

Introduction to Computer Graphics

– Modeling (1) –

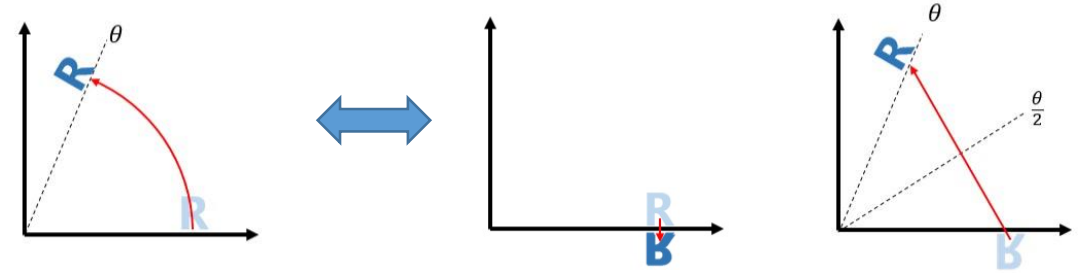
April 18, 2019

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Some additional notes on quaternions

Another explanation for quaternions (overview)

1. Any rotation can be decomposed into even number of reflections



2. Quaternions can concisely describe reflections in 3D

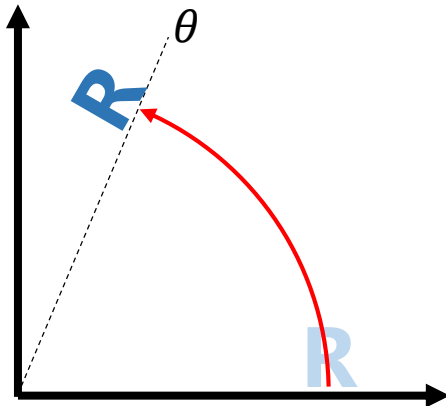
$$R_{\vec{f}}(\vec{x}) = -\vec{f} \vec{x} \vec{f}^{-1}$$

3. Combining two reflections equivalent to the rotation leads to the formula

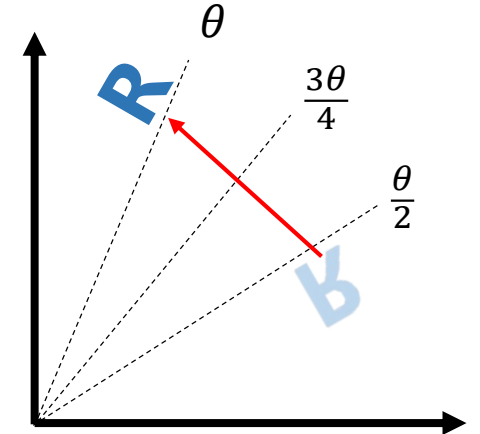
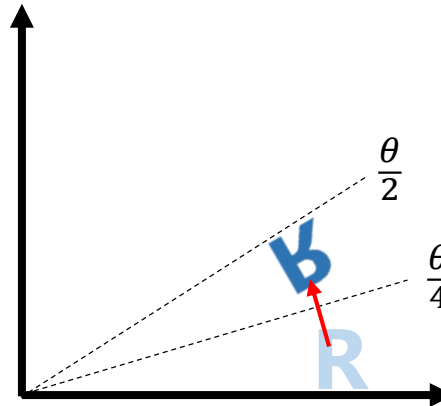
$$R_{\vec{g}} \left(R_{\vec{f}}(\vec{x}) \right) = \left(\cos \frac{\theta}{2} + \vec{\omega} \sin \frac{\theta}{2} \right) \vec{x} \left(\cos \frac{\theta}{2} - \vec{\omega} \sin \frac{\theta}{2} \right)$$

Any rotation can be decomposed into even number of reflections

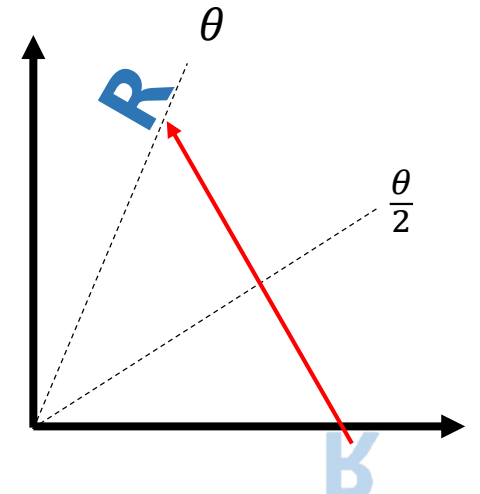
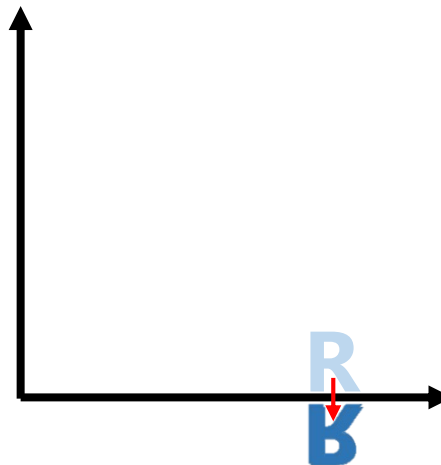
- Mathematically proven
 - Valid for any dimensions
- Not unique (of course!)



One way



Another way



Quaternions recap

- Complex number: real + imaginary

$$a + b \mathbf{i}$$

- Quaternion: scalar + vector

$$a + \vec{v}$$

- Definition of quaternion multiplication:

$$(a_1 + \vec{v}_1)(a_2 + \vec{v}_2) := \overbrace{a_1 a_2 - \vec{v}_1 \cdot \vec{v}_2}^{\text{Scalar part}} + \overbrace{a_1 \vec{v}_2 + a_2 \vec{v}_1 + \vec{v}_1 \times \vec{v}_2}^{\text{Vector part}}$$

- Pure vectors can take multiplication by interpreting them as quaternions:

$$\vec{v}_1 \vec{v}_2 = -\vec{v}_1 \cdot \vec{v}_2 + \vec{v}_1 \times \vec{v}_2$$

- Notable properties:
 - (Relevant later)

$$\vec{v} \vec{v} = -\|\vec{v}\|^2$$

$\vec{v} \times \vec{v}$ is always zero

$$\vec{v}^{-1} = -\frac{\vec{v}}{\|\vec{v}\|^2}$$

Multiplying \vec{v} to rhs produces 1

$$\text{If } \vec{v} \cdot \vec{w} = 0, \text{ then } \vec{v} \vec{w} = -\vec{w} \vec{v}$$

$$\vec{v} \vec{w} = \vec{v} \times \vec{w} = -\vec{w} \times \vec{v} = -\vec{w} \vec{v}$$

Describing reflections using quaternions

- Reflection of a point \vec{x} across a plane orthogonal to \vec{f} :

$$R_{\vec{f}}(\vec{x}) := -\vec{f} \vec{x} \vec{f}^{-1}$$

- Holds essential properties of reflections:

- Linearity:

$$R_{\vec{f}}(a \vec{x} + b \vec{y}) = a R_{\vec{f}}(\vec{x}) + b R_{\vec{f}}(\vec{y})$$

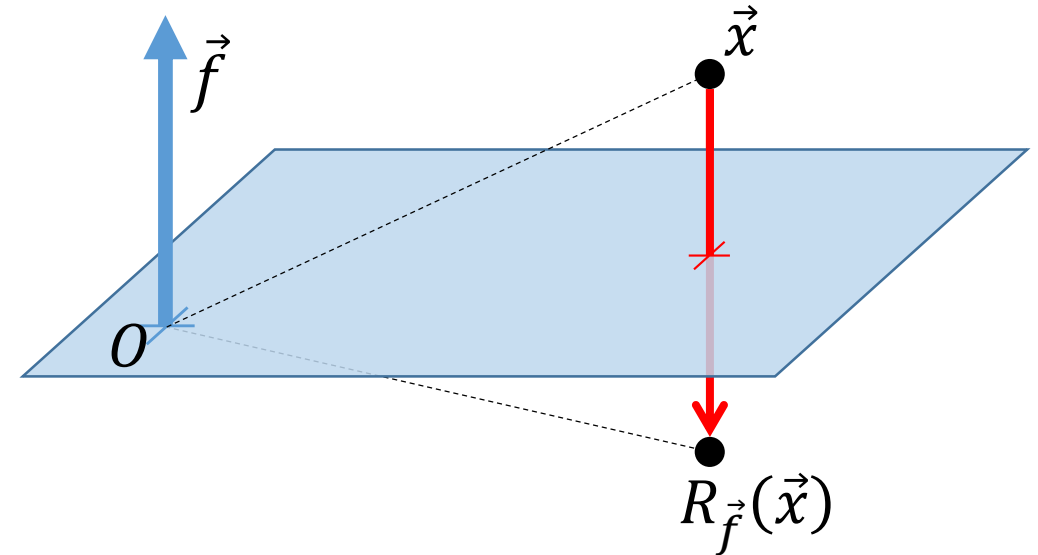
- \vec{f} gets mapped to $-\vec{f}$:

$$R_{\vec{f}}(\vec{f}) = -\vec{f} \vec{f} \vec{f}^{-1} = -\vec{f}$$

- If a point \vec{x} satisfies $\vec{x} \cdot \vec{f} = 0$ (i.e. on the plane), \vec{x} doesn't move:

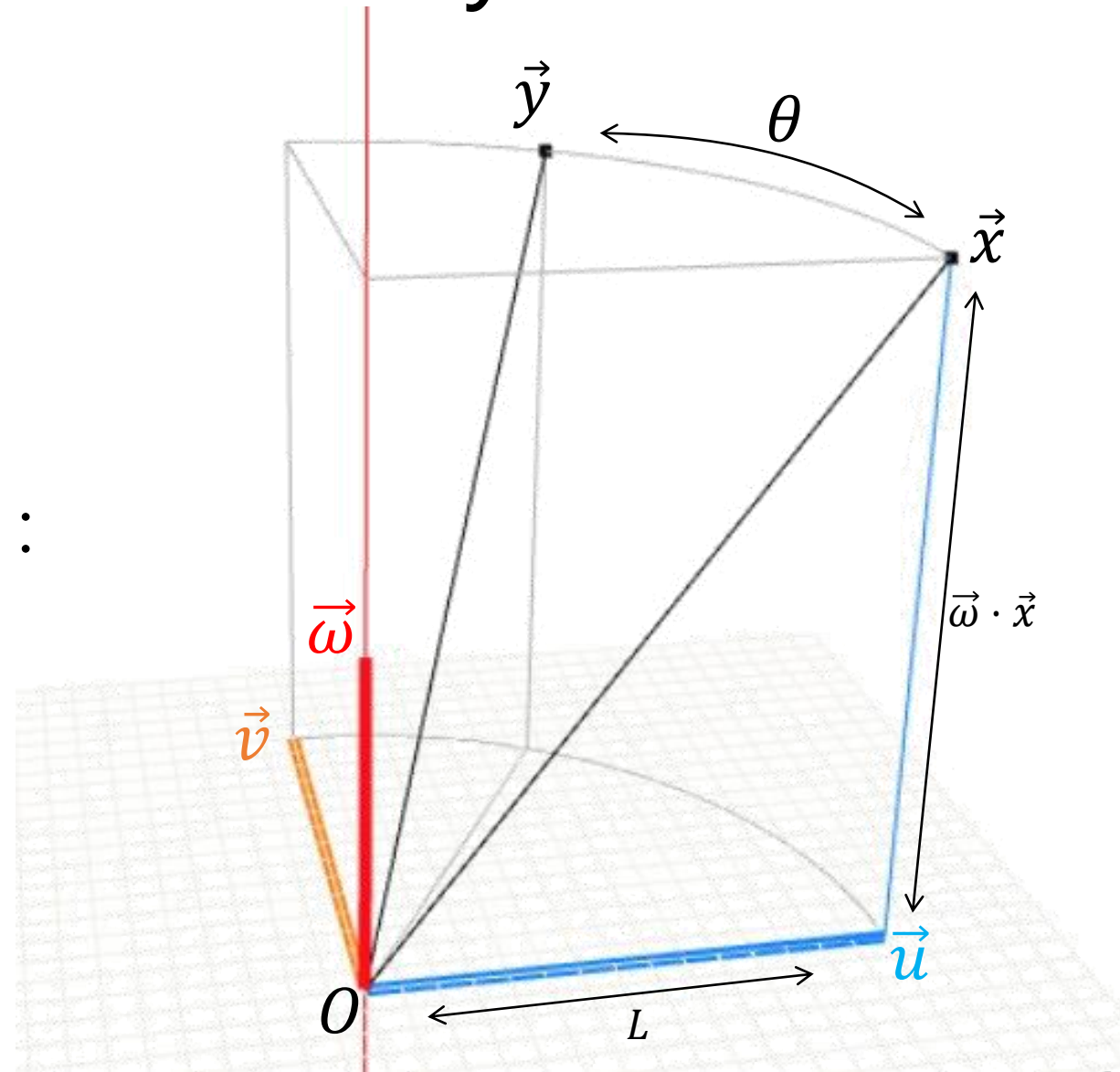
$$R_{\vec{f}}(\vec{x}) = -\vec{f} \vec{x} \vec{f}^{-1} = -(-\vec{x} \vec{f}) \vec{f}^{-1} = \vec{x}$$

Because if $\vec{x} \cdot \vec{f} = 0$, then $\vec{f} \vec{x} = -\vec{x} \vec{f}$



Setup for rotation around arbitrary axis

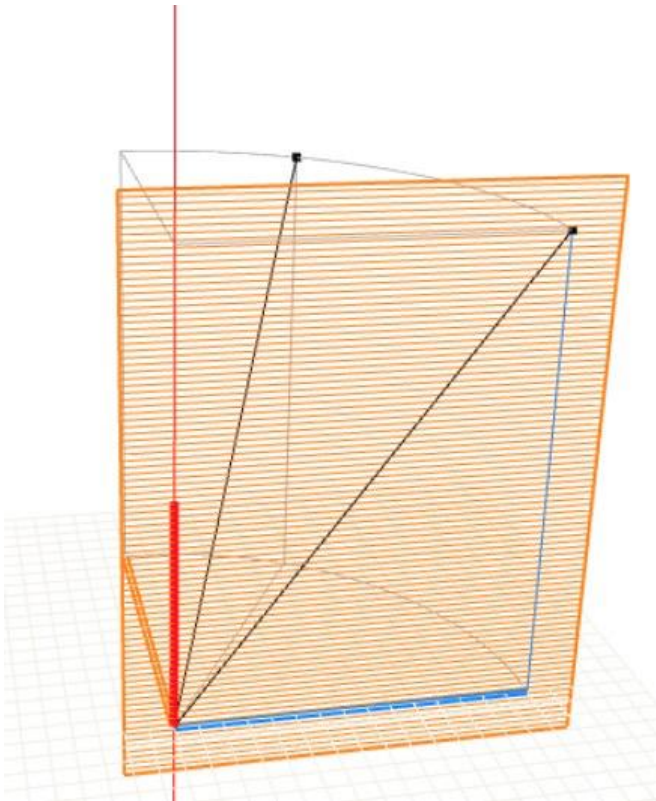
- Rotation axis (unit vector) : $\vec{\omega}$
- Rotation angle : θ
- Point before rotation : \vec{x}
- Point after rotation : $\vec{y} := R_{\vec{\omega}, \theta}(\vec{x})$
- Think of local 2D coordinate system :
 - "Right" vector : $\vec{u} := \vec{x} - (\vec{\omega} \cdot \vec{x})\vec{\omega}$
 - "Up" vector : $\vec{v} := \vec{\omega} \times \vec{x}$
 - Note that $\|\vec{u}\| = \|\vec{v}\|$
 - (Let's call it L)



Decompose rotation into two reflections

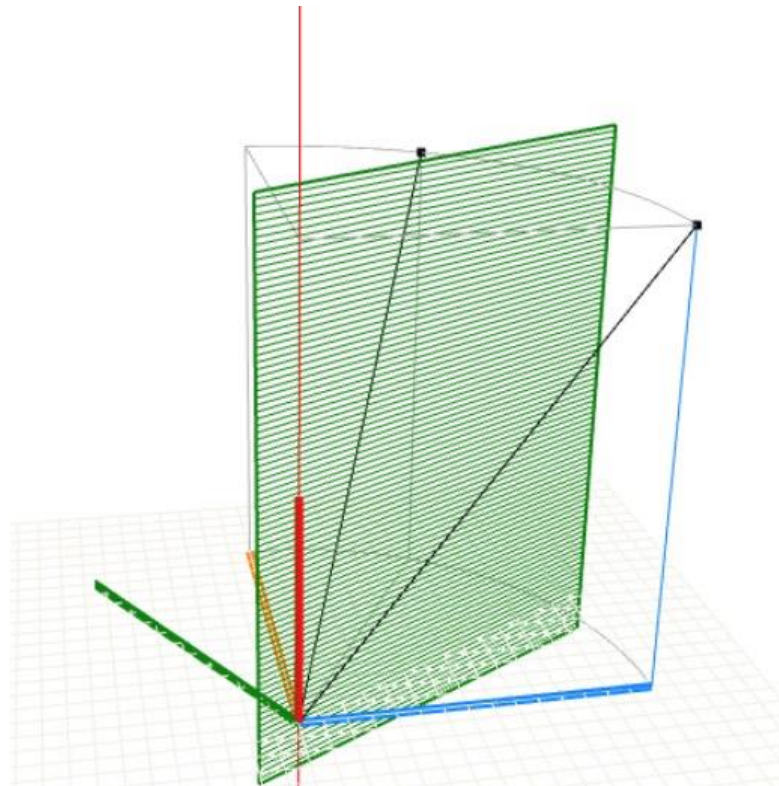
1st reflection :

$$\vec{f} := \vec{v}$$

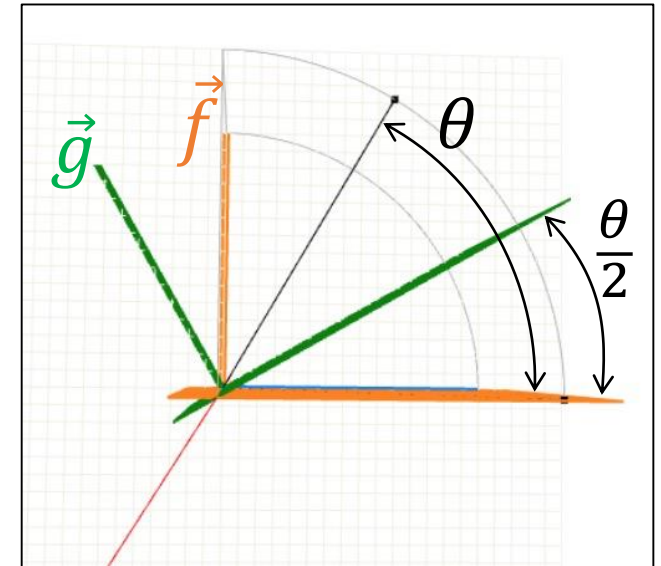


2nd reflection :

$$\vec{g} := -\sin \frac{\theta}{2} \vec{u} + \cos \frac{\theta}{2} \vec{v}$$



Top view



Combining two reflections

- Formula : $R_{\vec{g}} \left(R_{\vec{f}}(\vec{x}) \right) = R_{\vec{g}}(-\vec{f} \vec{x} \vec{f}^{-1}) = -\vec{g}(-\vec{f} \vec{x} \vec{f}^{-1})\vec{g}^{-1} = (\vec{g} \vec{f}) \vec{x} (\vec{f}^{-1} \vec{g}^{-1})$

- Substitute $\vec{f} := \vec{v}$, $\vec{g} := -\sin \frac{\theta}{2} \vec{u} + \cos \frac{\theta}{2} \vec{v}$ to the above

- For the left part $\vec{g} \vec{f}$:

$$\vec{g} \cdot \vec{f} = \left(-\sin \frac{\theta}{2} \vec{u} + \cos \frac{\theta}{2} \vec{v} \right) \cdot \vec{v} = L^2 \cos \frac{\theta}{2}$$

(because $\vec{u} \cdot \vec{v} = 0$)

$$\vec{g} \times \vec{f} = \left(-\sin \frac{\theta}{2} \vec{u} + \cos \frac{\theta}{2} \vec{v} \right) \times \vec{v} = -L^2 \sin \frac{\theta}{2} \vec{\omega}$$

(because $\vec{u} \times \vec{v} = L^2 \vec{\omega}$)

Therefore,

$$\vec{g} \vec{f} = -\vec{g} \cdot \vec{f} + \vec{g} \times \vec{f} = -L^2 \left(\cos \frac{\theta}{2} + \vec{\omega} \sin \frac{\theta}{2} \right)$$

- The right part $\vec{f}^{-1} \vec{g}^{-1} = \frac{\vec{f} \vec{g}}{L^4}$ is analogous : $\vec{f}^{-1} \vec{g}^{-1} = -L^{-2} \left(\cos \frac{\theta}{2} - \vec{\omega} \sin \frac{\theta}{2} \right)$

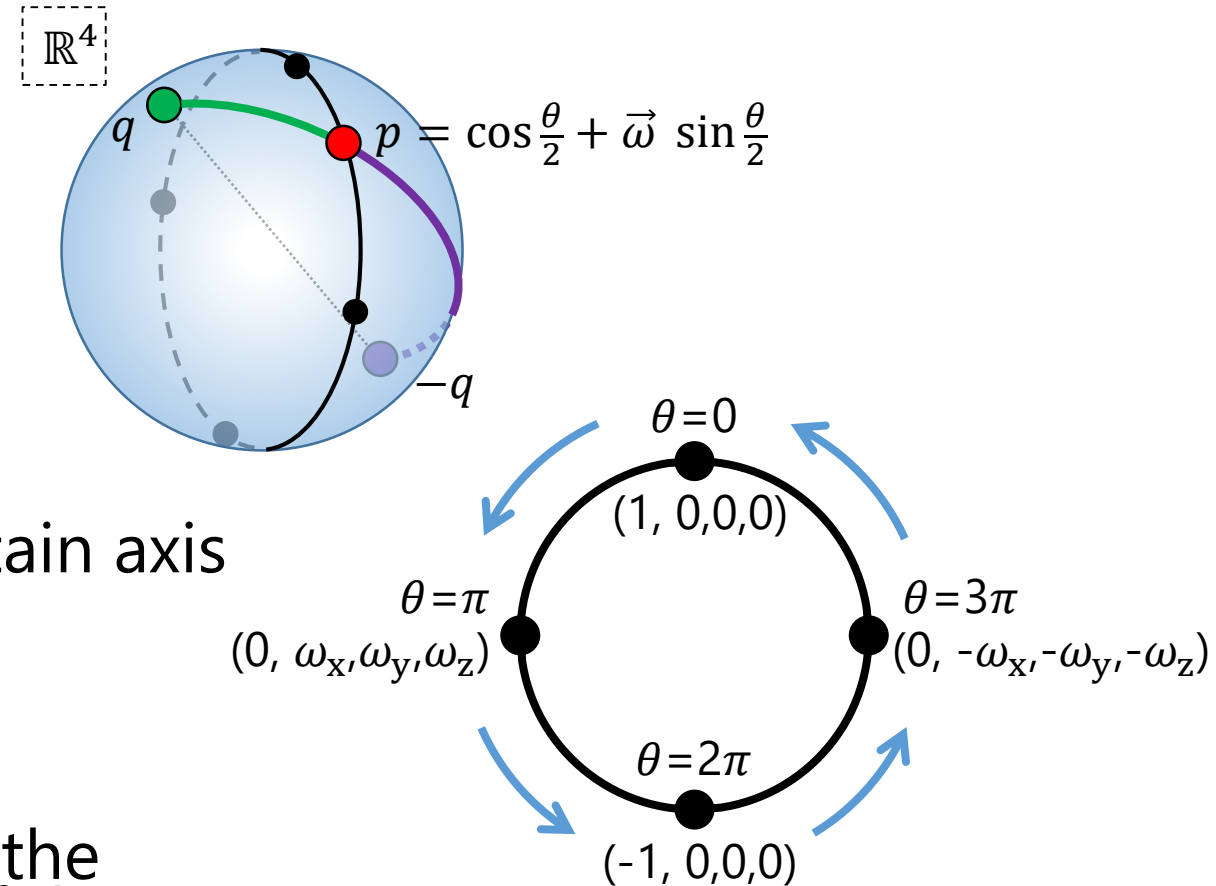
- Finally, we get the formula :

$$R_{\vec{\omega}, \theta}(\vec{x}) = R_{\vec{g}} \left(R_{\vec{f}}(\vec{x}) \right) = \left(-L^2 \left(\cos \frac{\theta}{2} + \vec{\omega} \sin \frac{\theta}{2} \right) \right) \vec{x} \left(-L^{-2} \left(\cos \frac{\theta}{2} - \vec{\omega} \sin \frac{\theta}{2} \right) \right)$$

$$= \left(\cos \frac{\theta}{2} + \vec{\omega} \sin \frac{\theta}{2} \right) \vec{x} \left(\cos \frac{\theta}{2} - \vec{\omega} \sin \frac{\theta}{2} \right)$$

Representing and blending poses using quaternions

- Any rotations (poses) can be represented as unit quaternions
 - Points on hypersphere of 4D space
- Fix $\vec{\omega}$ and vary θ
→ unit circle in 4D space
- A pose after rotating 360° about a certain axis is represented as another quaternion
 - One pose corresponds to two quaternions (double cover)
- A geodesic between two points p, q on the hypersphere represents interpolation of these poses
 - Should pick either q or $-q$ which is closer to p (i.e. 4D dot product is positive)



Normalize quaternions or not?

- Any quaternions can be written as scaling of unit quaternions

$$q = r(\cos \frac{\theta}{2} + \vec{\omega} \sin \frac{\theta}{2}), \quad q^{-1} = r^{-1}(\cos \frac{\theta}{2} - \vec{\omega} \sin \frac{\theta}{2})$$

- In the rotation formula, the scaling part is cancelled

$$q \vec{x} q^{-1} = \cancel{r} (\cos \frac{\theta}{2} + \vec{\omega} \sin \frac{\theta}{2}) \vec{x} \cancel{r^{-1}} (\cos \frac{\theta}{2} - \vec{\omega} \sin \frac{\theta}{2}) = (\cos \frac{\theta}{2} + \vec{\omega} \sin \frac{\theta}{2}) \vec{x} (\cos \frac{\theta}{2} - \vec{\omega} \sin \frac{\theta}{2})$$

→ so, normalization isn't needed?

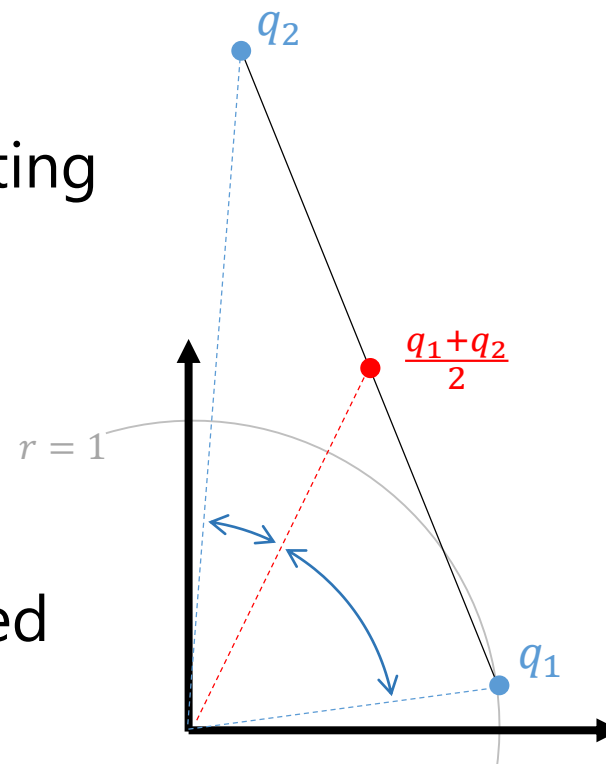
- In practice, don't use quaternion mults for computing coordinate transformation (because inefficient)

- Just do explicit vector calc using axis & angle

$$(\vec{x} - (\vec{\omega} \cdot \vec{x})\vec{\omega}) \cos \theta + (\vec{\omega} \times \vec{x}) \sin \theta + (\vec{\omega} \cdot \vec{x})\vec{\omega}$$

- Can get axis & angle only after normalization

- Un-normalized can cause artifact when interpolated



Modeling curves

Parametric curves

- X & Y coordinates defined by parameter t (\cong time)
 - Example: Cycloid

$$\begin{aligned}x(t) &= t - \sin t \\y(t) &= 1 - \cos t\end{aligned}$$



- Tangent (aka. derivative, gradient) vector: $(x'(t), y'(t))$
- Polynomial curve: $x(t) = \sum_i a_i t^i$

Cubic Hermite curves

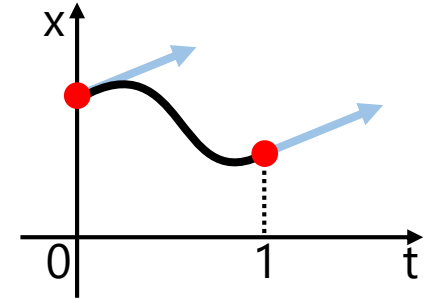
- Cubic polynomial curve interpolating derivative constraints at both ends (Hermite interpolation)

- 4 constraints \rightarrow 4 DoF needed
 \rightarrow 4 coefficients \rightarrow cubic

- $x(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$
 - $x'(t) = a_1 + 2a_2 t + 3a_3 t^2$

- Coeffs determined by substituting constrained values & derivatives

$$\begin{aligned}x(0) &= x_0 \\x(1) &= x_1 \\x'(0) &= x'_0 \\x'(1) &= x'_1\end{aligned}$$



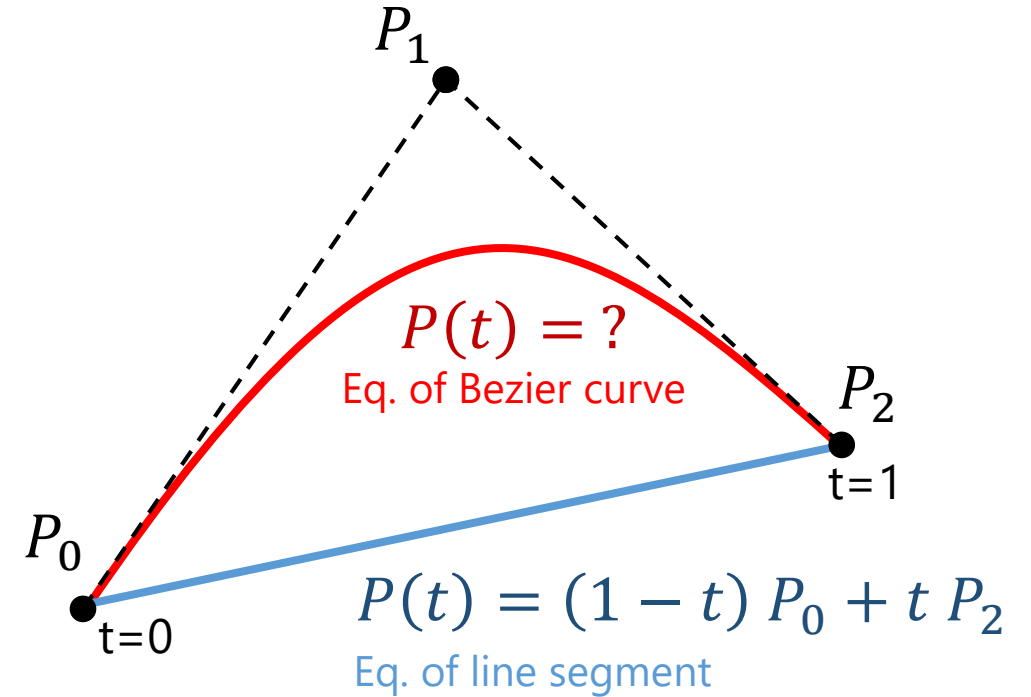
$$\begin{aligned}x(0) &= a_0 &= x_0 \\x(1) &= a_0 + a_1 + a_2 + a_3 = x_1 \\x'(0) &= a_1 &= x'_0 \\x'(1) &= a_1 + 2a_2 + 3a_3 = x'_1\end{aligned}$$

\rightarrow

$$\begin{aligned}a_0 &= x_0 \\a_1 &= x'_0 \\a_2 &= -3x_0 + 3x_1 - 2x'_0 - x'_1 \\a_3 &= 2x_0 - 2x_1 + x'_0 + x'_1\end{aligned}$$

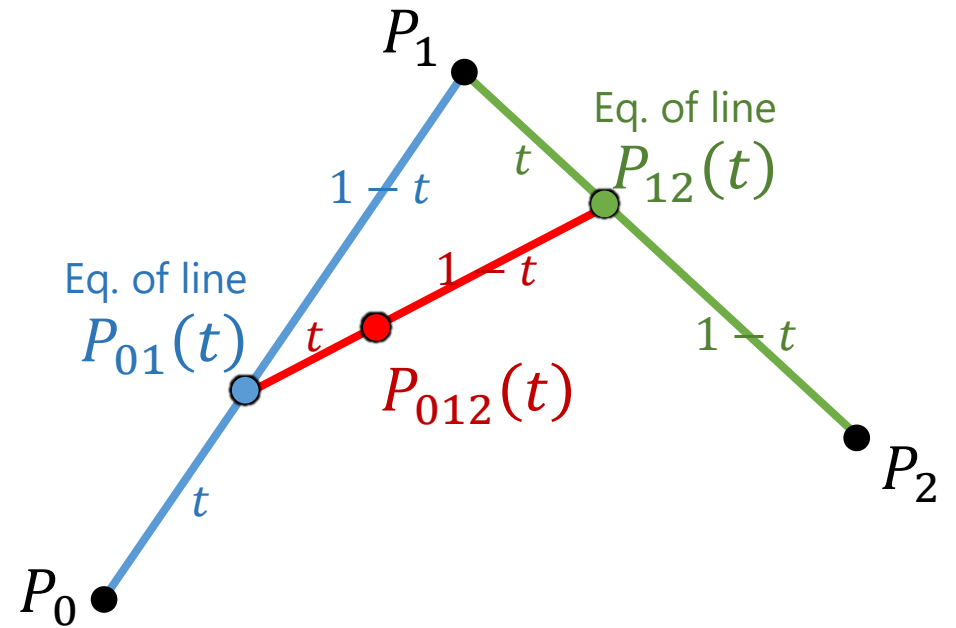
Bezier curves

- Input: 3 **control points** (CPs) P_0, P_1, P_2
 - Coordinates of points in arbitrary domain (2D, 3D, ...)
- Output: Curve $P(t)$ satisfying
$$P(0) = P_0$$
$$P(1) = P_2$$
while being "pulled" by P_1



Bezier curves

- $P_{01}(t) = (1 - t)P_0 + t P_1$
- $P_{12}(t) = (1 - t)P_1 + t P_2$
 - $P_{01}(0) = P_0$
 - $P_{12}(1) = P_2$



- Idea: "Interpolate the interpolation"
As t changes $0 \rightarrow 1$, smoothly transition from P_{01} to P_{12}
- $P_{012}(t) = (1 - t)P_{01}(t) + t P_{12}(t)$

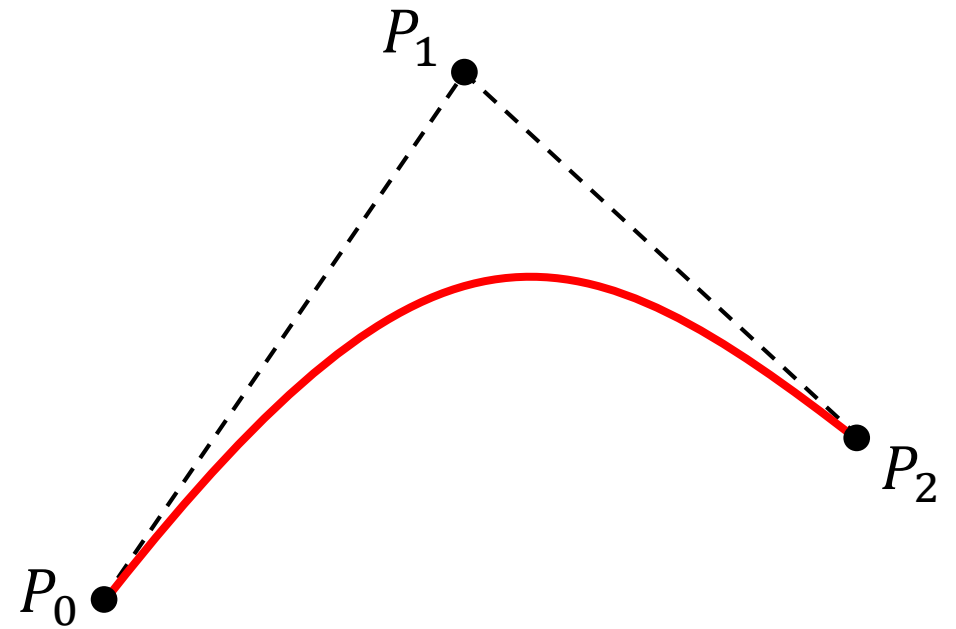
$$= (1 - t)\{(1 - t)P_0 + t P_1\} + t \{(1 - t)P_1 + t P_2\}$$

$$= (1 - t)^2 P_0 + 2t(1 - t)P_1 + t^2 P_2$$

Quadratic Bezier curve

Bezier curves

- $P_{01}(t) = (1 - t)P_0 + t P_1$
- $P_{12}(t) = (1 - t)P_1 + t P_2$
 - $P_{01}(0) = P_0$
 - $P_{12}(1) = P_2$



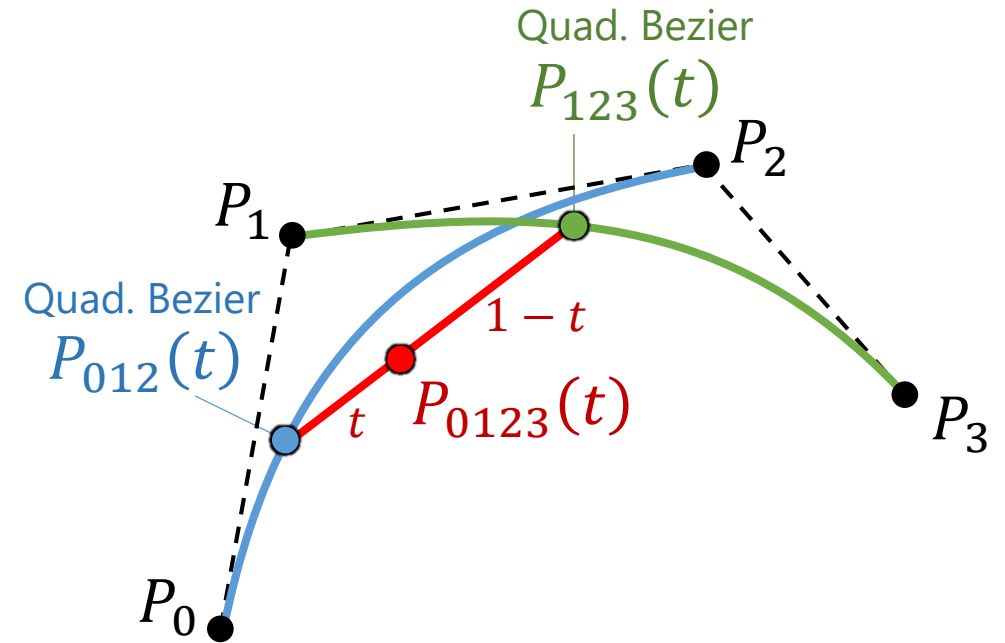
- Idea: "Interpolate the interpolation"
As t changes $0 \rightarrow 1$, smoothly transition from P_{01} to P_{12}

- $$P_{012}(t) = (1 - t)P_{01}(t) + t P_{12}(t)$$
$$= (1 - t)\{(1 - t)P_0 + t P_1\} + t \{(1 - t)P_1 + t P_2\}$$
$$= (1 - t)^2 P_0 + 2t(1 - t)P_1 + t^2 P_2$$

Quadratic Bezier curve

Cubic Bezier curve

- Exact same idea applied to 4 points P_0, P_1, P_2, P_3 :
 - As t changes $0 \rightarrow 1$, transition from P_{012} to P_{123}



- $P_{0123}(t) = (1 - t)P_{012}(t) + t P_{123}(t)$

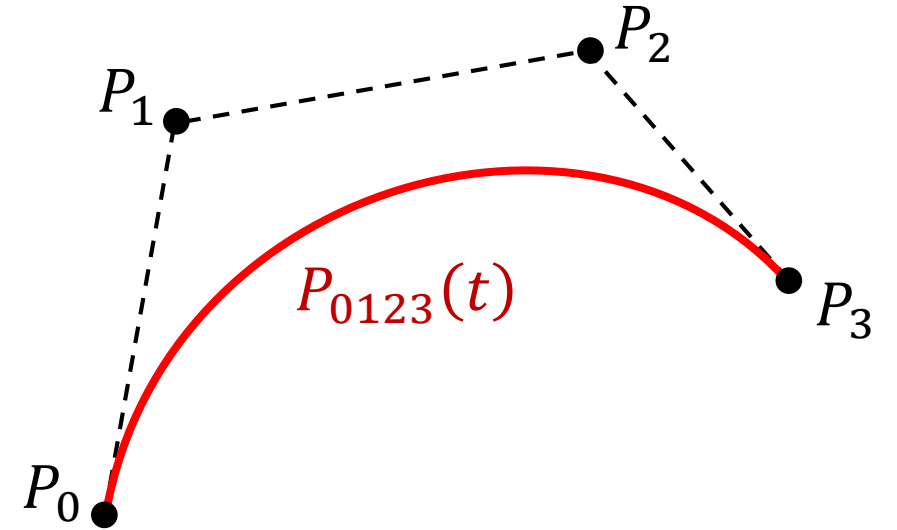
$$= (1 - t)\{(1 - t)^2 P_0 + 2t(1 - t)P_1 + t^2 P_2\} + t \{(1 - t)^2 P_1 + 2t(1 - t)P_2 + t^2 P_3\}$$

$$= (1 - t)^3 P_0 + 3t(1 - t)^2 P_1 + 3t^2(1 - t)P_2 + t^3 P_3$$

Cubic Bezier curve

Cubic Bezier curve

- Exact same idea applied to 4 points P_0, P_1, P_2, P_3 :
 - As t changes $0 \rightarrow 1$, transition from P_{012} to P_{123}



- $$P_{0123}(t) = (1 - t)P_{012}(t) + t P_{123}(t)$$
$$= (1 - t)\{(1 - t)^2 P_0 + 2t(1 - t)P_1 + t^2 P_2\} + t \{(1 - t)^2 P_1 + 2t(1 - t)P_2 + t^2 P_3\}$$
$$= (1 - t)^3 P_0 + 3t(1 - t)^2 P_1 + 3t^2(1 - t)P_2 + t^3 P_3$$

Cubic Bezier curve

- Can easily control tangent at endpoints \rightarrow ubiquitously used in CG

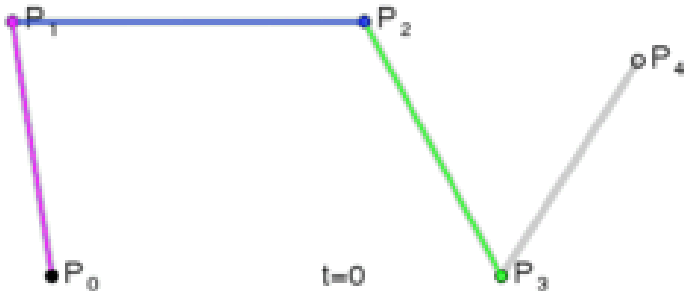
n-th order Bezier curve

- Input: $n+1$ control points P_0, \dots, P_n

$$P(t) = \sum_{i=0}^n \underbrace{{}_nC_i t^i (1-t)^{n-i}}_{b_i^n(t)} P_i$$

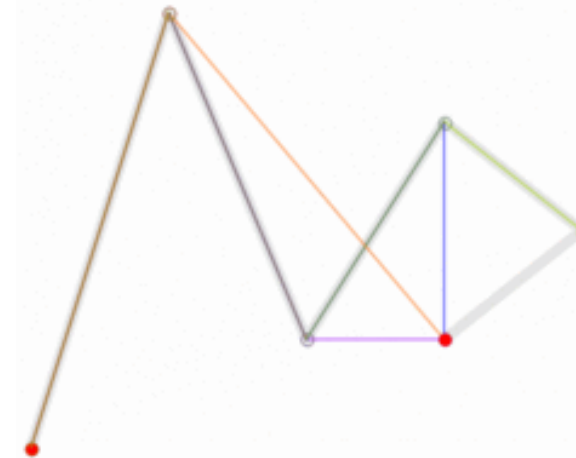
Bernstein basis function

Quartic (4th)



$$\begin{aligned} &(1-t)^4 P_0 + \\ &4t(1-t)^3 P_1 + \\ &6t^2(1-t)^2 P_2 + \\ &4t^3(1-t) P_3 + \\ &t^4 P_4 \end{aligned}$$

Quintic (5th)



$$\begin{aligned} &(1-t)^5 P_0 + \\ &5t(1-t)^4 P_1 + \\ &10t^2(1-t)^3 P_2 + \\ &10t^3(1-t)^2 P_3 + \\ &5t^4(1-t) P_4 + \\ &t^5 P_5 \end{aligned}$$

Cubic Bezier curves & cubic Hermite curves

- Cubic Bezier curve & its derivative:

- $P(t) = (1 - t)^3 P_0 + 3t(1 - t)^2 P_1 + 3t^2(1 - t) P_2 + t^3 P_3$

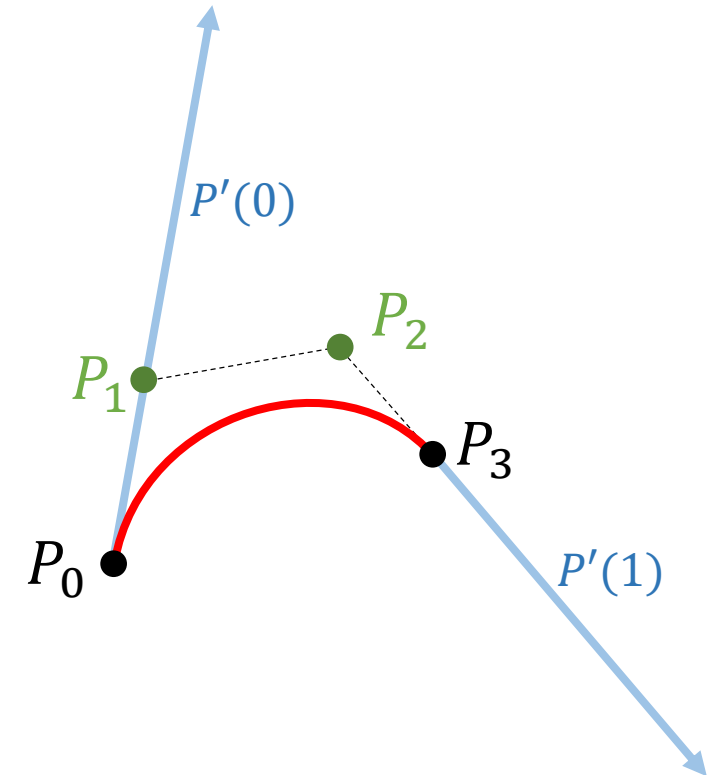
- $P'(t) = -3(1 - t)^2 P_0 + 3\{(1 - t)^2 - 2t(1 - t)\} P_1 + 3\{2t(1 - t) - t^2\} P_2 + 3t^2 P_3$

- Derivatives at endpoints:

- $P'(0) = -3P_0 + 3P_1 \quad \rightarrow \quad P_1 = P_0 + \frac{1}{3} P'(0)$

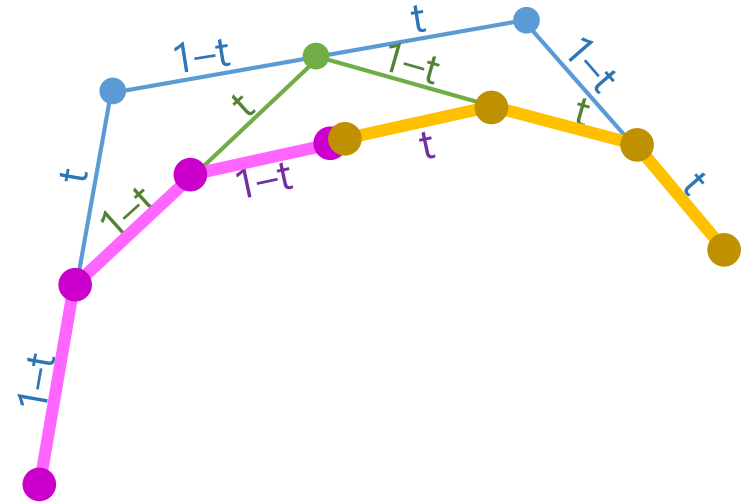
- $P'(1) = -3P_2 + 3P_3 \quad \rightarrow \quad P_2 = P_3 - \frac{1}{3} P'(1)$

- Different ways of looking at cubic curves, essentially the same



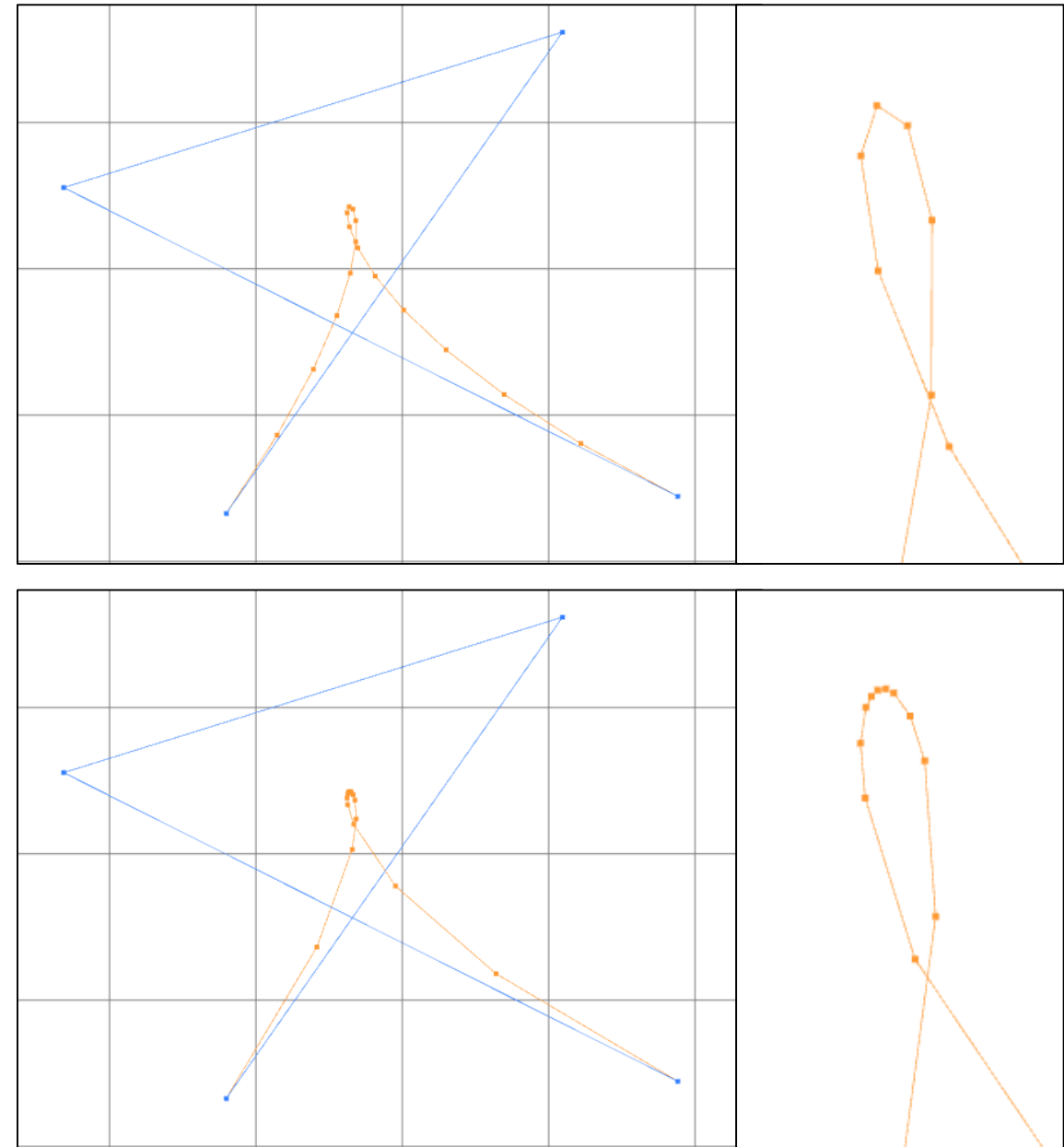
Evaluating Bezier curves

- Method 1: Direct evaluation of polynomials
 - Simple & fast 😊, could be numerically unstable ☹️
- Method 2: de Casteljau's algorithm
 - Directly after the recursive definition of Bezier curves
 - More computation steps ☹️, numerically stable 😊
 - Also useful for splitting Bezier curves



Drawing Bezier curves

- In the end, everything is drawn as polyline
 - Main question: How to sample parameter t ?
- Method 1: Uniform sampling
 - Simple
 - Potentially insufficient sampling density
- Method 2: Adaptive sampling
 - If control points deviate too much from straight line, split by de Casteljau's algorithm

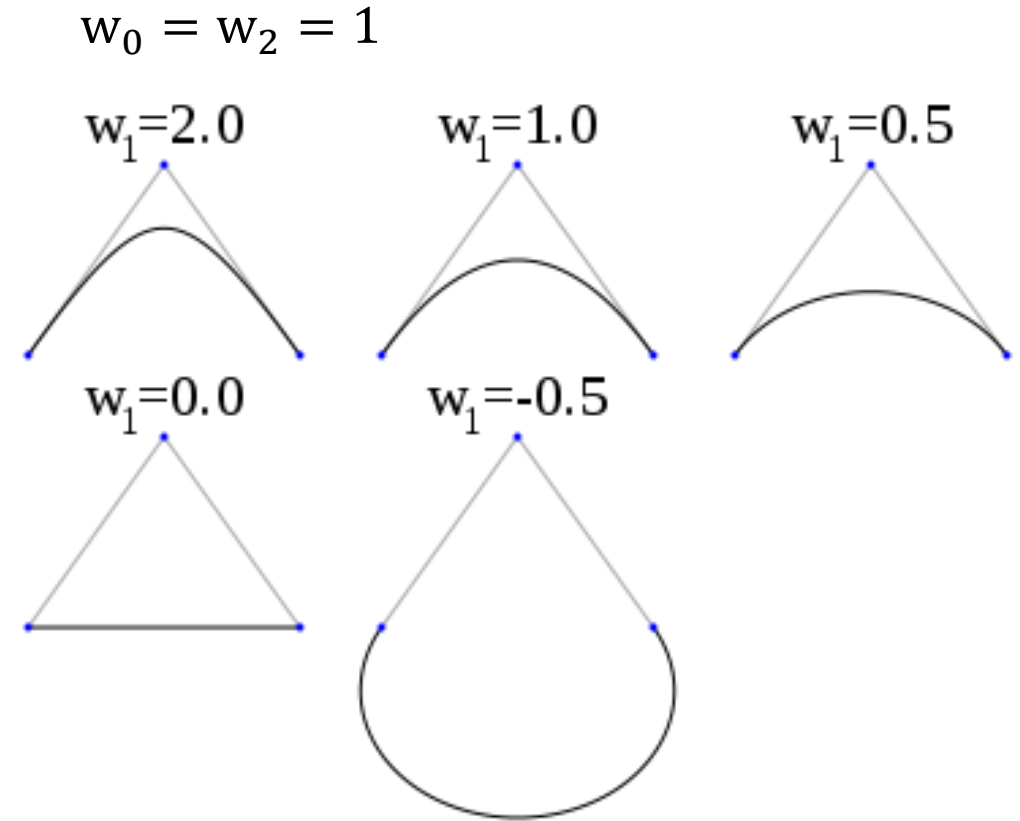


Further control: Rational Bezier curve

- Another view on Bezier curve:
"Weighted average" of control points
 - $P_{012}(t) = (1-t)^2 P_0 + 2t(1-t) P_1 + t^2 P_2$
 $= \lambda_0(t) P_0 + \lambda_1(t) P_1 + \lambda_2(t) P_2$
 - Important property: **partition of unity**
 $\lambda_0(t) + \lambda_1(t) + \lambda_2(t) = 1 \quad \forall t$
- Multiply each $\lambda_i(t)$ by arbitrary coeff w_i :
 $\xi_i(t) = w_i \lambda_i(t)$
- Normalize to obtain new weights:

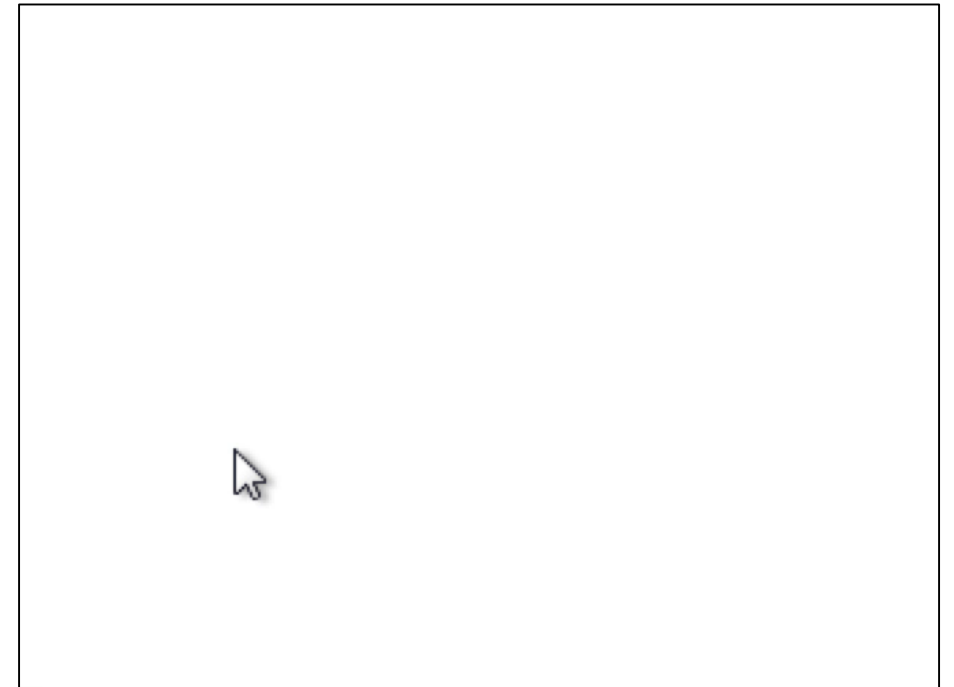
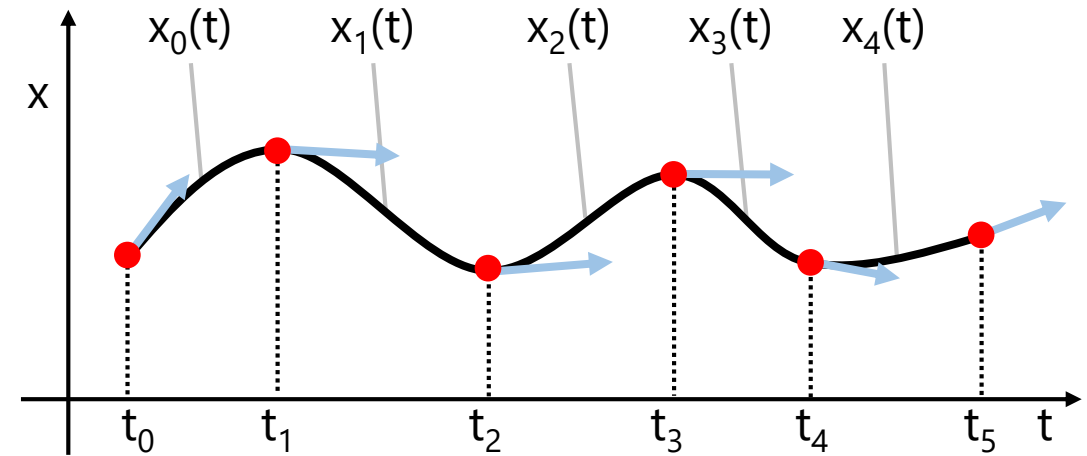
$$\lambda'_i(t) = \frac{\xi_i(t)}{\sum_j \xi_j(t)}$$

Non-polynomial curve → can represent arcs etc.



Cubic splines

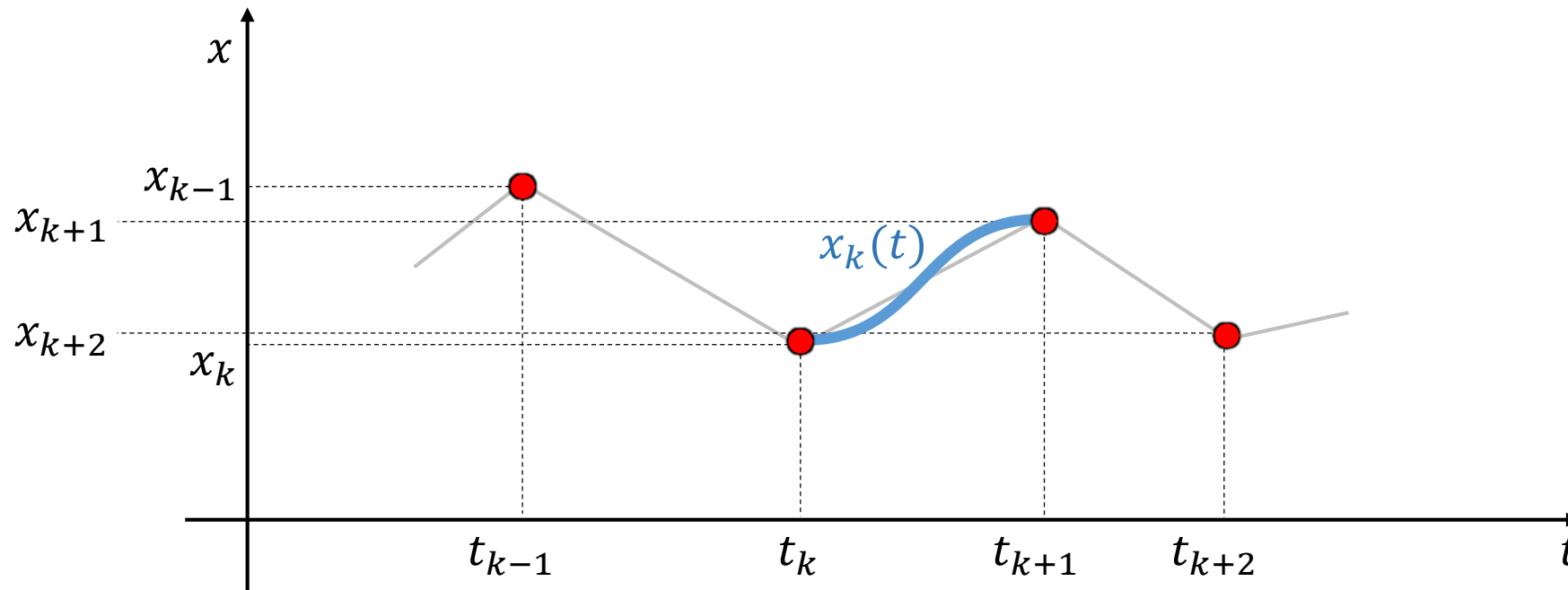
- Series of connected cubic curves
 - Piecewise-polynomial
 - Share value & derivative at every transition of intervals (C^1 continuity)
- Parameter range can be other than $[0, 1]$
 - Assumption: $t_k < t_{k+1}$
- Given values as only input, we want to automatically set derivatives



Curve tool in PowerPoint

Cubic Catmull-Rom spline

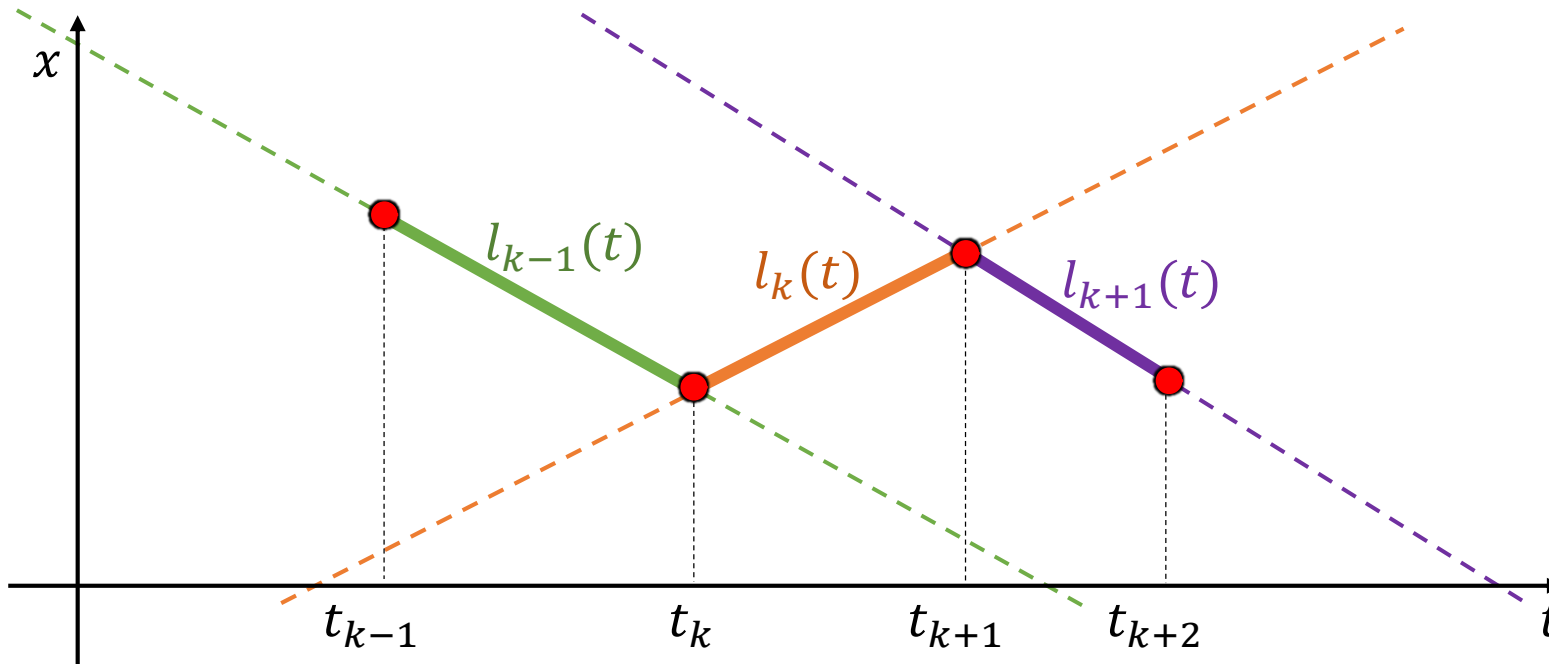
- Cubic function $x_k(t)$ for range $t_k \leq t \leq t_{k+1}$ is defined by adjacent constrained values x_{k-1} , x_k , x_{k+1} , x_{k+2}



Cubic Catmull-Rom spline: Step 1

- As $t_k \rightarrow t_{k+1}$, interpolate such that $x_k \rightarrow x_{k+1} \Rightarrow$ Line

$$l_k(t) = \left(1 - \frac{t - t_k}{t_{k+1} - t_k}\right) x_k + \frac{t - t_k}{t_{k+1} - t_k} x_{k+1}$$

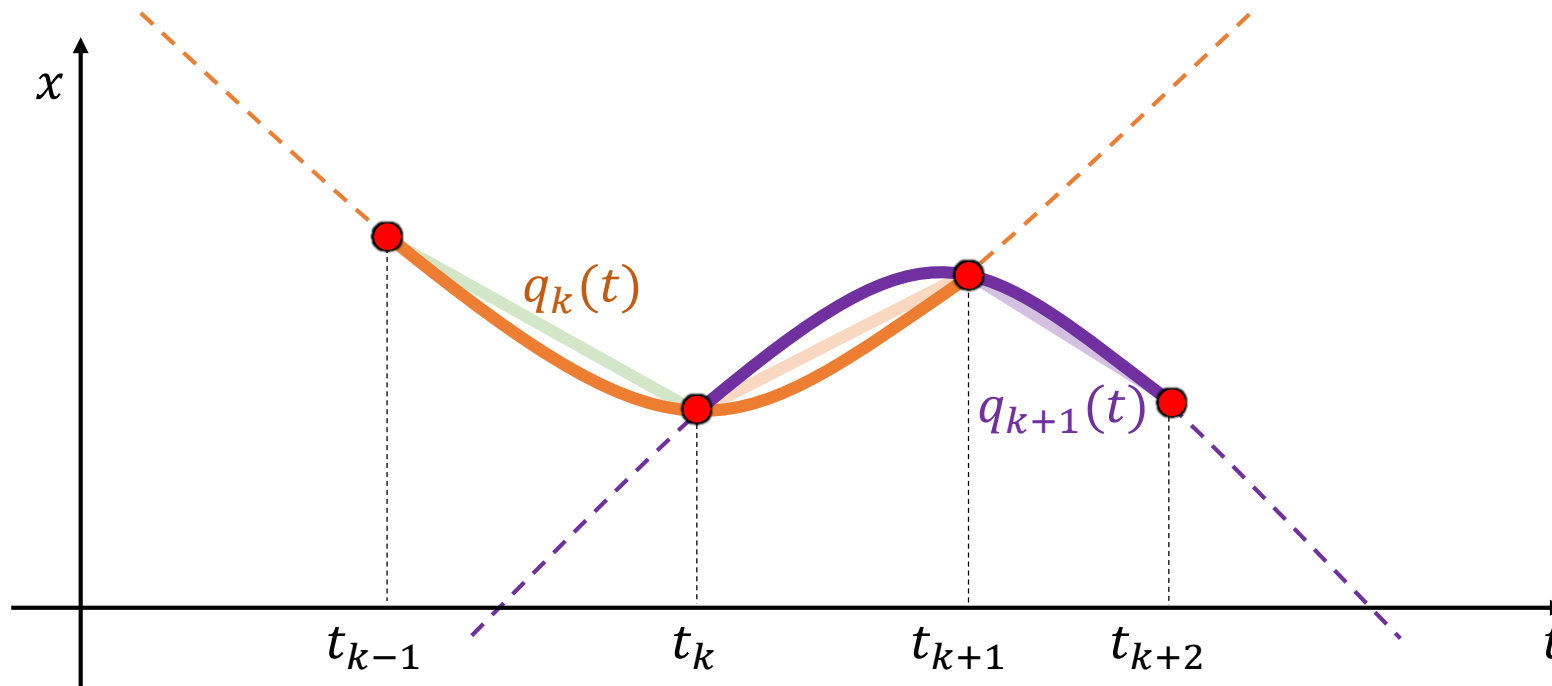


Cubic Catmull-Rom spline: Step 2

- As $t_{k-1} \rightarrow t_{k+1}$, interpolate such that $l_{k-1} \rightarrow l_k \Rightarrow$ Quadratic curve

$$q_k(t) = \left(1 - \frac{t - t_{k-1}}{t_{k+1} - t_{k-1}}\right) l_{k-1}(t) + \frac{t - t_{k-1}}{t_{k+1} - t_{k-1}} l_k(t)$$

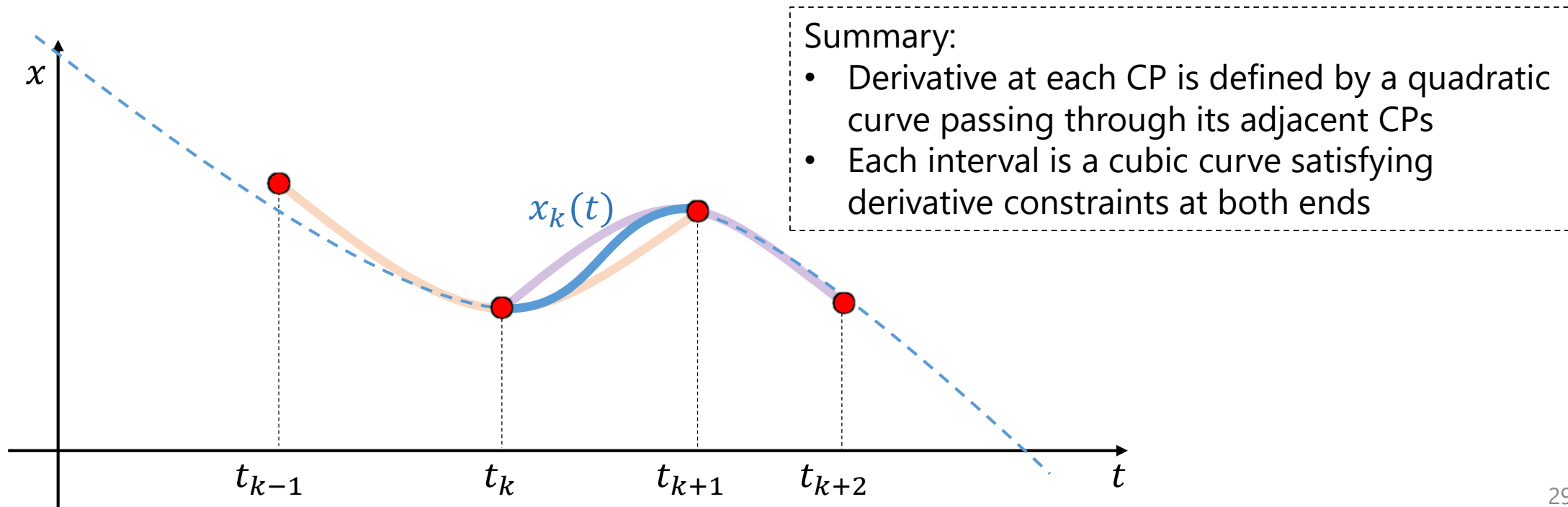
- Passes through 3 points (t_{k-1}, x_{k-1}) , (t_k, x_k) , (t_{k+1}, x_{k+1})



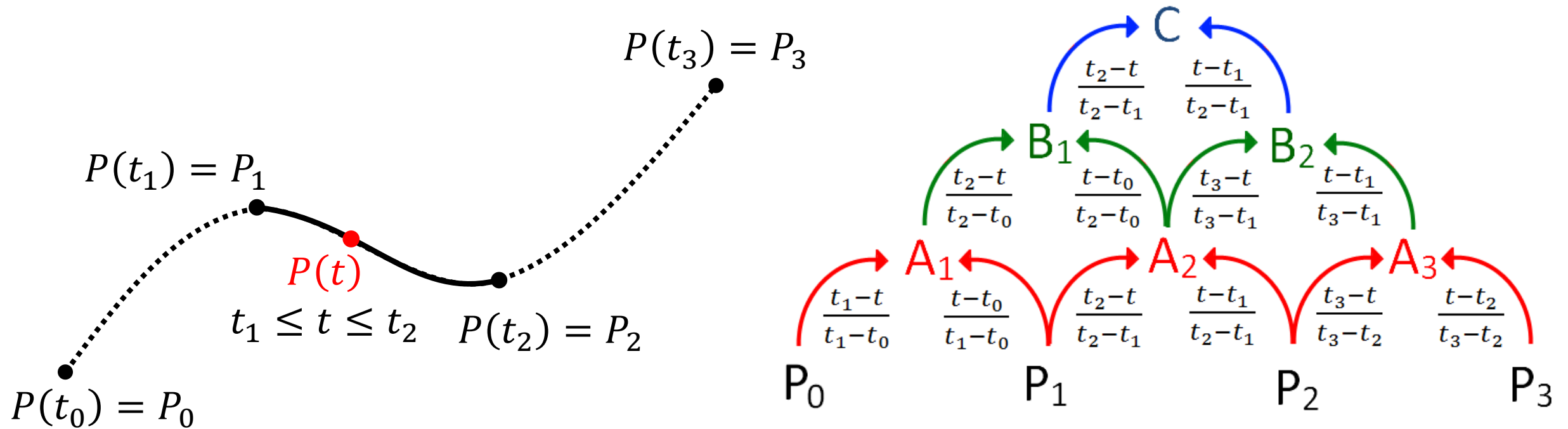
Cubic Catmull-Rom spline: Step 3

- As $t_k \rightarrow t_{k+1}$, interpolate such that $q_k \rightarrow q_{k+1} \rightarrow$ Cubic curve

$$x_k(t) = \left(1 - \frac{t - t_k}{t_{k+1} - t_k}\right) q_k(t) + \frac{t - t_k}{t_{k+1} - t_k} q_{k+1}(t)$$



Evaluating cubic Catmull-Rom spline



Ways of setting parameter values t_k (aka. knot sequence)

- Assume: $t_0 = 0$

- Uniform

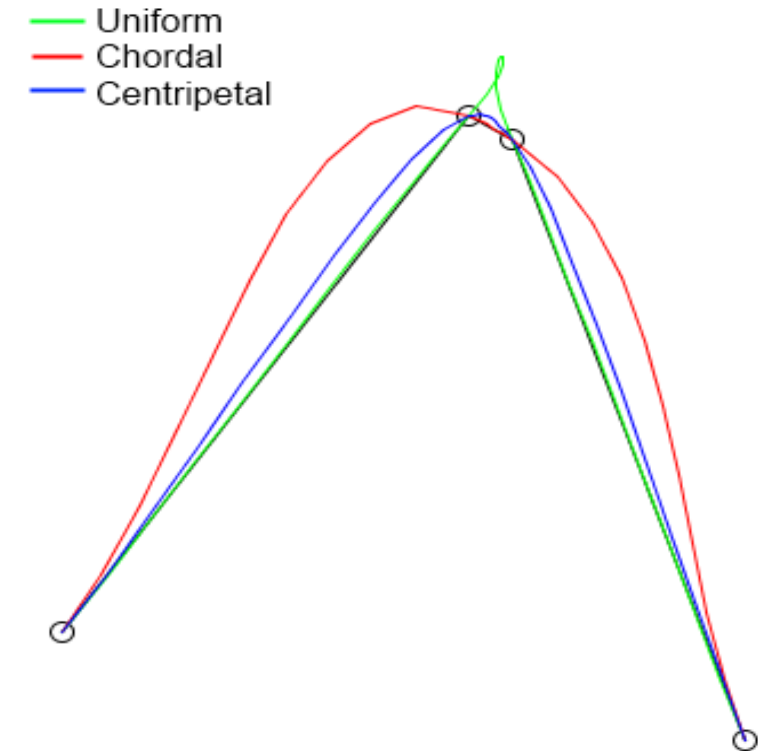
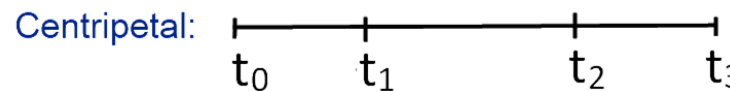
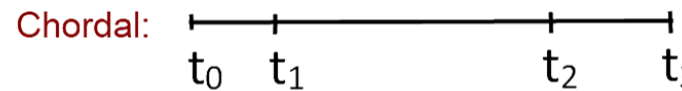
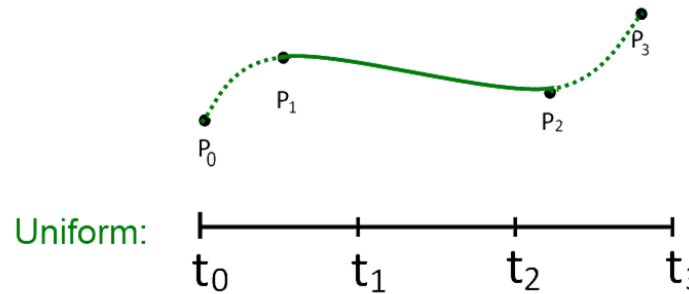
$$t_k = t_{k-1} + 1$$

- Chordal

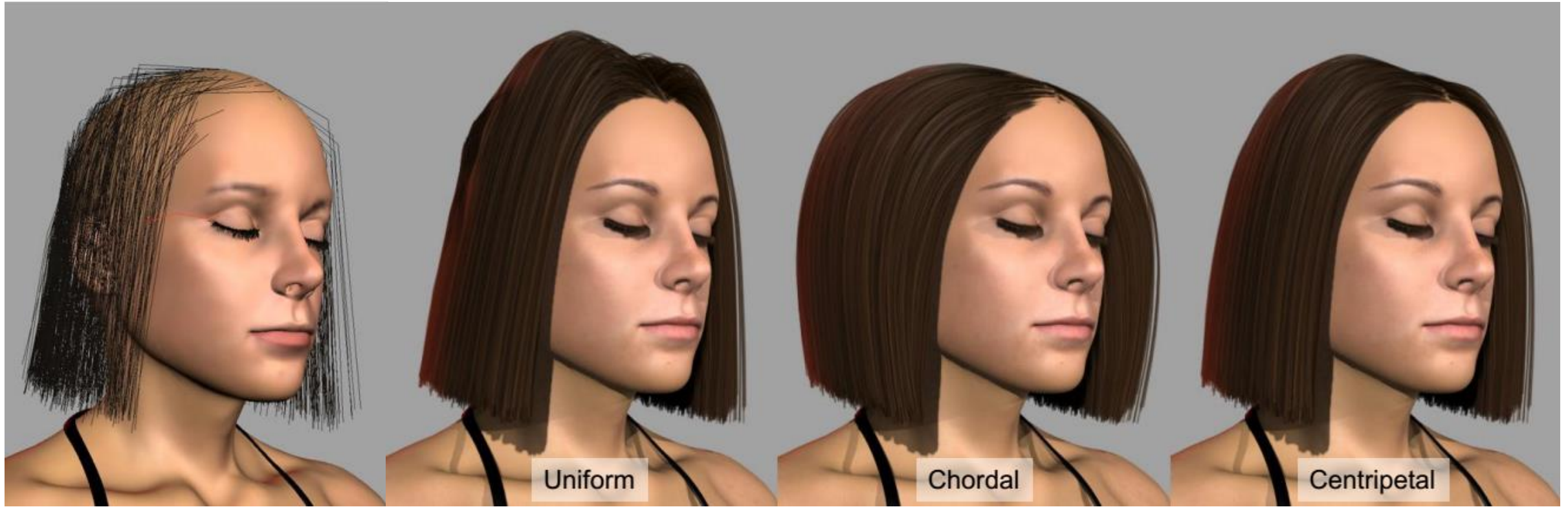
$$t_k = t_{k-1} + |P_{k-1} - P_k|$$

- Centripetal

$$t_k = t_{k-1} + \sqrt{|P_{k-1} - P_k|}$$

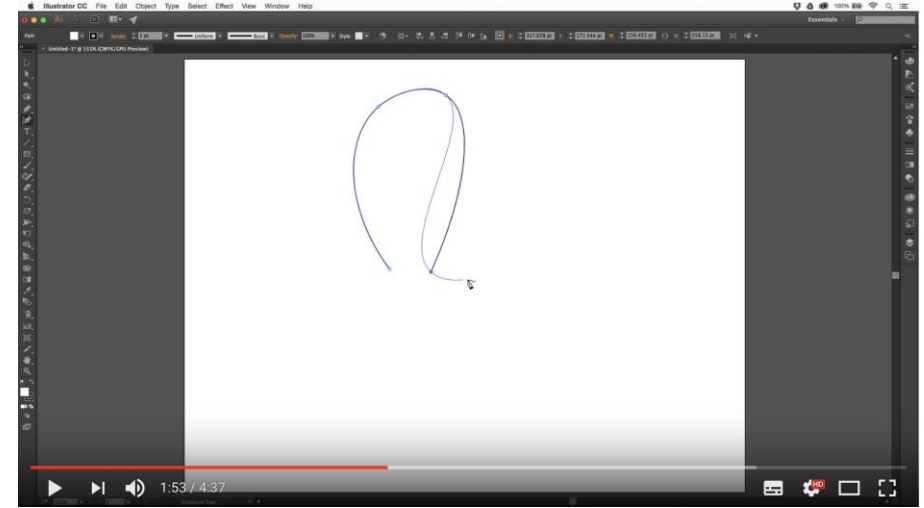


Application of cubic Catmull-Rom spline: Hair modeling



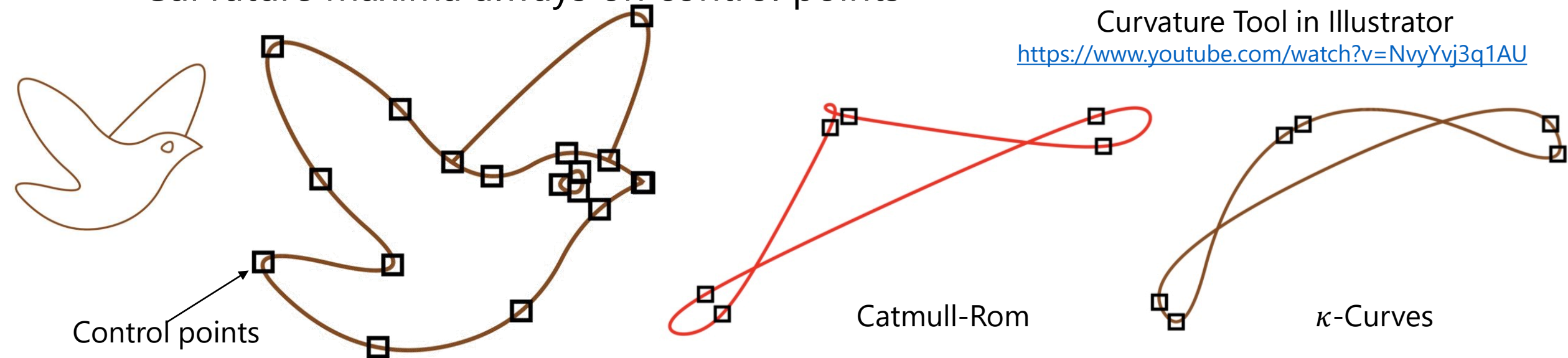
Recent exciting development: κ -Curves

- Collaboration between university & company (Adobe)
- Features:
 - C^2 continuous (smoother)
 - Curvature maxima always on control points



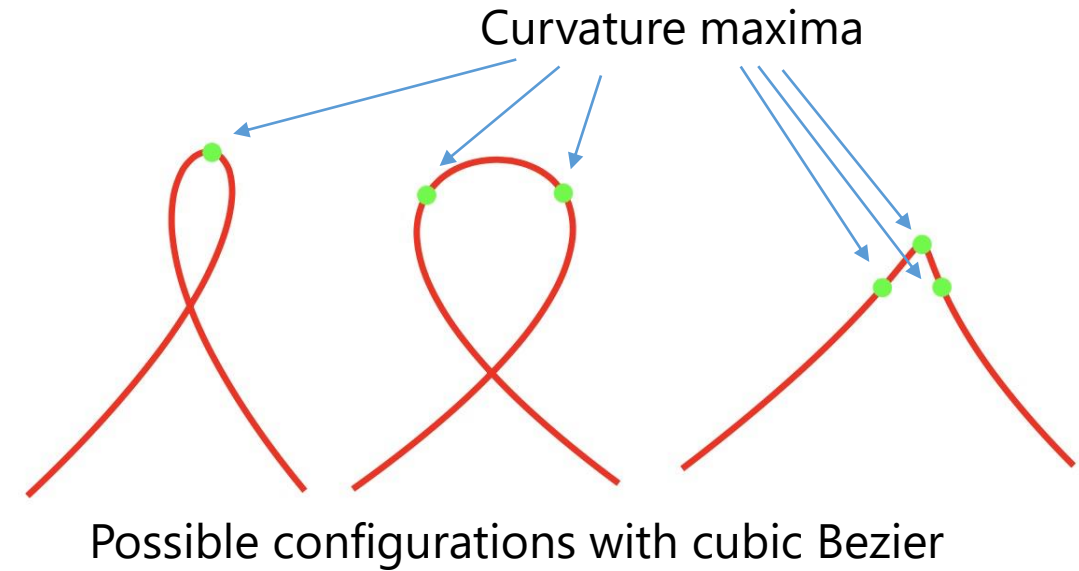
Curvature Tool in Illustrator

<https://www.youtube.com/watch?v=NvyYvj3q1AU>

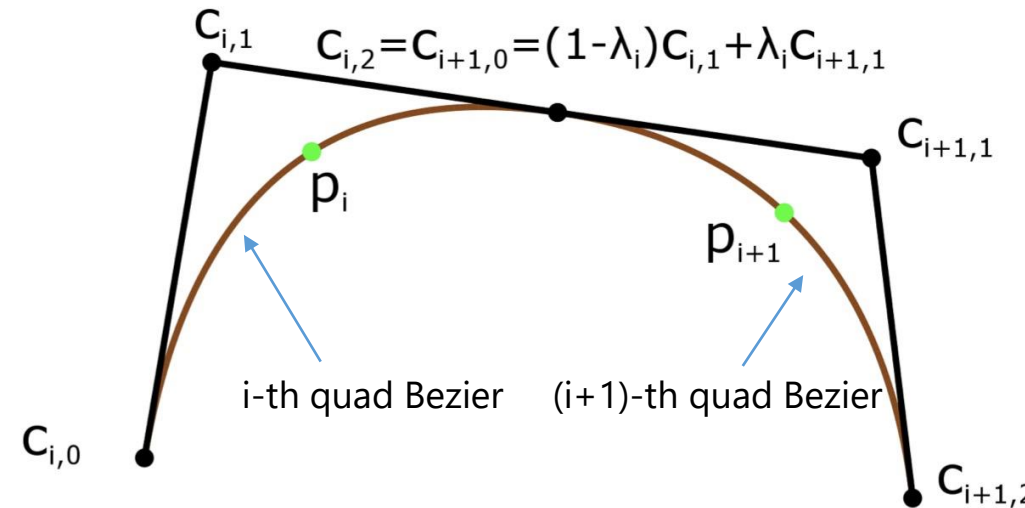


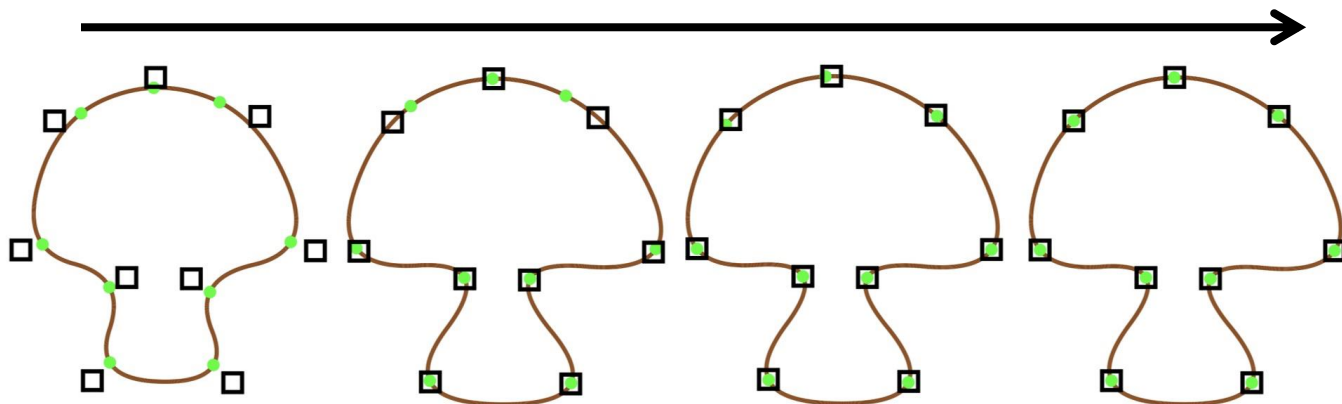
Key ideas of κ -Curves

- Cubic Bezier is difficult to control

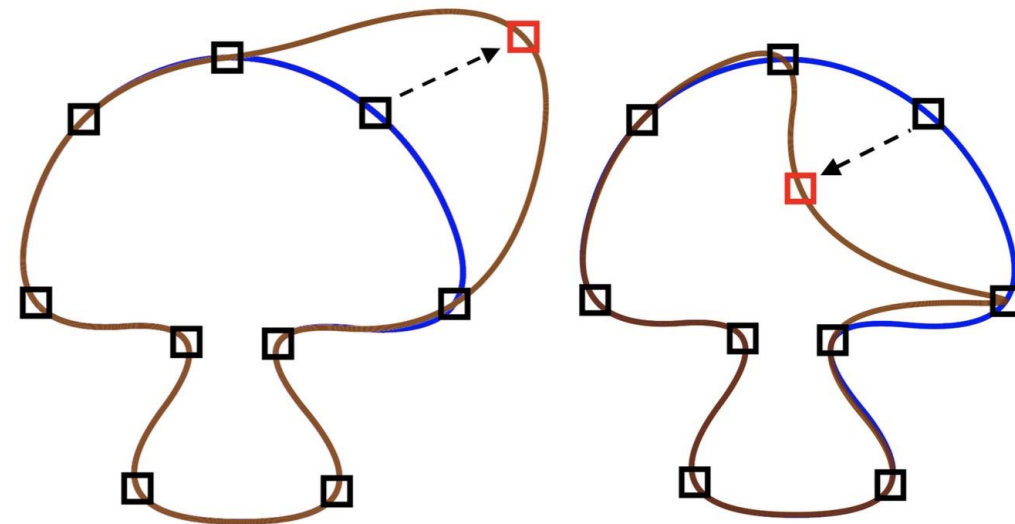


- Actually, *quadratic* Bezier is easier to use!
 - At most one curvature maximum can exist
 - User specifies curvature maxima
→ reverse compute control points of quadratic

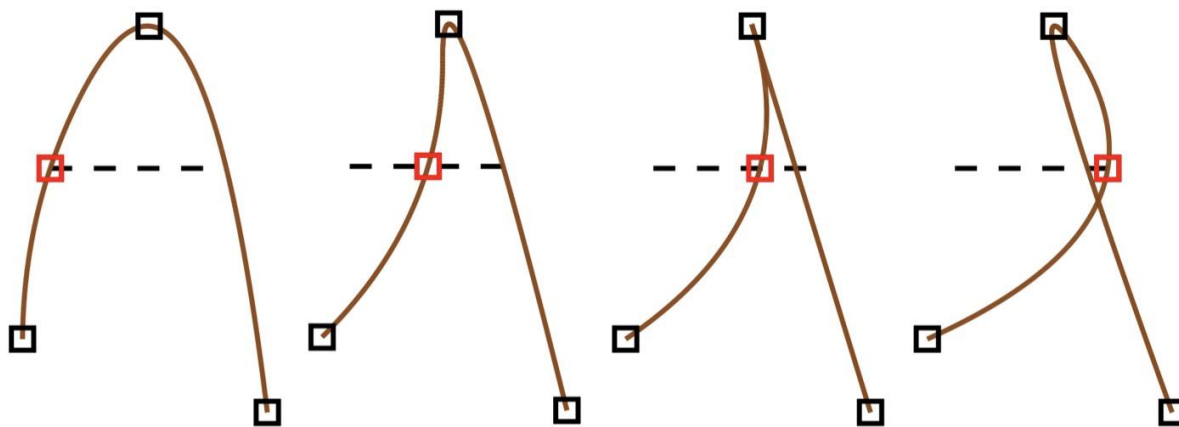




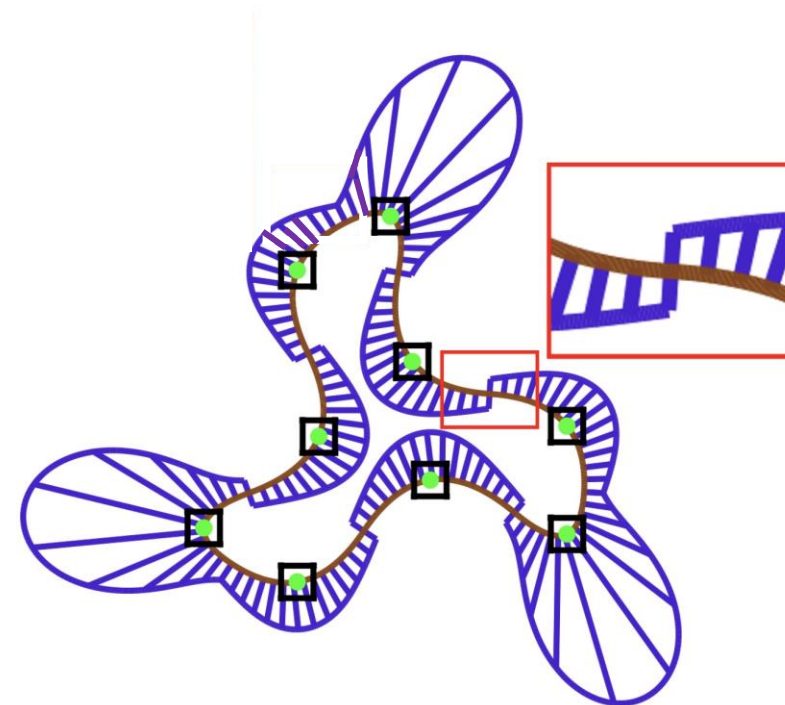
Global/nonlinear formulation = iterative computation



Change of one CP = change of entire shape



"Buckling" always occurs on CPs



Curvature discontinuity at convex/concave boundary₃₅

B-spline

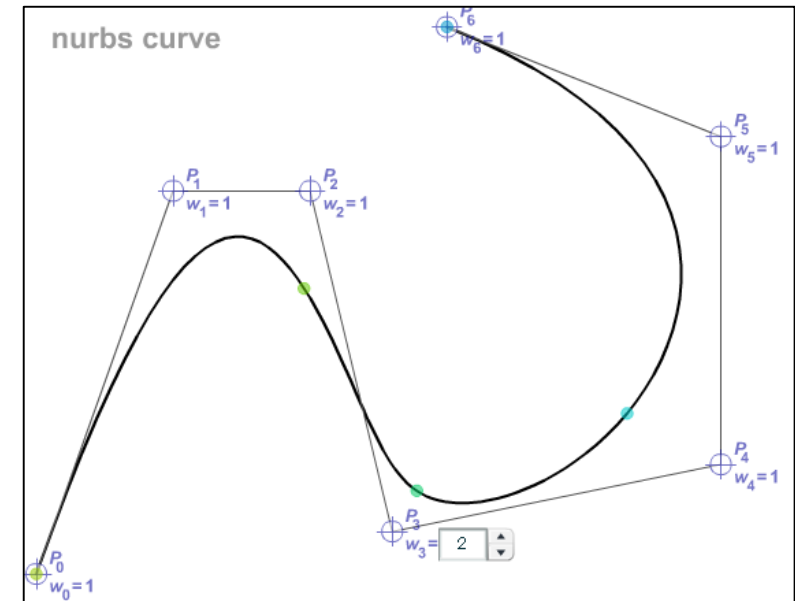
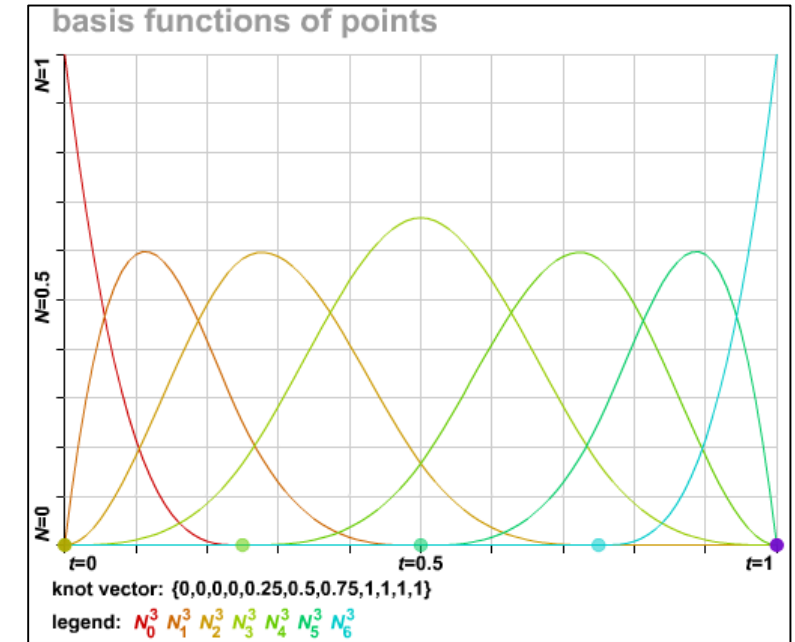
- Another way of defining polynomial spline
 - Represent curve as sum of **basis functions**
 - Cubic basis is the most commonly used
- Deeply related to subdivision surfaces
→ Next lecture

- **Non-Uniform Rational B-Spline**

- Non-Uniform = varying spacing of knots (t_k)
- Rational = arbitrary weights for CPs
- (Complex stuff, not covered)

- Cool Flash demo:

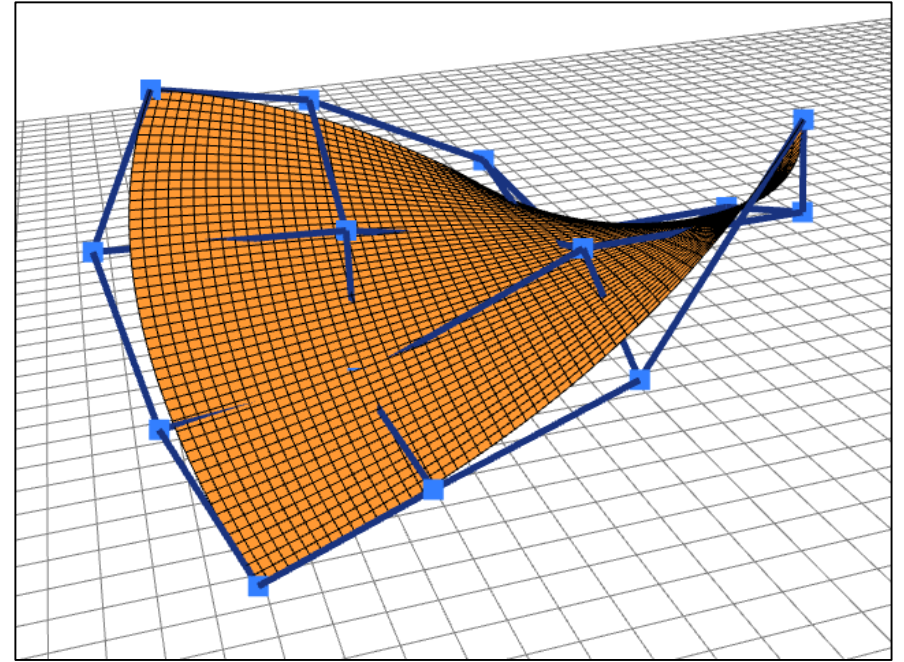
<http://geometrie.foretnik.net/files/NURBS-en.swf>



Parametric surfaces

- One parameter \rightarrow Curve $P(t)$
- Two parameters \rightarrow Surface $P(s, t)$
- Cubic Bezier surface:
 - Input: $4 \times 4 = 16$ control points P_{ij}

$$P(s, t) = \sum_{i=0}^3 \sum_{j=0}^3 b_i^3(s) b_j^3(t) P_{ij}$$



Bernstein basis functions

$$b_0^3(t) = (1 - t)^3$$

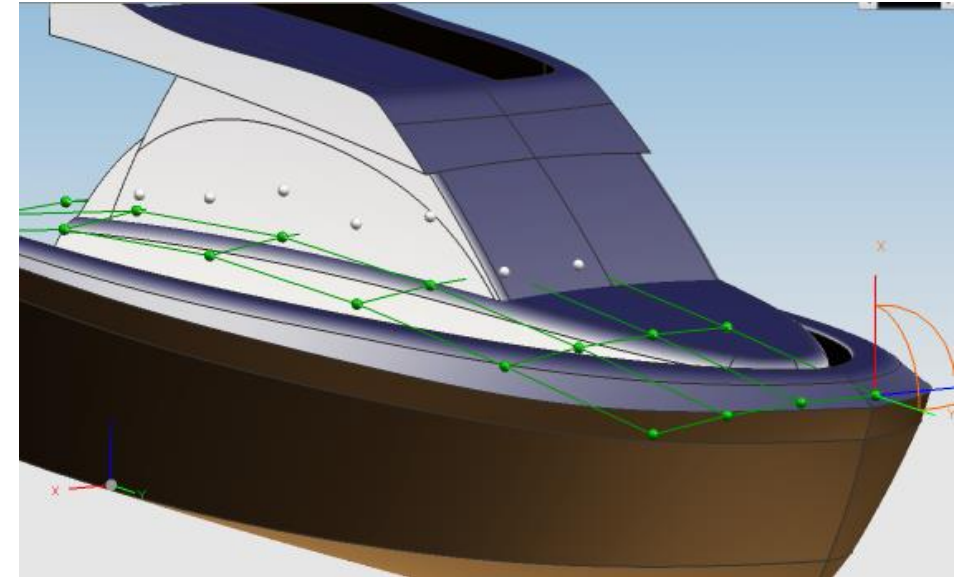
$$b_1^3(t) = 3t(1 - t)^2$$

$$b_2^3(t) = 3t^2(1 - t)$$

$$b_3^3(t) = t^3$$

3D modeling using parametric surface patches

- Pros
 - Can compactly represent smooth surfaces
 - Can accurately represent spheres, cones, etc
- Cons
 - Hard to design nice layout of patches
 - Hard to maintain continuity across patches
- Often used for designing man-made objects consisting of simple parts



Pointers

- http://en.wikipedia.org/wiki/Bezier_curve
- http://antigrain.com/research/adaptive_bezier/
- <https://groups.google.com/forum/#!topic/comp.graphics.algorithms/2FypAv29dG4>
- http://en.wikipedia.org/wiki/Cubic_Hermite_spline
- http://en.wikipedia.org/wiki/Centripetal_Catmull%E2%80%93Rom_spline