. Otherwise, the line intersects the surface of the ellipsoid.
 - A binary variable is used to represent intersections, and is constrained to zero.

$$\mathbf{L}(k + \tau/k) = \hat{\mathbf{N}}(k + \tau - 1/k) + \eta(k + \tau/k) \begin{bmatrix} \hat{\mathbf{N}}(k + \tau/k) \\ -\hat{\mathbf{N}}(k + \tau - 1/k) \end{bmatrix}$$

$$\eta_{1i}(k + \tau/k) = \frac{-b_i(k + \tau/k) + \sqrt{\varphi(k + \tau/k)}}{2a_i(k + \tau/k)}$$

$$\eta_{2i}(k + \tau/k) = \frac{-b_i(k + \tau/k) - \sqrt{\varphi(k + \tau/k)}}{2a_i(k + \tau/k)}$$

$$\varphi(k + \tau/k) = b_i^2(k + \tau/k) - 4a_i(k + \tau/k)c_i(k + \tau/k)$$

$$\hat{\mathcal{M}} = \hat{\mathbf{N}}(k + \tau - 1/k) - \mathbf{M}_i$$

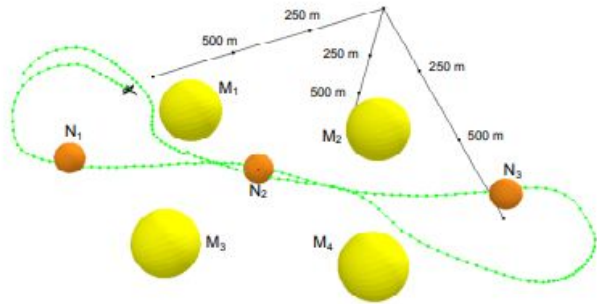
$$a_i(k + \tau/k) = \hat{\mathcal{N}}^T \mathbf{W}_i^{-2} \hat{\mathcal{N}}$$

$$b_i(k + \tau/k) = 2\hat{\mathcal{N}}^T \mathbf{W}_i^{-2} \hat{\mathcal{M}}$$

$$c_i(k + \tau/k) = \hat{\mathcal{M}}^T \mathbf{W}_i^{-2} \hat{\mathcal{M}} - 1$$

Constrained Model-Based Predictive Control For Obstacle Avoidance (Robotica 2017)

Implementation and Results



- MPC was implemented on an off-the-shelf UAV autopilot
 - Ground control station constraints guidance algorithms
 - MPC is implemented in C++ using NAG package, allowing for real time computation.
- A hardware-in-the-loop test was first conducted to minimize risk & complexity of outdoor flights
 - XPlane is used as a 3D viewer over UDP
- Real flights were then conducted, with simulated obstacles
 - Obstacle detection is only valid within simulated sensor range
 - *Plane was able to meet all targets and avoid all obstacles.*

Model Predictive Control for Aerial Collision Avoidance in dynamic environments (Journal: MED 2018)

Manuel Castillo-Lopez, Seyed Amin Sajadi-Alamdari, Jose Luis Sanchez-Lopez, Miguel A. Olivares-Mendez, Holger Voos

- A Non-linear MPC is used in order to generate a control command for a Drone UAV.
- Obstacle avoidance is achieved through soft constraints.
 - Increased distance to obstacles is achieved by propagating obstacle position using a constant velocity model throughout prediction horizon.

Model Predictive Control for Aerial Collision Avoidance in dynamic environments (Journal: MED 2018)

UAV Modeling (Quadcopter)

$$\dot{x} = v_x \cos(\psi) - v_y \sin(\psi) \quad (2a)$$

$$\dot{y} = v_x \sin(\psi) + v_y \cos(\psi) \quad (2b)$$

$$\dot{z} = v_z \quad (2c)$$

$$\dot{\psi} = v_\psi \quad (2d)$$

$$\dot{v}_i = (-v_i + k_i u_i) / \tau_i, \quad i \in \{x, y, z, \psi\} \quad (2e)$$

- Drone state: $\mathbf{x} = [x \ y \ z \ \psi \ v_x \ v_y \ v_z \ v_\psi]^T$
 - **Phi** represents the yaw angle, while xyz are ENU frame
 - **U** is the control input: $\mathbf{u} = [u_x \ u_y \ u_z \ u_\psi]^T$
- A Non-linear motion model is defined with **2**.
 - Model parameters **k_i** and **t_i** are chosen using the classical step response method:

$$k_i = \frac{v_i(\infty)}{u_i(\infty)} \quad \tau_i = \frac{3}{2}(t_{63} - t_{28})$$

Model Predictive Control for Aerial Collision Avoidance in dynamic environments (Journal: MED 2018)

MPC Trajectory Tracking

- Two cost terms are proposed:
 - **4** is used for trajectory tracking
 - Where \mathbf{x}^* is the reference state, and \mathbf{N} is the prediction horizon
 - **5** aims for stability and energy efficiency

$$J^t = \frac{1}{2} \sum_{i=0}^{N-1} \|\mathbf{x}_i - \mathbf{x}_i^*\|_P^2 + \|\mathbf{x}_N - \mathbf{x}_N^*\|_Q^2 \quad (4)$$

$$J^c = \frac{1}{2} \sum_{i=0}^{N-1} \|\mathbf{u}_i\|_R^2 \quad (5)$$

Model Predictive Control for Aerial Collision Avoidance in dynamic environments (Journal: MED 2018)

MPC Collision Avoidance

- Soft constraints are used to guarantee feasible solutions in tight situations
 - **(6)** is used to avoid ellipsoidal obstacles
 - Ellipsoidal term is defined by:
 - $\xi(\mathbf{r}_i, \mathbf{r}_i^o) = \sqrt{(\mathbf{r}_i - \mathbf{r}_i^o)^T Q_i (\mathbf{r}_i - \mathbf{r}_i^o)}$
 - **Q_i** is a metric from ellipsoidal dimensions, where **R_w** is the world frame transform.
 - $Q_i = {}^O R_W^T M_i {}^O R_W$ $M = \text{diag}(r_x^{-2}, r_y^{-2}, r_z^{-2})$
 - **S_i** is a slack term that relaxes the constraint with a sensitivity **theta^epsilon**, and is minimized by **(10)**.
 - Obstacles are assumed to have constant velocity such that:
 - $\mathbf{r}_i^o = \mathbf{r}_{i-1}^o + \dot{\mathbf{r}}_{i-1}^o \cdot \Delta t$
- **(11)** and **(12)** are used in a similar way to avoid walls and floor

$$\xi^2(\mathbf{r}_i, \mathbf{r}_i^o) + \theta^\epsilon s_i^\epsilon \geq 1 \quad (6)$$

$$J^\epsilon = \frac{1}{2} \sum_{i=0}^{N-1} \|s_i^\epsilon\|_S^2 \quad (10)$$

$$\pi(\mathbf{r}_i) + \theta^\pi s_i^\pi \geq 0 \quad (11)$$

$$J^\pi = \frac{1}{2} \sum_{i=0}^{N-1} \|s_i^\pi\|_T^2 \quad (12)$$

Model Predictive Control for Aerial Collision Avoidance in dynamic environments (Journal: MED 2018)

MPC Optimal Control Problem & Implementation

$$\underset{X,U}{\text{minimize}} \quad J = J^t + J^c + J^\xi + J^\pi$$

subject to: $\mathbf{x}_0 = \bar{\mathbf{x}}_0$

$$\mathbf{x}_{i+1} = \Phi_i(\mathbf{x}_i, \mathbf{u}_i) \quad i = 0, \dots, N-1$$

$$\xi(\mathbf{x}_i) + \theta^\xi s_i^\xi \geq 1 \quad i = 0, \dots, N-1$$

$$\pi(\mathbf{x}_i) + \theta^\pi s_i^\pi \geq 0 \quad i = 0, \dots, N-1$$

$$|\mathbf{u}_i| \leq \mathbf{u}_{max} \quad i = 0, \dots, N-1$$

- Combining previous equations, final form is a discrete nonlinear problem.
 - **u_max** introduces control limit constraints
- NMPC is implemented in C++ using the ACADO Toolkit.
 - Drone runs ROS, using V-REP as a SIL environment
- The implementation parameters are as follows:

Prediction horizon	4s
Discretization steps	20
Integrator type	Runge-Kutta 4
Maximum controls	1 m/s
Control Rate	20 Hz
Ellipsoidal obstacles sensitivity	0.15
Planar constraints sensitivity	0.25

Model Predictive Control for Aerial Collision Avoidance in dynamic environments (Journal: MED 2018)

Results - Street Crossing Scenario

- In a street crossing scenario, pedestrians are modeled with as a cylinder with infinite height, moving at a constant velocity.
- Two approaches were used:
 - The static approach samples the pedestrian position and assumes constant position throughout the prediction horizon
 - The dynamic approach propagates the pedestrian position with the constant velocity model.
- Dynamic approach was able to generate optimal paths that doesn't cross the future trajectory.

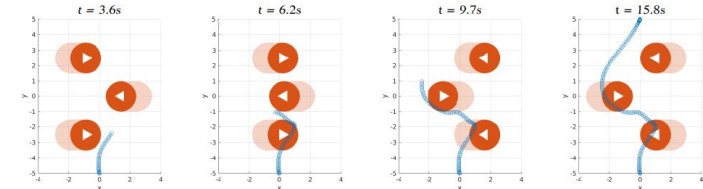


Fig. 7: UAV trajectory in street crossing scenario. Static approach.

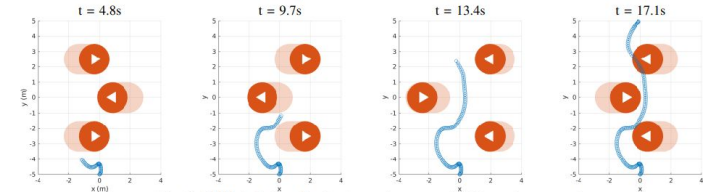


Fig. 8: UAV trajectory in street crossing scenario. Dynamic approach

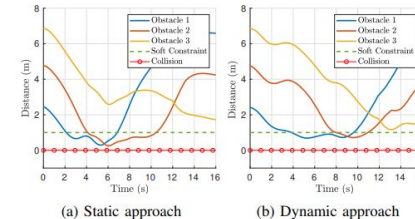


Fig. 4: Distance to obstacles in street crossing scenario

Model Predictive Control for Aerial Collision Avoidance in dynamic environments (Journal: MED 2018)

Results - Multiple Obstacle Scenario

- In the multiple object scenario, aerial robots are added in addition to the pedestrians.
- The UAV is able to avoid multiple collisions, despite soft constraint violation.

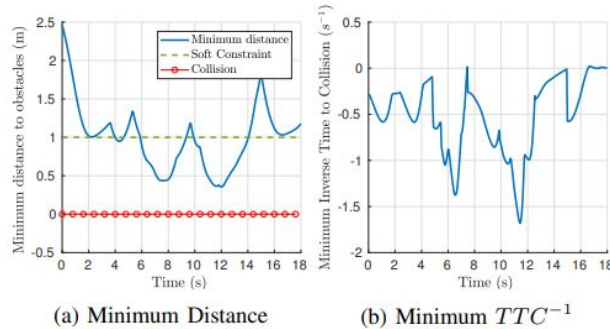
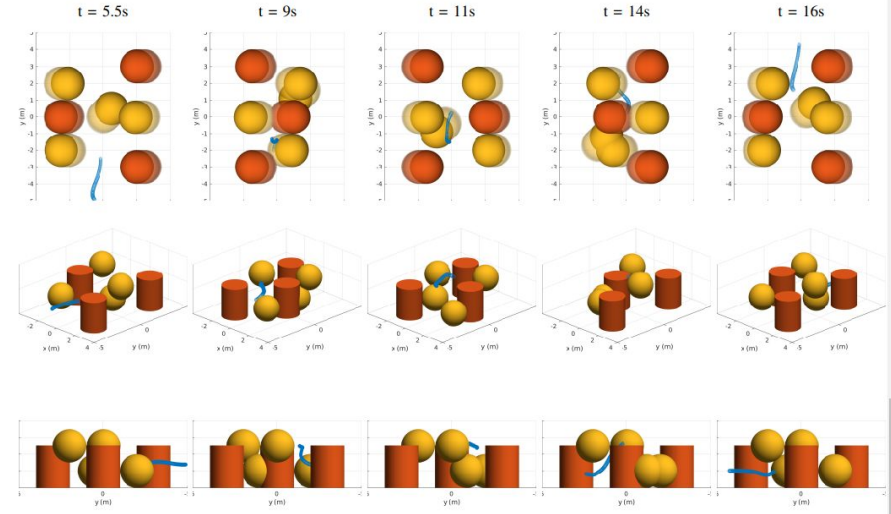


Fig. 9: Risk variables in the multiple obstacle scenario



Nonlinear MPC for Collision Avoidance and Control of UAVs with Dynamic Obstacles (R-AL 2020)

Bjorn Lindqvist , Sina Sharif Mansouri, Ali-akbar Agha-Mohammadi and George Nikolakopoulos

- Obstacle avoidance achieved through two novel methods:
 - Obstacle trajectory classification for more accurate trajectory prediction
 - Three classes for obstacles are proposed (static, linear, projectile)
 - Classification is done on-line to quickly and accurately predict different obstacle trajectories.
 - Increasing radius of safety sphere throughout prediction horizon
 - Accounts for sensor and prediction error

Nonlinear MPC for Collision Avoidance and Control of UAVs with Dynamic Obstacles (R-AL 2020)

UAV Modeling (Quadcopter)

$$\dot{\mathbf{p}}(t) = \mathbf{v}(t)$$

$$\dot{\mathbf{v}}(t) = R(\phi, \theta) \begin{bmatrix} 0 \\ 0 \\ T \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix} - \begin{bmatrix} A_x & 0 & 0 \\ 0 & A_y & 0 \\ 0 & 0 & A_z \end{bmatrix} \mathbf{v}(t)$$

$$\dot{\phi}(t) = 1/\tau_\phi (K_\phi \phi_{\text{ref}}(t) - \phi(t)),$$

$$\dot{\theta}(t) = 1/\tau_\theta (K_\theta \theta_{\text{ref}}(t) - \theta(t)),$$

- **p(t)** represents the position in xyz coordinates, with **v(t)** representing the linear velocity, viewed in a global fixed frame
- **R(phi, theta)** is a rotation matrix that describes the attitude in Euler form.
 - **Phi** is the roll angle along the X axis, while **Theta** is the pitch angle along the Y axis.
 - **T** is the total thrust
 - **A_x, A_y** and **A_z** are linear damping terms.
- **Phi_ref** and **Theta_ref** are the reference roll and pitch respectively.
 - The **K** and **Tao** values are gains and time constants respectively for the roll and pitch.

Nonlinear MPC for Collision Avoidance and Control of UAVs with Dynamic Obstacles (R-AL 2020)

Cost Function

- The state vector is: $x = [p, v, \phi, \theta]^\top$
- With input controls as: $u = [T, \phi_{\text{ref}}, \theta_{\text{ref}}]^\top$
- The forward euler method is used to predict using discrete time steps, allowing for the following equation to be used as the cost function:

$$J(\mathbf{x}_k, \mathbf{u}_k, u_{k-1|k}) = \sum_{j=0}^N \underbrace{\|\mathbf{x}_{\text{ref}} - \mathbf{x}_{k+j|k}\|_{\mathbf{Q}_x}^2}_{\text{State cost}} + \underbrace{\|u_{\text{ref}} - u_{k+j|k}\|_{\mathbf{Q}_u}^2}_{\text{Input cost}} + \underbrace{\|u_{k+j|k} - u_{k+j-1|k}\|_{\mathbf{Q}_{\Delta u}}^2}_{\text{Input smoothness cost}},$$

- where \mathbf{Q}_x , \mathbf{Q}_u and $\mathbf{Q}_{\Delta u}$ are positive definite weight matrices.
- The reference input is kept at steady-state hovering to minimize input commands:

$$u_{\text{ref}} = [g, 0, 0]$$

Nonlinear MPC for Collision Avoidance and Control of UAVs with Dynamic Obstacles (R-AL 2020)

Obstacle Avoidance Constraints

$$h_{\text{sphere}}(p, \xi^{\text{obs}}) = [(r^{\text{obs}} + r_s)^2 - (p_x - p_x^{\text{obs}})^2 - (p_y - p_y^{\text{obs}})^2 - (p_z - p_z^{\text{obs}})^2]_+ = 0, \quad (3)$$

$$h_{\text{sphere}}(\mathbf{p}_k, \boldsymbol{\xi}^{\text{obs}}) = \bar{0}, \quad (4)$$

$$[\phi_{\text{ref}, k+j-1|k} - \phi_{\text{ref}, k+j|k} - \Delta\phi_{\text{max}}]_+ = 0, \quad (5a)$$

$$[\phi_{\text{ref}, k+j|k} - \phi_{\text{ref}, k+j-1|k} - \Delta\phi_{\text{max}}]_+ = 0. \quad (5b)$$

$$u_{\min} \leq u_{k+j|k} \leq u_{\max}. \quad (6)$$

- In order to follow the constraint formulation structure, the following function is defined: $[h]_+ = \max\{0, h\}$.
- **(3)** ensures that the drone position is outside of the position of the obstacle
 - r_s is a safety radius that linearly increases along the horizon \mathbf{N} , accounting for measurement/prediction errors
 - r^{obs} and \mathbf{p}^{obs} are the radius and centers of the obstacles respectively.
- **(4)** extends 3 to allow for \mathbf{N} positions that describe obstacle trajectory at time k .
- **(5)** constrains the control delta for roll, and is extended for theta as well (pitch)
- **(6)** places hard bounds on possible control inputs that the low-level controller can handle.

Nonlinear MPC for Collision Avoidance and Control of UAVs with Dynamic Obstacles (R-AL 2020)

Obstacle Trajectory Classification

- Obstacle trajectory is divided into three classes:
 - Static, without any movement ($\dot{p}^{obs} = 0$).
 - Linear motion, where $\dot{p}^{obs}(t) = v^{obs}(t)$,
 - Projectile motion, represented by **(10)**.
 - **B** represents linear aerodynamic damping terms
 - Bouncing is simulated by applying a coefficient of restitution on the velocities to simulate energy loss
- Object motion is then discretized with forward euler, resulting in **(11)**.
- Classification is achieved by comparing the **M** last measured positions to the backwards prediction.
 - **(12)** is used to generate an error using each of the three classes
 - Lowest error class is chosen for future prediction.

$$\dot{p}^{obs}(t) = v^{obs}(t), \quad (10a)$$

$$\dot{v}^{obs}(t) = \begin{bmatrix} 0 \\ 0 \\ -g \end{bmatrix} - \begin{bmatrix} B_x & 0 & 0 \\ 0 & B_y & 0 \\ 0 & 0 & B_z \end{bmatrix} v^{obs}(t), \quad (10b)$$

$$x_{k|k+n+1}^{obs} = \alpha_t(x_{k|k+n}^{obs}), \quad (11)$$

$$x_{k|k+n-1}^{obs} = \beta_t(x_{k|k+n}^{obs}).$$

$$e^{traj} = \sum_{j=1}^M |p_j^{prev} - p_{k|k-j}^{obs}| + |v_j^{prev} - v_{k|k-j}^{obs}|. \quad (12)$$

Nonlinear MPC for Collision Avoidance and Control of UAVs with Dynamic Obstacles (R-AL 2020)

MPC Formulation and Implementation

$$\underset{\mathbf{u}_k, \mathbf{x}_k}{\text{Minimize}} J(\mathbf{x}_k, \mathbf{u}_k, u_{k-1|k}) \quad (8a)$$

$$\text{s. t.} \cdot x_{k+j+1|k} = \zeta(x_{k+j|k}, u_{k+j|k}), \quad j = 0, \dots, N-1, \quad (8b)$$

$$u_{\min} \leq u_{k+j|k} \leq u_{\max}, \quad j = 0, \dots, N, \quad (8c)$$

$$h_{\text{sphere}}^i(p_{k+j|k}, \xi_j^{\text{obs}, i}) = 0, \quad j = 0, \dots, N, \quad (8d)$$

$$i = 1, \dots, N_s \quad (8e)$$

$$\text{Constraints (5), } j = 0, \dots, N. \quad (8f)$$

- The NMPC problem can be formulated with **(8)** assuming **N_s** spherical obstacles
 - Solved using the PANOC algorithm, leveraging the OpEn framework.
- Vicon Motion capture is used to track UAV and obstacle.
- Computation is completed on a remote laptop running ROS.

Nonlinear MPC for Collision Avoidance and Control of UAVs with Dynamic Obstacles (R-AL 2020)

Results

- Dynamic NMPC model is able to avoid thrown objects by predicting future trajectory.
 - Dynamic model is even able to avoid bouncing obstacle.
- Traditional methods are too slow to detect when objects enter collision sphere, resulting in collision.
- Can also accurately track and avoid multiple objects.
- Video demo: <https://youtu.be/vO3xjvMMNJ4>

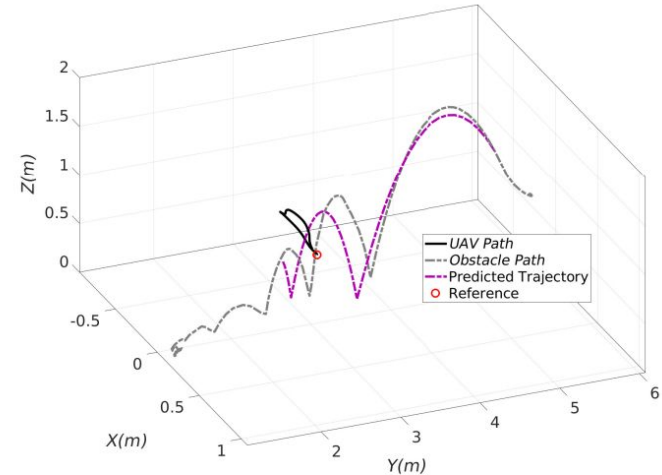


Fig. 6: Path of UAV and dynamic obstacle during experiment with bouncing ball.

Nonlinear Model Predictive Control-Based Guidance Algorithm for Quadrotor Trajectory Tracking with Obstacle Avoidance (JSSC 2021)

Zhao ChunHui, Wang Dong, Hu JinWen, Pan Quan

- Trajectory Tracking performance is enhanced by adding stability constraints
 - Non-linear lyapunov stability constraints are added to increase tracking performance with disturbances compared to Lyapunov-based backstepping control.
- Obstacle avoidance is achieved with a simple switching cost function
 - Cost function activates when the drone is within a defined radius of a known, static target.

Nonlinear Model Predictive Control-Based Guidance Algorithm for Quadrotor Trajectory Tracking with Obstacle Avoidance (JSSC 2021)

UAV Modeling (Quadcopter)

- The position and yaw vector is represented by $\boldsymbol{\eta} = [x, y, z, \psi]^T$
 - Where **xyz** are ENU frame, while **phi** represents the rotation about the **z** axis.
- The kinematics are then represented by: $\dot{\boldsymbol{\eta}} = \mathbf{R}(\psi)\mathbf{v}_b$,
 - Where
$$\mathbf{R}(\psi) = \begin{bmatrix} \cos(\psi) & -\sin(\psi) & 0 & 0 \\ \sin(\psi) & \cos(\psi) & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
- **v_b** is the body frame velocity.
 - The velocity response and reference velocity commands can be approximated by $\dot{\mathbf{v}}_b = \mathbf{S}\mathbf{v}_b + \mathbf{F}\mathbf{u}$,
 - $\mathbf{u} = [u_x, u_y, u_z, u_\psi]^T$ is the control input, while **S** and **F** are parameters based on the gains and time constants from their corresponding first-order transfer functions.
- As a result, the dynamic model is defined as:

$$\dot{\mathbf{x}} = \begin{bmatrix} \mathbf{R}(\psi)\mathbf{v}_b \\ \mathbf{S}\mathbf{v}_b + \mathbf{F}\mathbf{u} \end{bmatrix} \triangleq \mathbf{f}(\mathbf{x}, \mathbf{u}),$$

Nonlinear Model Predictive Control-Based Guidance Algorithm for Quadrotor Trajectory Tracking with Obstacle Avoidance (JSSC 2021)

NMPC Tracking

- The UAV is driven to follow a reference path $\mathcal{S}(\theta) = [x_{rr}(\theta), y_{rr}(\theta), z_{rr}(\theta)]^T$
 - This is used to generate a time-parameterized reference trajectory: $\eta_r(t) = [x_r(t), y_r(t), z_r(t), \psi_r(t)]^T$
 - Theta is time-dependant, following the predetermined timing law: $\theta(t) = v_t t$,
 - $v_t > 0$ to denote the forward velocity of the drone.
 - Singularities in the reference trajectory are avoided by assuming that the reference trajectory and its derivatives are bounded.
- NMPC is designed so that the real position of the drone converges to the reference trajectory: $\lim_{t \rightarrow \infty} \|\eta(t) - \eta_r(t)\| = 0$;

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NMPC Obstacle Avoidance

- Obstacles are defined with a position \mathbf{p}_o and a safety radius r_s .
- Switching behavior between trajectory tracking and obstacle avoidance is achieved through

$$J^{oa}(\mathbf{x}(t)) = \begin{cases} \lambda, & \|\mathbf{p}(t) - \mathbf{p}_o\| < r_s \quad (\text{obstacle avoidance}), \\ 0, & \|\mathbf{p}(t) - \mathbf{p}_o\| \geq r_s \quad (\text{trajectory tracking}), \end{cases} \quad (5)$$

- However, due to the lack of continuous differentiability, J^{oa} is defined instead by

$$J^{oa}(\mathbf{x}(t)) \approx \rho(t) = \frac{\lambda}{1 + e^{-k \cdot d(t)}},$$

- Where $d(t) = r_s^2 - (\mathbf{p}(t) - \mathbf{p}_o)^T (\mathbf{p}(t) - \mathbf{p}_o)$

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NMPC Formation

$$\begin{aligned} \mathcal{P}_0(\mathbf{x}) : \min_{\hat{\mathbf{u}}(\cdot)} J &= \int_{t_k}^{t_k+T} \|\tilde{\mathbf{x}}(s; t_k)\|_{\mathbf{Q}}^2 + J^{oa}(\hat{\mathbf{x}}(s; t_k)) + \|\hat{\mathbf{u}}(s; t_k)\|_{\mathbf{R}}^2 ds \\ \text{s.t. } \dot{\hat{\mathbf{x}}}(s; t_k) &= \mathbf{f}(\hat{\mathbf{x}}(s; t_k), \hat{\mathbf{u}}(s; t_k)), \quad s \in [t_k, t_k + T], \\ \hat{\mathbf{x}}(t_k; t_k) &= \mathbf{x}(t_k), \\ \|\hat{\mathbf{u}}(s; t_k)\|_{\infty} &\leq u_{\max}, \quad s \in [t_k, t_k + T], \\ \frac{\partial V}{\partial \mathbf{x}} \mathbf{f}(\hat{\mathbf{x}}(t_k; t_k), \hat{\mathbf{u}}(t_k; \hat{\mathbf{x}}(t_k; t_k))) &\leq \frac{\partial V}{\partial \mathbf{x}} \mathbf{f}(\hat{\mathbf{x}}(t_k; t_k), \mathbf{h}(\hat{\mathbf{x}}(t_k; t_k))), \end{aligned}$$

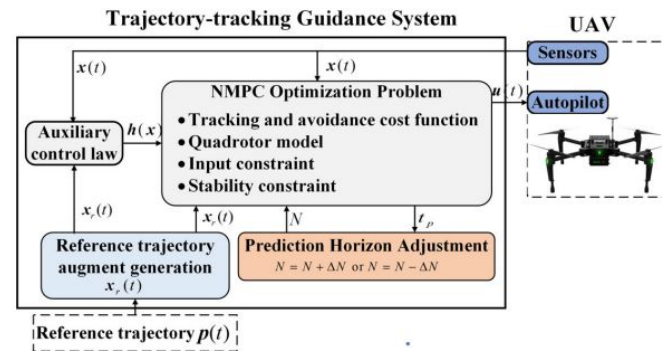
- The NMPC can now be formed as seen on the left.
 - The error state $\tilde{\mathbf{x}} = \hat{\mathbf{x}} - \mathbf{x}_r$
 - \mathbf{t}_k is the current time,
 - \mathbf{T} is the prediction horizon,
 - \mathbf{Q} and \mathbf{R} are positive-definite matrices that define cost.
- This formation also considers Lyapunov Stability:
 - $\mathbf{h}(\mathbf{x})$ is the lyapunov-based nonlinear tracking control law
 - $\mathbf{V}(\mathbf{x})$ is the corresponding Lyapunov function.

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NMPC Implementation

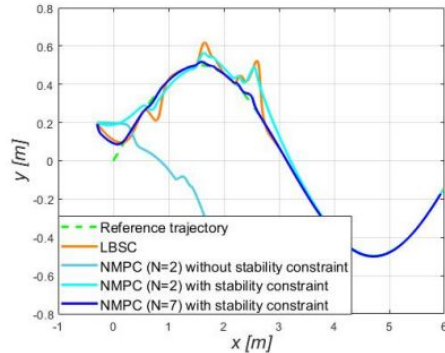
- The NMPC is converted to a discrete-time version as seen on the right.
- **delta** is the sampling period.
- **N** is the number of steps in the sampling period.
- **c_in** accounts for both the input and stability constraint.

$$\begin{aligned} \mathcal{P}_1(x) \quad & \min_{\hat{u}_i} J = \sum_{i=0}^N (\|\tilde{x}_i\|_Q^2 + \|\hat{u}_i\|_R^2 + J^{oa}(\hat{x}_i))\delta \\ \text{s.t.} \quad & \hat{x}_{i+1} = \hat{x}_i + f(\hat{x}_i, \hat{u}_i)\delta, \\ & \hat{x}_0 = x(t_k), \\ & c_{in}(\hat{x}_i, \hat{u}_i) \leq 0, \end{aligned}$$



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NMPC Experimental Results



- Trajectory tracking was tested with and without the stability constraint (left)
 - Under wind gusting conditions, the stability constraint allows the drone to better track the given trajectory.
- For collision avoidance, a static obstacle was placed with a known position (right).
 - As v_t increased, the controller was able to avoid the collision region.

