

Computational Object-Wrapping Rope Nets

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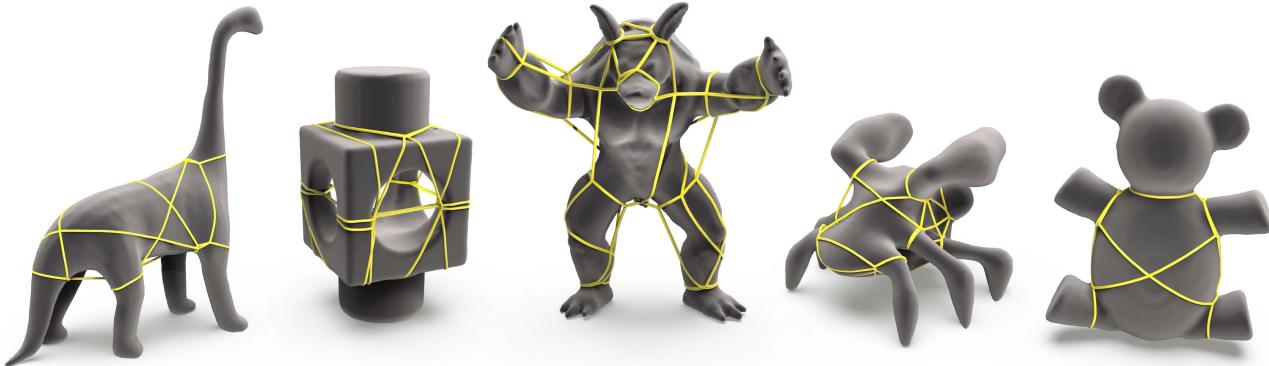


Fig. 1. Example object-wrapping rope nets generated from input 3D surfaces using our fully automatic pipeline.

Wrapping objects using ropes is a common practice in our daily life. However, it is difficult to design and tie ropes on a 3D object with complex topology and geometry features while ensuring wrapping security and easy operation. In this article, we propose to compute a rope net that can tightly wrap around various 3D shapes. Our computed rope net not only immobilizes the object but also maintains the load balance during lifting. Based on the key observation that if every knot of the net has four adjacent curve edges, then only a single rope is needed to construct the entire net. We reformulate the rope net computation problem into a constrained curve network optimization. We propose a discrete-continuous optimization approach, where the topological constraints are satisfied in the discrete phase and the geometrical goals are achieved in the continuous stage. We also develop a hoist planning to pick anchor points so that the rope net equally distributes the load during hoisting. Furthermore, we simulate the wrapping process and use it to guide the physical rope net construction process.

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We demonstrate the effectiveness of our method on 3D objects with varying geometric and topological complexity. In addition, we conduct physical experiments to demonstrate the practicability of our method.

CCS Concepts: • Computing methodologies → Shape analysis;

Additional Key Words and Phrases: Euler tour theorem, rope net, hoisting

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1 INTRODUCTION

Wrapping objects with rope nets finds many applications such as packing, hoisting, and transportation, among others. For example, when hoisting and carrying a sculpture, tying it up with ropes and then lifting up the ropes is historically a common practice and remains to be an economic, safe, and widely adopted solution today [Fu et al. 2017; Nets4You 2019; Sageman-Furnas et al. 2019; US Netting 2019; Wan et al. 2020]. Figure 2 shows a few real-world examples of tightly wrapped rope nets. However, planning and tying up such object-wrapping rope nets, with the requirements of tightness, load balance, and simplicity, is by no means an easy exercise. It heavily relies on human experience and can quickly frustrate a novice practitioner.

In this work, we study the problem of object-wrapping rope nets from both geometric and physical modeling points of views. We propose a computational method for designing rope nets

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Fig. 2. Examples of the object-wrapping rope net applications: Lifting the furniture (left, obtained from internet public domain) and wrapping the statue (right, courtesy of Shunk-Kender).

satisfying a few practical requirements. The main factor to be considered is safeness. We require that the rope net tightly wraps the object and evenly distributes load for safety under the hoisting scheme. Although tight wrapping confines the object movement within the rope net as much as possible, load balancing prevents the object and the rope from breaking. We also hope that the rope net can be composed by a *single* rope and the knotting is as easy as possible. The last aspect is economy. We stipulate that the total length of the rope is minimized.

Given a 3D object represented by a surface mesh, we introduce a simple and robust approach to generate an object-wrapping rope net satisfying the preceding requirements. A rope net is composed of knots and curve edges wired over the surface. Our method is based on two *key design principles*. First, the rope should sling over prominent geometric or topological features of the object surface, such as concave geometric features, forks, and branches, to ensure a safe and reliable tying [Johnson 2016]. Second, we hope the rope net could be composed with a *single* rope.

To make the rope net construction aware of geometric and topological features, we opt to start with a set of key loops induced by the segmentation boundaries of **Shape Diameter Function (SDF)** of the object [Shapira et al. 2007]. SDF is proven to capture well the prominent geometric and topological features of a 3D shape. In achieving single-rope composition, our key observation is that a rope net can be composed with a single rope if each node has a degree of 4 (e.g., has four incident curve edges). This observation has a rigorous theoretical guarantee based on the Euler tour theorem [Bondy and Murty 1976].

To form an evenly distributed rope net over the surface, the sparse key loops are connected with *assistant curves* while satisfying the 4-degree principle. To this end, we build a cross field constrained by the key loop directions. The assistant curves are then constructed from the field directions perpendicular to the key loops.

The preceding process amounts to a discrete-continuous optimization of both the topology and the geometry of the curve network. Although the discrete phase improves the topology of the curve network by selecting proper assistant curves, the continuous stage optimizes the curve geometry via altering the node positions and curve shapes.

In particular, in the discrete step, we design a dedicated algorithm to compute a sparsely distributed, coarse 4-degree

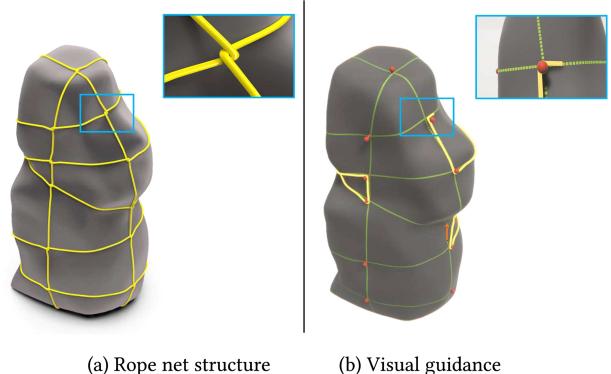


Fig. 3. (a) Our proposed new style (top right) can provide stronger force support for fastening the rope net on the object while remaining simple. (b) An illustration tool is provided to guide the physical rope net construction. The pins (colored in red) are needed to perform the assembly in practice.

initial curve network over the 3D surface through solving a mixed-integer programming problem. Starting with this initial curve network, we conduct an alternating optimization of all node positions to tightly fasten every curve edge by minimizing the length of all curve edges. During this process, a curve edge may leave the surface but is constrained to never penetrate the surface.

In realizing hoisting, we compute anchor points over the curve network so that the rope net is load balanced when being lifted. We develop a hoist planning method that chooses suitable anchors from a set of candidates to meet safety requirements [Johnson 2016]. It minimizes the stretching stress of all curve edges subject to the constraint of the yielding tolerance of rope. Furthermore, when the rope net is too sparse to come up with a suitable hoisting plan, we opt to re-optimize the curve network to add some *reinforcement loops* by tracing through the regions where the stress violates the yielding tolerance. Hence, our method alternates between curve network generation and anchor point selection until a valid hoisting plan is found.

For rope tying, we adopt a twisting knot, a simple and effective knot type for rope net composition (top right of Figure 3(a)). A twisting knot is physically firm while being easy to tie and material saving [Patil et al. 2020]. Note that the one-rope composition property still holds for this twisting knot type based on a rope-able Euler cycle (see Section 5.3 for the proof). In addition, we provide an illustration tool to demonstrate how to compose the rope net intuitively (see Figure 3(b)).

We demonstrate the efficacy of our method through computing rope nets for a variety of 3D objects with complex shapes and topology, and quantitatively evaluating them with a series of metrics. We also conduct physical experiments and present a prototype application in flexible hoisting to show the practical usage of our rope net generation. To sum up, the contributions of our work include the following:

- We solve a new problem of computational object-wrapping rope nets with a series of practical constraints such as safeness and economy.

- 113 • We propose a formulation of the rope net problem based on
 114 curve network optimization.
 115 • We devise a discrete-continuous optimization process that op-
 116 timizes both the topology and the geometry of the curve net-
 117 work.
 118 • We provide an illustration tool to guide users for rope net com-
 119 position and conduct extensive evaluations with not only sim-
 120 ulation but also physical experiments.

121 **2 RELATED WORK**

122 We first review the caging literature, which is highly related to our
 123 rope net wrapping. Then, we review state-of-the-art quad-meshing
 124 approaches since the layout of a quad mesh shares similarities with
 125 our rope net structure.

126 *3D caging.* Caging is to restrict the moving space of a target so
 127 that it will not escape [Diankov et al. 2008]. It has been an impor-
 128 tant topic in robotic research and is often addressed together with
 129 grasping [Diankov et al. 2008; Rodriguez et al. 2011; Wan et al. 2012,
 130 2013]. Caging and grasping of a 2D object have been thoroughly
 131 studied, and we refer the interested reader to the work of Makita
 132 and Wan [2017] for a complete survey.

133 Unlike the 2D caging, the 3D caging problem has no complete
 134 analysis. The main reason is that it is challenging the high dimen-
 135 sionality without considering mechanical implementation. Several
 136 works attempt to tackle the problem using shape analysis and ge-
 137 ometry processing methods. Through the usage of the topological
 138 characteristics of loops of both the objects and the robotic hands,
 139 approaches presented by Dey et al. [2010], Pokorny et al. [2013],
 140 and Stork et al. [2013] plan to cage and grasp on objects with holes.
 141 The method in the work of Zarubin et al. [2013] employs geodesic
 142 balls computed on the target surface to determine the caging re-
 143 gions. They propose circle caging and sphere caging. Whereas cir-
 144 cle caging allows robot hands to grasp the thin part of an object
 145 by computing closed curves wrapping around the object, sphere
 146 caging lets the robot hand wrap a solid part of the object. However,
 147 they do not consider the topological structure of the target. In con-
 148 trast, Kwok et al. [2016] compute a topological Reeb graph over
 149 the 3D surface and extract iso-value rings based on the geodesic
 150 field for the object rope caging. To deal with the common issue
 151 of these methods that the designed caging is oblivious to the rela-
 152 tive size between the target object and the gripper, Liu et al. [2018]
 153 present a method to compute feasible caging grasp that can form
 154 relative-scale-aware caging loops encompassing multiple handles.

155 In our work, we propose to immobilize a 3D target by comput-
 156 ing a tight rope net wrapping over the surface. Unlike caging that
 157 allows object moving and reorienting inside the caging space, our
 158 rope net is tightly fastened on the surface, ensuring the safety and
 159 effortless operation during hoisting big and heavy objects.

160 *Quad layout.* Quad meshing has been researched for more than
 161 two decades [Bommes et al. 2013b], and many approaches have
 162 been proposed. Among the many goals of quad-mesh generation
 163 and processing methods, generating a quad mesh with a coarse and
 164 feature-aligned quad layout is one of the most desired ones [Tarini
 165 et al. 2011a]. Quad meshes can be created either through user in-
 166 teractions [Bommes et al. 2008; Campen and Kobbelt 2014; Marcias

et al. 2015; Takayama et al. 2013], semi-automatic methods [Ji et al. 167
 2010; Tierny et al. 2012; Tong et al. 2006], or fully automatic ap- 168
 proaches [Bommes et al. 2011; Campen et al. 2012; Razafindrazaka 169
 et al. 2015; Tarini et al. 2011a; Zhang et al. 2015]. By tracing edge 170
 flows from irregular vertices of a quad mesh, a coarser quad lay- 171
 out than the quad mesh can be constructed. The dual graph of this 172
 quad layout could be embedded into our pipeline for initializing 173
 our rope net since it satisfies our topology requirement that ev- 174
 ery node has a valence of 4. However, the layouts extracted from 175
 quad meshes generated from existing approaches either are overly 176
 dense, which is impractical for physically composing the rope net, 177
 or require user interactions and are limited to specific types of 178
 shapes. Moreover, all quad-meshing methods optimize the singu- 179
 larities of a quad mesh that greatly affect its layout structure to be 180
 in high curvature regions. However, the dual graph of the layout 181
 may not capture the features well. It may lead to an unstable rope 182
 net. In our work, we propose a simple and effective initial rope net 183
 generation approach that directly addresses our object-wrapping 184
 goal, sidestepping the usually enforced complex geometrical 185
 constraints and misalignment issues during the typical quad meshing. 186
 Later, Figures 24 and 25 demonstrate the advantages of generat- 187
 ing rope nets initialized by our method over representative quad- 188
 meshing approaches. 189

3 OVERVIEW

We first introduce the basic definitions of the rope net, then 191
 state our objectives, and finally give a high-level overview of our 192
 method. 193

Rope net. A rope net $\mathcal{R} = (\mathcal{V}, \mathcal{E})$ wrapping around a 3D surface 194
 model \mathcal{M} consists of a set of nodes, \mathcal{V} , and a set of curve edges, \mathcal{E} 195
 (see Figure 3). 196

Objectives. Our input includes a 3D surface model \mathcal{M} , the cen- 197
 ter of gravity and weight of the model, and a rope with the maxi- 198
 mum stretching stress λ . Our method aims to generate an object- 199
 wrapping rope net used for hoisting by satisfying the following 200
 objectives: 201

- *Simplicity:* The rope net should be cost effective (e.g., short 202
 total length and a small number of nodes and could be com- 203
 posed with a single rope). 204
- *Tightness:* The rope net should be tight enough to both im- 205
 mobilize the object and not slide when lifted from any place of 206
 the rope net (see Figure 5). 207
- *Load balance:* To reduce bearing pressure, the rope net should 208
 equally distribute the load during lifting. 209

To generate a rope net that can be used for hoisting while sat- 210
 isfying the preceding goals, we design our approach by obeying 211
 the principle that tackles one goal at a time and once a goal is 212
 solved, the problem will not appear again. For example, we first 213
 ensure the simplicity of the to-be-generated rope net by generat- 214
 ing an initial rope net that can be composed using a single rope 215
 (Section 4), then achieve the tightness of the rope net on the object 216
 by simulating the tightening process via a geometric optimization 217
 (Section 5), and finally guarantee the load balance of the rope net 218
 through stress analysis and reinforcing weak regions of the rope 219
 net. In our work, we make the following assumptions to allow the 220

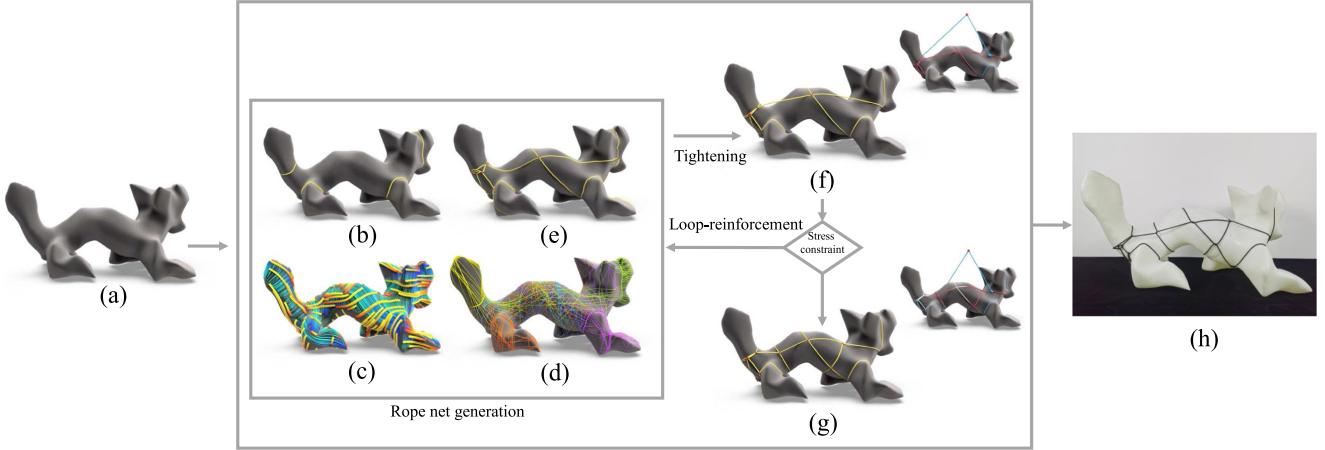


Fig. 4. Overview of our algorithm. Given an input model (a), we generate a rope net step by step. We first capture some key loops (b) that induce a cross field (c). Then, we construct a sufficiently large candidate curve set (d) and take a suitable curve subset as the initialization (e). After that, we refine it to a tight rope net (f) and reinforce the net when necessary (g). The final physically composed result is shown in (h).

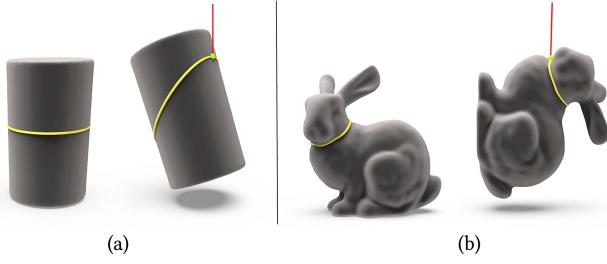


Fig. 5. A tight rope net we target that is able to tightly secure the object without slipping during lifting. The geodesic loop (a) is unstable (easy to slip), although it can be used to cage the object. A stable loop (b) wraps tightly around the object and does not slide during lifting.

221 solving of the rope net generation problem to be tractable: (i) materials are uniformly distributed throughout the object and the rope,
222 and (ii) the object to be hoisted is strong enough to support forces
223 from the rope net.

225 *Pipeline.* Starting from the input object (Figure 4(a)), our ap-
226 proach first relies on a mixed-integer programming to generate an
227 initial rope net that topologically satisfies the one rope construc-
228 tion property and geometrically captures critical regions to immo-
229 bilize the object (Figure 4(b)–(d), Section 4). After that, we perform
230 a tightening step of the rope net to achieve the tightness objective
231 while avoiding any penetrations (Figure 4(f), Section 5), which is
232 followed by a hoisting planning step (Figure 4(g), Section 5.2). We
233 look for a suitable hoisting plan if (i) there are anchor points sat-
234 isfying safety standards in lifting operation [Johnson 2016] and
235 (ii) the stress limit of the rope net is not violated when performing
236 the mechanics analysis of the rope net under the specific hoisting
237 configuration. If no such plan exists, we locate the weakest curve
238 edges that violate the stretch stress limit, and add *reinforcement*
239 *loops* through them as key loops, and iterate the aforementioned
240 steps until a suitable hoisting plan is found. We provide an intu-

itive user interface (Section 5.3, the attached video) to guide the
241 assembly process of the resulting rope net in practice (Figure 4(h)).
242

4 ROPE NET GENERATION

In this section, we generate an initial rope net that satisfies the
244 topology constraint—that is, it can be composed by one rope while
245 wrapping key regions of the object that provides a good starting
246 position for achieving both simplicity and load balancing for fur-
247 ther steps. Our rope net is computed by solving a mixed-integer
248 optimization on a curve network. Intuitively, the curve network is
249 composed of two types of curves: key loops that are critical to im-
250 mobilize the 3D object, and assistant curves that connect key loops
251 to ensure the correct topology of the rope net. Given a surface
252 model, from a view of shape analysis, we first compute key loops
253 (Figure 4(b)) that form a subset of curves of the to-be-constructed
254 rope net, and then we connect these key loops by inserting di-
255 rectional field (Figure 4(c)) guided assistant curves that are pos-
256 sibly redundant (Figure 4(d)), and finally we construct the rope net
257 (Figure 4(e)) by solving a mixed-integer optimization to remove
258 redundant assistant curves.
259

4.1 Key Loops

As discussed earlier, our rope net aims to immobilize the object
261 so that it does not slip during lifting. From the viewpoint of hoist-
262 ing in practice [Johnson 2016], it suggests that the ropes should be
263 tied to the critical wrapping regions (e.g., concave geometric fea-
264 tures, forks, branches) on the surface of an object, which can help
265 to secure the object tightly. Motivated by this finding, we consider
266 wrapping these regions with key loops as critical components of
267 the rope net.
268

To efficiently compute the key loop wrapping the critical re-
269 gions described earlier, we use the SDF-guided mesh partition
270 method [Shapira et al. 2007]. This is because, first, the SDF is
271 defined on facets of the mesh that measures the local object di-
272 ameter. It is used to intrinsically distinguish thin and thick ob-
273 ject parts. Thus, it can generate key loops lying at regions with
274

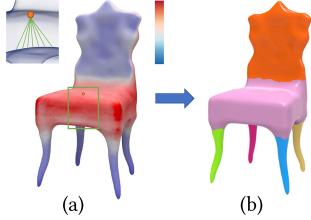


Fig. 6. An example of the SDF-guided mesh partition.

275 concave geometric features, forks, or branches that align well
 276 to the goal of identifying critical wrapping regions. Second, this
 277 method is also proposed to extract the skeleton of a 3D object, of
 278 which any segmentation can infer a branch of the object. Hence,
 279 it can help to generate key loops at the critical wrapping regions
 280 described earlier.

281 To obtain the SDF-based key loops, we followed the partitioning
 282 algorithm described in the work of Shapira et al. [2007]. For
 283 each face of the mesh, the approach first calculates its SDF value to
 284 be the weighted average of the penetration depths of all rays contained
 285 inside an inward cone (Figure 6(a)). The weight for a ray is
 286 the inverse of the angle between the ray and the center of the cone.
 287 Next, the partitioning approach fits k Gaussian distributions to the
 288 distribution of the SDF values of the facets and, finally, finds the
 289 actual partitioning into m clusters using an alpha-expansion graph
 290 cut algorithm [Boykov et al. 2001] by considering local mesh geo-
 291 metric properties. Note that k represents the number of levels of
 292 a segmentation, which is different from m . A large value of k can
 293 result in many small segments of the mesh. In our implementation,
 294 the default value $k = 5$ is used.

295 After running the mesh partition algorithm, the boundary edges
 296 of the segmentation form polyline loops. For a polyline loop, it is
 297 considered as a key loop if it does not share edges with all the other
 298 polyline loops. Otherwise, we choose the minimal loop (the one
 299 with the shortest length) from those polyline loops that share with
 300 edges as the key loop. Thus, the selected polyline loops are denoted
 301 as the key loop set \mathcal{L} (see Figure 6(b)). Note that small loops may
 302 occur due to noises or thin shape features. Since small loops are
 303 not helpful to the rope net design, we filter out these loops from
 304 \mathcal{L} if their lengths are shorter than 0.005 (the input model is scaled
 305 uniformly into a $1 \times 1 \times 1$ box).

306 4.2 Assistant Curves

307 After extracting the key loops \mathcal{L} , we now generate another set of
 308 curves \mathcal{S} , which are referred to as assistant curves, to connect the
 309 key loops. Our to-be-constructed rope net will be composed of all
 310 the key loops and some selected assistant curves.

311 According to the hoisting operation [Johnson 2016], large contact
 312 areas between the rope net and the object can greatly reduce
 313 the stresses on the rope net during hoisting. Based on the empirical
 314 observation, the orthogonal rope net is commonly used in daily life.
 315 The rational behind is that the orthogonal rope net can help distribute
 316 the force evenly, which is very useful for hoisting. Therefore,
 317 our assistant curves are trajectories traced on the surface of the
 318 object. We employ an optimized cross field that aligns directions of
 319 geometric features on the surface to guide the curve tracing. The

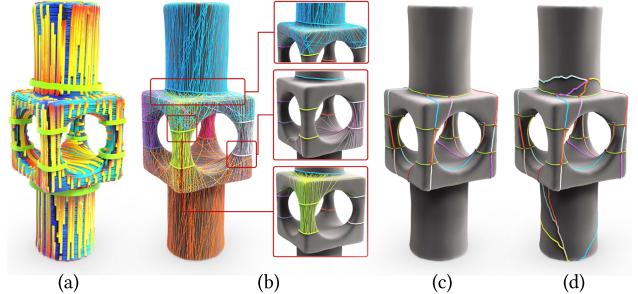


Fig. 7. The workflow of the rope net generation. (a) The cross field aligned with the directions of the key loops (plotted by green circles). (b) The field-guided geodesic curves (plotted by various colors) traced from both two sides of the key loops (colored the same as their curves). (c) We obtain the nodes (red dots) and the curve edges (colored in various colors) between them to compose the rope net by solving a mixed-integer optimization. (d) To guarantee 4-degree connectivity for the nodes on the ending loops, we use a simple linking operation to connect them with random sampling points through Dijkstra shortest paths on the surface model. The obtained curves and the nodes compose the rope net.

320 efficient instant meshes algorithm [Jakob et al. 2015] is used to gen-
 321 erate the directional field. To adapt to the preceding requirement—
 322 that is, generating assistant curves that are perpendicular to key
 323 loop directions so that contact areas between the rope net and the
 324 object can be increased and forces imposed on the rope net can be
 325 distributed over different directions [Johnson 2016], we generate a
 326 key loop direction constrained cross field (Figure 7(a)). Specifically,
 327 for each vertex p , we use a key loop dependent weight instead of
 328 their original one: $w(p) = \exp(-d^2/2)$, where d is the geodesic dis-
 329 tance between p and its nearest key loop. This weight encourages
 330 p to get its direction from its most relevant key loop.

331 After computing the direction field, we can now trace assistant
 332 curves. We start tracing from seed points uniformly sampled on
 333 the key loops. Note that to provide an enough amount of candidate
 334 assistant curves for the rope net generation, the sampling should
 335 be dense. In our experiments, we use the average edge length of
 336 the surface mesh as the step size for the seed point sampling. For
 337 each seed point at each key loop l , we use the field-guided tracing
 338 approach [Pietroni et al. 2016] to trace two curves with opposite
 339 directions (colored the same as their key loop) that are both per-
 340 pendicular to l (Figure 7(b)). Therefore, we have two sets of curves
 341 l^+ and l^- , one for each side of l . We filter out traced curves that are
 342 not ended at any key loop or intersect themselves during tracing,
 343 or both, and denote all the remaining ones as the assistant curve
 344 set \mathcal{S} .

345 So far, the curve network formed by the key loops and the assis-
 346 tant curves is not necessarily simple, and neither satisfies the
 347 topology constraints of the desired rope net. By taking the curve
 348 network as the initialization, we next present a mixed-integer pro-
 349 gramming approach to generate the rope net.

350 4.3 Mixed-Integer Optimization

351 As the 2D illustration in Figure 8, the initial node set \mathcal{V} consists
 352 of the intersection points (blue dots) between the assistant curves
 353 and the intersection points (orange dots) on the key loops. The

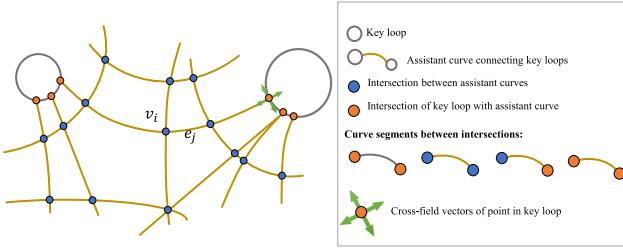


Fig. 8. Illustration of initialization of the curve edges and the nodes. The nodes are initialized with the intersections (blue dots) between the assistant curves (yellow curves) connecting with the key loops (gray circles) and the intersections (orange dots) of the key loops with the assistant curves. The curve edges are initialized with the curve segments between these intersections.

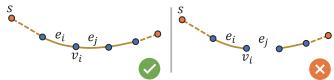


Fig. 9. Two adjacent nodes need to be consecutive in geometry.

354 initial curve edge set \mathcal{E} consists of the curve segments between
355 these intersections.

356 For each curve segment, we define an indicator function $(v_i, e_j) :
357 \mathcal{V} \times \mathcal{E} \rightarrow \{0, 1\}$ to represent its existence in the rope net. $(v_i, e_j) =
358 1$ indicates that the curve segment e_j , of which one endpoint is v_i ,
359 is used to compose the rope net. If $(v_i, e_j) = 0$, that means we
360 do not compose the rope net with e_j . Thus, we turn the rope net
361 generation into the problem of removing curve segments from the
362 curve network, which can be formulated as

$$\max_{v_i, e_j} E(v_i, e_j) \quad (1)$$

s.t. v_i, e_j satisfies the constraints of rope net (3 – 9).

363 Intuitively, we prefer to select long curve segments to reduce the
364 rope net complexity since the longer each segment is, the fewer
365 nodes or knot operations needed to construct the rope net. Hence,
366 the objective function will be formulated as linear energy with vari-
367 able (v_i, e_j) :

$$E(v_i, e_j) = \sum_{i, j} (v_i, e_j) \cdot \|e_j\|, \quad (2)$$

368 where $\|e_j\|$ denotes the length of the curve segment e_j . Next, we
369 introduce the topology constraints and the sparsity constraints to
370 ensure the reliability of the rope net.

371 *Topology constraint I.* The rope net should be a connected graph
372 to be possibly constructed by a single rope (Figure 9). Hence, for an
373 assistant curve s , two consecutive curve segments $e_i, e_j \subset s$ that share
374 one of their endpoints have the constraint $(v_i, e_i) = (v_i, e_j)$,
375 where v_i denotes their shared endpoint. For the two endpoints v_i
376 and v_j of a curve segment $e_j \in \mathcal{E}$, we have a constraint $(v_i, e_j) =
377 (v_j, e_j)$. However, every curve segment e_j on the key loop $l \in \mathcal{L}$
378 has $(v_i, e_j) = 1$ since all key loops need to be present in the rope
379 net. To sum up, we have the connectivity constraints as follows:

$$\begin{aligned} (v_i, e_j) &= (v_j, e_j), \forall e_j \in \mathcal{E}, \text{ where } v_i \text{ and } v_j \text{ are endpoints of } e_j; \\ (v_i, e_i) &= (v_i, e_j), \forall e_i, e_j \subset s \in \mathcal{S}, \text{ where } v_i = e_i \cap e_j; \\ (v_i, e_j) &= 1, \text{ where } e_j \text{ is on the key loop } l, \forall l \in \mathcal{L}. \end{aligned} \quad (3)$$

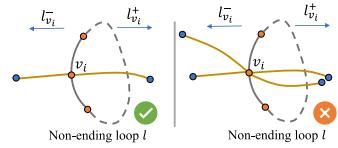


Fig. 10. The constraint of a node on the non-ending loop.

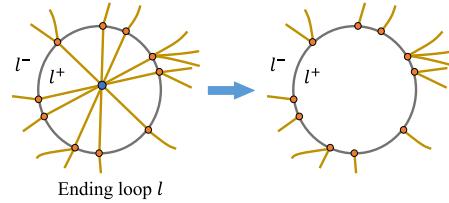


Fig. 11. Illustration of the ending loop. Left: We call a key loop an *ending loop* if all assistant curves on one side of it have endpoints both on the same key loop. Since the assistant curves are generated based on the direction field, they often converge at same intersection point at the ending regions of the branches. Right: For easy post-processing to meet the 4-degree requirement, we remove these curves and connect their nodes back in the post-processing step.

Topology constraint II. A node of the curve network may have an arbitrary valence (i.e., the number of adjacent segments), especially at the ending region of the branches. Since the assistant curves are generated based on the direction field, they often converge at the same intersection point. It is difficult to precisely achieve the 4-degree property for each node during optimization with a consistent topology constraint for all of them. Therefore, we divide the nodes into three cases and impose different constraints for all of them. The constraints are to ensure that the optimized rope net can be easily post-processed to meet the 4-degree requirement.

Case 1. For any node v_i on an assistant curve, we set the constraint

$$0 \leq \sum_j (v_i, e_j) \leq 4, \text{ if } v_i \text{ is on an assistant curve.} \quad (4)$$

After optimization, its valence will be either 0 (not selected), 2 (to be removed by merging its two adjacent curve segments), or 4 (to be preserved as a 4-degree node), due to both constraints Equation (4) and Equation (3).

Case 2. A key loop is called a *non-ending loop* if all connected assistant curves have the two endpoints on different key loops. For a node v_i on a non-ending loop, it should have the same number of curves from each side and at most one from each side (Figure 10). Thus, we set the constraint

$$0 \leq \sum_{e_j \in l^-_{v_i}} (v_i, e_j) = \sum_{e_j \in l^+_{v_i}} (v_i, e_j) \leq 1, \quad (5)$$

if v_i is on a non-ending loop l ,

where $l^-_{v_i}$ and $l^+_{v_i}$ denote the sets of curve segments connecting v_i located at the left and right sides of l , respectively. After optimization, the nodes on the non-ending loops will have the degree being either 2 (to be removed by merging its two adjacent curve segments) or 4 (preserved as a 4-degree node).

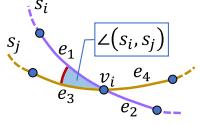


Fig. 12. The angle constraint of the node.

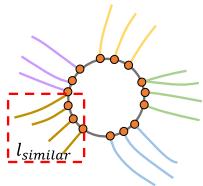


Fig. 13. Similar assistant curves (denoted by same color).

407 Case 3. For a node v_i on an ending loop, some of the connected
 408 curves will have both endpoints on the same key loop (left side
 409 of Figure 11). Therefore, we remove these curves from \mathcal{S} before
 410 optimization and reconnect their nodes in the post-processing step.
 411 During optimization, we formulate the constraint as:

$$2 \leq \sum_j (v_i, e_j) \leq 3, \quad (6)$$

if v_i is on an ending loop.

412 After optimization, the nodes on the ending loops will have de-
 413 grees either 2 (to be removed by merging its two adjacent curve
 414 segments) or 3 (to be preserved as a 4-degree node with the
 415 connected-back assistant curves).

416 *Sparsity constraint I.* To make the rope net as simple as possible,
 417 we need to limit the number of assistant curves passing through
 418 an ending loop by the constraint

$$\sum_{v_i \in l, e_j \subseteq s} (v_i, e_j) = 2k^*, \quad k_1 \leq k^* \leq k_2, \quad \text{if } l \text{ is ending loop,} \quad (7)$$

$$\forall s \in l^+ \cup l^- (l^+ \text{ or } l^- = \emptyset), \quad k_1 \leq k_2 \in \mathbb{N},$$

419 where the parameters k_1 and k_2 indicate the minimum and maxi-
 420 mum number of assistant curves allowed for one curve set l^+ or
 421 l^- , respectively. In our implementation, we set $k_1 = 2$ and $k_2 = 3$.
 422 Thus, the number of nodes on an ending loop is either four or six.

423 *Sparsity constraint II.* The nodes of the rope net should be cross-
 424 like so that the curve edges of the rope net are not too close to-
 425 gether after tightening the rope net. Hence, if the angle between
 426 two assistant curves s_i and s_j at v_i (Figure 12) is smaller than a
 427 threshold θ ($\pi/3$ is used in the implementation), we restrict the
 428 curve segments that are either on s_i or s_j as follows:

$$0 \leq \sum_j (v_i, e_j) \leq 2, \quad \forall e_j \subset s_i \cup s_j, \quad (8)$$

if $\angle(s_i, s_j) < \theta$.

429 *Sparsity constraint III.* Nearby assistant curves with simi-
 430 lar shapes should be clustered as one. Note that to improve efficiency,
 431 we cluster nearby assistant curves that connect to the same key
 432 loop and lie on the same side of that loop into one group (Figure 13).

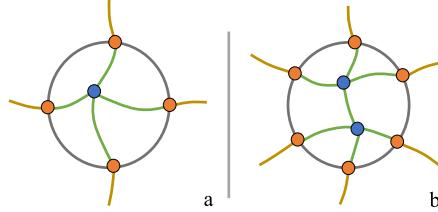


Fig. 14. Post-processing of the ending loop.

At most one assistant curve from each group can be used in the
 433 rope net. This results in the following restriction:
 434

$$0 \leq \sum_{v_i \in l, e_j \subseteq s} (v_i, e_j) \leq 1, \quad \forall s \in l_{\text{similar}}. \quad (9)$$

To cluster the similar assistant curves, we use the K-Means method.
 435 In the implementation, all the assistant curves are converted into
 436 2D embedding by the classical multidimensional scaling (CMDS)
 437 algorithm [Kong et al. 2019]. The distance between the assis-
 438 tant curves is calculated based on the discrete Frechet distance met-
 439 ric [Eiter and Mannila 1994]: $d_{\text{Frechet}}(e_i, e_j) = \min\{\|\Gamma\| \mid \Gamma$
 440 is a coupling between the curve e_i and curve $e_j\}$. The K-Means
 441 method takes the distance measure and the 2D points as inputs,
 442 and outputs the clustering results of assistant curves. To determine
 443 the optimal number of clusters of the K-Means method, we also
 444 use the Elbow method [Ketchen and Shook 1996], which is a fun-
 445 damental step in cluster analysis.
 446

Up to now, we have the necessary topology and sparsity con-
 447 straints for our optimization. We compute the curve segments that
 448 compose the rope net by solving the constrained integer linear pro-
 449 gramming (CILP) problem using the work of Achterberg [2009]. Af-
 450 ter merging the adjacent selected curve segments of the 2-degree
 451 nodes, the rope net then has the remaining nodes with degree 3 or
 452 4 (see Figure 7(c)).
 453

Post-processing. To further obtain the 4-degree rope net (see Fig-
 454 ure 7(d)), we add back the curves with endpoints on the same
 455 ending loop. According to Equation (7), the number of nodes on
 456 the ending loop l is either four or six. If l has four nodes (Fig-
 457 ure 14(a)), we connect them (orange dots) with one sampling point
 458 (blue dot) by Dijkstra's shortest paths (green curves) on the sur-
 459 face. When six nodes are selected on l (see Figure 14(b)), we
 460 sample two different points to connect them by geodesic paths
 461 as well. Each sampling point connects with three nodes along
 462 the clockwise direction of the ending loop. Then we connect the
 463 two sampling points with a geodesic path. Figure 7(d) shows
 464 the result after the post-processing step. Thus, all the 4-degree
 465 nodes and the obtained curves connected to them form the rope
 466 net.
 467

Discussion. The optimization may fail in extreme cases when
 468 the assistant curves are very sparse. For example, if only a few
 469 assistant curves cross through a key loop placed at the region like
 470 a handle, the sparsity constraints of Equation (9) will conflict with
 471 feasibility. However, our algorithm works well for most of our
 472 test examples because we sample a dense curve network before
 473 optimization.
 474

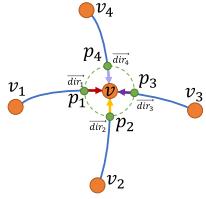


Fig. 15. 4-fork structure at the node.

475 5 ROPE NET CONSOLIDATION

476 Given the rope net generated in the previous section, the rope
 477 net needs to wrap tightly around the object so that it can con-
 478 fine the object movement within it as much as possible. We also
 479 need to find a suitable hoisting plan for the rope net that prevents
 480 overloading of the rope net and satisfies safety under the hoisting
 481 scheme [Johnson 2016]. Moreover, for rope tying in practical us-
 482 age, we need to assemble the rope net and tie the rope into a knot
 483 at each node as well so that it can provide a strong force while
 484 being easy to tie and material saving [Patil et al. 2020].

485 Thus, in this section, we propose a rope net consolidation
 486 method to achieve the preceding requirements. First, to tighten the
 487 rope net, we minimize the length of the rope net while avoiding
 488 any penetrations. Second, to find a suitable hoisting plan, we look
 489 for anchor points that satisfy safety in hoisting operation. From
 490 them, we find a suitable hoisting plan by minimizing the stresses
 491 on the rope net while considering the physical properties of the
 492 rope. If no suitable plan is available, we locate the weak curve
 493 edges that violate the stretch stress limit, add *reinforcement loops*
 494 through them as key loops, and recompute the rope net unit to
 495 find a suitable hoisting plan. Since our rope net can be viewed as
 496 a graph where each node has exactly a degree of 4, we can use a
 497 single rope to construct the rope net according to the theorem of
 498 the Eulerian circuit [Bondy and Murty 1976]. For rope tying, we
 499 adopt twisting knot, which is a simple and effective knot type for
 500 rope net composition. To assemble the rope net for practical usage,
 501 we present a rope-able Euler cycle to guide the assembly process of
 502 the resulting rope net in practice, which guarantees that the rope
 503 net can be constructed by a single rope and each node is tied into
 504 a twisting knot.

505 5.1 Rope Net Tightening

506 To tighten the rope net, we minimize the total length of the rope
 507 net:

$$\min_{\mathcal{V}} \sum_{e_{ij} \in \mathcal{E}} \|e_{ij}\|, \quad (10)$$

508 where e_{ij} denotes the curve edge between adjacent nodes v_i and v_j .
 509 By taking the node set \mathcal{V} as the variables, our optimization alter-
 510 natively moves the nodes with the L-BFGS solver and shrinks the
 511 curve edges $e_{ij} \in \mathcal{E}$ between adjacent nodes. Every curve edge e_{ij}
 512 is updated in each iteration as the shortest collision-free path be-
 513 tween adjacent nodes. The pseudo-code is available in Algorithm 1.
 514 Note that during the optimization, both the nodes and the curve
 515 edges are allowed to leave the surface model rather than strictly
 516 constrained on the surface but are prohibited to penetrate into the
 517 surface model (collision between the rope net and surface model).

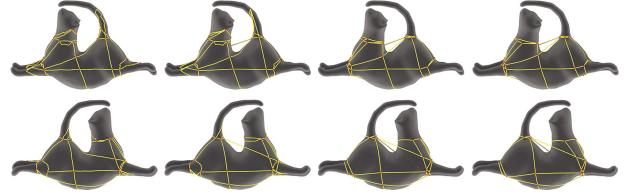
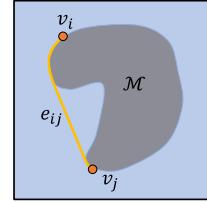
Fig. 16. We only need a few iterations to shrink the initial rope net to a tight one. Here we show the results of the front (top row) and back (bottom row) of an object respectively in the 0th, 1th, 2th, 3th iteration.

Fig. 17. Illustration of collision-free path.

ALGORITHM 1: The algorithm for tightening rope net.

Input: an initial node set \mathcal{V} and an initial rope net configuration \mathcal{E}
Output: a tight rope net \mathcal{R}
 Compute the total length of the rope net $\sum_{i,j} \|e_{ij}\|$;
 Compute the gradients of $\sum_{i,j} \|e_{ij}\|$ w.r.t. each node v_i ;
while the norm of the gradient vector is larger than the specified tolerance **do**
 Move every node $v \in \mathcal{V}$ by Equation (11);
 Update the collision-free path e_{ij} between v_i and v_j by [Crane et al. 2013];
end

Node movement. For a node, the L-BFGS solver moves it from its initial position to a locally stable position by the gradient vectors of the object function (Equation (10)). Suppose every node v is adjacent to four neighboring points p_1, p_2, p_3, p_4 . We use $\vec{\text{dir}}_i = \frac{v-p_i}{\|v-p_i\|}, i = 1, 2, 3, 4$, to represent four unit vectors at the node v of the rope net (Figure 15). Thus, the gradient of each node v is computed as follows:

$$\begin{aligned} \frac{\partial \sum_{e_{ij} \in \mathcal{E}} \|e_{ij}\|}{\partial v} &= \sum_{e_{ij} \in \mathcal{E}} \frac{\partial \|e_{ij}\|}{\partial v} \\ &= \frac{v-p_1}{\|v-p_1\|} + \frac{v-p_2}{\|v-p_2\|} + \frac{v-p_3}{\|v-p_3\|} + \frac{v-p_4}{\|v-p_4\|} \\ &= \sum_{i=1}^4 \frac{v-p_i}{\|v-p_i\|} = \sum_{i=1}^4 \vec{\text{dir}}_i, \end{aligned} \quad (11)$$

where e_{ij} is the curve edge (shortest collision-free path) between the nodes v_i and v_j . To ensure that the rope net does not penetrate the surface model, all nodes should be on or outside the surface. Therefore, during the optimization process, we check the position of each node and pull it onto the surface using [Larsen et al. 1999] if lying inside (leave it alone if it is located on the surface or in the exterior).

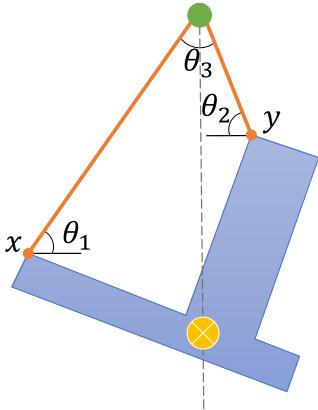


Fig. 18. 2D illustration of our hoist configuration for hoisting an object (blue). Given the object's center of gravity (yellow dot) and one lifting point (green dot) directly above it, we compute a pair of anchor points (orange dots) x and y . The sling angles θ_1 and θ_2 are formed by their slings (orange lines) with the horizontal axis.

Figure 16 shows an example of the optimization process. For this example, it has 51 nodes and each node takes 0.65 seconds on average to run the L-BFGS optimization. Moreover, it only needs 3 iterations (1 iteration refers to all nodes moving once), which is due to the fact that the initial rope net is good enough. In our experiments, the number of iterations required for all models ranges from 3 to 68, with 5 as the average. The cactus example (see Figure 33(c)) requires the most iterations.

Collision-free path. For any two adjacent nodes, we compute the collision-free path using the heat-based method proposed in the work of Cranet et al. [2013]. This method computes the shortest path going through the specified domain (i.e., the surface and the exterior in our problem).

Specifically, in the implementation, we first discretize the space (colored blue) bounded by the surface M and a large box covering the model (drawn by the black rectangle) into a tetrahedral mesh. Figure 17 shows a 2D example. Limiting the path inside the blue space can naturally prevent the penetration of the rope net. We then compute the discrete gradient, divergence, and Laplace operator for the tet-mesh, which are well-established in the work of Desbrun et al. [2008]. Finally, we employ the heat-based method [Crane et al. 2013] to compute the shortest distance field, from which the shortest distance $\|e_{ij}\|$ and the collision-free path e_{ij} can be quickly found. In particular, by running the heat-based method in the tetrahedral mesh of the exterior space, the collision-free path between the node v_i and the node v can be traced along the negative gradient direction, assuming that the distance field is linear in each tetrahedral element. Therefore, the collision-free path consists of a sequence of corner points, each being the intersection between the path and a triangle face of the tetrahedral mesh. In Equation (11), p_1, p_2, p_3, p_4 are four corner points incident to the node v .

5.2 Hoist Planning

So far, we have a rope net that secures the object tightly. Next, we introduce how to use our rope net in lifting practice. Specif-

ically, we consider the most used sling configuration of bridle hitch, where two anchor points are used together to lift an object with one lifting point (Figure 18). The goal is to distribute stresses evenly across the entire rope net to avoid overloading and ensure safety in lifting operation [Johnson 2016].

Our solution is to first search for a set of candidate anchor pairs and then perform mechanics analysis to find the best one, as is done in the industry practice [Johnson 2016]. Note that the lifting point is always located on the object's plumb line, so we do not optimize the lifting point in our algorithm. In our implementation, the lifting point is placed above the object's center of gravity (0.3 as the default height).

Candidate pairs of anchor points. Our guidelines to select the candidate anchors come from the standard constraints [Johnson 2016] in the industry practice:

- The anchor points should be always visible from the lifting point since we never drag the slings over the object surface.
- The object's center of gravity must be not only directly under the lifting point but also below the lowest anchor point before the object being lifted, to reduce the forces on the slings and the anchor points.
- The sling angles of anchors θ_1 and θ_2 (formed by their slings with the horizontal direction) need to be greater than $\pi/4$ and smaller than $\pi/3$.

Given the object's center of gravity (yellow dot) and a lifting point (green dot) directly above it (see Figure 18), we assume that the orientation of the input object conforms to the guidelines as described earlier. The first step is to uniformly sample points on the entire rope net. The unit length of rope (0.001 in our implementation) is taken as the step size for the dense sampling. Next, following the guidelines, we remove the sampling points if they lie beneath the horizontal plane through the center of gravity or the connecting line to the lifting point penetrates the surface model.

For the remaining sampling points, we generate a set of point pairs. Since accurately measuring the sling angle for any free-shape object is difficult, we instead use the angle θ_3 formed at the lifting point [Johnson 2016] (the angle between the two orange lines). For a pair of sampling points, its two points and the lifting point form a triangle. We refer to this pair as a candidate if the object's plumb line passes through the triangle and the angle θ_3 formed at the lifting point is greater than $\pi/3$ and less than $\pi/2$. We denote the set containing all pairs of points as \mathcal{A} .

Mechanics analysis of the rope net. We search for a suitable point pair $(x, y) \in \mathcal{A}$ via mechanic analysis. To ensure safety, the stresses acting on the rope net during lifting should be as small as possible, whereas the stress of each curve edge should not exceed the stress limit of the rope. Therefore, the problem can be formulated as

$$\begin{aligned} & \min_{(x, y) \in \mathcal{A}} E(x, y, \mathcal{R}, F) \\ & \text{s.t. } I(x, y, e, F) < \lambda, \forall e \in \mathcal{E}, \end{aligned} \quad (12)$$

where λ is the yielding point of a specific material (by default we use $\lambda = 5.48e^7 N/m^2$ for elastic). $I(x, y, e, F)$ is the stress of a curve edge $e \in \mathcal{E}$ when taking points x and y as the anchors and applying

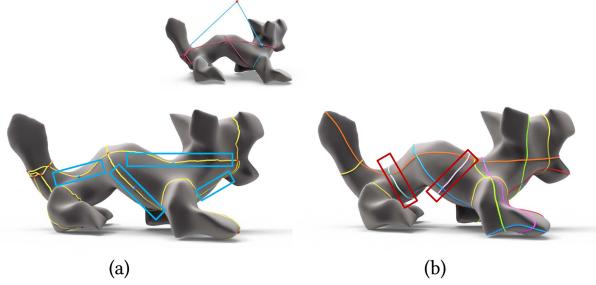


Fig. 19. An example of the loop-reinforcement processing. (a) The weak curve edges (highlighted by the blue rectangles) whose stresses are greater than λ . (b) The non-trivial loops (highlighted by the red rectangles) searched from the traced closed curves (with various colors).

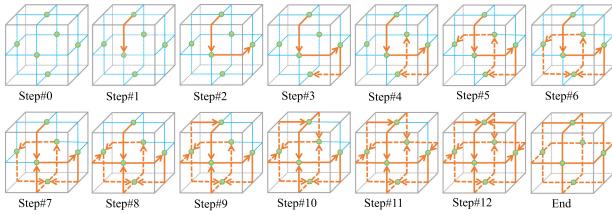


Fig. 20. 2D illustration of the assembling process of our rope-able circuit net. The green dots denote the nodes of rope net and the rope-able circuit net consists of the order lines in orange. The circuit net starts with a first direction for the starting node. Then we turn left or turn right, rather than straight ahead to the next exit direction.

618 the lifting force F . The objective function is then formulated by

$$E(x, y, \mathcal{R}, F) = \int_{e \in \mathcal{E}} I(x, y, e, F) de. \quad (13)$$

619 Our goal is to compute a pair of anchor points so that the rope net
620 is not overloaded and the sum of the stresses on the rope net is
621 minimal.

622 In the implementation, since the mechanical analysis takes on
623 average 3 minutes for each candidate pair, to reduce the time con-
624 sumption, we sort the pairs in set \mathcal{A} in descending order by their
625 angles θ_3 formed at the lifting point. We then select the first 10
626 sampling point pairs in \mathcal{A} as the candidate. Our input consists of
627 a 3D object positioned in a physically simulated environment,
628 a rope net whose material is specified as nylon, and two sampling
629 points called *anchor points*. The lifting forces at the anchor points
630 are determined by the gravity of the object. We compute the stress
631 field of the rope net based on the finite element analyses in a popu-
632 lar FEM software [Abaqus 2018]. Let V_e denote all the elements in
633 the curve edge e . The stress value of the curve edge e is computed
634 as: $I(x, y, e, F) = \max_{t \in V_e} \sigma(t)$, where $\sigma(t)$ is the stress value of
635 the element t in the curve edge e .

636 *Loop-reinforcement processing.* In case no anchor point pair is
637 found that is capable of lifting the object under the safety con-
638 straint, we perform the following reinforcement of the rope net.
639 As shown in Figure 19(a), we find the weak curve edges (high-
640 lighted by the blue rectangles) whose stresses are greater than λ .
641 For every weak curve edge, we first project it onto the surface,
642 and start tracing closed curves passing through the midpoint of

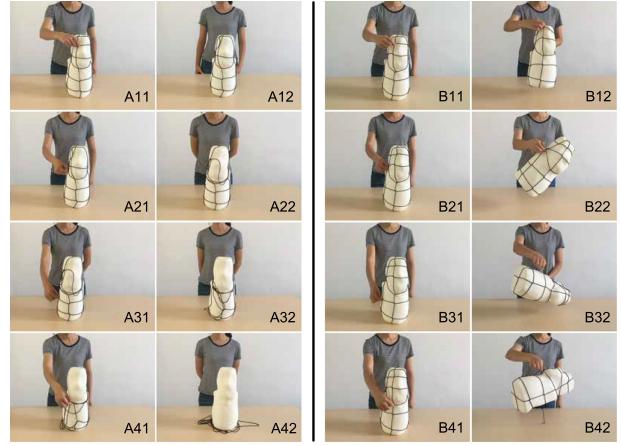


Fig. 21. Comparison to the rope net with various assembling way in physical reliability. The left two columns show the general Euler cycle based rope net before lifting and after shaking at the four different hoisting points in order. The right two columns are the results of rope net with our rope-able Euler cycle.

the projection, guided by the directional field. From the newly
643 traced closed curves (with different colors in Figure 19(b)), we
644 search for non-trivial loops (highlighted by the red rectangles in
645 Figure 19(b)) that are short and field aligned by minimizing the
646 measure described in the work of Campen et al. [2012]: $c_\alpha(l) =$
647 $\sum_{p \in l} \sqrt{\cos^2 \theta(p) + \alpha^2 \sin^2 \theta(p)}$, where $\theta(p)$ is the angle between the
648 loop's tangent and the field direction at the point p on the loop l
649 and $\alpha = 30$ is the balanced parameter. After that, these non-trivial
650 loops, which we call *reinforcement loops*, are added to \mathcal{L} and re-
651 compute the tightened rope net through the approaches described
652 in Section 4 and Section 5.1. Note that we do not add such a non-
653 trivial loop to \mathcal{L} if it intersects with a key loop in \mathcal{L} . Moreover, if
654 two non-trivial loops intersect, we add the shorter one to \mathcal{L} .
655

5.3 Assembly

Our rope net can be seen
656 as a graph with each
657 node has exact a 4 degree.
658 According to the theo-
659 rem of the Eulerian cir-
660 cuit [Bondy and Murty
661 1976], every piece of the graph can be visited exactly once, the
662 starting and ending nodes of the traversal is the same, and the
663 starting node can be chosen arbitrarily. We employ the Fleury algo-
664 rithm [Skiena 1990] that fully exploits these properties to assemble
665 the rope net. However, the constructed rope net using the original
666 Fleury algorithm cannot guarantee to hold the object tight, since
667 the rope is not knotted at the nodes (see the inset, right). We pro-
668 pose to practically construct a *rope-able* circuit net by physically
669 pinning each node to enhance the stability (see the inset, left).
670

Based on the Fleury algorithm, we modify the rope tracing on
671 how to select the in-path and out-path at every node. Each 4-
672 degree node forms a local 4-fork structure located on a plane that
673 allows a counter-clockwise order for the four directions, as in Fig-
674 ure 15. For a node v , we assume the $\overrightarrow{\text{dir}_1}$ is the first entry direc-
675 tion

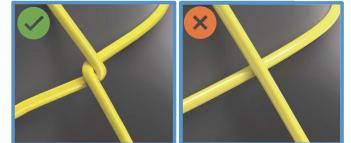




Fig. 22. We compared the final rope net initialized with the dual loops (field-aware geodesic loops) computed in DLM method [Campen et al. 2012] and optimization.

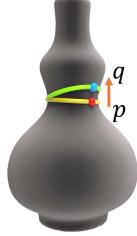


Fig. 23. An example of a perturbation, such as pulling p to q .

for v , and then we choose $-\vec{\text{dir}}_2$ (right turn) or $-\vec{\text{dir}}_4$ (left turn), rather than $-\vec{\text{dir}}_3$ (straight ahead), as the next exit direction. In this way, the algorithm starts from an arbitrary node and chooses the next curve edge at each step as described earlier. It then moves to the other endpoint of the curve edge and deletes the current curve edge. At the end of the algorithm, there are no curve edges left, and the tracing path forms a single-rope based Eulerian circuit. An example of the rope net assembly process can be found in Figure 20.

We conduct a real shaking experiment to compare our rope-able circuit net with the Eulerian circuit generated from the original Fleury algorithm. As shown in Figure 21, our rope net exhibits stable resistance to forces with varying strength and directions, which also demonstrates the physical reliability of our method.

6 RESULTS AND EVALUATION

In this section, we propose a set of metrics (Section 6.2) to quantitatively measure the effectiveness of the computed rope nets for 3D

objects with various complexities. We also perform ablation studies (Section 6.3) and compare to alternative approaches to demonstrate the advantages of our method. Last, we give additional experimental results (Section 6.4) to analyze the performance of the algorithm under the conditions such as different parameters and high genus, and show physical results.

6.1 Implementation

We implement the rope net computation on a 64-bit version of the Win10 system with an Intel CoreTM i7-7700 CPU at 4.2 GHz and 8 GB of memory. We test our algorithm on 37 meshes from Thingi10K [Zhou and Jacobson 2016], the McGill 3D Shape Benchmark [Siddiqi et al. 2007], and the AIM@SHAPE Shape Repository. The computation of our workflow from rope net generation to rope net tightening has an average of 5 to 10 minutes per model.

6.2 Evaluation Metrics

We design a series of evaluation metrics to quantitatively evaluate various aspects of our rope net (i.e., its tightness, stress distribution, and simplicity).

Tightness. Recall that the resulting optimized rope net \mathcal{R} may contain some parts lying in the exterior space but must have at least a point on the surface \mathcal{M} . Let $p \in \mathcal{R}$ be an arbitrary point exactly lying on the surface \mathcal{M} , and let $q \in \mathcal{M}$ be a point in a small neighborhood of p . Generally speaking, if we slightly perturb \mathcal{R} at p (keeping the rope net structure unchanged) such that the new rope net \mathcal{R}_q (we call it q -based rope net) passes through q , the length of the q -based rope net must be greater than or at least equal to that of the p -based rope net since \mathcal{R} is stable (length-minimized), as illustrated in Figure 23. We can compute the length change rate of $\|\mathcal{R}\|$ w.r.t. p by

$$\max_{q \in \text{Neigh}(p)} \frac{\|\mathcal{R}_q\| - \|\mathcal{R}\|}{\|p - q\|},$$

where $\text{Neigh}(p)$ denotes the neighborhood of p on the surface \mathcal{M} . Note that since the rope net is allowed to leave the surface, we use geodesic distance to measure the lengths of the parts of the rope net lying on the surface and use Euclidean distance to compute the lengths of the other parts not on the surface. The tightness of \mathcal{R} can be thus defined by

$$\mathcal{F}_{\text{Tightness}}(\mathcal{R}) = \max_{p \in \mathcal{R} \cap \mathcal{M}} \max_{q \in \text{Neigh}(p)} \frac{\|\mathcal{R}_q\| - \|\mathcal{R}\|}{\|p - q\|}. \quad (14)$$

In implementation, we sample p to be the middle point of each curve edge. For a fixed p , we select the point q along the direction that is orthogonal to the curve edge of the rope net and tangent to the surface. The bigger $\mathcal{F}_{\text{Tightness}}(\mathcal{R})$ is, the tighter the rope net is, indicating that the rope net can tightly secure the target without slipping.

Stress distribution. The stress distribution of a rope net depends on where to lift the rope net and where to wrap the target object. Hence, we compute the stress distribution $\mathcal{F}_{\text{stress}}(\mathcal{R})$ as the sum of the stresses on each curve edge based on formula $E(x, y, \mathcal{R}, F)$ (Equation (13)). The lower value of $\mathcal{F}_{\text{stress}}(\mathcal{R})$, the smaller of the stresses on the rope net, which implies that the rope net can perform the load-balance lifting task better.



Fig. 24. Comparing with the dual layout-based rope net. The final rope nets (a–c) are initialized by IM [Jakob et al. 2015], QF [Huang et al. 2018], and SQD [Tarini et al. 2011a] and tightened using our tightening algorithm.

730 *Simplicity.* We use the number of the rope nodes $|\mathcal{V}|$ and the
 731 length of the rope net $\|\mathcal{R}\|$ to measure the simplicity of the rope
 732 net. It is apparent that the fewer nodes the rope net has, the simpler
 733 the rope net is. For fair comparisons, we uniformly scale the input
 734 model to a $1 \times 1 \times 1$ box.

735 6.3 Ablation Studies

736 Although we cannot find prior work solving the same problem,
 737 we demonstrate the rationality of our designed pipeline by com-



Fig. 25. Comparison on the models with sharp feature and high genus. The rope nets (left column) are the results of the Skeleton-driven method [Usai et al. 2015] and IGM method [Bommes et al. 2013a] taken as initializers and tightened by our tightening algorithm. The rope nets (right column) are our results.

paring our method against a set of possible alternatives using the
 738 proposed metrics. 739

Various key loop strategies. We look into an ablation experiment
 740 that replaces our SDF-based key loop with dual loops (field-aware
 741 geodesic loops) computed in the DLM method [Campen et al. 2012].
 742 We extract dual loops from the quad layout of its results. These
 743 loops automatically construct a rope net that guarantees the 4-
 744 degree property but are not necessarily satisfy the specific rope
 745 net requirements. As shown in Figure 22, our method yields bet-
 746 ter performance in covering the critical wrapping regions of the
 747 rope net. 748

Various initial rope nets. We note that the dual of a quad lay-
 750 out is naturally a curve network with every node having a va-
 751 lence of 4, which can be directly used for the initialization of our
 752 rope net. However, as shown in Figure 24, we compare our gener-
 753 ated rope nets with the ones from instant meshing [Jakob et al.
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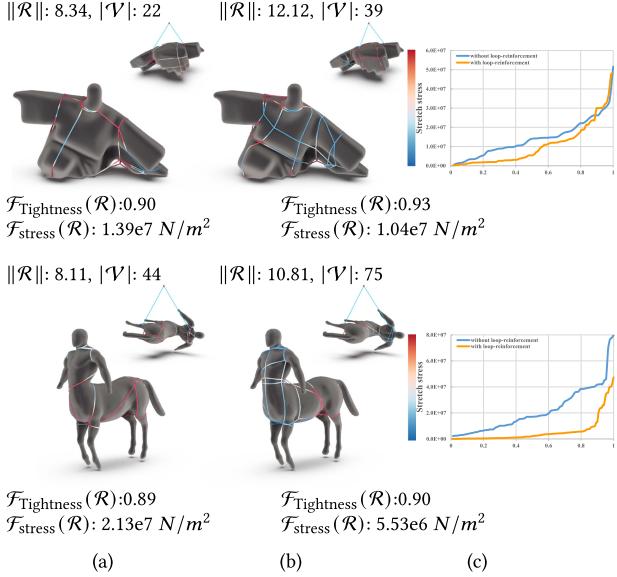


Fig. 26. Comparing the stress distribution of the rope net with (a) and without (b) the loop-reinforcement step under the similar hoisting plan. (c) The distribution of the stress on each edge with and without loop reinforcement. The reinforcing rope nets have smaller maximum stress and perform better in load balancing than those without reinforcements.

2015], feature-aligned meshing [Huang et al. 2018], and simple quad domain [Tarini et al. 2011a], respectively. Our results are considerably simpler and cost less materials for all the models. Moreover, our rope nets capture more easily of the crease regions than the other approaches. The main reason is that our initial rope net generation is directly guided by a shape descriptor that segments parts of an object effectively. The misalignment of the separatrices traced out from irregular vertices is a long-standing problem in quad meshing [Tarini et al. 2011b], and it can lead to arbitrarily long separatrices and a complex quad layout. Even there is no singularity misalignment problem present in the quad layouts, as shown in Figure 25, our results are still simpler since the quad-meshing methods usually need to take into consideration the mesh quality that is irrelevant to our rope net generation.

With vs. without the loop-reinforcement processing. To study the effectiveness of the reinforced rope net with more key loops, we compare our method to itself without any reinforcement. The results of the stress distribution are shown in Figure 26. Note the additional key loops of weak curve edges after applying the reinforcement processing step. Naturally, the rope net becomes denser as demonstrated in Figure 26(b). With the reinforcement step, the stresses distributed over the rope net are much smaller than the one without, as shown in Figure 26.

6.4 Additional Results

Gallery. Our method can compute the rope nets and hoisting plans over 3D models with various complexities. In Figure 27, we show a gallery of examples generated by our method. For each model, its hoisting plan consists of one lifting point (dotted by a red sphere) and a pair of anchor points (dotted by blue spheres) on the rope net.

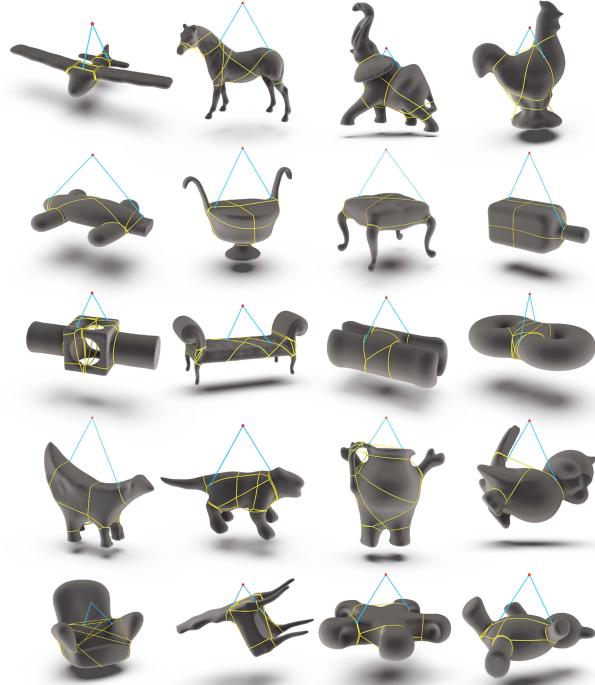


Fig. 27. Gallery of examples generated by our method. We compute the rope nets and hoisting plans over 3D models with various complexities. For each model, its hoisting plan consists of one lifting point (dotted by a red sphere) and a pair of anchor points (dotted by blue spheres) on the rope net.

red sphere) and a pair of anchor points (dotted by blue spheres) on the rope net. 783
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Key parameters. Our approach allows the easy change of parameters k_1 and k_2 in Equation (7) to adjust the simplicity of the generated rope net. In Figure 28, we use different k_1 and k_2 to generate rope nets with varying simplicity. We also expose the variant λ of our method to users for controlling safety aspect during hoisting. As shown in Figure 29, we compare the performances of the rope nets made of carbon fiber (Figure 29(a)) with that made of nylon (Figure 29(b)). Note that when using a strong rope (carbon fiber rope), we can provide a simpler rope net while satisfying the stress constraint. 785
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Robustness to high genus. As shown in Figures 22, 25, and 27, our approach can handle models with high genus. The complexity of the rope net depends on the cross field. High genus shapes often have complicated cross field. We can easily simplify the complexity of such kind of models by wrapping the rope nets around their enveloping surfaces presented by the nested cage [Sacht et al. 2015], as shown in Figure 30. However, this method only can work for high genus shapes with tiny holes since the enveloping surface could cover the small holes. The rope net is still complex if the shape models with many large holes in geometry (see Figure 22 and Figure 25). 795
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Physical results. As shown in Figure 31, we printed 12 models and realized our computed rope nets on the corresponding 806
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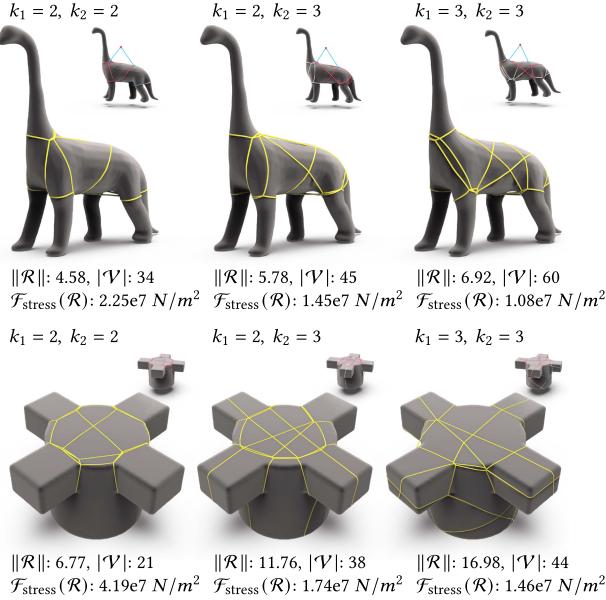


Fig. 28. We can easily vary k_1 and k_2 for different simplicity to generate the rope nets.

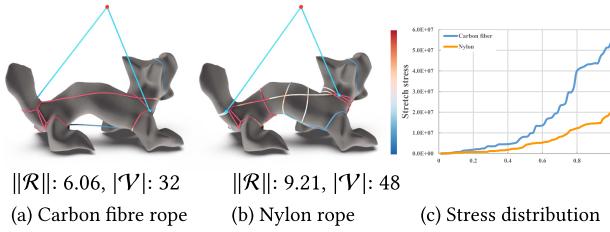


Fig. 29. Our method can incorporate rope usages to generate the rope nets formed by different physical materials.

808 physical objects. We employ four people and provide them with
809 our assembly GUI for constructing the rope net. As expected, ev-
810 ery rope net can be assembled using a single rope. The assembly
811 time ranges from 30 minutes to 180 minutes for one model with an
812 average of 60 minutes over all 12 models.

7 DISCUSSION AND CONCLUSION

813 We introduce an interesting problem of a computational object-
814 wrapping rope net, which not only tightly secures the object in
815 practice but can also be composed with a single rope. We present a
816 shape-aware curve network to effectively solve the problem. Both
817 topology and geometry of the curve network are optimized via a
818 discrete-continuous optimization to satisfy the requirements of the
819 rope net. Through extensive experiments, we demonstrate that our
820 approach is noticeably effective in terms of robustness and gener-
821 ally applicable for 3D models with different shape complexities. Us-
822 ing the visual guidance tool that we provide for users, the assemble
823 property of our rope net is also demonstrated through physical ex-
824 periments. Moreover, our method produces high-quality rope nets
825 for a wide variety of shapes and proposes extensive metrics for the

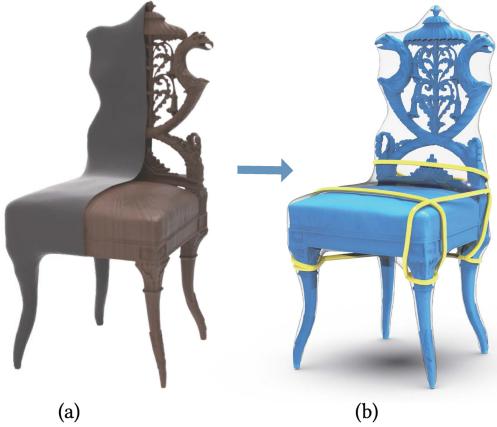


Fig. 30. An example of the simplification process for high genus shapes with many small holes. To simplify the complex of rope net, we compute an enveloping surface (plotted by the gray color) of the original chair model (a) by the nested cage [Sacht et al. 2015] and compute the rope net wrapping on our method (b).

rope net evaluation that can be well generalized to new problem instances. 827
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As a first attempt to solve the new problem, our current solution 829 still has some limitations. Our method starts with the key loop 830 generation, which is such an important step of our pipeline since every 831 other step (e.g., assistant curves, initial rope net, rope net consol- 832 idation) is computed from this initial set of loops. After that, the 833 rope net consolidation step moves the curve edges by minimizing 834 the total length of the rope. However, in some rare cases, the two 835 steps do not connect well, such as in the example of the cactus 836 model (Figure 33(c)), which is due to the requirements of the rope 837 net are not directly embedded in generating the initial key loops. 838 In Figure 33(c), the optimized rope net is quite different from the 839 initial result, indicating that our initial key loops are not helpful 840 for this case. Directly incorporating mechanical aspects into our 841 formulation to find stable key loops would be a better choice. If 842 considering the frictional property of a surface, the rope net, after 843 being shortened, may not be exactly a geodesic net, as shown in 844 Figure 33(d). Then the interesting observation is that the lateral 845 frictional force is proportional to the geodesic curvature. There- 846 fore, in real-life scenarios, the rope net is not a geodesic net even 847 if in the stable state. A promising direction is to solve a coupled 848 problem by jointly learning or optimizing the key loop generation 849 and the rope net consolidation together. 850

However, the heuristic key loop strategy based on the SDF ap- 851 proach is motivated by real-world lifting experience and works 852 well for most shapes, although it still has some space to be im- 853 proved. For example, it may extract no key loops for some extreme 854 cases, such as primitive shapes and very thin parts (see Figure 33(a) 855 and (b)). In addition, it generates inconsistent key loops across var- 856 ious mesh resolutions, resulting in different rope nets of the same 857 object (see Figure 32). Nevertheless, how to obtain the stable loops 858 of 3D objects is an exciting research problem. Our algorithm, in 859 its current form, still lacks enough physics considerations, which 860 needs to be further improved in the future. 861



Fig. 31. Some rope nets physically realized using our method.

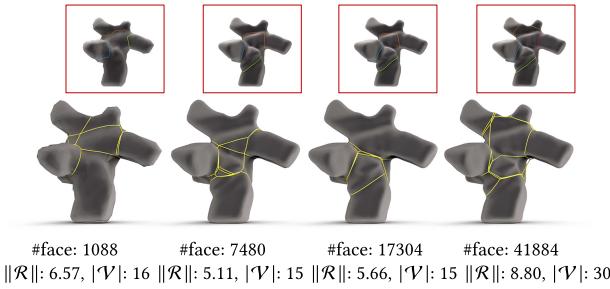


Fig. 32. The number of faces used in the input model can effect its critical wrapping regions extracted by the SDF-based key loops (plotted by various colors in the top row). Although exhibiting similar shape, our rope net is still not invariant to different resolutions.

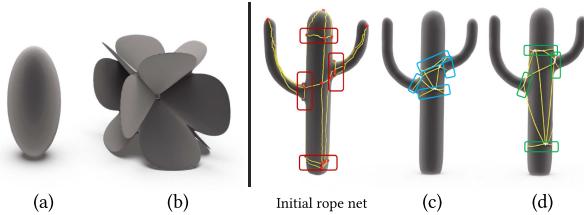


Fig. 33. Limitations of our rope net. Our method may fail for objects where no key loops are extracted such as primitive shape objects (a), and shapes composed with extremely thin features that may break ropes (b). (c) Without considering the frictional coefficient of the surface, the rope net after optimization is far from the initial result. (d) The stabilized rope net when fractional force exists.

862 Interesting results are observed when the input models are sym-
 863 metric. The rope nets tend to be also symmetric. However, our
 864 current approach does not explicitly guarantee this property. We
 865 also believe that this would be a future work of our algorithm.

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