

Handwritten Notes

Below are some handwritten notes that helped me in completing the project. They're ordered as follows.

#1: Runge-Kutta Method: As there were no chapters in Chopra that presented how to lay out the iteration loops for the Runge-Kutta Fourth-Order Method, a YouTube lecture (cited in the Report) showing a pseudocode was used extensively to create a script specific to single degree of freedom structures to dynamic response.

#2: Stiffness Matrix Condensing: The chimney displacement example presented in Chopra assumes that the reader knows how to derive a statically condensed stiffness matrix, and I go through the process in the notes of deriving the text's stiffness matrix, while noting the patterns in the matrix so that it is programmable depending on the amount of degrees of freedom the user chooses.

#3: Eigenvector calculations: Assuming that ϕ_{11} equals 1, I found out by writing out the matrices by hand, that the rest of the ϕ 's can be found by crossing out the 1st row, and the 1st column, and then inverting the matrix.

#4: Fast Fourier Transform: Concepts discussed with Prof. Loh on Fast Fourier Transform, and Power Spectral Density Function have been neatly organized into a single sheet.

Runge-Kutta Method

$$dv1 = h * F(t, x, v)$$

$$me \Rightarrow dv(i) = \Delta t * \left(\frac{(p_{i-1})}{m} - rkc * v_{i-1} - rkk * u_{i-1} \right)$$

$\underbrace{\hspace{10em}}_{F(t, x, v)}$

$$du_1(i) = \Delta t * v_{i-1}$$

$$dv_1(i) = \Delta t * \left(\frac{(p_{i-1})}{m} - c * \dot{u}_{i-1} - k * u_{i-1} \right)$$

$$du_2(i) = \Delta t * (\dot{u}_{i-1} + \ddot{u})$$

$$\checkmark du_{1i} = \Delta t * v_{i-1} \checkmark$$

Full step

$$\checkmark dv_{1i} = \frac{\Delta t}{m} \left[\frac{p_{i-1}}{m} - c * v_{i-1} - k * u_{i-1} \right]$$

$$\checkmark du_{2i} = \Delta t * \left[v_{i-1} + \frac{dv_{1i}}{2} \right]$$

Calculate out to linear interpolation

$$\checkmark dv_{2i} = \frac{\Delta t}{m} \left[\frac{1}{2} (p_i + p_{i-1}) - \frac{c}{m} \left(v_{i-1} + \frac{dv_{1i}}{2} \right) - \frac{k}{m} \left(u_{i-1} + \frac{du_{2i}}{2} \right) \right]$$

$$\checkmark du_{3i} = \Delta t * \left(v_{i-1} + \frac{dv_{2i}}{2} \right)$$

$$\checkmark dv_{3i} = \frac{\Delta t}{m} \left[\frac{1}{2} (p_i + p_{i-1}) - \frac{c}{m} \left(v_{i-1} + \frac{dv_{2i}}{2} \right) - \frac{k}{m} \left(u_{i-1} + \frac{du_{3i}}{2} \right) \right]$$

$$\checkmark du_{4i} = \Delta t * (v_{i-1} + dv_{3i})$$

Full step

$$\checkmark dv_{4i} = \frac{\Delta t}{m} \left[\frac{p_i}{m} - \frac{c}{m} (v_{i-1} + dv_{3i}) - \frac{k}{m} (u_{i-1} + du_{3i}) \right]$$

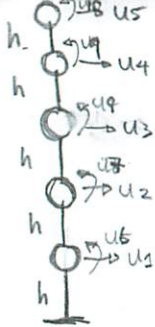
$$du_i = [du_{1i} + du_{2i} + du_{3i} + du_{4i}] / 6$$

$$dv_i = [dv_{1i} + dv_{2i} + dv_{3i} + dv_{4i}] / 6$$

$$u_i = u_{i-1} + du_i$$

$$\phi * g = (u) \rightarrow sm.$$

$$\phi * g$$



Stiffness Matrix
Condensing

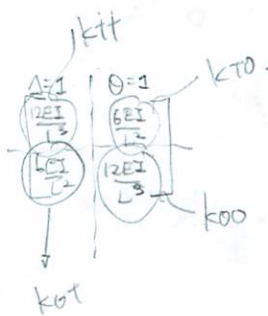
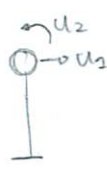
k_{tt} k_{to}
 k_{ot} k_{oo}

	1	2	3	4	5	6	7	8	9	10
1	$\frac{24EI}{L^3}$	$-\frac{12EI}{L^3}$	0	0	0	$\frac{6EI}{L^2}$	$-\frac{6EI}{L^2}$	0	0	0
2	$-\frac{12EI}{L^3}$	$\frac{24EI}{L^3}$	$-\frac{12EI}{L^3}$	0	0	$\frac{6EI}{L^2}$	0	$-\frac{6EI}{L^2}$	0	0
3	0	$-\frac{12EI}{L^3}$	$\frac{24EI}{L^3}$	$-\frac{12EI}{L^3}$	0	0	$\frac{6EI}{L^2}$	0	$-\frac{6EI}{L^2}$	0
4	0	0	$-\frac{12EI}{L^3}$	$\frac{24EI}{L^3}$	$-\frac{12EI}{L^3}$	0	0	$\frac{6EI}{L^2}$	0	$-\frac{6EI}{L^2}$
5	0	0	0	$-\frac{12EI}{L^3}$	$\frac{24EI}{L^3}$	0	0	0	$\frac{6EI}{L^2}$	$\frac{6EI}{L^2}$
6	0	0	0	0	0	$\frac{8EI}{L}$	$\frac{2EI}{L}$	0	0	0
7	0	0	0	0	0	$\frac{2EI}{L}$	$\frac{8EI}{L}$	$\frac{2EI}{L}$	0	0
8	0	0	0	0	0	0	$\frac{2EI}{L}$	$\frac{8EI}{L}$	$\frac{2EI}{L}$	0
9	0	0	0	0	0	0	0	$\frac{2EI}{L}$	$\frac{8EI}{L}$	$\frac{2EI}{L}$
10	0	0	0	0	0	0	0	0	$\frac{2EI}{L}$	$\frac{4EI}{L}$

k_{71} :

	$\Delta=1$	$\theta=1$	$\Delta=1$	$\theta=1$
Shear @ L	$\frac{12EI}{L^3}$	$\frac{6EI}{L^2}$	$-\frac{12EI}{L^3}$	$\frac{6EI}{L^2}$
Moment @ L	$\frac{6EI}{L^2}$	$\frac{4EI}{L}$	$-\frac{6EI}{L^2}$	$\frac{2EI}{L}$
Shear @ R	$-\frac{12EI}{L^3}$	$-\frac{6EI}{L^2}$	$\frac{12EI}{L^3}$	$-\frac{6EI}{L^2}$
Moment @ R	$\frac{6EI}{L^2}$	$\frac{2EI}{L}$	$-\frac{6EI}{L^2}$	$\frac{4EI}{L}$

$ph(0, i)$



$$k = k_{tt} - k_{ot} \cdot k_{oo}^{-1} \cdot k_{to}$$

$$\frac{6EI}{L^3} - \frac{6EI}{L^2} \cdot \frac{1}{\frac{8EI}{L} + \frac{2EI}{L}} \cdot \frac{6EI}{L^2}$$

$$\frac{6EI}{L^3} - \frac{6EI}{L}$$

$$w_1 = 1.7011$$

$$[K - w_1^2 M]$$

$$\begin{bmatrix} \phi_{11} \\ \phi_{21} \\ \phi_{31} \\ \phi_{41} \\ \phi_{51} \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

Figuring out eigenvector (ϕ) vector calculations.

$$\begin{bmatrix} 595322 & -376627 & 151062 & -37758 & 6295 \\ -376627 & 463028 & -338964 & 132199 & -22031 \\ 151062 & -338964 & 444355 & -301111 & 81845 \\ -37758 & 132199 & -301111 & 311998 & -115393 \\ 6295 & -22031 & 81845 & -115393 & 50575 \end{bmatrix} \begin{Bmatrix} 1 \\ \phi_{21} \\ \phi_{31} \\ \phi_{41} \\ \phi_{51} \end{Bmatrix} = \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$

C q D

Concept behind Fourier Series

Amp_1, f_2
 $+ \text{Amp}_2, f_2$
 $+ \text{Amp}_1, f_3$

$$\sum_8 \text{ or } \sum_5 = 22$$

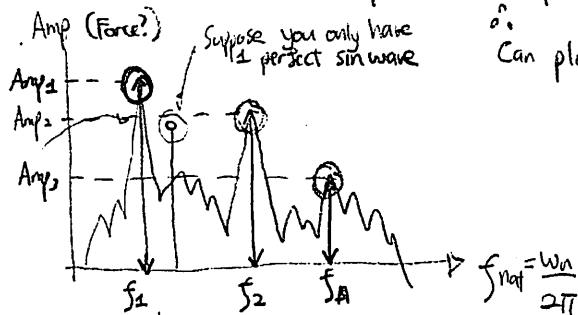
$$\omega_n = \left[\text{rad/s} \right]$$

$$f_n = \frac{\omega_n}{2\pi} \left[\frac{1}{\sqrt{1-\zeta^2}} \right]$$

how many waves pass

Every sin curve has an amplitude & frequency

Can plot how amplitude varies along frequency.



Matlab \Rightarrow $\text{FFT}(\text{signal})$ \Rightarrow produces complex #

$$z = a + bi$$

WANT TO DO. look.

Power Spectral Density Function: allows you to plot real and complex value. and just plot as frequency

It's discrete: how to get 45, range of freq, so on and so forth.

Should expect:

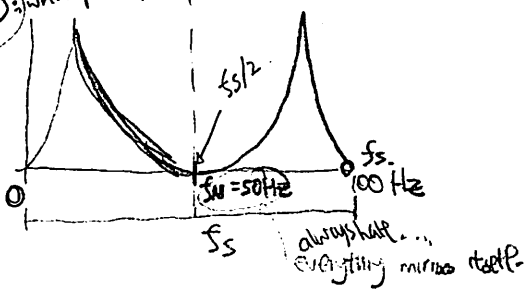
time step - discretizes. -

a lot has to do w. sampling rate = $\frac{1}{\Delta t} = 100 \text{ Hz} = f_s$

should be the norm of this -
(SD) when possible

Time step = Δt

0.01s



$f_N = \frac{1}{2} f_s$: Nyquist frequency

- effectively only cure about left hand.

