

EE3235 Analog Integrated Circuit Analysis and Design I

Homework 6

2-Stage Opamp with CMFB

In this homework, you are asked to build the circuit shown in Fig. 1, and the specifications you need to meet are listed in Table. 1. Please make sure your circuit meets all specs in TT, FF, and SS corners.

Please note that there's no restriction on how to design the CM SENSE and CMFB blocks, if only the common-mode feedback loops are stable; however, you are welcomed to refer to Fig. 5. for a basic implementation.

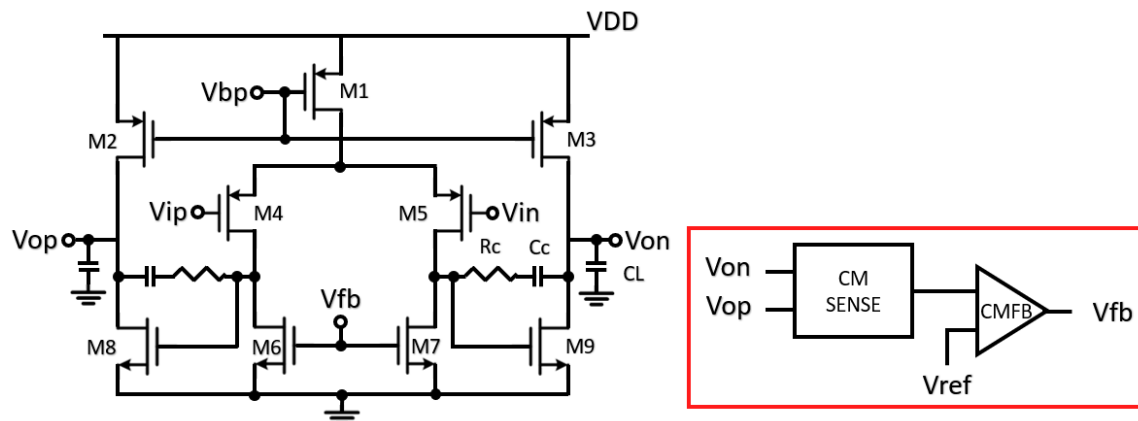


Fig. 1. 2-Stage Opamp with Common Mode Feedback.

Parameters	Specification	This Work		
		TT	FF	SS
Supply Voltage(V)		1.8		
Temp. (°C)		27		
Loading Cap. (pF)		1		
Output CM Voltage (V) @ Vin, cm=0.8V	0.9±20mV	899.9916m	899.9872m	899.9943
Open Loop Gain(dB)	>70	75.7115	74.6379	77.6288
GBW (MHz)	>5	14.4632	26.7331	5.3342
Phase Margin (degree)	> 60	80.2694	60.2790	104.2876
Phase Margin Mode Range (V)	≥ 1	1.26	1.33	1.06
Power Consumption(uW)	< 50	17.2189	28.7019	9.9794

Table. 1. Specification and Performance

- Elaborate on your design strategy, including how you intend to meet each specification and how you determine the size of the transistors. Please note that every design strategy must come from certain reasonable inferences or calculations, no SPICE monkeys are allowed in the class!
- Step1. Use ideal E element first and choose the size of NMOS and PMOS and CM SENSE

- r_1 and r_2 are used as CM SENSE, so r_1 and r_2 must be large enough to ensure that M8 or M9 is not starved when a large differential swing appears at the output. Therefore, I choose $r_1=r_2=80\text{M}\Omega$ which are large enough to maintain the output CM level.
- Choose the size of NMOS and PMOS
 - Assume the mobility of NMOS is three times of that of PMOS, so the $W_{\text{PMOS}} = 3W_{\text{NMOS}}$
 - M1 is the current source and is divided into two path (M4 and M5), so the I_d of M1 should be two times the I_d of M4 or M5 so I assume width of M1 is two times of M4 or M5.
 - Choose bias voltage $V_{bp}=1.2\text{V}$ since threshold voltage of PMOS in this process is about 450mV to 550mV so I set bias voltage equal 1.2 so $V_{SG} = 1.8 - 1.2 = 600\text{mV}$. In this way, M1 will not go to subthreshold region.
 - All transistors should be in saturation region.
 - $V_{GS} > V_{TH}$. Otherwise, it will go to subth or cut off. So, V_{TH} should be small enough which means the length of transistors should be large enough.
 - $V_{DS} > V_{GS} - V_{TH}$. Otherwise, it will go to linear region. So, V_{TH} should also no too small which means the length of transistors should be larger enough.
 - So I considers using $l = 1.4\mu$ for all transistors which gives $V_{TH} = 375\text{mV}$
 - Gain should be larger than 70dB (3162.3V/V), and by the gain equation I derive below:

$$\begin{aligned}
 -\text{gain} &= (\text{gm first stage}) \times (\text{gm second stage}) \\
 &= (g_{m4 \text{ or } 5} \times R_{out1}) \times (g_{m8,9} \times R_{out2}) \\
 &= g_{m4 \text{ or } 5} \times (r_{o4,5} \parallel r_{o6,7}) \times g_{m8,9} \times (r_{o8,9} \parallel r_{o2,3} \parallel r_{1 \text{ or } 2}) \\
 &= g_{m4 \text{ or } 5} \times \left(\frac{1}{g_{d34,5}} \parallel \frac{1}{g_{d36,7}} \right) \times g_{m8,9} \times \left(\frac{1}{g_{d18,9}} \parallel \frac{1}{g_{d15,2,3}} \parallel 80\text{M}\Omega \right)
 \end{aligned}$$

We can see the best way to boost the gain is to increase the gm, since there are two gm factors. And we know.

$$g_m = \frac{2I_0}{V_{GS} - V_{th}}$$

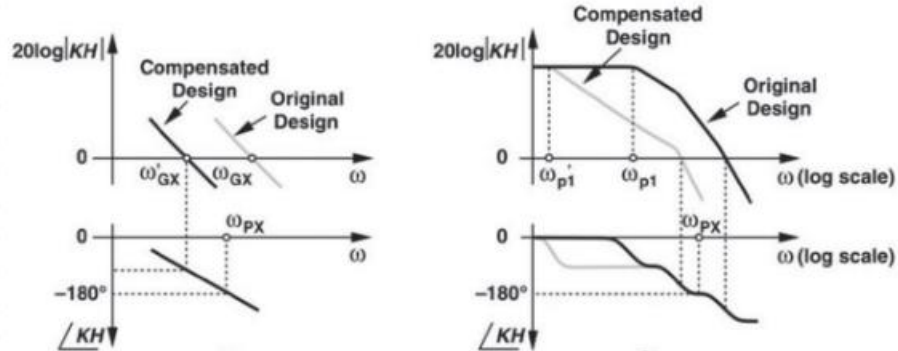
Since I fixed the length(V_{TH}) and bias voltage so $V_{GS} - V_{TH}$ does not change a lot, so I decided to increase I_D (do not increase too much, or the power consumption would be too large). By the I_D equation:

$$M_1 = \frac{1}{2} \mu n C_{ox} \frac{w}{L} (V_{GS} - V_{th})^2$$

we can see that as I fixed the length and bias voltage, so I can only increase current by increase the width. And consider M1 which is the current source of the circuit, I decided to use $w = 8.4\mu$, which has enough but not too much power consumption. Since I have decided the ratio of all NMOS and PMOS, I can derive the width of all other transistors(M2~M9).

Step2. Adjust Rc and Cc

- in step1, I only check gain and power consumption meet the spec. or not. To satisfy GBW and phase margin, we use miller compensation with Rc and Cc. According to frequency compensation learned in class:



So, by adjust Rc and Cc, we can have enough phase margin.

- Look at the pole and zero in my design:

Look Rc and Cc as an impedance $Z_c = R_c + \frac{1}{sC_c}$
then do the Miller compensation

$$\begin{cases} Z_1 = Z_c \times \left(\frac{1}{1 - A_{V2}} \right) = -\frac{1}{A_{V2}} \left(R_c + \frac{1}{sC_c} \right) \\ Z_2 = Z_c \times \left(\frac{1}{1 - \frac{1}{A_{V2}}} \right) \approx R_c + \frac{1}{sC_c} \end{cases}$$

at ①:

$$\omega_{p1} = \frac{1}{R_{out, stage1} \cdot C_{out, stage1}} \approx \frac{1}{\left((r_{o1} \parallel r_{o2}) + \frac{-R_c}{A_{V2}} \right) \cdot (-A_{V2} \cdot C_c)}$$

at ②:

input output together

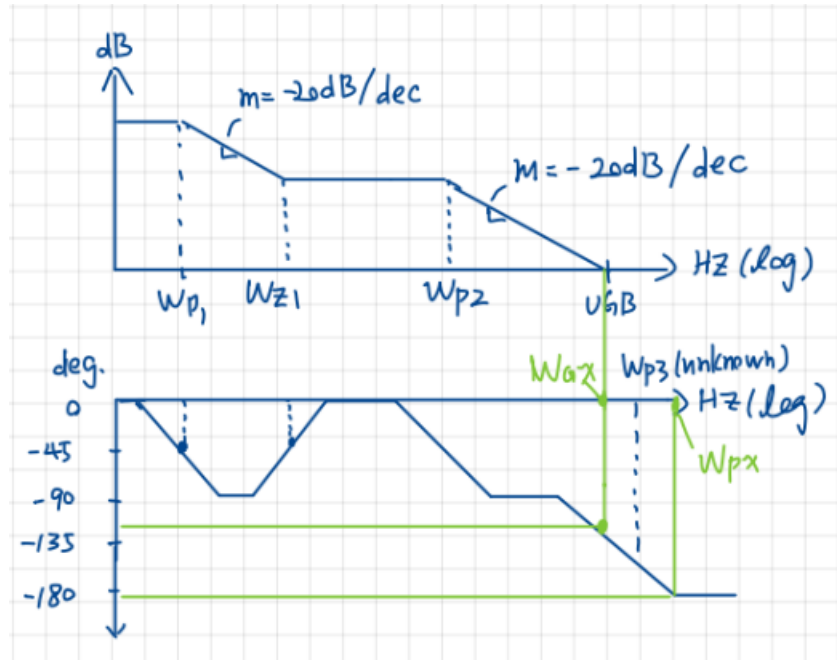
for C_L :

$$\omega_p = \frac{1}{(r_{o1} \parallel r_{o2} \parallel \frac{1}{g_{m1}}) C_L}$$

for C_c :

$$\omega_z = \frac{1}{\left(\frac{1}{g_{m1}} - R_c \right) C_c}$$

- Bode plot.



- I found that adjust C_c doesn't affect the simulation result too much. I think it is because:

$$W_{p1} = \frac{1}{R_{out, stage1} \cdot C_{out, stage1}} \approx \frac{1}{(R_{os1} || R_{D1}) + \frac{R_c}{A_{V1}}} \cdot (-A_{V1} \cdot C_c)$$

$$W_z = \frac{1}{(\frac{1}{g_{m1}} - R_c) C_c}$$

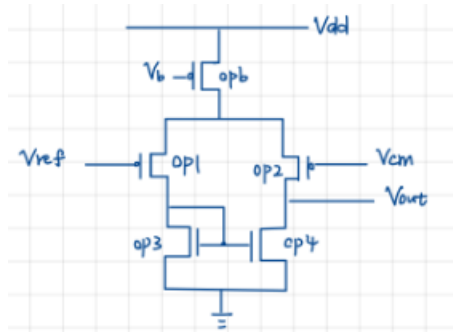
if we adjust C_c , both pole and zero will move,

if we adjust R_c , since $\frac{R_1}{A_{V1}}$ is small, W_{p1} will not change a lot, but W_z will change so change R_c will change phase Margin and UGB.

$R_c \uparrow, W_{p1} \downarrow, W_z \uparrow$ $C_c \uparrow, W_{p1} \downarrow, W_z \downarrow$
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So, I decided to change R_c to 250k Ω and C_c I used my original value (50pF)

Step3. Design CMFB: replace the ideal CMFB with the following design:



- Using same strategy in step1, PMOS width is three times of NMOS and since MOPB is the current source and is divided into two path (MOP1 and MOP2), so the Id of MOPB should be two times the Id of MOP1 or MOP2 so I assume width of MOPB is two times of MOP1 or MOP2.
- When using ideal E element, I assume that gain equal 1000, so the gain of my design should be larger as possible, so using the same strategy in step1, I use $(W/L)_{NMOS} = 1.4u/1.4u$, $(W/L)_{PMOS} = 4.2u/1.4u$ and bias voltage $V_B = 1.2V$ to have larger gain and keep the power not too large.
- Input is connected to PMOS gate. Compare with input connected to NMOS:

I found that it is easier to enter linear region when input connected to NMOS. I think it is because in my design under this process, V_{TH} of PMOS is higher than that of NMOS so:

$V_{DS} > V_{GS} - V_{th}$
 V_{GS} is fixed (V_{GS} is V_{ref} or V_{cm})
 so if V_{th} is larger, $V_{GS} - V_{th}$ is smaller
 , it's easier to enter sat.

Step4. Return to check if I meet all the spec. or not.

subckt	element	0:m1	0:m2	0:m3	0:m4	0:m5	0:m6	subckt	element	0:m7	0:m8	0:m9	0:mopb	0:mop1	0:mop2	subckt	element	0:m3	0:m4
model	0:p 18.1	0:p 18.1	0:p 18.1	0:p 18.1	0:p 18.1	0:p 18.1	0:n 18.1	model	0:n 18.1	0:n 18.1	0:n 18.1	0:p 18.1	0:p 18.1	0:p 18.1	0:p 18.1	model	0:n 18.1	0:n 18.1	
region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	region	Saturation	Saturation	
id	-3.1824u	-1.6139u	-1.6139u	-1.5912u	-1.5912u	-1.5912u	1.5912u	id	1.5912u	1.6139u	1.6139u	-3.1558u	-1.5778u	-1.5788u	id	1.5778u	1.5788u		
ibs	4.510e-22	2.531e-22	2.531e-22	98.9238a	98.9238a	-5.641e-22	-5.641e-22	ibs	-5.641e-22	-5.721e-22	-5.721e-22	4.473e-22	74.2319a	74.2319a	ibs	1.5778u	1.5788u		
ibd	178.7788a	285.8362a	285.8362a	424.2736a	424.2736a	-109.8365a	-109.8365a	ibd	-109.8365a	-214.7342a	-214.7342a	134.1539a	423.4148a	423.2288a	ibd	-110.4842a	-110.6265a		
vgs	-600.0000m	-600.0000m	-600.0000m	-607.6469m	-607.6469m	463.6577m	463.6577m	vgs	463.6577m	460.3467m	460.3467m	-600.0000m	-605.6120m	-605.6204m	vgs	463.0610m	463.0610m		
vds	-312.3531m	-900.0004m	-900.0004m	-1.0273	-1.0273	460.3467m	460.3467m	vds	460.3467m	899.9916m	899.9916m	-234.3880m	-1.1026	-1.1026	vds	463.0610m	463.6577m		
vbs	0	0	0	312.3531m	312.3531m	0	0	vbs	0	0	0	0	234.3880m	234.3880m	vbs	0	0		
vth	-480.9090m	-480.6972m	-480.6972m	-375.8095m	-375.8095m	375.2334m	375.2334m	vth	375.2334m	372.5647m	372.5647m	-480.0090m	-555.2350m	-555.2350m	vth	375.2169m	375.2133m		
vdsat	-120.6114m	-129.2602m	-129.2602m	-134.2345m	-134.2345m	107.3303m	107.3303m	vdsat	107.3303m	106.9271m	106.9271m	-120.6111m	-132.2771m	-132.2771m	vdsat	106.9656m	106.9679m		
vod	-111.9902m	-111.3020m	-111.3020m	-111.7513m	-111.7513m	88.4243m	88.4243m	vod	88.4243m	87.7820m	87.7820m	-111.9902m	-110.3769m	-110.3853m	vod	87.8441m	87.8477m		
beta	424.7954u	209.6698u	209.6698u	196.0040u	196.0040u	301.9646u	301.9646u	beta	301.9646u	301.8915u	301.8915u	424.7954u	199.9312u	199.9308u	beta	301.9574u	301.9573u		
gam eff	557.0847m	557.0847m	557.0847m	554.9713m	554.9713m	507.4460m	507.4460m	gam eff	507.4460m	507.4460m	507.4460m	557.0847m	555.4707m	555.4707m	gam eff	507.4460m	507.4460m		
gm	40.7298u	20.6658u	20.6658u	20.2658u	20.2658u	23.6267u	23.6267u	gm	23.6267u	23.9341u	23.9341u	40.2420u	20.2285u	20.2285u	gm	23.4946u	23.4962u		
gds	253.0841n	49.7514n	49.7514n	44.7198n	44.7198n	242.7020n	242.7020n	gds	242.7020n	225.4346n	225.4346n	491.2756n	43.0826n	43.0974n	gds	240.8166n	240.7610n		
gmb	12.4845u	6.2893u	6.2893u	5.4364u	5.4364u	4.8111u	4.8111u	gmb	4.8111u	4.8293u	4.8293u	12.2579u	5.5820u	5.5823u	gmb	4.7847u	4.7850u		
cdtot	10.8661f	4.7513f	4.7513f	4.4763f	4.4763f	2.0681f	2.0681f	cdtot	2.0681f	1.9014f	1.9014f	11.6711f	4.4769f	4.4772f	cdtot	2.0666f	2.0663f		
cgtot	74.5345f	37.1806f	37.1806f	36.8262f	36.8262f	12.9906f	12.9906f	cgtot	12.9906f	12.9716f	12.9716f	74.9139f	36.8524f	36.8527f	cgtot	12.9833f	12.9834f		
cstot	85.1467f	42.6675f	42.6675f	41.2103f	41.2103f	14.2086f	14.2086f	cstot	14.2086f	14.1886f	14.1886f	85.8138f	41.4709f	41.4712f	cstot	14.1991f	14.1992f		
cbtot	39.2337f	19.1978f	19.1978f	16.8783f	16.8783f	6.5216f	6.5216f	cbtot	6.5216f	6.3666f	6.3666f	39.5072f	17.3110f	17.3113f	cbtot	6.5206f	6.5204f		
cgs	65.5249f	32.5313f	32.5313f	32.6696f	32.6696f	11.3508f	11.3508f	cgs	11.3508f	11.3264f	11.3264f	65.6642f	32.5950f	32.5953f	cgs	11.3558f	11.3558f		
cgd	3.1695f	1.5092f	1.5092f	1.5084f	1.5084f	1.5084f	495.1088a	cgd	495.1088a	490.7838a	490.7838a	3.4157f	1.5080f	1.5080f	cgd	495.0775a	495.0576a		

TT: All transistors are in saturation.

subckt	0:m1	0:m2	0:m3	0:m4	0:m5	0:m6	subckt	0:m7	0:m8	0:m9	0:mopb	0:mop1	0:mop2	subckt	0:mop3	0:mop4
element	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	element	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	element	0:n 18.1	0:n 18.1
region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	region	Saturation	Saturation
id	-5.2840u	-2.7165u	-2.7165u	-2.6420u	-2.6420u	-2.6420u	id	2.6420u	2.7165u	2.7165u	-5.2285u	-2.6141u	-2.6144u	id	2.6141u	2.6144u
lbs	7.487e-22	4.258e-22	4.258e-22	108.2219u	108.2219u	-9.304e-22	lbs	-9.304e-22	-9.567e-22	-9.567e-22	7.409e-22	75.3909u	75.3909u	lbs	-9.206e-22	-9.207e-22
lbd	180.0000u	205.0592u	205.0592u	426.6419u	426.6419u	-109.9015u	lbd	-109.9015u	-216.6750u	-216.6750u	136.0720u	426.1087u	425.9215u	lbd	-118.3059u	-118.5076u
vgs	-600.0000u	-600.0000u	-600.0000u	-604.4584u	-604.4584u	459.0090u	vgs	459.0090u	456.7410u	456.7410u	-600.0000u	-662.6375u	-662.6503u	vgs	458.1677u	458.1677u
vds	-315.5416u	-900.0120u	-900.0120u	-1.0277	-1.0277	456.7410u	vds	456.7410u	899.9872u	899.9872u	-237.3625u	-1.1045	-1.1036	vds	458.1677u	459.0090u
vbs	0	0	0	315.5416u	315.5416u	0	vbs	0	0	0	237.3625u	237.3625u	0	vbs	0	0
vth	-452.5666u	-452.5644u	-452.5644u	-537.2271u	-537.2271u	341.0607u	vth	341.0607u	338.3576u	338.3576u	-452.5666u	-517.2850u	-517.2850u	vth	341.0520u	341.0406u
vdسات	-155.1721u	-156.5774u	-156.5774u	-161.6227u	-161.6227u	127.3774u	vdسات	127.3774u	127.6721u	127.6721u	-155.1718u	-159.0710u	-159.0808u	vdسات	126.9155u	126.8109u
vod	-147.4334u	-147.6436u	-147.6436u	-147.2212u	-147.2212u	117.9483u	vod	117.9483u	118.3834u	118.3834u	-147.4334u	-145.3525u	-145.3653u	vod	117.1157u	117.1209u
beta	456.8398u	226.1769u	226.1769u	212.3268u	212.3268u	331.8475u	beta	331.8475u	331.7714u	331.7714u	456.8398u	215.6337u	215.6339u	beta	331.8344u	331.8343u
gm eff	557.0846u	557.0846u	557.0846u	554.9512u	554.9512u	507.4466u	gm eff	507.4466u	507.4466u	507.4466u	557.0846u	555.4514u	555.4514u	gm eff	507.4466u	507.4466u
gm	57.2119u	29.3681u	29.3681u	28.4868u	28.4868u	33.9157u	gm	33.9157u	34.6578u	34.6578u	56.1999u	28.4458u	28.4467u	gm	33.6962u	33.6991u
gds	484.4332u	81.8204u	81.8204u	72.0396u	72.0396u	367.4424u	gds	367.4424u	333.8863u	333.8863u	1.1093u	68.7014u	68.7387u	gds	364.1506u	363.9651u
gmb	16.9173u	8.6828u	8.6828u	7.4213u	7.4213u	6.6335u	gmb	6.6335u	6.7110u	6.7110u	16.6274u	7.6201u	7.6205u	gmb	6.5920u	6.5925u
cdtot	10.4802f	4.5194f	4.5194f	4.2712f	4.2712f	1.9734f	cdtot	1.9734f	1.8137f	1.8137f	11.7124f	4.2706f	4.2710f	cdtot	1.9724f	1.9720f
cgstot	78.4274f	39.0444f	39.0444f	38.6868f	38.6868f	13.7090f	cgstot	13.7090f	13.6961f	13.6961f	78.8863f	38.7420f	38.7422f	cgstot	13.7051f	13.7050f
cbtot	87.9824f	44.1928f	44.1928f	42.6385f	42.6385f	14.7493f	cbtot	14.7493f	14.7422f	14.7422f	87.8622f	42.9369f	42.9371f	cbtot	14.7444f	14.7444f
cgs	37.4821f	18.3605f	18.3605f	16.1138f	16.1138f	6.2288f	cgs	6.2288f	6.0866f	6.0866f	37.6749f	16.5341f	16.5345f	cgs	6.2287f	6.2283f
cgd	3.4883f	1.6215f	1.6215f	1.6222f	1.6222f	534.8457u	cgd	534.8457u	527.6920u	527.6920u	3.9239f	1.6216f	1.6217f	cgd	534.7049u	534.6504u

FF: All transistors are in saturation.

subckt	0:m1	0:m2	0:m3	0:m4	0:m5	0:m6	subckt	0:m7	0:m8	0:m9	0:mopb	0:mop1	0:mop2	subckt	0:mop3	0:mop4
element	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	element	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	0:n 18.1	element	0:n 18.1	0:n 18.1
region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	region	Saturation	Saturation
id	-1.8610u	-917.5766u	-917.5766u	-930.4951u	-930.4951u	930.4965u	id	930.4965u	917.5766u	917.5766u	-1.8480u	-923.0469u	-924.0129u	id	923.9484u	924.0143u
lbs	2.638e-22	1.440e-22	1.440e-22	97.5510u	97.5510u	-3.310e-22	lbs	-3.310e-22	-3.273e-22	-3.273e-22	2.620e-22	73.0177u	73.0177u	lbs	-3.295e-22	-3.296e-22
lbd	176.6912u	283.9308u	283.9308u	417.2131u	417.2131u	-113.0062u	lbd	-113.0062u	-212.9695u	-212.9694u	132.1874u	415.8992u	415.7493u	lbd	-113.9918u	-114.1942u
vgs	-600.0000u	-600.0000u	-600.0000u	-600.7926u	-600.7926u	482.1970u	vgs	482.1970u	477.5573u	477.5573u	-600.0000u	-668.5558u	-668.5616u	vgs	481.7221u	481.7221u
vds	-309.2074u	-900.0057u	-900.0058u	-1.0132	-1.0132	477.5573u	vds	477.5573u	899.9943u	899.9942u	-231.4442u	-1.0868	-1.0864	vds	481.7221u	482.1970u
vbs	0	0	0	309.2074u	309.2074u	0	vbs	0	0	0	231.4442u	231.4442u	0	vbs	0	0
vth	-516.8058u	-519.8340u	-519.8340u	-607.6159u	-607.6159u	411.3252u	vth	411.3252u	408.9751u	408.9751u	-516.8058u	-586.4683u	-586.4683u	vth	411.3020u	411.2904u
vdسات	-108.5583u	-108.1802u	-108.1802u	-113.6215u	-113.6215u	94.8166u	vdسات	94.8166u	93.4848u	93.4848u	-108.5581u	-112.0589u	-112.0627u	vdسات	94.5528u	94.5544u
vod	-83.1942u	-80.9600u	-80.9600u	-83.1767u	-83.1767u	70.8718u	vod	70.8718u	68.5822u	68.5822u	-83.1942u	-82.0955u	-82.1012u	vod	70.4281u	70.4227u
beta	374.0022u	183.8773u	183.8773u	172.7108u	172.7108u	236.2273u	beta	236.2273u	236.1722u	236.1722u	374.0022u	175.3462u	175.3459u	beta	236.2236u	236.2236u
gm eff	557.0847u	557.0847u	557.0847u	554.9911u	554.9911u	507.4466u	gm eff	507.4466u	507.4466u	507.4466u	557.0847u	555.4899u	555.4899u	gm eff	507.4466u	507.4466u
gm	27.2107u	13.4973u	13.4973u	13.5372u	13.5372u	15.8470u	gm	15.8470u	14.9391u	14.9391u	26.9637u	13.5043u	13.5049u	gm	14.9728u	14.9737u
gds	129.0664u	27.2501u	27.2501u	25.4338u	25.4338u	139.8550u	gds	139.8550u	130.8501u	130.8501u	230.0078u	24.6791u	24.6852u	gds	138.9000u	138.8857u
gmb	8.4659u	4.1962u	4.1962u	3.7099u	3.7099u	3.2099u	gmb	3.2099u	3.1623u	3.1623u	8.3894u	3.8084u	3.8086u	gmb	3.1942u	3.1944u
cdtot	11.4228f	5.0136f	5.0136f	4.7199f	4.7199f	2.1540f	cdtot	2.1540f	1.9840f	1.9840f	12.0541f	4.7217f	4.7220f	cdtot	2.1517f	2.1515f
cgstot	75.3562f	37.2892f	37.2892f	37.1507f	37.1507f	13.8397f	cgstot	13.8397f	13.7742f	13.7742f	75.5839f	37.1443f	37.1446f	cgstot	13.8287f	13.8287f
cbtot	86.4467f	43.0541f	43.0541f	41.8278f	41.8278f	15.2161f	cbtot	15.2161f	15.1295f	15.1295f	86.3389f	42.0401f	42.0406f	cbtot	15.2014f	15.2015f
cgs	42.0815f	20.0276f	20.0276f	18.3530f	18.3530f	7.2835f	cgs	7.2835f	7.1224f	7.1224f	42.9688f	18.8189f	18.8192f	cgs	7.2016f	7.2013f
cgd	65.2882f	32.1936f	32.1936f	32.5974f	32.5974f	12.0265f	cgs	12.0265f	11.9283f	11.9283f	65.4213f	32.4644f	32.4648f	cgs	12.0126f	12.0126f
cgd	2.9481f	1.4178f	1.4178f	1.4173f	1.4173f	453.1779u	cgd	453.1779u	450.2457u	450.2457u	3.1107f	1.4178f	1.4178f	cgd	453.1116u	453.1084u

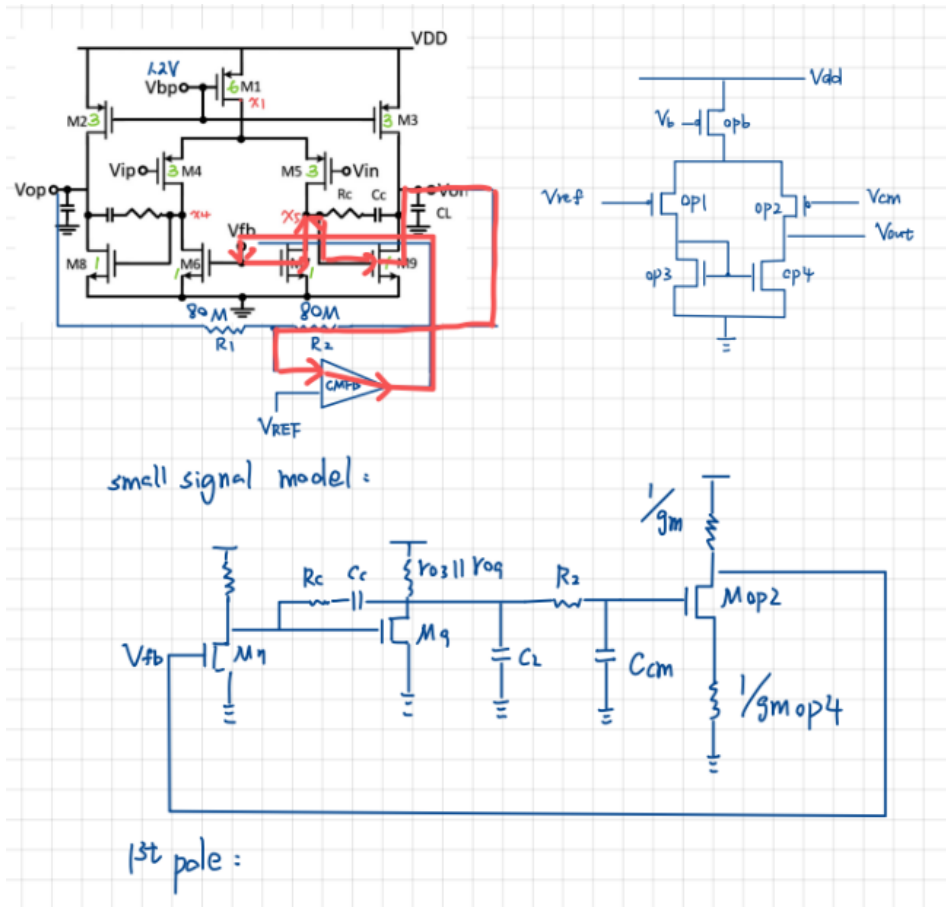
SS: All transistors are in saturation.

phase_margin	gain_db	gbw	temper
alter#			
80.2785	75.3294	1.446e+07	27.0000
phase_margin	gain_db	gbw	temper
alter#			
60.2839	74.3817	2.673e+07	27.0000
phase_margin	gain_db	gbw	temper
alter#			
104.3118	76.9882	5.333e+06	27.0000

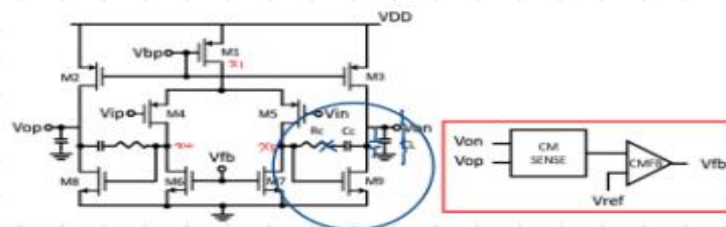
Meet spec. in TT FF and SS

- From fig. 1, we can observe a common-mode feedback loop in this circuit. Please analyze the loop by hand, the content must include the breakdown of the entire loop gain and also the distribution of poles.

Breakdown the loop:



Gain:



gain :

first stage: $gain = g_{m4,5} (R_{o6,7} \parallel R_{o4,5})$

second stage: $gain = g_{m8,9} (R_{o2,3} \parallel R_{o8,9} \parallel 80M\Omega)$

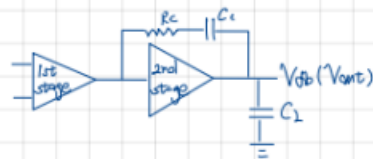
$20.2658\mu \times \left(\frac{1}{44.7158n} \parallel \frac{1}{242.7020n} \right) \cong 70.5089$

$23.9341\mu \times \left(\frac{1}{223.4346n} \parallel \frac{1}{49.7514n} \parallel 80M\Omega \right) \cong 82.5$

$\therefore \text{total gain} = 5816.984 \text{ V/V} \cong 75.293 \text{ dB}$

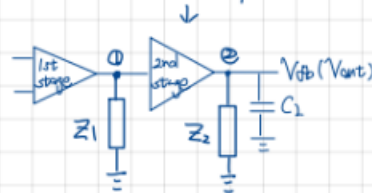
Poles:

pole and zero:



$$\begin{cases} Z_1 = Z_c \times \left(\frac{1}{1 - A_{V2}} \right) = -\frac{1}{A_{V2}} \left(R_C + \frac{1}{sC_c} \right) \\ Z_2 = Z_c \times \left(\frac{1}{1 - \frac{1}{A_{V2}}} \right) \approx R_C + \frac{1}{sC_c} \end{cases}$$

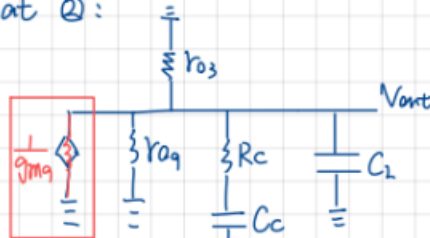
look R_C and C_c as an impedance $Z_c = R_C + \frac{1}{sC_c}$
then do the Miller compensation



at ①:

$$\begin{aligned} \omega_{p1} &= \frac{1}{R_{out, stage1} \cdot C_{out, stage1}} \approx \frac{1}{\left((r_{o1} \parallel r_{o2}) + \frac{R_C}{A_{V2}} \right) \cdot (-A_{V2} \cdot C_c)} \\ &\approx 69.626 \text{ rad/s} \approx 11.087 \text{ Hz} \rightarrow 1^{st} \text{ pole} \end{aligned}$$

at ②:



input output together

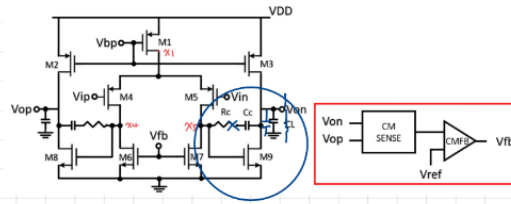
for C_L :

$$\begin{aligned} \omega_p &= \frac{1}{(r_{o1} \parallel r_{o2} \parallel \frac{1}{g_{m2}}) C_L} \approx 24.2 \text{ M rad/s} \\ &= 3.833 \text{ MHz} \rightarrow 2^{nd} \text{ pole} \end{aligned}$$

for C_c :

$$\begin{aligned} \omega_z &= \frac{1}{\left(\frac{1}{g_{m2}} - R_C \right) C_c} = -96.053 \text{ k rad/s} \\ &= -15.287 \text{ kHz} \end{aligned}$$

- Compare the SPICE simulation result with the hand analysis you do in question number 1, and explain what causes the error between the simulation and your calculation (at least include open loop gain, GBW, and Power Consumption).
Open loop gain:



gain:

first stage: $gain = g_{m4,5} (r_{o6,7} \parallel r_{o4,5})$

second stage: $gain = g_{m8,9} (r_{o2,3} \parallel r_{o8,9} \parallel 80M\Omega)$

$$20.2658 \mu \times \left(\frac{1}{44.7198 n} \parallel \frac{1}{242.7020 n} \right) \cong 70.5089$$

$$23.9341 \mu \times \left(\frac{1}{223.4346 n} \parallel \frac{1}{49.7514 n} \parallel 80M\Omega \right) \cong 82.5$$

$$\therefore \text{total gain} = 5816.984 (V/V) \cong 75.293 dB$$

$$\text{error} = \frac{5816.984 - 5865.9}{5816.984} \cong -0.84\%$$

output R:

$$\left(\frac{1}{223.4367 n} \parallel \frac{1}{49.7514 n} \parallel 80M\Omega \right) \times 2 \cong 6893.92 k\Omega$$

$$\text{error} = \frac{6893.92 - 6952.2}{6893.92} \cong -0.845\%$$

Error discussion: CM sense resistance is not large enough, so in stage2, the resistance will affect output resistance which make some error.

Power consumption:

Power :

$$V_{dd} \times i_{\text{total to } V_{dd}}$$

$$= V_{dd} \times (I_{dM1} + I_{dM2} + I_{dM3} + I_{dOpb})$$

$$= 1.8 \times (3.1824 \mu + 1.6139 \mu + 1.6139 \mu + 3.1558 \mu)$$

$$= 17.2188 \mu W$$

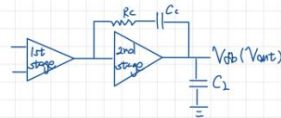
$$\text{error} = \frac{17.2189 - 17.2188}{17.2189} \cong 5.8 \times 10^{-4} \%$$

Error discussion: simulation result round to the fourth decimal place, so it will have a little difference with my calculations.

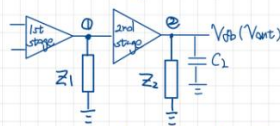
GBW:

1. Find pole and zero.

pole and zero:



look R_c and C_c as an impedance $Z_c = R_c + \frac{1}{sC_c}$
then do the Miller compensation



$$\begin{cases} Z_1 = Z_c \times \left(\frac{1}{1-A_{V2}} \right) = -\frac{1}{A_{V2}} \left(R_c + \frac{1}{sC_c} \right) \\ Z_2 = Z_c \times \left(\frac{1}{1-A_{V2}} \right) \approx R_c + \frac{1}{sC_c} \end{cases}$$

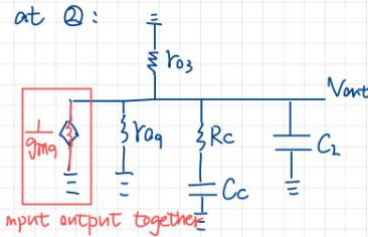
3418742
3030.70

at ①:

$$W_{p1} = \frac{1}{R_{out, stage1} \cdot C_{int, stage1}} \approx \frac{1}{\left((r_{o1} || r_{o2}) + \frac{-R_c}{A_{V2}} \right) \cdot (-A_{V2} \cdot C_c)}$$

$$\approx 69.626 \text{ rad/s} \approx 11.087 \text{ Hz} \rightarrow 1^{st} \text{ pole}$$

$$\text{error} = \frac{11.087 - 10.7268}{11.087} = 3.249\%$$



for C_L :

$$W_p = \frac{1}{(r_{o3} || r_{o9} || \frac{1}{g_{m9}}) C_L} \approx 24.2 \text{ M rad/s}$$

$$= 3.853 \text{ MHz} \rightarrow 2^{nd} \text{ pole}$$

$$\therefore \text{error} = \frac{3.853 - 3.9881}{3.853} \approx -3.5\%$$

for C_c :

$$W_z = \frac{1}{\left(\frac{1}{g_{m9}} - R_c \right) C_c} = -96.053 \text{ k rad/s}$$

$$= -15.287 \text{ kHz}$$

$$\therefore \text{error} = \frac{15.2873 - 15.2874}{15.2874} = 1.242 \times 10^{-2} \%$$

***** pole/zero analysis

input = 0:vdif

output = v(vop,von)

poles (rad/sec)

real	imag
-67.3987	0.
-25.0581x	0.
-199.360x	0.

poles (hertz)

real	imag
-10.7268	0.
-3.98813x	0.
-31.7292x	0.

zeros (rad/sec)

real	imag
-96.0537k	0.
13.2705g	0.
36.0740g	0.

zeros (hertz)

real	imag
-15.2874k	0.
2.11207g	0.
5.74136g	0.

Pole and zero in simulation

Error discussion: I think it is because we neglect parasitic capacitance.

2. Use bode plot to estimate unit gain bandwidth.

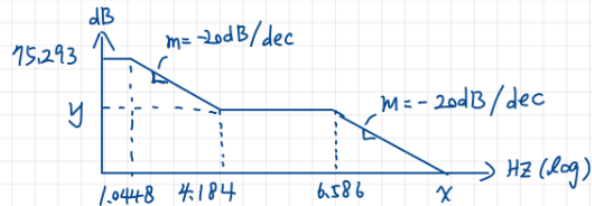
∴ by hand cal. =

$$g_{pm} = 74.2035 \text{ dB}$$

$$pole1 = 11.087 \text{ Hz} \xrightarrow{\log} 1.0448$$

$$pole2 = 3.853 \text{ MHz} \xrightarrow{\log} 6.586$$

$$zero1 = 15.287 \text{ kHz} \xrightarrow{\log} 4.184$$



$$\frac{75.293 - y}{4.184 - 1.0448} = 20 \rightarrow y = 12.589$$

$$\frac{12.589 - 0}{x - 6.586} = 20 \rightarrow x \approx 7.21$$

$$\therefore UGB = 10^{7.2052} \approx 16.04 \text{ MHz}$$

$$\rightarrow \text{error} = \frac{16.04 - 14.46}{16.04} \approx 9.85\%$$

Error discussion: first, we neglect parasitic capacitance. Second, bode plot is just an estimation, if two pole or zero are too close, there will be some error.

4. Run the ac simulation to make sure your common-mode feedback loop is stable. Please note that the content must include the graph of gain and phase margin. Hints are provided in Fig. 4.

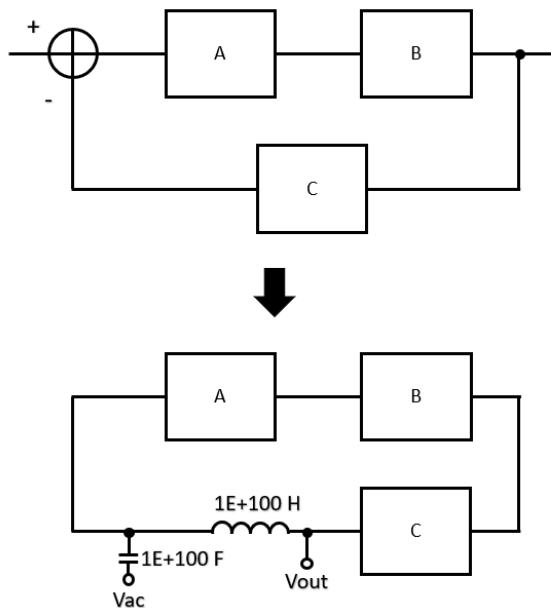
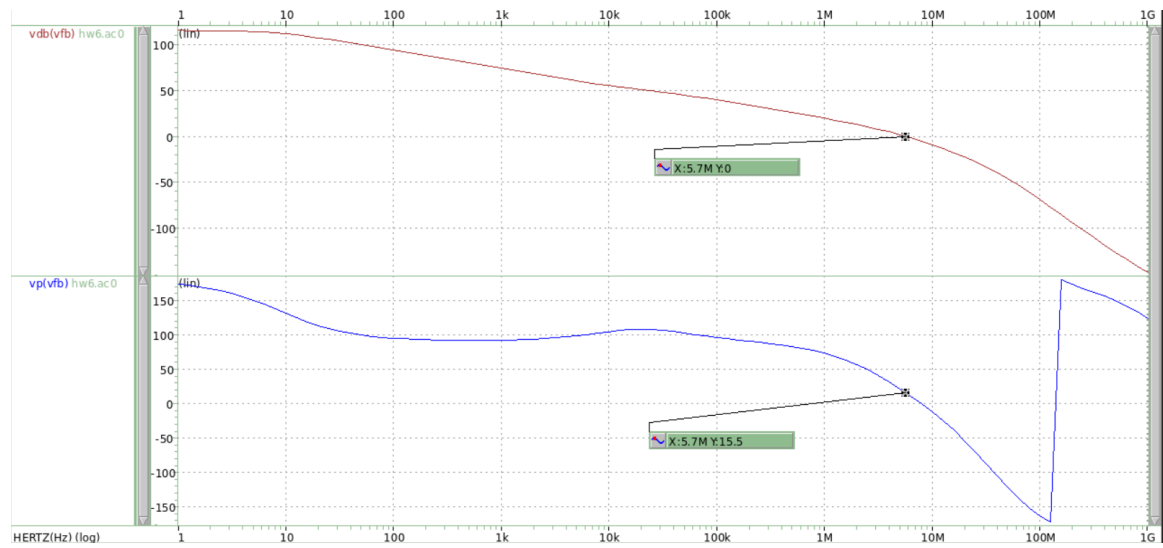


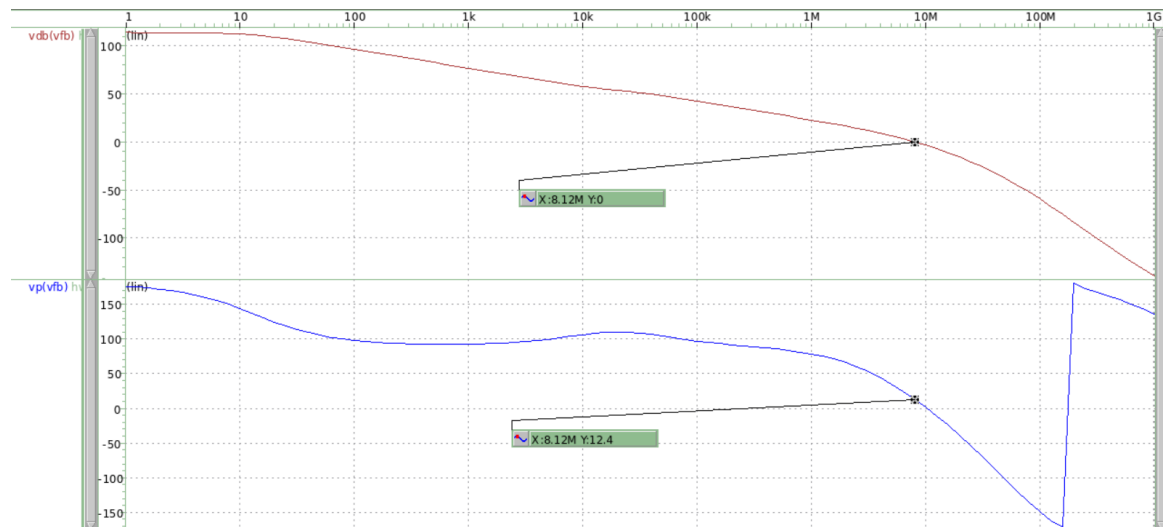
Fig. 4. Frequency Analysis of a Feedback Loop

TT:



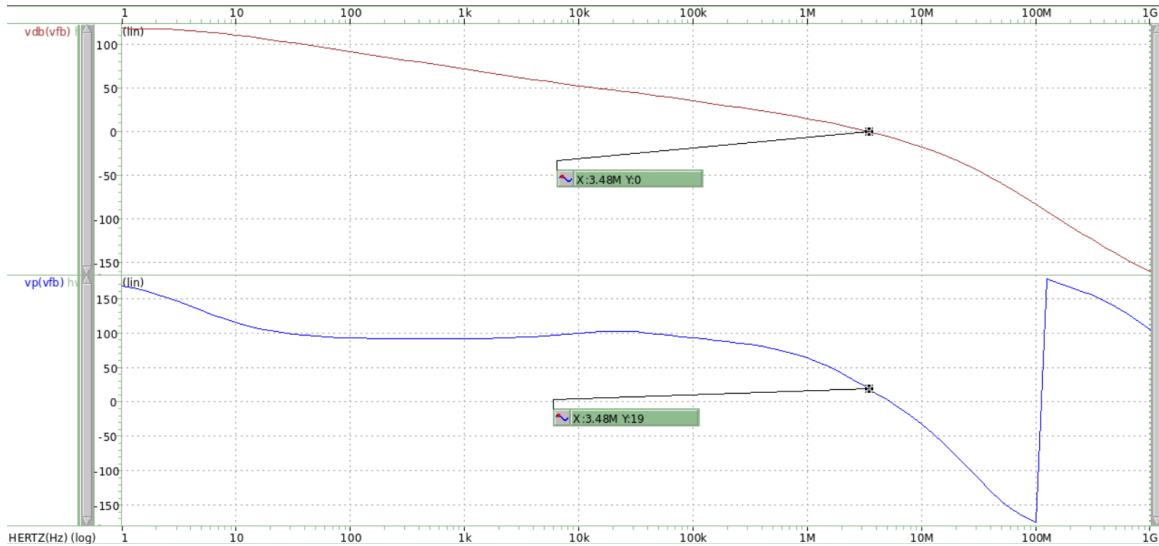
x-axis: frequency in log(Hz) – y-axis: gain in dB(red line) and phase in degree(blue line)

FF:



x-axis: frequency in log(Hz) – y-axis: gain in dB(red line) and phase in degree(blue line)

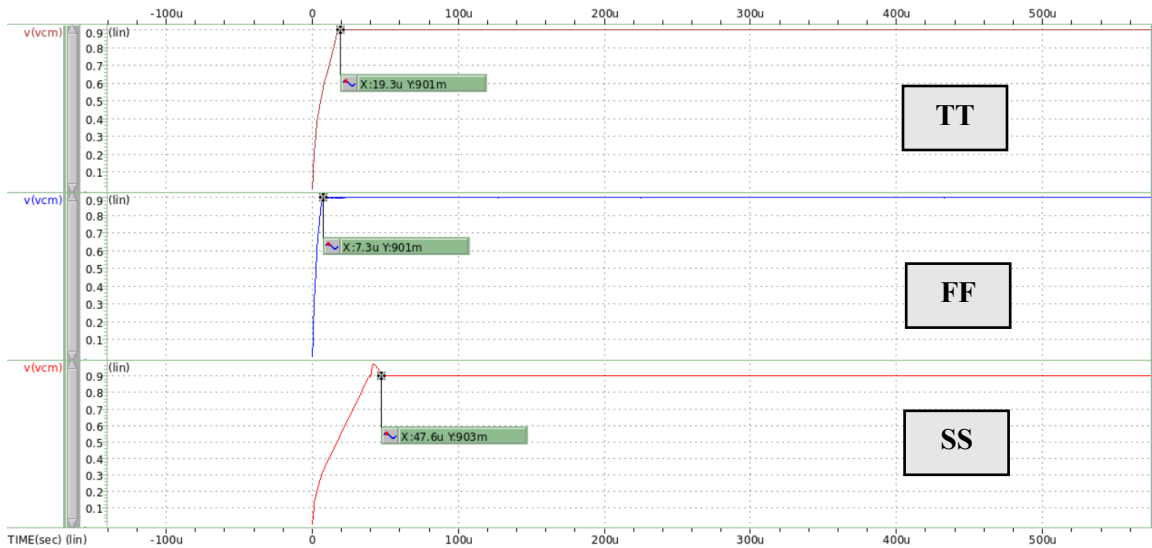
SS:



x-axis: frequency in log(Hz) – y-axis: gain in dB(red line) and phase in degree(blue line)

From the above 3 figures, we can see that under the 3 different corners, before gain reaches 0dB, the phase of Vfb is always positive, which make that the design remains negative feedback and provide stability in the output node.

- Run the transient simulation. Insert an input signal with an amplitude of 0.1mVpp and set the initial value of both output nodes to 0V. Observe whether, after a period of time, the output common mode stabilizes back to $0.9V \pm 20mV$.



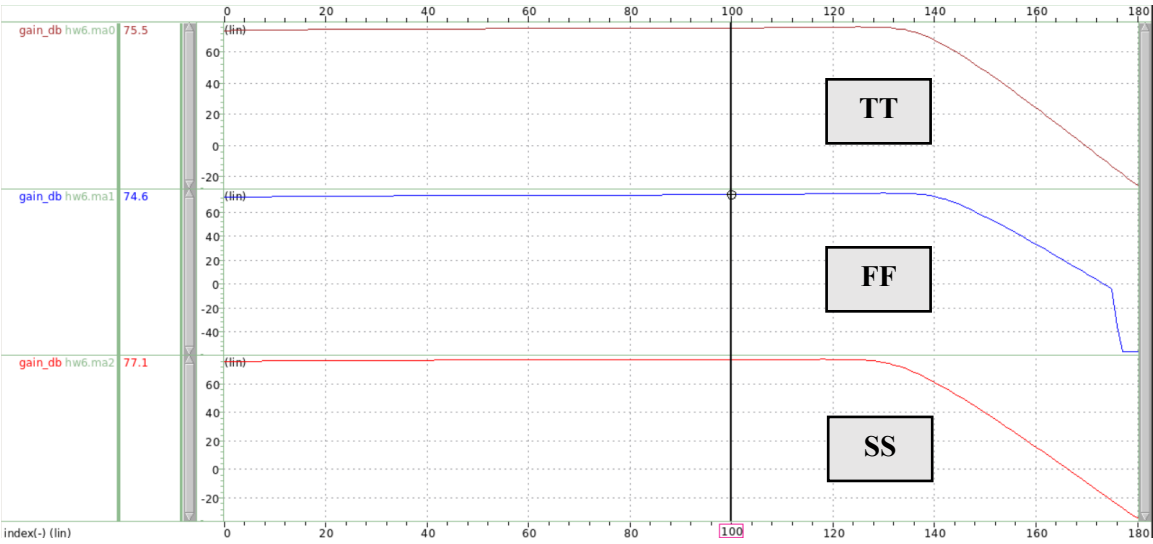
x-axis: time(second) – y-axis: common mode voltage(V)

By measuring the voltage output common mode at time when vcm is stable in each corner, we can see that the voltage matches the requirement of $0.9 \pm 20mV$. and FF corner become stable fastest and SS corner become stable slower.

- Sweep input common-mode voltage to make sure your input CM range meets the spec.

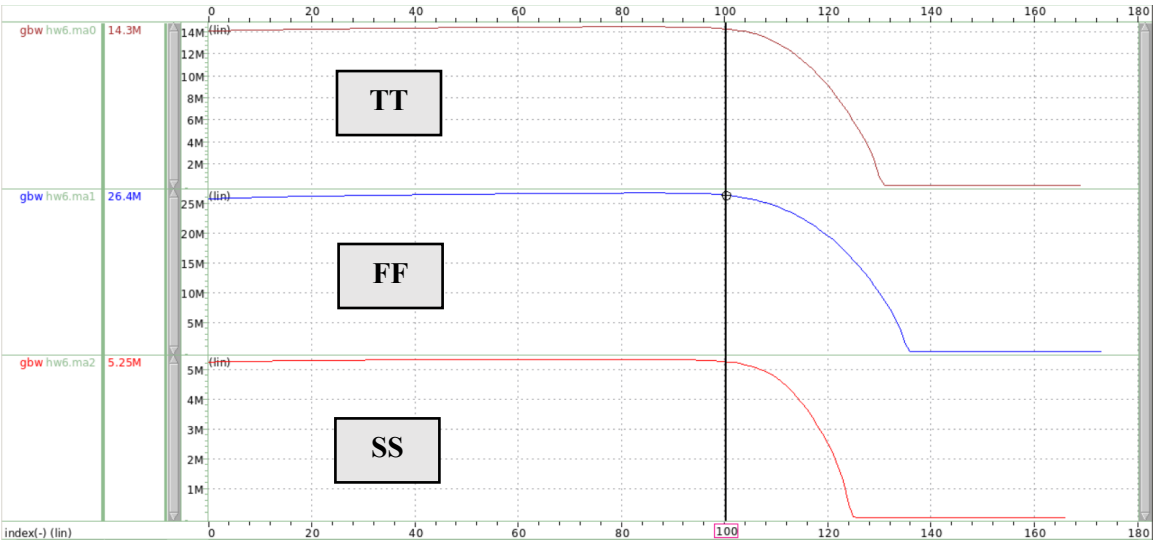
Check when $v_{incm}=0V$, $v_{incm}=0.5V$ and $v_{incm}=1V$ all transistors are in saturation

Gain:



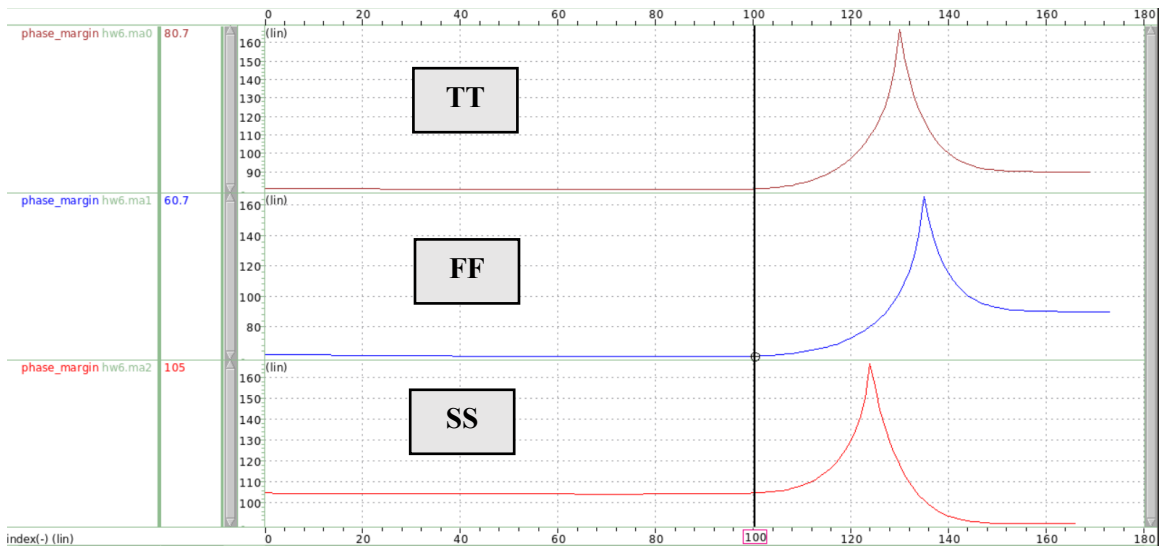
x-axis: input common mode(V) – y-axis: gain in dB

UGB:



x-axis: input common mode (V) – y-axis: gain bandwidth (MHz)

phase margin:



x-axis: input common mode (V) – y-axis: phase margin in degree

saturation of all transistors when input common mode is 0V:

TT

subckt	element	0:m1	0:m2	0:m3	0:m4	0:m5	0:m6	subckt	element	0:m7	0:m8	0:m9	0:mopb	0:mop1	0:mop2	subckt	element	0:mop3	0:mop4
model	0:p.18.1	0:p.18.1	0:p.18.1	0:p.18.1	0:p.18.1	0:p.18.1	0:n.18.1	model	0:n.18.1	0:n.18.1	0:n.18.1	0:p.18.1	0:p.18.1	0:p.18.1	0:p.18.1	model	0:n.18.1	0:n.18.1	
region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	region	Saturation	Saturation	
id	-3.2705u	-1.6139u	-1.6139u	-1.6352u	-1.6352u	-1.6352u	1.6352u	id	1.6352u	1.6139u	1.6139u	-3.1558u	-1.5776u	-1.5782u	1.5782u	id	1.5776u	1.5782u	
lbs	4.635e-22	2.531e-22	2.531e-22	301.5763a	301.5763a	-5.707e-22	-5.707e-22	lbs	-5.707e-22	-5.721e-22	-5.721e-22	4.473e-22	74.2346a	74.2346a	-5.592e-22	lbs	-5.592e-22	-5.594e-22	
lbd	545.0192a	205.0445a	205.0445a	424.2735a	424.2735a	-109.8366a	-109.8366a	lbd	-109.8366a	-214.7280a	-214.7280a	134.1588a	422.4170a	422.4170a	-110.4819a	lbd	-110.4819a	-111.6072a	
vgs	-600.0000m	-600.0000m	-600.0000m	-847.7677m	-847.7677m	465.5046m	465.5046m	vgs	465.5046m	460.3470m	460.3470m	-600.0000m	-605.6034m	-605.6378m	463.0517m	vgs	463.0517m	463.0517m	
vds	-952.2323m	-900.0344m	-900.0344m	-387.4207m	-387.4207m	460.3470m	460.3470m	vds	460.3470m	899.9656m	899.9656m	-234.3966m	-1.1026	-1.1001	463.0517m	vds	463.0517m	463.5046m	
vbs	0.	0.	0.	0.	0.	0.	0.	vbs	0.	0.	0.	234.3966m	234.3966m	234.3966m	0.	vbs	0.	0.	
vth	-488.0099m	-488.6972m	-488.6972m	-726.4924m	-726.4924m	375.2334m	375.2334m	vth	375.2334m	372.5648m	372.5648m	-488.0099m	-555.2374m	-555.2374m	375.2170m	vth	375.2170m	375.2021m	
vdSAT	-128.6143m	-129.2682m	-129.2682m	-147.0177m	-147.0177m	108.4950m	108.4950m	vdSAT	108.4950m	106.9272m	106.9272m	-128.6111m	-132.2641m	-132.2885m	106.9597m	vdSAT	106.9597m	106.9691m	
vod	-111.9901m	-111.3028m	-111.3028m	-121.2742m	-121.2742m	90.2712m	90.2712m	vod	90.2712m	87.7822m	87.7822m	-111.9902m	-110.3661m	-110.4005m	87.8347m	vod	87.8347m	87.8496m	
beta	424.7049u	209.6690u	209.6690u	175.9542u	175.9542u	301.0861u	301.0861u	beta	301.0861u	301.8915u	301.8915u	424.7954u	199.9314u	199.9297u	301.9573u	beta	301.9573u	301.9571u	
gam_eff	557.0847m	557.0847m	557.0847m	551.3608m	551.3608m	507.4460m	507.4460m	gam_eff	507.4460m	507.4460m	507.4460m	555.4707m	555.4707m	555.4707m	507.4460m	gam_eff	507.4460m	507.4460m	
gm	41.8856m	20.6650m	20.6650m	19.9668u	19.9668u	24.0596u	24.0596u	gm	24.0596u	23.9342u	23.9342u	40.2421u	20.2267u	20.2311u	23.4024u	gm	23.4024u	23.4990u	
gds	98.3664m	49.7506m	49.7506m	90.3835m	90.3835m	247.7770m	247.7770m	gds	247.7770m	225.4351m	225.4351m	491.2208m	43.0772m	43.1383m	240.7921m	gds	240.7921m	240.5657m	
gmb	12.7625u	6.2893u	6.2893u	4.4595u	4.4595u	4.8965u	4.8965u	gmb	4.8965u	4.8293u	4.8293u	12.2579u	5.5815u	5.5827u	4.7843u	gmb	4.7843u	4.7854u	
cdtot	9.2900f	4.7511f	4.7511f	4.5006f	4.5006f	2.0684f	2.0684f	cdtot	2.0684f	1.9014f	1.9014f	11.6709f	4.4768f	4.4762f	2.0666f	cdtot	2.0666f	2.0653f	
cbtot	74.3806f	37.1086f	37.1086f	36.7408f	36.7408f	13.0122f	13.0122f	cbtot	13.0122f	12.9716f	12.9716f	74.9399f	36.8522f	36.8531f	12.0832f	cbtot	12.0832f	12.0832f	
csTot	85.2907f	42.6675f	42.6675f	39.6707f	39.6707f	14.2375f	14.2375f	csTot	14.2375f	14.1886f	14.1886f	85.0338f	41.4704f	41.4717f	14.1990f	csTot	14.1990f	14.1992f	
cbtot	37.9720f	19.1978f	19.1978f	14.4328f	14.4328f	6.5209f	6.5209f	cbtot	6.5209f	6.3666f	6.3666f	39.5071f	17.3110f	17.3123f	6.5207f	cbtot	6.5207f	6.5196f	
cgs	65.5080f	32.5313f	32.5313f	33.1536f	33.1536f	11.3922f	11.3922f	cgs	11.3922f	11.3264f	11.3264f	65.6641f	32.5947f	32.5958f	11.3557f	cgs	11.3557f	11.3557f	
cgd	3.6176f	1.5092f	1.5092f	1.5559f	1.5559f	495.1746a	495.1746a	cgd	495.1746a	490.7830a	490.7830a	3.4156f	1.5080f	1.5080f	495.0778a	cgd	495.0778a	494.9568a	

FF

subckt	element	0:m1	0:m2	0:m3	0:m4	0:m5	0:m6	subckt	element	0:m7	0:m8	0:m9	0:mopb	0:mop1	0:mop2	subckt	element	0:mop3	0:mop4
model	0:p.18.1	0:p.18.1	0:p.18.1	0:p.18.1	0:p.18.1	0:p.18.1	0:n.18.1	model	0:n.18.1	0:n.18.1	0:n.18.1	0:p.18.1	0:p.18.1	0:p.18.1	0:p.18.1	model	0:n.18.1	0:n.18.1	
region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	region	Saturation	Saturation	
	-5.4354u	-2.7165u	-2.7165u	-2.7177u	-2.7177u	2.7177u	2.7177u	id	2.7177u	2.7165u	2.7165u	-5.2285u	-2.6137u	-2.6148u	id	2.6137u	2.6148u		
lbs	7.702e-22	4.250e-22	4.250e-22	304.3371a	304.3371a	-9.571e-22	-9.571e-22	lbs	-9.571e-22	-9.567e-22	-9.567e-22	7.409e-22	75.3944a	75.3944a	-9.204e-22	lbs	-9.204e-22	-9.208e-22	
lbd	549.3018a	205.0700a	205.0699a	426.6417a	426.6417a	-109.9616a	-109.9616a	lbd	-109.9616a	-216.6669a	-216.6669a	136.0791a	426.1924a	426.2104a	-110.3022a	lbd	-110.3022a	-111.0405a	
vgs	-600.0000m	-600.0000m	-600.0000m	-841.8134m	-841.8134m	461.2226m	461.2226m	vgs	461.2226m	456.7414m	456.7414m	-600.0000m	-662.6264m	-662.6730m	458.1560m	vgs	458.1560m	458.1560m	
vds	-950.1866m	-900.0460m	-900.0460m	-385.0720m	-385.0720m	456.7414m	456.7414m	vds	456.7414m	899.9534m	899.9534m	-237.3736m	-1.1845	-1.1014	458.1560m	vds	458.1560m	461.2226m	
vbs	0.	0.	0.	0.	0.	0.	0.	vbs	0.	0.	0.	237.3736m	237.3736m	237.3736m	0.	vbs	0.	0.	
vth	-452.5666m	-452.3564m	-452.3564m	-682.8906m	-682.8906m	341.0670m	341.0670m	vth	341.0670m	338.3570m	338.3570m	-452.5666m	-517.2079m	-517.2079m	341.0521m	vth	341.0521m	341.0334m	
vdSAT	-155.1740m	-156.5774m	-156.5774m	-177.4640m	-177.4640m	120.8751m	120.8751m	vdSAT	120.8751m	127.6722m	127.6722m	-155.1710m	-159.0606m	-159.0961m	120.8075m	vdSAT	120.8075m	120.8262m	
vod	-147.4334m	-147.6436m	-147.6436m	-158.9228m	-158.9228m	120.1619m	120.1619m	vod	120.1619m	118.3836m	118.3836m	-147.4334m	-145.3385m	-145.3852m	117.1040m	vod	117.1040m	117.1277m	
beta	456.8393u	226.1769u	226.1769u	189.5170u	189.5170u	331.8815u	331.8815u	beta	331.8815u	331.7714u	331.7714u	456.8398u	215.6341u	215.6341u	331.8342u	beta	331.8342u	331.8340u	
gam_eff	557.0846m	557.0846m	557.0846m	551.3304m	551.3304m	507.4460m	507.4460m	gam_eff	507.4460m	507.4460m	507.4460m	557.0846m	555.4513m	555.4513m	507.4460m	gam_eff	507.4460m	507.4460m	
gm	50.9620m	29.3082u	29.3082u	27.6004u	27.6004u	34.5070u	34.5070u	gm	34.5070u	34.6570u	34.6570u	50.2002u	20.4425u	20.4487u	33.6930u	gm	33.6930u	33.7030u	
gds	158.0994m	81.0184m	81.0184m	171.3437m	171.3437m	375.3257m	375.3257m	gds	375.3257m	333.8875m	333.8875m	1.1092u	68.6920m	68.8280m	304.1120m	gds	304.1120m	303.4426m	
gmb	17.4470m	8.6828u	8.6828u	6.0343u	6.0343u	6.7445u	6.7445u	gmb	6.7445u	6.7110u	6.7110u	16.6275u	7.6193u	7.6211u	6.5914u	gmb	6.5914u	6.5930u	
cdtot	8.8221f	4.5194f	4.5194f	4.4501f	4.4501f	1.9739f	1.9739f	cdtot	1.9739f	1.8137f	1.8137f	11.7121f	4.2706f	4.2721f	1.9724f	cdtot	1.9724f	1.9708f	
cbtot	70.0770f	39.0444f	39.0444f	38.4085f	38.4085f	13.7104f	13.7104f	cbtot	13.7104f	13.6961f	13.6961f	70.8062f	38.7419f	38.7424f	13.7051f	cbtot	13.7051f	13.7048f	
csTot	88.1423f	44.1928f	44.1928f	40.8753f	40.8753f	14.7618f	14.7618f	csTot	14.7618f	14.7422f	14.7422f	87.8622f	42.9367f	42.9373f	14.7443f	csTot	14.7443f	14.7445f	
cbtot	36.2608f	18.3605f	18.3605f	13.7364f	13.7364f	6.2276f	6.2276f	cbtot	6.2276f	6.0866f	6.0866f	37.6749f	16.5340f	16.5354f	6.2287f	cbtot	6.2287f	6.2275f	
cgs	69.2125f	34.5474f	34.5474f	34.8173f	34.8173f	12.1003f	12.1003f	cgs	12.1003f	12.0589f	12.0589f	69.5580f	34.5338f	34.5344f	12.0827f	cgs	12.0827f	12.0824f	
cgd	3.2397f	1.6235f	1.6235f	1.7042f	1.7042f	535.0119a	535.0119a	cgd	535.0119a	527.6921a	527.6921a	3.9238f	1.6216f	1.6217f	534.7048a	cgd	534.7048a	534.5367a	

SS

subckt	element	0:m1	0:m2	0:m3	0:m4	0:m5	0:m6
model	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1
region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation
id	-1.9806u	-917.5771n	-917.5771n	-954.3222n	-954.3222n	954.3222n	954.3222n
lbs	2.706e-22	1.440e-22	1.440e-22	298.8210a	298.8210a	-3.404e-22	
lbd	546.9718a	283.9459a	283.9459a	417.2130a	417.2130a	-113.0603a	
vgs	-600.0000u	-600.0000u	-600.0000u	-652.8262u	-652.8262u	481.7665u	
vds	-947.1738u	-900.0240u	-900.0240u	-375.2687u	-375.2687u	477.5575u	
vbs	0.	0.	0.	947.1738u	947.1738u	0.	
vth	-516.8058u	-519.0340u	-519.0340u	-761.6547u	-761.6547u	411.3252u	
vsdat	-180.5560u	-180.1892u	-180.1892u	-124.0187u	-124.0187u	95.7365u	
vod	-83.1942u	-80.9660u	-80.9660u	-91.1715u	-91.1715u	72.4413u	
beta	374.8019u	183.8773u	183.8773u	154.4515u	154.4515u	236.2389u	
gm eff	557.0847u	557.0847u	557.0847u	551.3866u	551.3866u	507.4460u	
gm	27.9695u	13.4973u	13.4973u	13.4185u	13.4185u	15.3169u	
gds	59.6787u	27.2558u	27.2558u	47.9695u	47.9695u	142.0497u	
gmb	8.6861u	4.1962u	4.1962u	3.0619u	3.0619u	3.2659u	
cdtot	9.8193f	5.0136f	5.0136f	4.7987f	4.7987f	2.1542f	
cgto1	75.1469f	37.2892f	37.2892f	37.3089f	37.3089f	13.8759f	
cgto2	86.5044f	43.0544f	43.0544f	40.6094f	40.6094f	15.2653f	
cbtot	41.2912f	20.8276f	20.8276f	15.7215f	15.7215f	7.2832f	
cgs	65.1226f	32.1936f	32.1936f	33.4699f	33.4699f	12.0717f	
cgd	2.8418f	1.4178f	1.4178f	1.4531f	1.4531f	453.0729u	

subckt	element	0:m7	0:m8	0:m9	0:m0pb	0:m0p1	0:m0p2
model	0:n:18.1	0:n:18.1	0:n:18.1	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1
region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation
id	954.3229u	917.5771n	917.5771n	-1.8480u	-923.8382n	-924.1231n	
lbs	-3.404e-22	-3.273e-22	-3.273e-22	2.620e-22	73.0197a	73.0197a	
lbd	-113.0603a	-212.9649a	-212.9649a	132.1918a	415.9814a	415.2542a	
vgs	483.7665u	477.5575u	477.5575u	600.0000u	-660.5495u	-660.5714u	
vds	477.5575u	899.9751u	899.9752u	-231.4509u	-1.0868u	-1.0848u	
vbs	0.	0.	0.	0.	231.4509u	231.4509u	
vth	411.3252u	408.9752u	408.9752u	-516.8058u	-586.4621u	-586.4621u	
vsdat	95.7365u	93.4848u	93.4848u	-180.5581u	-112.0538u	-112.0780u	
vod	72.4413u	68.5823u	68.5823u	-83.1942u	-82.8079u	-82.1123u	
beta	236.2389u	236.1722u	236.1722u	374.8022u	175.3463u	175.3453u	
gm eff	507.4460u	507.4460u	507.4460u	557.0847u	555.4899u	555.4899u	
gm	15.3169u	14.9391u	14.9391u	26.9637u	13.5832u	13.5899u	
gds	142.0497u	130.9503u	130.9503u	230.0714u	24.6765u	24.7029u	
gmb	3.2659u	3.1623u	3.1623u	8.3894u	3.8088u	3.8089u	
cdtot	2.1542f	1.9840f	1.9840f	12.0540f	4.7217f	4.7229f	
cgto1	13.8759f	13.7742f	13.7742f	75.5839f	37.1438f	37.1453f	
cgto2	15.2653f	15.1295f	15.1295f	86.3390f	42.0394f	42.0415f	
cbtot	7.2832f	7.1224f	7.1224f	42.9679f	18.8188f	18.8201f	
cgs	12.0717f	11.9283f	11.9283f	65.4213f	32.4638f	32.4657f	
cgd	453.0729u	450.2457a	450.2457a	3.1107f	1.4178f	1.4178f	

subckt	element	0:m0p3	0:m0p4
model	0:n:18.1	0:n:18.1	0:n:18.1
region	Saturation	Saturation	Saturation
id	923.8396u	924.1245u	
lbs	-3.295e-22	-3.296e-22	
lbd	-113.9901a	-114.4756a	
vgs	481.7140u	481.7140u	
vds	481.7140u	483.7665u	
vbs	0.	0.	
vth	411.3021u	411.2907u	
vsdat	94.5406u	94.5553u	
vod	70.4128u	70.4243u	
beta	236.2235u	236.2234u	
gm eff	507.4460u	507.4460u	
gm	14.9716u	14.9751u	
gds	138.8877u	138.8268u	
gmb	3.1940u	3.1946u	
cdtot	2.1517f	2.1507f	
cgto1	13.8289f	13.8287f	
cgto2	15.2017f	15.2016f	
cbtot	7.2816f	7.2806f	
cgs	12.0124f	12.0125f	
cgd	453.1123a	453.0641a	

saturation of all transistors when input common mode is 1V:

TT

subckt	element	0:m1	0:m2	0:m3	0:m4	0:m5	0:m6
model	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1
region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation
id	-3.0748u	-1.6139u	-1.6139u	-1.5378u	-1.5378u	1.5378u	
lbs	4.257e-22	2.531e-22	2.531e-22	50.8330u	50.8330u	-5.448e-22	
lbd	90.4208a	285.8258a	285.8258a	424.2738a	424.2738a	-199.8365a	
vgs	-600.0000u	-600.0000u	-600.0000u	-642.0206u	-642.0206u	461.3359u	
vds	-457.0974u	-899.9756u	-899.9756u	-1.1817	-1.1817	460.3463u	
vbs	0.	0.	0.	557.0847u	557.0847u	0.	
vth	-180.5560u	-488.6972u	-488.6972u	-534.3279u	-534.3279u	375.2331u	
vsdat	-121.9107u	-129.2682u	-129.2682u	-129.3241u	-129.3241u	105.0748u	
vod	-111.9902u	-111.3020u	-111.3020u	-107.6927u	-107.6927u	86.1025u	
beta	424.7955u	209.6690u	209.6690u	203.0990u	203.0990u	301.9374u	
gm eff	557.0847u	557.0847u	557.0847u	555.9770u	555.9770u	507.4460u	
gm	38.1668u	20.6658u	20.6658u	19.9603u	19.9603u	23.0848u	
gds	2.3836u	49.7524u	49.7524u	40.9664u	40.9664u	236.3952u	
gmb	11.6537u	6.2893u	6.2893u	5.6724u	5.6724u	4.7848u	
cdtot	14.4014f	4.7514f	4.7514f	4.4747f	4.4747f	2.0877f	
cgto1	75.5781f	37.1886f	37.1886f	36.8465f	36.8465f	12.9615f	
cgto2	84.8113f	42.6675f	42.6675f	41.7011f	41.7011f	14.1695f	
cbtot	39.9320f	19.1978f	19.1978f	17.7717f	17.7717f	6.5225f	
cgs	65.9361f	32.5313f	32.5313f	32.4699f	32.4699f	11.3283f	
cgd	4.4619f	1.5092f	1.5092f	1.5077f	1.5077f	495.1766u	

subckt	element	0:m7	0:m8	0:m9	0:m0pb	0:m0p1	0:m0p2
model	0:n:18.1	0:n:18.1	0:n:18.1	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1
region	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation
id	1.5378u	1.6139u	1.6139u	-3.1558u	-1.5781u	-1.5777u	
lbs	-5.448e-22	-5.721e-22	-5.721e-22	4.478e-22	74.2285u	74.2285u	
lbd	-109.8365a	-214.7421a	-214.7421a	134.1774a	423.4183a	423.9684a	
vgs	461.3359u	460.3463u	460.3463u	-600.0000u	-665.6228u	-665.5984u	
vds	460.3463u	900.0244u	900.0244u	-234.3772u	-1.1026	-1.1043	
vbs	0.	0.	0.	0.	234.3772u	234.3772u	
vth	375.2331u	372.5645u	372.5645u	-488.0090u	-555.2321u	-555.2321u	
vsdat	105.0748u	106.9270u	106.9270u	-128.6111u	-132.2813u	-132.2640u	
vod	86.1025u	87.7818u	87.7818u	-111.9902u	-110.3960u	-110.3663u	
beta	301.9374u	301.8915u	301.8915u	424.7954u	199.9360u	199.9321u	
gm eff	507.4460u	507.4460u	507.4460u	557.0847u	555.4780u	555.4780u	
gm	23.0848u	23.9341u	23.9341u	40.2419u	20.2387u	20.2276u	
gds	236.3952u	225.4340u	225.4340u	491.3445u	43.0893u	43.0462u	
gmb	4.7848u	4.8293u	4.8293u	12.2578u	5.5827u	5.5818u	
cdtot	2.0877f	1.9014f	1.9014f	11.6713f	4.4769f	4.4759f	
cgto1	12.9615f	12.9710f	12.9710f	74.9340f	36.8528f	36.8522f	
cgto2	14.1695f	14.1886f	14.1886f	85.8337f	41.4714f	41.4705f	
cbtot	6.5225f	6.3666f	6.3666f	39.5072f	17.3111f	17.3102f	
cgs	11.3283f	11.3264f	11.3264f	65.6642f	32.5955f	32.5946f	
cgd	495.1766u	490.7837a	490.7837a	3.4158f	1.5080f	1.5080f	

subckt	element	0:m0p3	0:m0p4
model	0:n:18.1	0:n:18.1	0:n:18.1
region	Saturation	Saturation	Saturation
id	1.5781u	1.5777u	
lbs	-5.594e-22	-5.592e-22	
lbd	-110.4878a	-110.0762a	
vgs	463.0727u	463.0727u	
vds	463.0727u	461.3359u	
vbs	0.	0.	
vth	375.2166u	375.2227u	
vsdat	106.9738u	106.9664u	
vod	87.8559u	87.8453u	
beta	301.9575u	301.9570u	
gm eff	507.4460u	507.4460u	
gm	23.4973u	23.4926u	
gds	240.8474u	241.0110u	
gmb	4.7853u	4.7845u	
cdtot	2.0666f	2.0675f	
cgto1	12.9835f	12.9835f	
cgto2	14.1993f	14.1991f	
cbtot	6.5206f	6.5214f	
cgs	11.3560f	11.3560f	
cgd	495.0770u	495.1355u	

FF

subckt	0:m1	0:m2	0:m3	0:m4	0:m5	0:m6
element	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1	0:p:18.1
model	Saturation	Saturation	Saturation	Saturation	Saturation	Saturation
region	0.0252u	-2.7105u	-2.7105u	-2.5126u	-2.5126u	2.5126u
id	7.121e-22	4.258e-22	4.258e-22	51.3591a	51.3591a	-0.848e-22
lbs	92.6975u	285.8404a	285.8404a	426.6421a	426.6421a	-109.9614a
vgs	-600.0000u	-600.0000u	-600.0000u	-638.3001u	-638.3001u	455.1350u
vds	-161.6099u	-899.9535u	-899.9535u	-1.1816	-1.1816	456.7403u
vbs	0.	0.	0.	161.6099u	161.6099u	0.
vth	-452.5655u	-452.3564u	-452.3564u	-407.3512u	-407.3512u	341.0607u
vsdat	-155.1715u	-156.5774u	-156.5774u	-154.5555u	-154.5555u	124.7695u
vod	-147.1334u	-147.6430u	-147.6430u	-140.9489u	-140.9489u	114.0743u
beta	456.8399u	226.1769u	226.1769u	219.1337u	219.1337u	331.7875u
gm eff	557.0846u	557.0846u	557.0846u	555.9519u	555.9519u	507.4460u
gm	51.2653u	29.3681u	29.3681u	27.9256u	27.9256u	32.8820u
gds	5.8561u	81.8238u	81.8238u	64.1695u	64.1695u	353.8471u
gmb	15.2551u	8.6828u	8.6828u	7.6961u	7.6961u	6.4399u
cdtot	16.3487f	4.5195f	4.5195f	4.2689f	4.2689f	1.9724f
cgto	80.5044f	39.0467f	39.0467f	38.7748f	38.7748f	13.6968f
cgtd	44.2424f	24.1928f	24.1928f	23.9242f	23.9242f	9.4242f
cgst	80.1590f	18.3605f	18.3605f	16.9043f	16.9043f	6.2309f
cgs	69.7233f	34.5474f	34.5474f	34.4638f	34.4638f	12.0635f
cys <td>9.7428f</td> <td>1.6235f</td> <td>1.6235f</td> <td>1.6212f</td> <td>1.6212f</td> <td>0.345755a</td>	9.7428f	1.6235f	1.6235f	1.6212f	1.6212f	0.345755a

7. Neatly list the sizes of all transistors, capacitance of the compensation capacitors and resistance of the compensation resistors.

Size of NMOS and PMOS in the circuit								
	Width	Length		Width	Length		Width	Length
M1	8.4um	1.4um	M4	4.2um	1.4um	M7	1.4um	1.4um
M2	4.2um	1.4um	M5	4.2um	1.4um	M8	1.4um	1.4um
M3	4.2um	1.4um	M6	1.4um	1.4um	M9	1.4um	1.4um
Size of NMOS and PMOS in the CMFB								
	Width	Length		Width	Length		Width	Length
Mopb	8.4um	1.4um	Mop2	4.2um	1.4um	Mop4	1.4um	1.4um
Mop1	4.2um	1.4um	Mop3	1.4um	1.4um	-		
Compensation capacitor								
Cc1	50pF		Cc2	50pF		-		
Compensation resistors								
Rc1	250k Ω		Rc2	250k Ω		-		

R-Sense CMFB loop

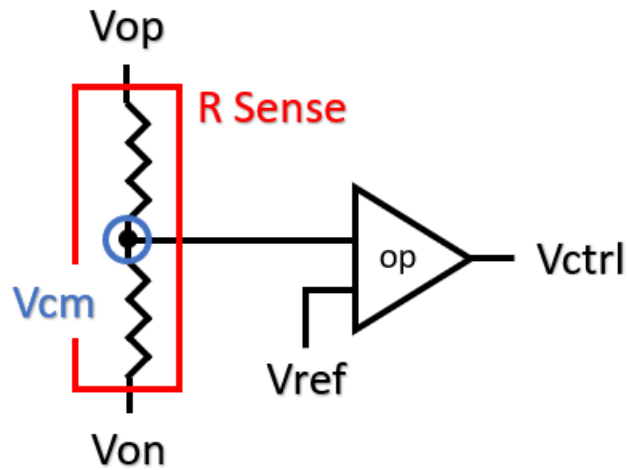


Fig. 5. R-Sense Common-Mode Feedback Loop