

# Minimizing Cost in Bistatic Radar Placement for Belt Coverage

Ethan Hunt\*, Bing-Hong Liu†, Tu N. Nguyen\*, Yong Shi\*, and Kun Suo\*

\*Department of Computer Science, Kennesaw State University, Marietta, GA 30060, USA.

†Department of Electronic Engineering, National Kaohsiung University of Science and Technology, Kaohsiung, Taiwan.

**Abstract**—With the rapid growth of threats, sophistication and diversity in the manner of intrusion, traditional belt barrier systems are now faced with a major challenge of providing high and concrete coverage quality to expand the guarding service market. Recent efforts aim at constructing a belt barrier by deploying bistatic radar(s) on a specific line regardless of the limitation on deployment locations, to keep the width of the barrier from going below a specific threshold and the total bistatic radar placement cost is minimized, referred to as the Minimum Cost Linear Placement (MCLP) problem. The existing solutions are *heuristic* and their validity is tightly bound by the *barrier width* parameter that these solutions only work for a fixed barrier width value. In this work, we propose an optimal solution, referred to as the Opt\_MCLP, for the “open MCLP problem” that works for full range of the barrier width. Through rigorous theoretical analysis and experimentation, we demonstrate that the proposed algorithms perform well in terms of placement cost reduction and barrier coverage guarantee.

**Index Terms**—Bistatic radar deployment, barrier coverage, network optimization, sensor networks.

## I. INTRODUCTION

Images of moats remind us of the system of guarding ancient castles and the idea is still used today, yet at a higher level. With the development of sensing and communication technology, instead of using moat, barriers of sensors and radars, referred to as the bistatic radar systems, have been building to guard not only critical places but also spaces and national borders. Many applications (e.g., typically for military to detect targets and intruders) use a bistatic radar system that comprises at least a radar signal transmitters and at a radar signal least receiver, wherein the transmitter(s) and the receiver(s) are located in a different location, to form the *barrier coverage* [1], [2], [3], [4], [5], [6].

In recent years, there are efforts in the existing literature to design barrier coverage using radar [7], [8], [9], [10], [11], [12], wherein a radar uses radio waves to detect an object by producing the radio waves and collecting the echo signal reflected off from the target, giving information about the object’s location and speed. Emerging research problems in recent years are how to enhance the quality of barrier coverage and how to efficiently deploy bistatic radar systems while meeting quality requirements. In terms of barrier coverage quality, one of the important aspects that reflects the quality of bistatic radar systems is the width of the barrier coverage

This research was partially supported by the U.S. National Science Foundation under Grants AMPS-2229073, SHF-2210744, and OAC-2413540, and by the National Science and Technology Council of Taiwan under Grants NSTC 114-2221-E-992-056 and NSTC 109-2221-E-992-067. Corresponding author: Tu N. Nguyen.

area. Recent efforts aim at constructing a linear belt barrier with pre-defined width by deploying bistatic radar(s) on a specific line such that the total bistatic radar placement cost is minimized, referred to as the Minimum Cost Linear Placement (MCLP) problem [7], [1]. The sensing model of bistatic radars (Cassini oval sensing model [7], [1]) is in fact very complex and the shape of sensing areas are, therefore, varied according to the variation of distance between the transmitter(s) and the receiver(s) in the bistatic radar system. The validity of the most recent solutions [7], [8] is unfortunately tightly bound by the “barrier width” parameter that these solutions only work for a pre-fixed barrier width value. Thus, they fail to solve the MCLP problem with flexible width ranges of barrier.

Specifically, the most recent solutions proposed for the MCLP problem [7], [8], [1] can only work for covering a belt-shaped area having width less than or equal to  $\frac{2\zeta_{max}}{\sqrt{3}}$ , namely  $0 \leq 2\omega \leq \frac{2\zeta_{max}}{\sqrt{3}}$ , where  $2\omega$  denotes the width of the belt-shaped area and  $\zeta_{max}$  is the radius of the coverage circle centered at the location of transmitter and receiver when the transmitter and the receiver are located at the same location (we will present how to obtain  $\zeta_{max}$  in detail in §II-A). In other words, the barrier built by the bistatic radar system using their solution cannot cover the belt-shaped with width greater than  $\frac{2\zeta_{max}}{\sqrt{3}}$ , namely  $\frac{2\zeta_{max}}{\sqrt{3}} < 2\omega < 2\zeta_{max}$ <sup>1</sup>. In this work, we seek to design an optimal algorithm for the “open MCLP problem” that works for full range of the barrier width, to achieve maximum coverage for the barrier. In addition, the existing solutions [7] proposed for the MCLP problem are still “heuristic” (not an optimal solution) because boundary conditions are not considered. The main contributions of this paper are summarized as follows.

- We investigate the problem in both cases when  $0 \leq 2\omega \leq \frac{2\zeta_{max}}{\sqrt{3}}$  and  $\frac{2\zeta_{max}}{\sqrt{3}} < 2\omega < 2\zeta_{max}$ . We propose an optimal algorithm – dubbed the Opt\_MCLP – to find the optimal solution for the “open MCLP problem” that works for full range of the barrier width ( $0 \leq 2\omega < 2\zeta_{max}$ ).
- We provide rigorous theoretical analyses to demonstrate the correctness of the proposed optimal solution.
- Extensive simulations are conducted to demonstrate the performance of the Opt\_MCLP for the MCLP problem. The obtained results show that the Opt\_MCLP provides a significantly higher performance than the existing one.

<sup>1</sup> $\zeta_{max}$  is the radius of the coverage circle centered at the location of transmitter and receiver when the transmitter and the receiver are located at the same location, therefore, the maximum width of the belt-shaped area in the MCLP problem has to be less than  $2\zeta_{max}$ .

**Organization:** The remaining sections of this paper are organized as follows. The basic mathematical notations and system model are initially introduced, and simple examples are used to present the key ideas behind the proposed work in §II. An optimal solution, termed the Opt\_MCLP is proposed for the full range of the MCLP problem in §III. Simulations are evaluated in Section IV, and the paper is concluded in Section V.

## II. PRELIMINARIES

### A. System Model and Problem Definition

A bistatic radar is composed of at least a transmitter and a receiver that are separated and often located at different positions. In a bistatic radar, the transmitter  $t$  is responsible for producing and propagating the radio waves and the receiver  $r$  can detect an object (target)  $x$  using the echo signal reflected off from  $x$  if the received signal-to-noise ratio (SNR) is not less than a threshold  $\gamma$ . For any target  $x$  and a bistatic radar paired by transmitter  $t$  and receiver  $r$ , the SNR of the radar signal that is sent from  $t$ , reflected by  $x$ , and received by  $r$  can be obtained [13] as follows:

$$SNR(t, x, r) = \frac{K}{d^2(t, x) \cdot d^2(x, r)}, \quad (1)$$

where  $d(t, x)$  (or  $d(x, r)$ ) denotes the Euclidean distance between  $t$  (or  $r$ ) and  $x$ ; and  $K$  represents a constant that is determined by a bistatic radar's physical characteristics, such as the antenna's power gain and the transmission power. When the minimum threshold  $\gamma$  is given, for any pair of transmitter  $t$  and receiver  $r$ , the possible locations of targets  $x$  with  $SNR(t, x, r) = \gamma$  can be characterized by the locus of points such that the product of the distances to  $t$  and  $r$ , namely  $d(x, t) \cdot d(x, r)$ , is the constant equal to  $\zeta_{max}^2$ , where  $\zeta_{max}$  is a constant and denotes  $\sqrt[4]{\frac{K}{\gamma}}$ . The locus of points  $x$ , which will be a *closed curve or a pair of closed curves*, is known as a Cassini oval [14] as depicted in Fig. 1. For any target  $y$  within the Cassini oval, the product of the distances from  $y$  to  $t$  and  $r$  is not greater than  $\sqrt{\frac{K}{\gamma}}$ , that is,  $d(y, t) \cdot d(y, r) \leq \zeta_{max}^2$ ; and therefore, we have that  $SNR(t, y, r) \geq \gamma$  and  $y$ , therefore, can be detected by  $r$ . Hereafter, a point  $z$  in the plane is said to be covered by a bistatic radar paired by transmitter  $t$  and receiver  $r$  if  $z$  is within the area surrounded by the Cassini oval with focal points at  $t$  and  $r$ .

When  $\zeta_{max}$  is given, the shape of the Cassini oval with focal points at transmitter  $t$  and receiver  $r$  is determined by the distance between  $t$  and  $r$ , that is,  $d(t, r)$ . Four shape types of the Cassini oval depicted in Fig. 1 are listed as follows with different range of  $d(t, r)$  [7]:

- an ellipse curve (Fig. 1(a)) if  $0 \leq d(t, r) < \sqrt{2}\zeta_{max}$ ;
- a waist curve (Fig. 1(b)) if  $\sqrt{2}\zeta_{max} \leq d(t, r) < 2\zeta_{max}$ ;
- a lemniscate of Bernoulli (Fig. 1(c)) if  $d(t, r) = 2\zeta_{max}$ ;
- a pair of closed curves (Fig. 1(d)) if  $d(t, r) > 2\zeta_{max}$ .

When multiple transmitters and receivers are deployed in an area, transmitters and receivers can be paired to form multiple bistatic radars. Here, transmitters are assumed to operate

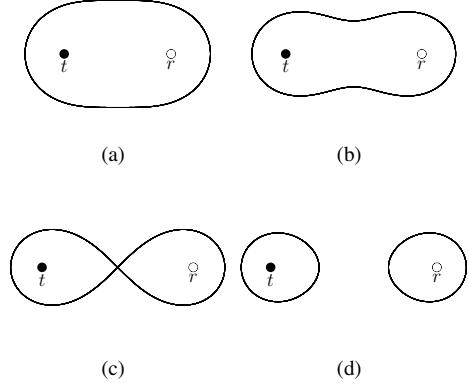


Fig. 1: Four shape types of the Cassini oval with focal points at transmitter  $t$  and receiver  $r$ , where small solid and hollow circles denote transmitters and receivers, respectively. The shape types with  $0 \leq d(t, r) < \sqrt{2}\zeta_{max}$ ,  $\sqrt{2}\zeta_{max} \leq d(t, r) < 2\zeta_{max}$ ,  $d(t, r) = 2\zeta_{max}$ , and  $d(t, r) > 2\zeta_{max}$  are shown in (a), (b), (c), and (d), respectively.

with orthogonal frequency such that mutual interferences at a receiver can be avoided [15]. Therefore, each receiver can be paired with different transmitters to form bistatic radars by switching the frequency. In addition, because receivers can receive the radar signal sent from a transmitter, multiple receivers can also be paired with the same transmitter as shown in Fig. 2. Because multiple bistatic radars are often used to detect targets, an area is said to be covered by the set of transmitters  $T$  and the set of receivers  $R$  hereafter, if for any point  $z$  in the area,  $z$  is covered by at least one bistatic radar paired by a transmitter  $t \in T$  and a receiver  $r \in R$ .

Let  $c_t$  and  $c_r$  be the placement/deployment costs of a transmitter and a receiver, respectively. Also let  $Area$  be a belt-shaped (rectangle) area with length  $L$  and width  $W$ , where  $L \geq W > 0$ . In addition, when a transmitter and a receiver are located at the same location, the shape of the generated Cassini oval will be a circle centered at the transmitter/receiver with radius  $\zeta_{max}$  [14]. While we are given  $\zeta_{max}$ ,  $c_t$ ,  $c_r$ , and  $Area$  with width less than  $2\zeta_{max}$ , the Minimum Cost Linear Placement (MCLP) problem is to deploy a set of transmitters  $T$  and a set of receivers  $R$  on the *line* that goes through the middle points of the shorter sides of the  $Area$ , such that the  $Area$  is fully covered and the total placement cost of bistatic radar(s), namely  $c_t \times |T| + c_r \times |R|$ , is minimized, where  $|T|$  and  $|R|$  denote the cardinalities of  $T$  and  $R$ , respectively.

For the MCLP problem, let  $2\omega$  be the width of the  $Area$ , and  $\beta$  denote  $\frac{\zeta_{max}}{\omega}$ . Although solutions for the MCLP problem are proposed in [7], the solutions only work for the case of  $\beta \geq \sqrt{3}$ , that is,  $\frac{\zeta_{max}}{\omega} \geq \sqrt{3}$  ( $2\omega \leq \frac{2\zeta_{max}}{\sqrt{3}}$ ). In addition, the width of the  $Area$  in the MCLP problem is always less than  $2\zeta_{max}$ , which implies that these solutions are not valid for the case of  $\frac{2\zeta_{max}}{\sqrt{3}} < 2\omega < 2\zeta_{max}$  ( $1 < \beta < \sqrt{3}$ ). This motivates us to explore an optimal solution for the MCLP problem that especially works for *full range of the coverage Area width* ( $0 \leq 2\omega < 2\zeta_{max}$ ).

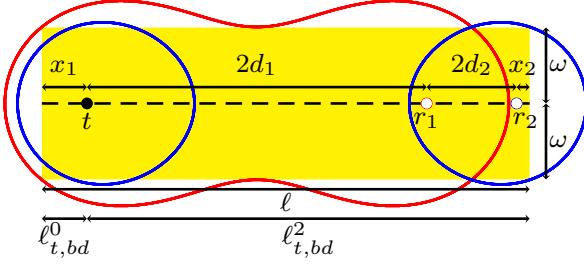


Fig. 2: Examples of covering a rectangle area by using one transmitter and two receivers (best viewed in color).

### III. THE OPTIMAL SOLUTION FOR THE MINIMUM COST LINEAR PLACEMENT (MCLP) PROBLEM

By Fig. 1, we have that when transmitter  $t$  and receiver  $r$  are close enough, the area covered by  $t$  and  $r$  will be an ellipse or waist shape. In order to cover a rectangle area with width  $2\omega$ , the distance between the upper and the lower parts of the ellipse (or the waist) curve has to be not less than  $2\omega$ . Take Fig. 3, for example, where  $\omega = \frac{\zeta_{max}}{\sqrt{3}}$ . When the covered area is a waist shape as shown in Fig. 3(a), because the upper and the lower parts of the curve generated by transmitter  $t$  and receiver  $r$  are symmetric, and  $d(E, F) = d(t, D) = d(r, C) = \frac{\zeta_{max}}{\sqrt{3}}$ ,  $t$  and  $r$  can cover a rectangle area with width  $2\omega$ . Similar example with an ellipse shape is shown in Fig. 3(b). This motivates us to find an optimal deployment of a transmitter and a receiver such that the width of the covered rectangle can be satisfied and its length can be maximized. As the examples in Fig. 3, when a rectangle is fully covered by transmitter  $t$  and receiver  $r$ ,  $t$  (or  $r$ ) may be at a distance of  $\theta$  from the closest vertical boundary of the covered rectangle. By the observation, we show that transmitter  $t$  and receiver  $r$  with  $d(t, r) = \sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$  can cover a rectangle with width  $2\omega$  and length  $\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ ; and that transmitter  $t$  and receiver  $r$  with  $d(t, r) = \omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1} - \theta'$  can cover a rectangle with width  $2\omega$  and maximum length  $\omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1} + \theta'$  by Lemmas 1-2, where  $\theta'$  denotes the  $\theta$  in  $[0, \sqrt{\beta^2 \zeta_{max}^2 - \omega^2}]$  having maximum value of  $\omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1} + \theta$  and can be obtained by Newton's method [16]. In addition, Lemma 3 shows that the length of the rectangle with width  $2\omega$  covered by one transmitter and any number of receivers is at most  $2\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ . Note that we can use one transmitter  $t$  and two receivers,  $r_1$  and  $r_2$ , by the sequence  $(r_1, t, r_2)$ , to cover a rectangle with width  $2\omega$  and length  $2\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$  by Lemma 2, as the example in Fig. 4.

**Lemma 1:** When  $1 < \beta < \sqrt{3}$  and a rectangle with width  $2\omega$  is covered by transmitter  $t$  and receiver  $r$ ,  $d(t, r) + \theta$  is maximized if and only if  $d(t, r) = \sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$  and  $\theta = 0$ , where  $\theta$  denotes the distance between  $t$  (or  $r$ ) and the closest vertical boundary of the rectangle. In addition,  $d(t, r) + 2\theta$  is maximized if and only if  $d(t, r) = \omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1} - \theta'$ , where

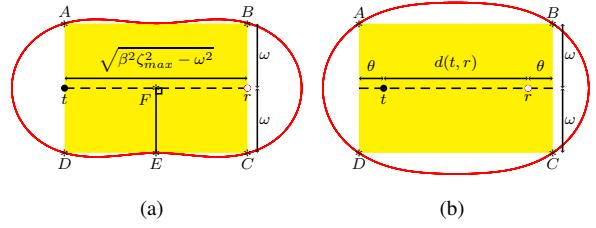


Fig. 3: Examples of deploying transmitter  $t$  and receiver  $r$ , where  $\omega = \frac{\zeta_{max}}{\sqrt{3}}$ . The distances between  $r$  and the boundary in (a) and (b) are 0 and  $\theta$ , respectively.

$\theta'$  denotes the  $\theta$  in  $[0, \sqrt{\beta^2 \zeta_{max}^2 - \omega^2}]$  having maximum value of  $\omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1} + \theta$ .

*Proof:* Without loss of generality, let  $\square ABCD$  be the rectangle covered by  $t$  and  $r$ , as the rectangle in Fig. 3(a) or Fig. 3(b). Because the upper and the lower parts (or, the left and the right parts) of the curve generated by  $t$  and  $r$  are symmetric, the proof suffices to show that the cases hold when the point  $B$  is covered. When the point  $B$  is exactly covered by  $t$  and  $r$ , we have that  $d(t, B) \cdot d(r, B) = \zeta_{max}^2$ , which implies that  $\sqrt{(d(t, r) + \theta)^2 + \omega^2} \cdot \sqrt{\theta^2 + \omega^2} = \zeta_{max}^2$ . We thus have that  $d(t, r) = \omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1} - \theta$ . Therefore,

$d(t, r) + \theta = \omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1}$ . Because  $\omega$  and  $\beta$  are constants,  $d(t, r) + \theta$  is maximized if and only if  $\theta = 0$ . When  $\theta = 0$ ,  $d(t, r) + \theta = d(t, r) = \omega \sqrt{\beta^4 - 1} = \sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ . In addition,  $d(t, r) + 2\theta = \omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1} + \theta$ . It is clear that  $d(t, r) + 2\theta$  is maximized if and only if  $\theta \geq 0$ . Assume that  $\theta = \sqrt{\beta^2 \zeta_{max}^2 - \omega^2} + \epsilon$ , where  $\epsilon > 0$ . Because  $d(t, r) \geq 0$  and  $1 < \beta < \sqrt{3}$ , we have that  $d(t, B) \cdot d(r, B) = \sqrt{(d(t, r) + \theta)^2 + \omega^2} \cdot \sqrt{\theta^2 + \omega^2} \geq (\sqrt{\theta^2 + \omega^2})^2 = (\sqrt{\beta^2 \zeta_{max}^2 - \omega^2} + \epsilon)^2 + \omega^2 = \beta^2 \zeta_{max}^2 + 2\epsilon \sqrt{\beta^2 \zeta_{max}^2 - \omega^2} + \epsilon^2 > \zeta_{max}^2$ . This constitutes a contradiction because the point  $B$  has to be covered, that is,  $d(t, B) \cdot d(r, B) \leq \zeta_{max}^2$ . Therefore, we have that  $\epsilon \leq 0$ , that is,  $\theta \leq \sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ . Because  $\theta \geq 0$ , we have that  $d(t, r) + 2\theta$  is maximized if and only if  $0 \leq \theta \leq \sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ . Let  $\theta'$  be the  $\theta$  in  $[0, \sqrt{\beta^2 \zeta_{max}^2 - \omega^2}]$  having maximum value of  $\omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1} + \theta$ . We have that  $d(t, r) + 2\theta$  is maximized if and only if  $d(t, r) + 2\theta' = \omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1} + \theta'$ ,

that is,  $d(t, r) = \omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1} - \theta'$ , which completes the proof. ■

**Lemma 2:** When  $1 < \beta < \sqrt{3}$ , the transmitter  $t$  and the receiver  $r$  that are at a distance of  $\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$  apart can cover a rectangle with width  $2\omega$  and length equal to  $\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ . In addition, the transmitter  $t$  and the receiver  $r$  that are at a distance of  $d(t, r) = \omega \sqrt{\frac{\beta^4}{\omega^2+1} - 1} - \theta'$  apart can cover a rectangle with width  $2\omega$  and length equal to  $d(t, r) + 2\theta'$ , where  $\theta'$  is defined in Lemma 1.

*Proof:* The proof has to show that S1) if  $d(t, r) = \sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ ,  $t$  and  $r$  can fully cover a rectangle with width  $2\omega$  and length  $\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ , and that S2) if  $d(t, r) = \omega \sqrt{\frac{\beta^4}{\theta'^2 + 1} - 1} - \theta'$ ,  $t$  and  $r$  can fully cover a rectangle with width  $2\omega$  and length  $\omega \sqrt{\frac{\beta^4}{\theta'^2 + 1} - 1} + \theta'$ , where  $\theta'$  denotes the  $\theta$  in  $[0, \sqrt{\beta^2 \zeta_{max}^2 - \omega^2}]$  having maximum value of  $\omega \sqrt{\frac{\beta^4}{\omega^2 + 1} - 1} + \theta$ . The proof of S2 is omitted here due to the similarity.

For S1, because  $\frac{\zeta_{max}}{\sqrt{3}} < \omega < \zeta_{max}$ , we have that  $d(t, r) = \sqrt{\beta^2 \zeta_{max}^2 - \omega^2} = \sqrt{\frac{\zeta_{max}^4 - \omega^4}{\omega^2}} < \sqrt{\frac{\zeta_{max}^4 - (\frac{\zeta_{max}}{\sqrt{3}})^4}{(\frac{\zeta_{max}}{\sqrt{3}})^2}} = \sqrt{\frac{8\zeta_{max}^2}{3}} < 2\zeta_{max}$ , which implies that the area covered by  $t$  and  $r$  will be an ellipse or waist shape by the results in Fig. 1 [7]. Let  $\square ABCD$  be a rectangle with width  $2\omega$  and length  $\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ , as the rectangle in Fig. 3(a). Due to the fact that the upper and the lower parts of the curve generated by  $t$  and  $r$  are symmetric, the proof of S1 suffices to show that  $\square trCD$  is within the area covered by  $t$  and  $r$ . Let  $tD'$  (or  $rC'$ ) be the line from  $t$  (or, from  $r$ ), perpendicular to  $\overline{tr}$ , and intersected by the lower part of the generated curve at point  $D'$  (or  $C'$ ). Also let the curve  $\widetilde{D'C'}$  be the lower part of the curve generated by  $t$  and  $r$  with endpoints  $D'$  and  $C'$ . Because the curve generated by  $t$  and  $r$  is an ellipse or waist shape, and the left and the right parts of the generated curve are symmetric, we have that the minimum distance between  $\overline{tr}$  and  $\widetilde{D'C'}$  is the minimum value of  $d(D', \overline{tr})$ ,  $d(C', \overline{tr})$ , and  $d(E', \overline{tr})$ , where  $d(D', \overline{tr})$ ,  $d(C', \overline{tr})$ , and  $d(E', \overline{tr})$  denote the minimum distance from  $D'$ ,  $C'$ , and  $E'$ , respectively, to  $\overline{tr}$ , and  $E'$  denotes the midpoint of  $\widetilde{D'C'}$ . We thus also have that  $\square trCD$  is fully covered if  $d(D', \overline{tr}) \geq d(D, \overline{tr}) = \omega$ ,  $d(C', \overline{tr}) \geq d(C, \overline{tr}) = \omega$ , and  $d(E', \overline{tr}) \geq d(E, \overline{tr}) = \omega$ , that is, the points  $C$ ,  $D$ , and  $E$  have to be covered by  $t$  and  $r$ , where the point  $E$  is the midpoint of  $\overline{CD}$ . For the point  $D$ , we have that  $d(t, D) \cdot d(r, D) = \omega \cdot \sqrt{d^2(r, t) + d^2(t, D)} = \zeta_{max}^2$ , implying that  $D$  is covered by  $t$  and  $r$ . Similarly, the point  $C$  is also covered by  $t$  and  $r$ . For the point  $E$ , we assume that  $E$  is not covered by  $t$  and  $r$ . That is,  $d(t, E) \cdot d(r, E) = (\sqrt{\frac{d(t, r)}{2}} + \omega)^2 > \zeta_{max}^2$ , and thus, we have that  $3\omega^4 - 4\omega^2\zeta_{max}^2 + \zeta_{max}^4 > 0$ , implying that  $(3\omega^2 - \zeta_{max}^2)(\omega^2 - \zeta_{max}^2) > 0$ . We have that  $\omega < \frac{\zeta_{max}}{\sqrt{3}}$  or  $\omega > \zeta_{max}$ , which constitutes a contradiction because  $\frac{\zeta_{max}}{\sqrt{3}} < \omega < \zeta_{max}$ . Therefore, the points  $C$ ,  $D$ , and  $E$  are covered by  $t$  and  $r$ , and  $\square ABCD$  is fully covered by  $t$  and  $r$ . This completes the proof of S1, and thus, the proof of the lemma is also completed. ■

*Lemma 3:* When  $1 < \beta < \sqrt{3}$  and a transmitter  $t$  is given, the maximum length of the rectangle with width  $2\omega$  covered by  $t$  and any number of receivers is equal to  $2\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ .

*Proof:* Assume that there exists a sequence  $\Psi = (R^{n_{p_0}}, t, R^{n_{p_1}})$  deployed on a line such that the length of the rectangle covered by  $\Psi$ , denoted by  $\ell(\Psi)$ , is greater than

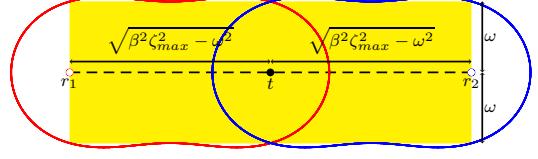


Fig. 4: Example of deploying one transmitter with two receivers when  $\omega = \frac{\zeta_{max}}{\sqrt{3}}$ .

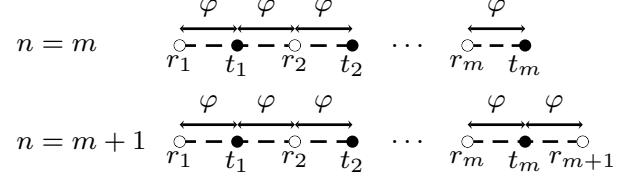


Fig. 5: Examples of deploying  $m$  transmitters and  $n$  receivers by the Rotated Placement, where  $\varphi$  denotes  $\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ .

$2\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ , where  $n_{p_0}, n_{p_1} \geq 0$  and  $R^{n_{p_i}}$  denotes the set of  $n_{p_i}$  receivers. By Lemmas 1-2, we have that the maximum length of the covered rectangle from  $t$  to one side boundary is at most  $\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ . This implies that  $2\sqrt{\beta^2 \zeta_{max}^2 - \omega^2} \geq \ell(\Psi) > 2\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$ , which constitutes a contradiction. This thus completes the proof. ■

Let  $I_n^m$  be the sequence  $(r_1, t_1, r_2, t_2, \dots, r_m, t_m)$  if  $n = m$ , and be the sequence  $(r_1, t_1, r_2, t_2, \dots, r_m, t_m, r_{m+1})$  if  $n = m + 1$ . The proposed placement for  $1 < \beta < \sqrt{3}$ , termed the Rotated Placement hereafter, is to place  $m$  transmitters and  $n$  receivers following the sequence  $I_n^m$  sequentially, where the distance between a transmitter and its adjacent receiver is  $\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$  by Lemma 2, as the examples in Fig. 5.

The procedure MinCost\_RP is designed to find a sequence of transmitters and receivers with minimum cost to cover a rectangle area *Area* with length  $\ell$  and width  $2\omega$ . By Lemma 1-2, if  $\ell \leq \omega \sqrt{\frac{\beta^4}{\theta'^2 + 1} - 1} + \theta'$ , the *Area* can be covered by one transmitter and one receiver. Otherwise, by Lemma 1-3, one transmitter coupled with two receivers can be used to cover a rectangle with length  $2\sqrt{\beta^2 \zeta_{max}^2 - \omega^2}$  that is called a unit hereafter. The procedure MinCost\_RP is then to see at least how many units are required. The necessary numbers of transmitters and receivers are calculated and stored in *numTx* and *numRx*, respectively. When the *Area* is not fully covered, additional one transmitter is added if the length of the remaining uncovered part of the *Area* is not greater than the half length of a unit; and otherwise, additional one transmitter and one receiver are added. Finally, by the obtained *numTx* and *numRx*, the Rotated Placement is used to generate the optimal solution  $I_{numRx}^{numTx}$ , which is proved in Theorem 1.

*Theorem 1:* When  $1 < \beta < \sqrt{3}$ , the procedure MinCost\_RP can find an optimal solution to cover a rectangle area *Area* with length  $\ell$  and width  $2\omega$ .

*Proof:* By Lemma 1-2, we have that deploying one transmitter and one receiver to cover the *Area* is an optimal solution if  $\ell \leq \omega \sqrt{\frac{\beta^4}{\theta'^2 + 1} - 1} + \theta'$ . In addition, because it

is easy to verify that the difference between  $numTx$  and  $numRx$  in the procedure MinCost\_RP is at most one, the proof suffices to show that the solution generated by the procedure MinCost\_RP has a minimum cost. Three cases, including C1)  $\ell = 2k\sqrt{\beta^2\zeta_{max}^2 - \omega^2}$ , C2)  $2k\sqrt{\beta^2\zeta_{max}^2 - \omega^2} < \ell \leq (2k+1)\sqrt{\beta^2\zeta_{max}^2 - \omega^2}$ , and C3)  $(2k+1)\sqrt{\beta^2\zeta_{max}^2 - \omega^2} < \ell < (2k+2)\sqrt{\beta^2\zeta_{max}^2 - \omega^2}$ , are considered, where  $k \geq 0$  and  $\ell > \omega\sqrt{\frac{\beta^4}{\theta'^2+1}} - 1 + \theta'$ . Because the proofs of C2 and C3 are similar to that of C1, the proofs of C2 and C3 are omitted.

---

```

1: procedure MinCost_RP( $\omega, \ell$ )
2:   if  $\ell \leq \omega\sqrt{\frac{\beta^4}{\theta'^2+1}} - 1 + \theta'$ , where  $\theta'$  is defined in
   Lemma 1 then
3:     Let  $I$  be the sequence  $(r, t)$  with  $d(t, r) =$ 
    $\omega\sqrt{\frac{\beta^4}{\theta'^2+1}} - 1 - \theta'$ 
4:      $minValue \leftarrow c_t + c_r$ 
5:     return ( $minValue, I$ )
6:   end if
7:    $numTx \leftarrow \left\lfloor \frac{\ell}{2\sqrt{\beta^2\zeta_{max}^2 - \omega^2}} \right\rfloor$ 
8:    $numRx \leftarrow numTx + 1$ 
9:    $remainingLen \leftarrow \ell \pmod{2\sqrt{\beta^2\zeta_{max}^2 - \omega^2}}$ 
10:  if  $remainingLen > 0$  then
11:     $numTx \leftarrow numTx + 1$ 
12:    if  $\lceil \frac{remainingLen}{\sqrt{\beta^2\zeta_{max}^2 - \omega^2}} \rceil = 2$  then
13:       $numRx \leftarrow numRx + 1$ 
14:    end if
15:  end if
16:  Let  $I_{numTx}^{numTx}$  be the sequence generated by the Rotated Placement with  $numTx$  transmitters and  $numRx$  receivers
17:   $minValue \leftarrow numTx \times c_t + numRx \times c_r$ 
18:  return ( $minValue, I_{numRx}^{numTx}$ )
19: end procedure

```

---

For C1, let  $I_{n_1}^{m_1}$  and  $\Psi_{n_2}^{m_2}$  be the sequences obtained by the procedure MinCost\_RP and the optimal solution, respectively. Assume that  $I_{n_1}^{m_1}$  is not an optimal solution. This implies that  $\varsigma(I_{n_1}^{m_1}) > \varsigma(\Psi_{n_2}^{m_2})$ , where  $\varsigma(I_{n_1}^{m_1})$  (or  $\varsigma(\Psi_{n_2}^{m_2})$ ) denotes the placement cost of  $I_{n_1}^{m_1}$  (or  $\Psi_{n_2}^{m_2}$ ), and  $m_1 \neq m_2$  or  $n_1 \neq n_2$ . Because  $\ell = 2k\sqrt{\beta^2\zeta_{max}^2 - \omega^2}$ , we have that  $m_1 = k$  and  $n_1 = k + 1$  by the procedure MinCost\_RP. By Lemma 3, due to the fact that one transmitter with receivers can cover a rectangle with length at most  $2\sqrt{\beta^2\zeta_{max}^2 - \omega^2}$ , at least  $\left\lfloor \frac{2k\sqrt{\beta^2\zeta_{max}^2 - \omega^2}}{2\sqrt{\beta^2\zeta_{max}^2 - \omega^2}} \right\rfloor = k$  transmitters are required to cover the Area. Because  $m_1 = k$ , we have that C1.1)  $m_2 > k$ , or C1.2)  $m_2 = k$  and  $n_2 < n_1 = k + 1$ . Due to the fact that the proof of C1.2 is similar to that of C1.1, the proof of C1.2 is omitted here. For C1.1, if  $m_2 > k$ , because  $\varsigma(I_{n_1}^{m_1}) > \varsigma(\Psi_{n_2}^{m_2})$ , we have that  $c_t \times k + c_r \times (k+1) > c_t \times (k+y) + c_r \times n_2$ , where  $m_2 = k + y$  and  $y \geq 1$ . Because  $y \geq 1$  and  $c_t \geq c_r$ , we have that  $n_2 < (k+1) - \frac{y c_t}{c_r} \leq k$ . Due to the fact that the covered

area is the same when receivers and transmitters are swapped, by Lemma 3, we have that one receiver with transmitters can cover a rectangle with length at most  $2\sqrt{\beta^2\zeta_{max}^2 - \omega^2}$ . In addition, because  $n_2 < k$ , that is,  $n_2 \leq k - 1$ , the rectangle with length at most  $2(k-1)\sqrt{\beta^2\zeta_{max}^2 - \omega^2}$  can be covered by  $n_2$  receivers with transmitters, which implies that the Area cannot be covered by  $\Psi_{n_2}^{m_2}$ . This constitutes a contradiction, and completes the proof of C1.1. This thus completes the proof of the theorem. ■

For an *Area* with width  $W = 2\omega$  and length  $L = \ell$ , the algorithm Opt\_MCLP is designed as shown in Algorithm 1 to combine the function ComputeMinCost, which is proposed in [7] and used for  $2\omega \leq \frac{2\zeta_{max}}{\sqrt{3}}$ , with the procedure MinCost\_RP and used for  $\frac{2\zeta_{max}}{\sqrt{3}} < 2\omega < 2\zeta_{max}$ .

---

**Algorithm 1** Opt\_MCLP( $\omega, \ell$ )

---

```

1:  $S \leftarrow \emptyset$ ;  $minValue \leftarrow \infty$ 
2: if  $\omega \leq \frac{\zeta_{max}}{\sqrt{3}}$  then
3:   Use ComputeMinCost function in [7] to get the total
   cost  $minValue$  and the placement sequence  $S$  by given
    $\omega$  and  $\ell$ 
4: else
5:    $(minValue, S) \leftarrow$  MinCost_RP ( $\omega, \ell$ )
6: end if
7: return ( $minValue, S$ )

```

---

#### IV. PERFORMANCE EVALUATION

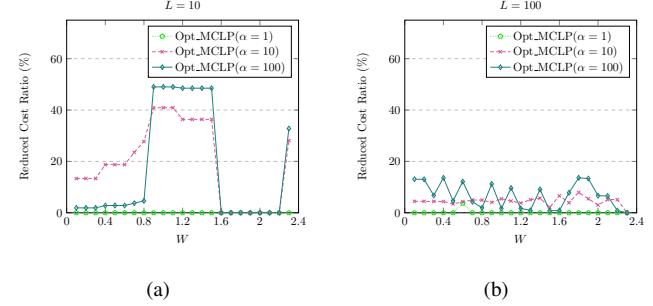


Fig. 6: The reduced cost ratio when  $\zeta_{max} = 2$ ,  $\mu = 0.1$ ,  $W$  ranges from 0.1 to 2.3, and  $\alpha$  ranges from 1 to 100. The values of  $L$  are 10 in (a) and 100 in (b), respectively.

Here, simulations developed by C++ were used to evaluate the performance of the Opt\_MCLP for the MCLP problem. In the simulations,  $\mu$  and  $c_r$  were set to 0.1 and 1, respectively. In addition,  $W$ ,  $L$ ,  $\zeta_{max}$ , and  $\alpha$  were set from 0.1 to 10, from 10 to 100, from 1 to 4, and from 1 to 100, respectively, where  $\alpha$  denoted  $\frac{c_t}{c_A}$ . Let the reduced cost ratio of  $B$  compared with  $A$  be  $\frac{c_A - c_B}{c_A}$ , where  $A$  and  $B$  were solutions of the MCLP problem and  $c_A$  (or,  $c_B$ ) denoted the total placement cost required by  $A$  (or,  $B$ ). For the MCLP problem, because transmitters and receivers had to be deployed on a line to form a linear barrier, the Algorithm 2 in [7] with one linear barrier was compared in terms of the reduced cost ratio in §IV-A.

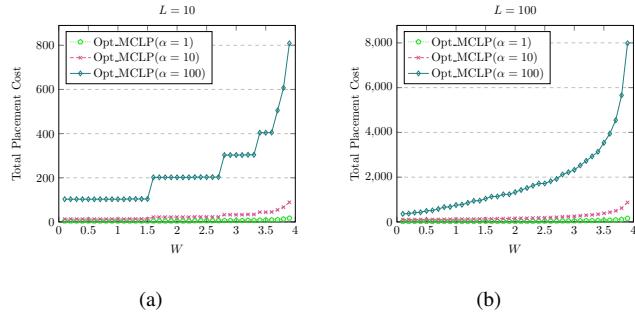


Fig. 7: The total placement cost when  $\zeta_{max} = 2$ ,  $\mu = 0.1$ ,  $W$  ranges from 0.1 to 3.9, and  $\alpha$  ranges from 1 to 100. The values of  $L$  are 10 in (a) and 100 in (b), respectively.

Because the Algorithm 2 proposed in [7] can be only used for covering a rectangle area with width less than or equal to  $\frac{2\zeta_{max}}{\sqrt{3}}$ ,  $W$  was set from 0.1 to 2.3 when  $\zeta_{max} = 2$ . In addition, due to the fact that the width of the *Area* had to be less than  $2\zeta_{max}$  in the MCLP problem, we also evaluated the total placement cost of the Opt\_MCLP in §IV-A when  $\zeta_{max} = 2$  and  $W$  ranged from 0.1 to 3.9.

#### A. The MCLP Problem

Let the reduced cost ratio of the Opt\_MCLP( $\alpha = k$ ) denote the reduced cost ratio of the Opt\_MCLP compared with the Algorithm 2 in [7] having one linear barrier when  $\alpha = k$ . Fig. 6(a) and Fig. 6(b) show the reduced cost ratios of the Opt\_MCLP( $\alpha = 1$  and Opt\_MCLP( $\alpha = 100$ ), respectively, when the values of  $L$  are equal to 10, 50, and 100, respectively. It is clear that the Opt\_MCLP provides better performance than the Algorithm 2 proposed in [7] with one linear barrier. In addition, the Opt\_MCLP reduces the placement cost by up to 49% in comparison with the other method.

Let the total placement cost of the Opt\_MCLP( $\alpha = k$ ) denote the total placement cost of the Opt\_MCLP when  $\alpha = k$ . Fig. 7(a) and Fig. 7(b) show the total placement costs of the Opt\_MCLP( $\alpha = 1$ ) and Opt\_MCLP( $\alpha = 100$ ), respectively, when the values of  $L$  are equal to 10, 50, and 100, respectively. It is clear that in Fig. 7(a) or Fig. 7(b), the total placement cost of the Opt\_MCLP increases with the increasing of  $\alpha$ . This is because the cost of a transmitter increases when  $\alpha$  increases. In addition, it is also clear that the greater the value of  $W$ , the higher the total placement cost required by the Opt\_MCLP( $\alpha = 1$ ), Opt\_MCLP( $\alpha = 10$ ), or Opt\_MCLP( $\alpha = 100$ ). This is due to the fact that transmitters and receivers are closely deployed in order to cover the *Area* with greater width, and therefore, more transmitters and receivers are required. Moreover, when the value of  $L$  increases from 10 to 100, the total placement cost of the Opt\_MCLP( $\alpha = 1$ ), Opt\_MCLP( $\alpha = 10$ ), or Opt\_MCLP( $\alpha = 100$ ) increases because more area has to be covered.

#### V. CONCLUSION

The sensing model of bistatic radars (Cassini oval sensing model [7]) is in fact very complex and the shape of sensing areas are, therefore, varied according to the variation of distance between the transmitter(s) and the receiver(s) in the bistatic radar system. In this paper, we study the MCLP problem for constructing a belt barrier with minimum placement cost. For the MCLP problem with  $0 \leq 2\omega \leq \frac{2\zeta_{max}}{\sqrt{3}}$ , a function, termed the MinCost\_RP, is proposed to find an optimal solution. In addition, for  $\frac{2\zeta_{max}}{\sqrt{3}} < 2\omega < 2\zeta_{max}$ , an optimal solution, termed the Opt\_MCLP, is proposed. Theoretical analysis is also provided for proving the optimality of the Opt\_MCLP. Simulation results show that the Opt\_MCLP has a significantly lower placement cost than the existing solution.

#### REFERENCES

- [1] D. H. P. Nguyen, Y.-C. Chen, Y.-X. Yang, and B.-H. Liu, "Minimum cost deployment of bistatic radar sensors for perimeter barrier coverage of critical square grids," *IEEE Transactions on Green Communications and Networking*, pp. 1–1, 2024.
- [2] Q. Liu, Z. Zhang, N. Khanh Le, J. Qin, F. Liu, and S. Hirche, "Distributed coverage control of constrained constant-speed unicycle multi-agent systems," *IEEE Transactions on Automation Science and Engineering*, vol. 22, pp. 2225–2240, 2025.
- [3] P. Wang, Y. Xiong, J. She, and A. Yu, "Optimization method for node deployment of closed-barrier coverage in hybrid directional sensor networks," *IEEE Sensors Journal*, vol. 24, no. 9, pp. 15 421–15 433, 2024.
- [4] M. Karatas, "Optimal deployment of heterogeneous sensor networks for a hybrid point and barrier coverage application," *Computer Networks*, vol. 132, pp. 129 – 144, 2018.
- [5] C. Yang, L. Feng, H. Zhang, S. He, and Z. Shi, "A novel data fusion algorithm to combat false data injection attacks in networked radar systems," *IEEE Transactions on Signal and Information Processing over Networks*, vol. 4, no. 1, pp. 125–136, 2018.
- [6] J. Chen, B. Wang, and W. Liu, "Constructing perimeter barrier coverage with bistatic radar sensors," *Journal of Network and Computer Applications*, vol. 57, pp. 129 – 141, 2015.
- [7] B. Wang, J. Chen, W. Liu, and L. T. Yang, "Minimum cost placement of bistatic radar sensors for belt barrier coverage," *IEEE Transactions on Computers*, vol. 65, no. 2, pp. 577–588, Feb 2016.
- [8] X. Xu, C. Zhao, T. Ye, and T. Gu, "Minimum cost deployment of bistatic radar sensor for perimeter barrier coverage," *Sensors (Basel)*, vol. 19, no. 2, p. 225, January 2019.
- [9] F. Colone, T. Martelli, and P. Lombardo, "Quasi-monostatic versus near forward scatter geometry in wifi-based passive radar sensors," *IEEE Sensors Journal*, vol. 17, no. 15, pp. 4757–4772, 2017.
- [10] K. Tian, J. Li, and X. Yang, "A novel method of micro-doppler parameter extraction for human monitoring terahertz radar network," *Ad Hoc Networks*, vol. 58, pp. 222 – 230, 2017, hybrid Wireless Ad Hoc Networks.
- [11] R. Xie, K. Luo, and T. Jiang, "Joint coverage and localization driven receiver placement in distributed passive radar," *IEEE Transactions on Geoscience and Remote Sensing*, pp. 1–12, 2020.
- [12] M. Malanowski, M. Źywek, M. Płotka, and K. Kulpa, "Passive bistatic radar detection performance prediction considering antenna patterns and propagation effects," *IEEE Transactions on Geoscience and Remote Sensing*, vol. 60, pp. 1–16, 2022.
- [13] N. J. Willis, *Bistatic radar*. SciTech Publishing, 2005, vol. 2.
- [14] D. L. Jones, "A collection of loci using two fixed points," *Missouri Journal of Mathematical Sciences*, vol. 19, no. 2, pp. 141–150, 2007.
- [15] J. Liang and Q. Liang, "Design and analysis of distributed radar sensor networks," *IEEE Transactions on Parallel and Distributed Systems*, vol. 22, no. 11, pp. 1926–1933, Nov 2011.
- [16] K. Atkinson, *An Introduction to Numerical Analysis*, 2nd Edition. Wiley India Pvt. Limited, 2008.