

Forelesning 6, kapittel 6

Deformasjoner / tegninger i 3D

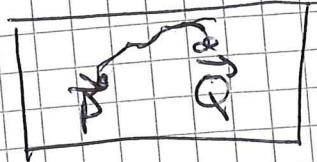
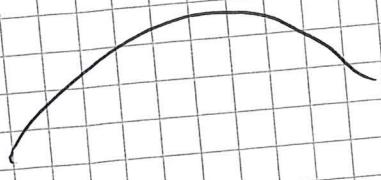
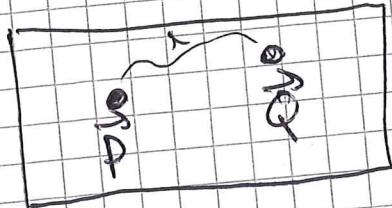
Deformasjoner :

Det er relative

hastighet / forskyvningssforskjeller

$$t = t$$

$$t = 0$$

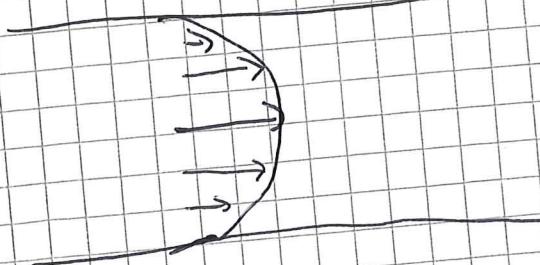


F.eks i en blodåre renner det

fortest i midten, salter mot
kanten

Altså

$$t = 0$$



$$t = t$$

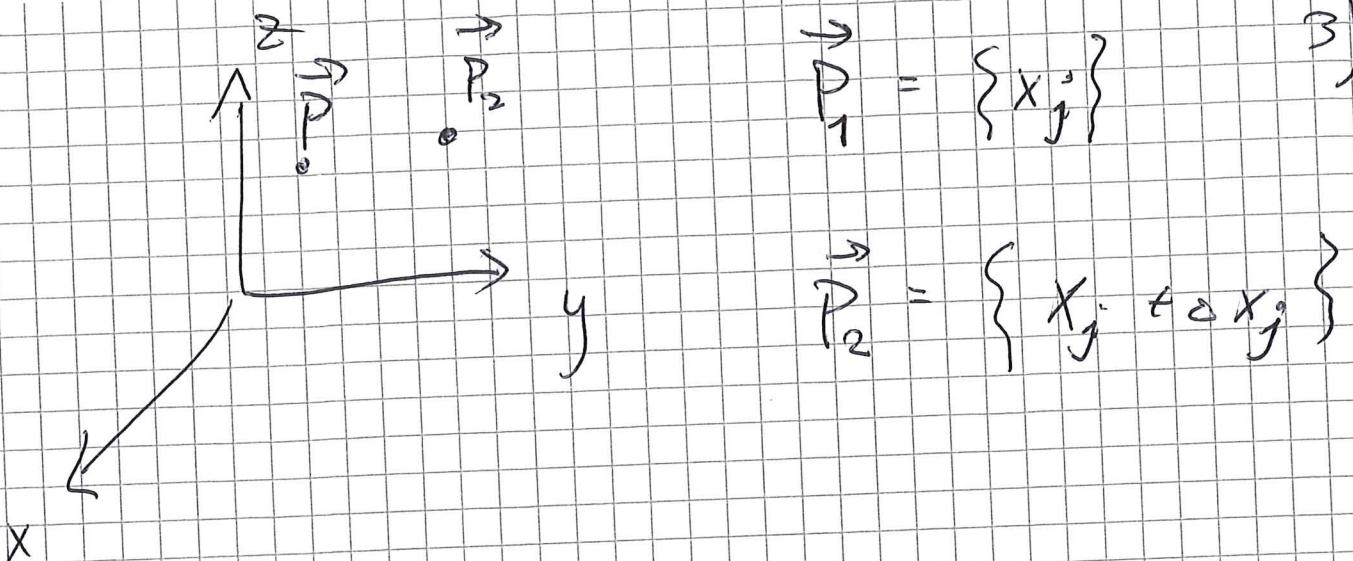


2)

Dersom \vec{P} beveger seg mer
 enn \vec{Q} og de er naboen
 med det næsten bety
 at \vec{P} er utsatt for støtne
 ketter ~~med~~ eller har
 høyre moment enn \vec{Q} .

Persom \vec{Q} er tilstrekkelig mør
 \vec{P} vil \vec{Q} bremse \vec{P}
 og i den prosessen fôr
 store moment.

3)



Felt hastighet

$$\vec{v} = \{v_i\}$$

Forskyvning

$$\vec{u} = \{u_i\}$$

Forskyll \vec{u} i hastighet
mellan P_1 og P_2 er

$$\Delta v_i = v_i(x_j + \Delta x_j, t) - v_i(x_j, t)$$

$$\Delta u_i = u_i(x_j + \Delta x_j, t) - u_i(x_j, t)$$

~~v~~

Legg merke til

notasjonen



V_i: tilnærmer

$$\Delta V_i \approx \frac{\partial V_i}{\partial x_j} \Delta x_j$$

$$\Delta V_i \approx \frac{\partial u_i}{\partial x_j} \Delta x_j$$

Hvor vi har kuttet høyek-ordenstall.

V_i skrives

$$D = \nabla V = \left\{ \frac{\partial V_i}{\partial x_j} \right\} = \begin{pmatrix} \frac{\partial V_1}{\partial x_1} & \frac{\partial V_1}{\partial x_2} & \frac{\partial V_1}{\partial x_3} \\ \frac{\partial V_2}{\partial x_1} & \frac{\partial V_2}{\partial x_2} & \frac{\partial V_2}{\partial x_3} \\ \frac{\partial V_3}{\partial x_1} & \frac{\partial V_3}{\partial x_2} & \frac{\partial V_3}{\partial x_3} \end{pmatrix}$$

$$D = \nabla u = \left\{ \frac{\partial u_i}{\partial x_j} \right\} = \begin{pmatrix} \frac{\partial u_1}{\partial x_1} & \frac{\partial u_1}{\partial x_2} \\ \frac{\partial u_2}{\partial x_1} & \frac{\partial u_2}{\partial x_2} \\ \dots & \dots \end{pmatrix}$$

3 tilfeller med forslyelling

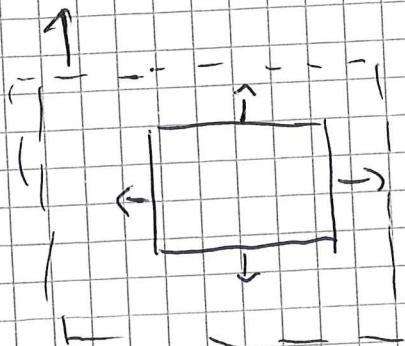
5)

fysisk betydning:

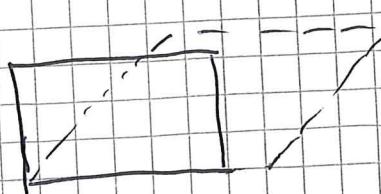
1. Ekspansjon/kontraksjon uten
form endring

2. Deformasjon uten form
volumendring

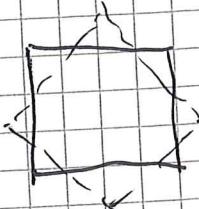
3. Stiv bevegelse
(rotasjon/translasjon)



2.



3



Intuitivt vet vi at

disse tre tingene er forslyellige
og at forslyellige materialer
reager forslyellig.

6)

La oss derfor prøve å skrive

$$D = D_e + D_d + D_r$$

$\uparrow \quad \uparrow \quad \nearrow$

expansjon deformasjon stink bøvelgs

Ren ekspanjon i

7)

$$V_i^o = d X_i \neq c_i \quad \text{origo for ekspanasjonen.}$$

$$\nabla \cdot V = \frac{\partial V_i}{\partial x_i} = 3\alpha.$$

$$\Delta V_i^o \approx \frac{\partial V_i}{\partial x_j} \Delta x_j = \left\{ \begin{array}{l} \alpha \\ \alpha \\ \alpha \end{array} \right\} \Delta x_j = \left\{ \begin{array}{l} \alpha \\ \alpha \\ \alpha \end{array} \right\} \left\{ \begin{array}{l} \Delta x_1 \\ \Delta x_2 \\ \Delta x_3 \end{array} \right\}$$

$$= \left\{ \begin{array}{l} \frac{\nabla \cdot V}{3} \\ \frac{\nabla \cdot V}{3} \\ \frac{\nabla \cdot V}{3} \end{array} \right\} \Delta x_j$$

$$= \frac{\nabla \cdot V}{3} \delta_{ij} \Delta x_j$$

$$\overset{\circ}{D}_e = \left\{ \begin{array}{l} \frac{\nabla \cdot V}{3} \delta_{ij} \end{array} \right\}$$

8)

Stive beregninger

2D:

$$\begin{pmatrix} a - cx \\ b + cx \end{pmatrix} = \begin{pmatrix} a \\ b \end{pmatrix} + \underset{\rightarrow}{C} \begin{pmatrix} x \\ y \end{pmatrix}$$

hvor $\underset{\rightarrow}{C} = \begin{pmatrix} 0 & -c \\ c & 0 \end{pmatrix}$

$\underset{\rightarrow}{C}$ er skyversymmetrisk

$$\underset{\rightarrow}{C} = -\underset{\rightarrow}{C}^T$$

3D:

$$\begin{pmatrix} a \\ b \\ c \end{pmatrix} + \underset{\rightarrow}{C} \begin{pmatrix} x \\ y \\ z \end{pmatrix} = \begin{pmatrix} a \\ b \\ c \end{pmatrix} + C \underset{\rightarrow}{X} \begin{pmatrix} x \\ y \\ z \end{pmatrix}$$

hvor $\underset{\rightarrow}{C}$ er skjær symmetrisk

$$\underset{\rightarrow}{C} = \begin{pmatrix} 0 & e & f \\ -e & 0 & g \\ -f & -g & 0 \end{pmatrix}, \quad C = \begin{pmatrix} e \\ f \\ g \end{pmatrix}$$

Innferer så litt mer fysikk:

9)

$$\vec{r}$$

er

vindekhastighetsvektoren

$$\vec{r} = \begin{pmatrix} r_x \\ r_y \\ r_z \end{pmatrix}$$

$$\Delta \vec{v} = \vec{r} \times \vec{\omega}$$

$$\Delta \vec{v} = \begin{vmatrix} i & j & k \\ r_x & r_y & r_z \\ \Delta x & \Delta y & \Delta z \end{vmatrix}$$

$$= \begin{pmatrix} (r_y \Delta z - r_z \Delta y) i \\ -(r_x \Delta z - r_z \Delta x) j \\ (r_x \Delta y - r_y \Delta x) k \end{pmatrix}$$

eller

$$\Delta \vec{V} = \begin{pmatrix} 0 & -\Delta z & \Delta y \\ \Delta z & 0 & -\Delta x \\ -\Delta y & \Delta x & 0 \end{pmatrix} \begin{pmatrix} \Delta x \\ \Delta y \\ \Delta z \end{pmatrix}$$

Tensoren kan deles i en symmetrisk og en skjær-symmetrisk del

$$\overset{\circ}{D} = \nabla V = \left\{ \frac{\partial v_i}{\partial x_j} \right\}$$

$$= \frac{1}{2} \left\{ \frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right\} + \frac{1}{2} \left\{ \frac{\partial v_i}{\partial x_j} - \frac{\partial v_j}{\partial x_i} \right\}$$

Den symmetriske delen vil vi

bruke mye

i kaller den $\overset{\circ}{\epsilon}$

$$\Rightarrow \overset{\circ}{\epsilon}_{ij} = \frac{1}{2} \left(\frac{\partial v_i}{\partial x_j} + \frac{\partial v_j}{\partial x_i} \right)$$

11)

Vi har at

$$\left\{ \overset{\circ}{\epsilon}_{ij} \right\} = \overset{\circ}{D}_e + \overset{\circ}{D}_d$$

Vi har dessuten at

$\overset{\rightarrow}{\epsilon}(\vec{r}) = \textcircled{0}$ dersom
 \vec{r} er en str. bevægelse.



(2)

$\nabla \cdot$ har en off gjevnin

en dekomponering av

hastighetsgradienten

$$\nabla \vec{V}$$

som er en tensor,

$$\overset{\circ}{D}$$

Tilsvarande kan gjev s

med

$$\nabla \vec{u}$$

som kallas

$$D$$

Altå

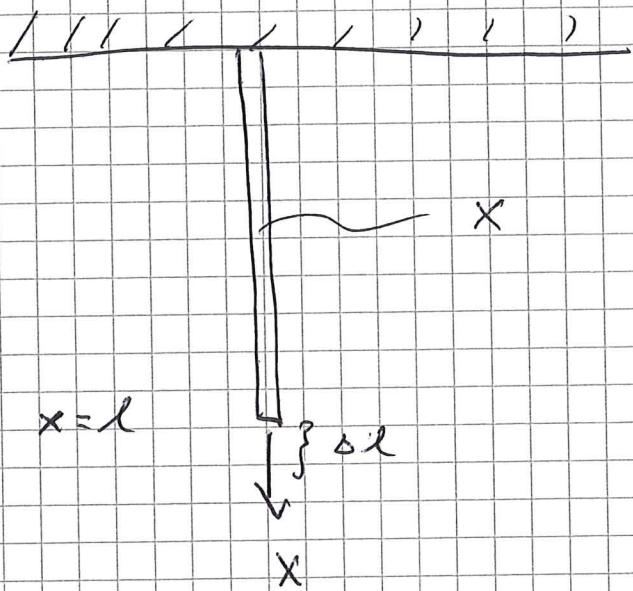
$$\vec{D} = \vec{D}_e + \vec{D}_d + \vec{D}_r$$



høyningstensoren

13)

Eksempler:



Strekking av stav

Efter strekningen v.l ~~strekning~~

$$x(t) = x(0) + \Delta x, \quad \Delta x = \frac{\Delta l}{l} x$$

$$\Rightarrow u = \frac{\Delta l}{l} x$$

Forslaysningen er størst ved $x = l$.

Er kraftene størst der?

Nu:

14)

Tegningsteknisen

$$\left\{ \epsilon_{ij} \right\} = \left\{ \frac{\partial u_i}{\partial x_j} \right\} = \left\{ \begin{matrix} \frac{\Delta l}{l} & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{matrix} \right\}$$

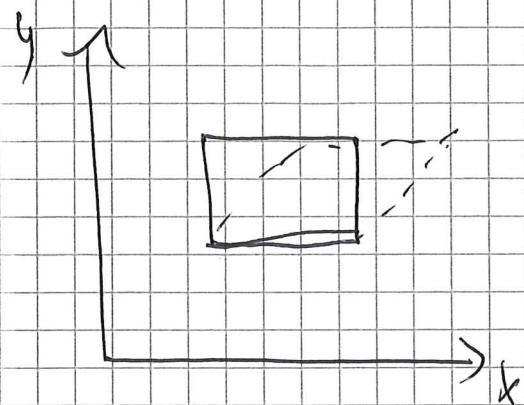
hvor vi her ignorerer faktum

at staven antagelig har blitt

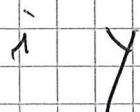
litt
tynne

15

2. Skjørdeformasjoner



forskyvningen i
x-retning er linjær



$$u = \alpha y$$

Person det ikke er forskyvninger

i andre retninger blir

$$\{u_i\} = \begin{Bmatrix} u \\ 0 \\ 0 \end{Bmatrix}$$

$$E_{ij} = \frac{1}{2} (\nabla u + (\nabla u)^T) =$$

$$\frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

$$= \begin{pmatrix} 0 & \frac{1}{2}\alpha & 0 \\ \frac{1}{2}\alpha & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$