```
S k1[i] = HsVd2 VECT6[i] - iHsVm VECT6[i]
al m Vd d1[i] = iAnew[0] \times HsVd1 VECT6[i]
a2_mVd_d2[i] = iAnew[1] \times HsVd2_VECT6[i]
lamc_M_S1_k1_esti[i] = S1_k1_esti[i] × ilambda
Clock 9-14:
Output_diff[i] = S_k1[i] - S1_k1_esti[i]
Clock 15-23:
Vd s alVdl[i] = iHsVd VECT6[i] - a1 m Vd dl[i]
Vd_s_a1Vd1_s_a2Vd2[i] = Vd_s_a1Vd1[i] - a2_m_Vd_d2[i]
mVolt 6x1 3 = Output diff
mTransf MAT6x6 3 = i Almatrix s lambda
mVolt 6x1 2 = Output_diff
mTransf_MAT6x6_2 = i_L2_esti
Clock 18-23:
S1_esti_correct[i] = L1 × Output_diff[i] // L1 = iAnew[2]
Clock 24-32:
S2 esti correct[i] = L2 × Output diff[i] // L2 = iAnew[3]
Clock 25-30:
S1 esti[i] = lamc M S1 k1 esti[i] + S1 esti correct[i]
Clock 34-39:
S2 esti[i] = S1 k1 esti[i] + S2 esti correct[i]
allamc m S1 esti[i] = a1 s lamc × S1 esti[i] // a1 s lamc =
iAnew[4]
Clock 41-46:
```

Clock 0-5:

```
Vd_s_a1Vd_s_a2Vd2_p_a1lamc_m_S1_esti[i] =
    Vd s a1Vd1 s a2Vd2[i] + a1lamc m S1 esti[i]
a2 m S2 esti[i] = iAnew[1] \times S2 esti[i]
Clock 49-54:
u before Binv[i] = Vd s a1Vd s a2Vd2 p a1lamc m S1 esti[i] +
a2 m S2 esti[i]
Clock 56-67:
one p Betam m westi d1[i] = one p Betam × westi d1[i]
Betam_m_w2esti_d1[i] = iBeta_m × w2esti_d1[i]
w1 before correct[i] = westi d1[i] + w2esti d1[i]
Clock 64:
mVolt 6x1 4 = u before Binv
mTransf_MAT6x6_4 = i_inv_B // B^{-1}
Clock 92-93
w correct = Rst 6x6 6x1 3
w2 correct = Rst 6x6 6x1 2
Clock 101-118:
westi[i] = w1 before correct[i] + w correct[i]
w2esti[i] = w2esti_d1[i] + w2_correct[i]
Clock 133:
u_before_w = Rst_6x6_6x1_4
Clock 134-147:
  u_total_new[i] = u_before_w[i] - westi[i]
```

```
westi_d1[i] ≤= westi[i]
w2esti_d1[i] ≤= w2esti[i]
S1_k1_esti[i] ≤= S1_esti[i]
S2_k1_esti[i] ≤= S2_esti[i]
HsVd2_VECT6[i] ≤= HsVd1_VECT6[i]
HsVd1_VECT6[i] ≤= iHsVd_VECT6[i]
```

FPGA 控制器核心數學運算表達式

1. 基本控制變數定義

狀態變數:

• S_k : 追蹤誤差 (tracking error)

• S₁ : 狀態估測器輸出

• S_2^{esti} : 延遲狀態估測器

• w^{esti}: 擾動估測

• w₂^{esti}: 二階擾動估測

2. 主要控制律運算

Step 1: 追蹤誤差計算

$$S_k = V_d - V_m$$

Step 2: 前饋控制

$$V_{\rm ff} = V_d - a_1 \times V_{d-1} - a_2 \times V_{d-2}$$

Step 3: 狀態估測誤差

$$e = S_k - S_1^{\text{esti}_{k-1}}$$

Step 4: 估測器更新

$$\begin{split} S_1^{\text{esti}} &= \lambda_c \times S_1^{\text{esti}_{k-1}} + L_1 \times e \\ \\ S_2^{\text{esti}} &= S_1^{\text{esti}_{k-1}} + L_2 \times e \end{split}$$

Step 5: 回饋控制

$$u_{\mathrm{fb}} = (a_1 - \lambda_c) \times S_1^{\mathrm{esti}} + a_2 \times S_2^{\mathrm{esti}}$$

Step 6: 控制輸入(未解耦)

$$u_{\mathrm{before}} = V_{\mathrm{ff}} + u_{\mathrm{fb}}$$

Step 7: 矩陣解耦

$$u_{\rm decoupled} = B^{-1} \times u_{\rm before}$$

Step 8: 擾動補償

$$u_{\rm final} = u_{\rm decoupled} - w^{\rm esti}$$

3. 擾動估測器運算

擾動估測更新:

增強版本 (with β_m):

$$w_1^{\text{before}} = (1 + \beta_m) \times w^{\text{esti}_{k-1}} + \beta_m \times w_2^{\text{esti}_{k-1}}$$

4. 關鍵系統參數

固定參數:

- $a_1 = 1.595052025060797$ (來自系統極點 p_1)
- $a_2 = -0.599079946700523$ (來自系統極點 p_2)
- $\lambda_c = 0.9391$ (控制頻寬 1000 Hz)
- $\lambda_w = 0.7304$ (估測器頻寬 **5000 Hz)**
- β_m: 模型參數 (可調)

5. 估測器增益計算

Augmented Version (當前活躍版本):

$$L_1 = -\left(-\beta + (1+\beta)^2 - 4(1+\beta)\lambda_w + 6\lambda_w^2 - \frac{\lambda_w^4}{\beta}\right)$$

$$\begin{split} L_2 &= - \Bigg(1 + \beta - 4 \lambda_w - (1 + \beta) \frac{\lambda_w^4}{\beta^2} + 4 \frac{\lambda_w^3}{\beta} \Bigg) \\ L_3 &= \text{tune_L3} \end{split}$$

(來自 ThreeD sine theta)

iAnew 參數映射:

- iAnew[0] = a_1 = 1.595052025060797
- $iAnew[1] = a_2 = -0.599079946700523$
- iAnew[2] = L_1 (單一增益值)
- iAnew[3] = L_2 (單一增益值)
- iAnew[4] = $a_1 \lambda_c$

6. 矩陣運算

解耦矩陣 B^(-1):

$$B^{-1} = \begin{pmatrix} 1254.4 & 365.9 & 362.7 & 509.3 & 510.7 & 478.1 \\ 354.7 & 1162.4 & 387.9 & 669.9 & 692.5 & 448.6 \\ 427.5 & 453.9 & 1258.9 & 439.3 & 488.0 & 520.8 \\ 442.5 & 654.6 & 353.8 & 1460.7 & 800.5 & 448.8 \\ 414.2 & 572.5 & 337.4 & 687.5 & 1274.4 & 374.7 \\ 412.2 & 400.9 & 368.5 & 474.4 & 407.4 & 1371.6 \end{pmatrix} \times L_3$$

擾動估測矩陣:

A1matrix_s_lambda =
$$B^{-1} \times L_1$$

L2 esti = $B^{-1} \times L_2$

7. 完整控制輸入計算流程 (Control Effort Computation) Step 1: 追蹤誤差計算

$$\delta \boldsymbol{v}[k] = \boldsymbol{v}_d[k] - \boldsymbol{v}_m[k]$$

Step 2: 前饋控制項 (Feedforward)

$$v_{\text{ff}}[k] = v_d[k+1] - a_1 v_d[k] - a_2 v_d[k-1]$$

Step 3: 估測追蹤誤差 (使用增強狀態估測器)

$$\widehat{\delta v}[k] = \hat{s}_1[k]$$

Step 4: 回饋控制項 (Feedback)

$$\delta \boldsymbol{v}_{\mathrm{fb}}[k] = (a_1 - \lambda_c) \widehat{\delta \boldsymbol{v}}[k] + a_2 \widehat{\delta \boldsymbol{v}}[k-1]$$

Step 5: 總控制輸入(未解耦)

$$oldsymbol{v}_{ ext{total}}[k] = oldsymbol{v}_{ ext{fb}}[k] + \delta oldsymbol{v}_{ ext{fb}}[k]$$

Step 6: 矩陣解耦與擾動補償

$$oldsymbol{u}[k] = oldsymbol{B}^{-1} oldsymbol{v}_{ ext{total}}[k] - \hat{oldsymbol{w}}[k]$$

其中 B^{-1} 為預先計算的解耦矩陣, $\hat{w}[k]$ 來自擾動估測器

Step 7: 最終控制輸出 (Control Effort)

$$\boldsymbol{u}_{\text{final}}[k] = \boldsymbol{B}^{-1} \left[\boldsymbol{v}_d[k+1] - a_1 \boldsymbol{v}_d[k] - a_2 \boldsymbol{v}_d[k-1] + (a_1 - \lambda_c) \widehat{\delta \boldsymbol{v}}[k] + a_2 \widehat{\delta \boldsymbol{v}}[k-1] \right] - \hat{\boldsymbol{w}}[k]$$

此控制輸入將產生磁通:

$$\varphi[k] = \boldsymbol{B}\boldsymbol{u}_{\text{final}}[k]$$

進而產生磁力:

$$oldsymbol{f}_m = g_{arphi} oldsymbol{arphi}^T oldsymbol{L}(oldsymbol{p}) oldsymbol{arphi}$$

iAnew

```
Anew[0][0] = Almatrix[0][0] = 1.595052025060797
Anew[0][1] = A2matrix[0][0]=-0.599079946700523;
Anew[0][2] = 1 + beta_model + Almatrix[0][0] - 4 * lambda_w;
Anew[0][3] = lambda_w*lambda_w*lambda_w*lambda_w / (A2matrix[0][0] * beta_model) + 1;
Anew[0][4] = Almatrix[0][0] - lambda_inner;
```

Augmented Version (活躍版本): $\operatorname{tune}_{\mathrm{L}1} = -\left(-\beta + (1+\beta)^2 - 4(1+\beta)\lambda + 6\lambda^2 - \frac{\lambda^4}{\beta}\right)$ $\operatorname{tune}_{\mathrm{L}2} = -\left(1 + \beta - 4\lambda - (1+\beta)\frac{\lambda^4}{\beta^2} + 4\frac{\lambda^3}{\beta}\right)$ $\operatorname{tune}_{\mathrm{L}3} = \operatorname{ThreeD_sine_theta}$

其中: $\beta = \text{beta_model}, \lambda = \text{lambda_w}$

```
其他版本(已註解):
// Simple version (PT3DView.cpp line 3321-3322, 3324-3325)
tune L1 = 2 * lambda w - 1 - beta model;
tune L2 = lambda w*lambda w / beta model - 1;
// Polynomial version (PT3DView.cpp line 3332-3333)
tune L1 = (lambda w - 1)*(lambda w - 1)*(lambda w - 1)*(lambda w
+ 3);
tune L2 = -(lambda w - 1)*(lambda w - 1)*(lambda w -
1)*(lambda w - 1);
// M-delay version (PT3DView.cpp line 3326-3327)
tune L1 = ((2*lambda w -
(1+beta_model))*((1+beta_model)*(A1matrix[0][0]-lambda_inner) +
beta_model)
          - (lambda w*lambda w - beta model)*(A1matrix[0][0]-
lambda inner))
          / ((1+beta_model)*(A1matrix[0][0]-lambda_inner) +
beta_model
          + (Almatrix[0][0]-lambda_inner)*(Almatrix[0][0]-
lambda inner));
tune L2 = ((2*lambda w - (1+beta model))*(A1matrix[0][0]-
lambda inner)
          + (lambda w*lambda w - beta model))
          / ((1+beta model)*(A1matrix[0][0]-lambda inner) +
beta model
          + (Almatrix[0][0]-lambda inner)*(Almatrix[0][0]-
lambda inner));
```

inv B

```
inv_B = [
  [1254.4, 365.9, 362.7, 509.3, 510.7, 478.1],
  [ 354.7, 1162.4, 387.9, 669.9, 692.5, 448.6],
  [ 427.5, 453.9, 1258.9, 439.3, 488.0, 520.8],
  [ 442.5, 654.6, 353.8, 1460.7, 800.5, 448.8],
  [ 414.2, 572.5, 337.4, 687.5, 1274.4, 374.7],
  [ 412.2, 400.9, 368.5, 474.4, 407.4, 1371.6]
* tune_L3;
```

Almatrix s lambda

```
Almatrix_s_lambda = [
    [1254.4, 365.9, 362.7, 509.3, 510.7, 478.1],
    [ 354.7, 1162.4, 387.9, 669.9, 692.5, 448.6],
    [ 427.5, 453.9, 1258.9, 439.3, 488.0, 520.8],
    [ 442.5, 654.6, 353.8, 1460.7, 800.5, 448.8],
    [ 414.2, 572.5, 337.4, 687.5, 1274.4, 374.7],
    [ 412.2, 400.9, 368.5, 474.4, 407.4, 1371.6]
] * tune_L1 * tune_L3;
```

L2_esti

```
L2_esti = [
    [1254.4, 365.9, 362.7, 509.3, 510.7, 478.1],
    [ 354.7, 1162.4, 387.9, 669.9, 692.5, 448.6],
    [ 427.5, 453.9, 1258.9, 439.3, 488.0, 520.8],
    [ 442.5, 654.6, 353.8, 1460.7, 800.5, 448.8],
    [ 414.2, 572.5, 337.4, 687.5, 1274.4, 374.7],
    [ 412.2, 400.9, 368.5, 474.4, 407.4, 1371.6]
] * tune_L2 * tune_L3;
```

論文理論算法數學表達式總結

1. 六輸入六輸出磁通控制系統 (Six-Input-Six-Output Magnetic

Flux Control)

系統離散模型 (方程式 6):

$$v_m[k+1] = a_1 v_m[k] + a_2 v_m[k-1] + B\{u[k] + w[k]\}$$

其中:

• v_m : 6×1 Hall sensor 電壓向量

• u: 6×1 控制輸入向量

• w: 6×1 擾動向量

• $a_1 = 0.9898, a_2 = 0.6053$ (系統極點)

• B: 6×6 輸入矩陣

2. 控制律設計 (方程式 7)

控制目標: $\delta v[k+1] = \lambda_c \delta v[k]$, 其中 $0 \le \lambda_c < 1$

控制律:

$$oldsymbol{u}[k] = oldsymbol{B}^{-1}\{oldsymbol{v}_{ ext{ff}}[k] + \delta oldsymbol{v}_{ ext{fb}}[k]\} - \hat{oldsymbol{w}}[k]$$

前饋控制:

$$v_{\rm ff}[k] = v_d[k+1] - a_1 v_d[k] - a_2 v_d[k-1]$$

回饋控制:

$$\delta \boldsymbol{v}_{\mathrm{fb}}[k] = (a_1 - \lambda_c) \widehat{\delta \boldsymbol{v}}[k] + a_2 \widehat{\delta \boldsymbol{v}}[k-1]$$

3. 追蹤誤差動態 (方程式 8)

$$\delta \boldsymbol{v}[k+1] = \lambda_c \delta \boldsymbol{v}[k] - \boldsymbol{B} \boldsymbol{e}_w[k] + (a_1 - \lambda_c) \boldsymbol{e}_{\text{delta v}}[k] + a_2 \boldsymbol{e}_{\text{delta v}}[k-1]$$

其中:

• $e_w = w - \hat{w}$: 擾動估測誤差

• $e_{\text{delta v}} = \delta v - \hat{\delta v}$: 狀態估測誤差

4. 增強狀態估測器 (方程式 9)

$$\begin{split} \hat{s}_1[k+1] &= \lambda_c \hat{s}_1[k] + \boldsymbol{L}_1 \{ \delta \boldsymbol{v}[k] - \hat{s}_1[k] \} \\ \hat{s}_2[k+1] &= \hat{s}_1[k] + \boldsymbol{L}_2 \{ \delta \boldsymbol{v}[k] - \hat{s}_1[k] \} \\ \hat{w}[k+1] &= \hat{w}[k] + \delta \hat{w}[k] + \boldsymbol{L}_3 \{ \delta \boldsymbol{v}[k] - \hat{s}_1[k] \} \\ \delta \hat{w}[k+1] &= \delta \hat{w}[k] + \boldsymbol{L}_4 \{ \delta \boldsymbol{v}[k] - \hat{s}_1[k] \} \end{split}$$

5. 估測器回饋矩陣 (方程式 11)

$$\begin{split} \boldsymbol{L}_1 &= (2 + a_1 - 4\lambda_e)\boldsymbol{I} \\ \boldsymbol{L}_2 &= \left(1 + \frac{\lambda_e^4}{a_2}\right)\boldsymbol{I} \\ \boldsymbol{L}_3 &= -(1 - \lambda_e)^3(3 + \lambda_e)\boldsymbol{B}^{-1} \\ \boldsymbol{L}_4 &= -(1 - \lambda_e)^4\boldsymbol{B}^{-1} \end{split}$$

6. 最優磁通分配 (Optimal Flux Allocation) Hall sensor 磁力模型 (方程式 3):

$$oldsymbol{f}_{m(oldsymbol{p},oldsymbol{v}_H)} = g_H oldsymbol{v}_H^T \hat{oldsymbol{D}}_H^T oldsymbol{L} \Big(rac{oldsymbol{p}}{\ell}\Big) \hat{oldsymbol{D}}_H oldsymbol{v}_H$$

最優電壓分配 (方程式 5):

$$\boldsymbol{v}_{\mathrm{opt}}(\boldsymbol{f}_d,\boldsymbol{p}) = \sqrt{\frac{f_d}{g_H}} \hat{\boldsymbol{D}}_H^{-1} \hat{\boldsymbol{\varphi}}_{\mathrm{opt}}(\boldsymbol{\varphi},\boldsymbol{\theta},\boldsymbol{p})$$

- 7. 關鍵系統參數控制器參數:
- $\lambda_c = 0.9391 \rightarrow$ 控制頻寬 1000 Hz
- $\lambda_e = 0.7304 \rightarrow$ 估測器頻寬 **5000 Hz**
- 採樣頻率: 100 kHz (採樣週期 10 μs)

系統極點 (z-domain):

- $p_1 = 0.9898 \rightarrow 主導極點$
- $p_2 = 0.6053 \rightarrow 次要極點$
- 開迴路頻寬: 160 Hz
- 閉迴路頻寬: 1000 Hz

$$oldsymbol{u}[k] = oldsymbol{B_{ ext{tune}}}^{-1} \{oldsymbol{v_{ ext{ff}}}[k] + \delta oldsymbol{v_{ ext{fb}}}[k]\} - \hat{oldsymbol{w}}[k]$$

$$\boldsymbol{v}_{\mathrm{ff}}[k-1] = \boldsymbol{v}_d[k] - a_1 \boldsymbol{v}_d[k-1] - a_2 \boldsymbol{v}_d[k-2]$$

$$\delta \boldsymbol{v}_{\mathrm{fb}}[k] = (a_1 - \lambda_c) \widehat{\delta \boldsymbol{v}}[k] + a_2 \widehat{\delta \boldsymbol{v}}[k-1]$$

$$egin{aligned} \hat{m{s}}_1[k] &= \lambda_c \hat{m{s}}_1[k-1] + m{L}_1 \{ \delta m{v}[k-1] - \hat{m{s}}_1[k-1] \} \ &\hat{m{s}}_2[k] &= \hat{m{s}}_1[k-1] + m{L}_2 \{ \delta m{v}[k-1] - \hat{m{s}}_1[k-1] \} \ &\hat{m{w}}[k] &= \hat{m{w}}[k-1] + \delta \hat{m{w}}[k-1] + m{L}_3 \{ \delta m{v}[k-1] - \hat{m{s}}_1[k-1] \} \ &\delta \hat{m{w}}[k] &= \delta \hat{m{w}}[k-1] + m{L}_4 \{ \delta m{v}[k-1] - \hat{m{s}}_1[k-1] \} \end{aligned}$$

$$L_1 = 1 + \beta + a_1 + 4\lambda_e$$

$$L_2 = 1 + \frac{\lambda_e^4}{a_2\beta}$$

$$\begin{split} L_3 &= - \Bigg(-\beta + (1+\beta)^2 - 4(1+\beta)\lambda_e + 6\lambda_e^2 - \frac{\lambda_e^4}{\beta} \Bigg) \boldsymbol{B}_{\mathrm{tune}}^{-1} \\ L_4 &= - \Bigg(1 + \beta - 4\lambda_e - (1+\beta)\frac{\lambda_e^4}{\beta^2} + 4\frac{\lambda_e^3}{\beta} \Bigg) \boldsymbol{B}_{\mathrm{tune}}^{-1} \end{split}$$

$$st eta = \lambda_e^2$$