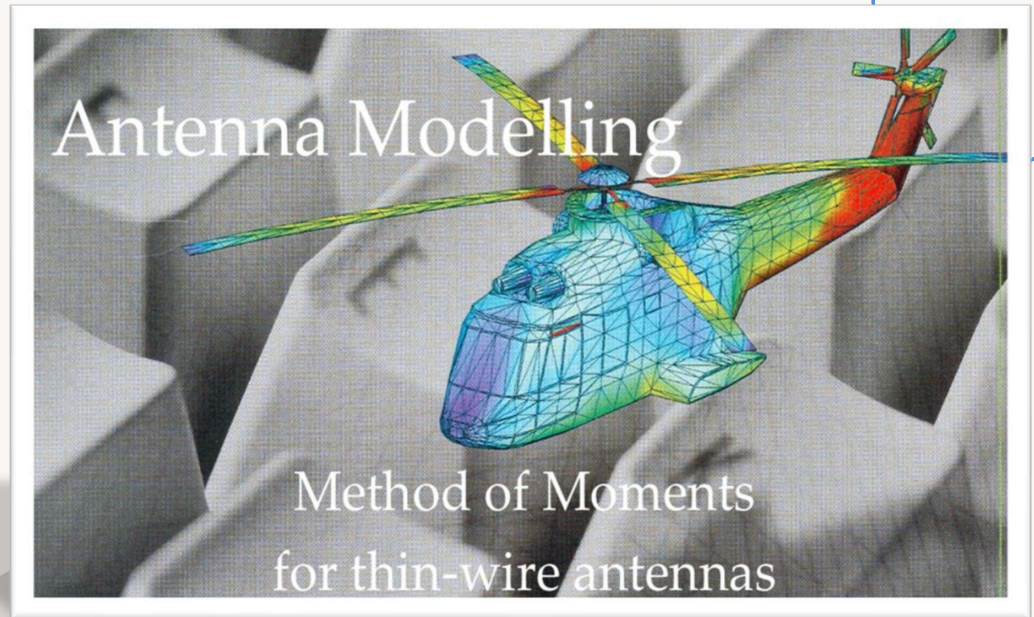


METHOD OF MOMENT FOR THIN WIRE

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Picture taken from the course slides



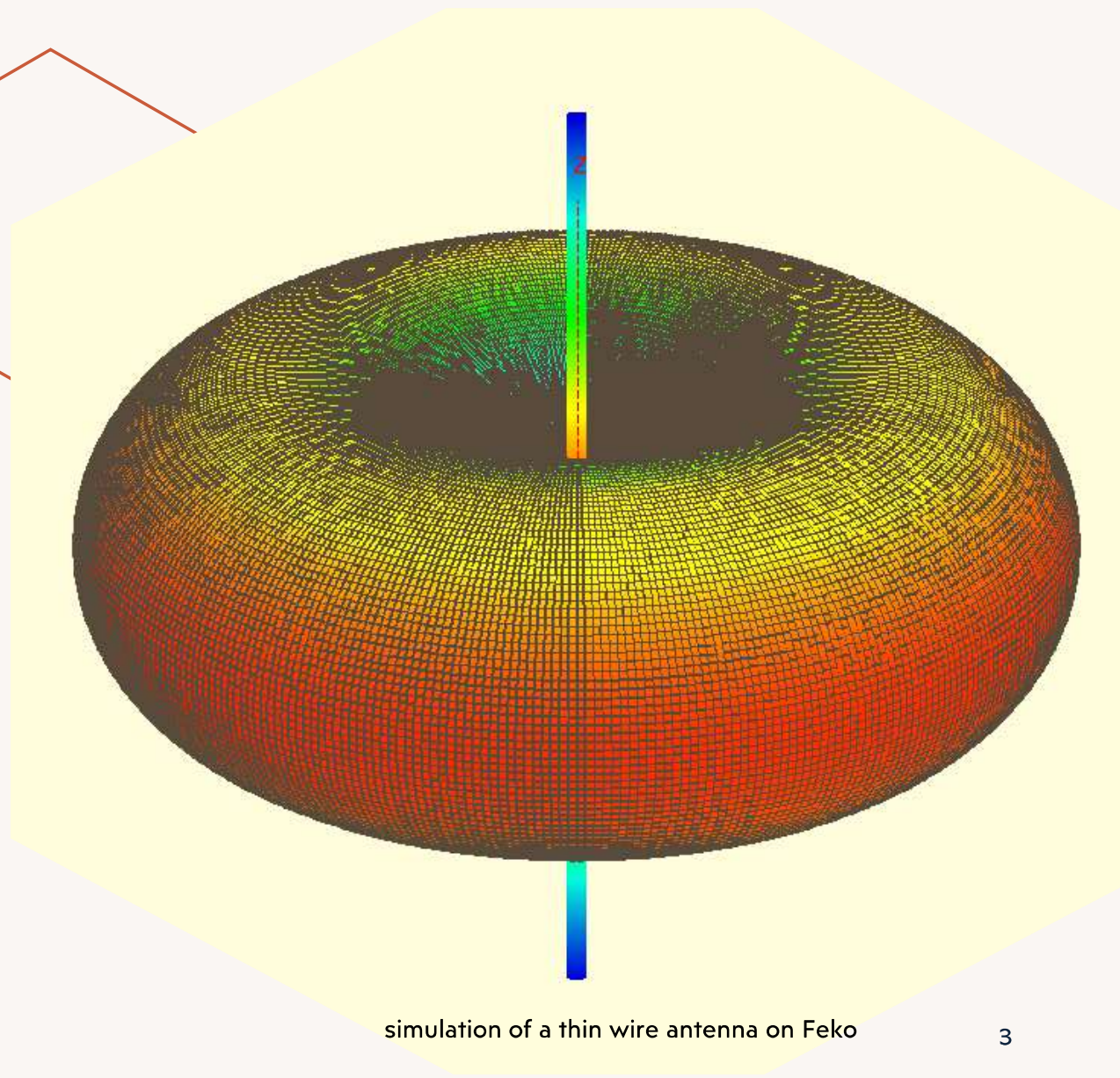
Summary

Presentation Title
Presentation title



Introduction

The *Method of Moments (MoM)* is a numerical technique used to solve integral equations in electromagnetics, particularly for antenna analysis. It transforms continuous equations into solvable linear systems, ideal for modeling thin-wire antennas. MoM calculates important parameters like current distribution and input impedance, essential for antenna design. It is especially valuable for complex structures where analytical solutions are not possible.



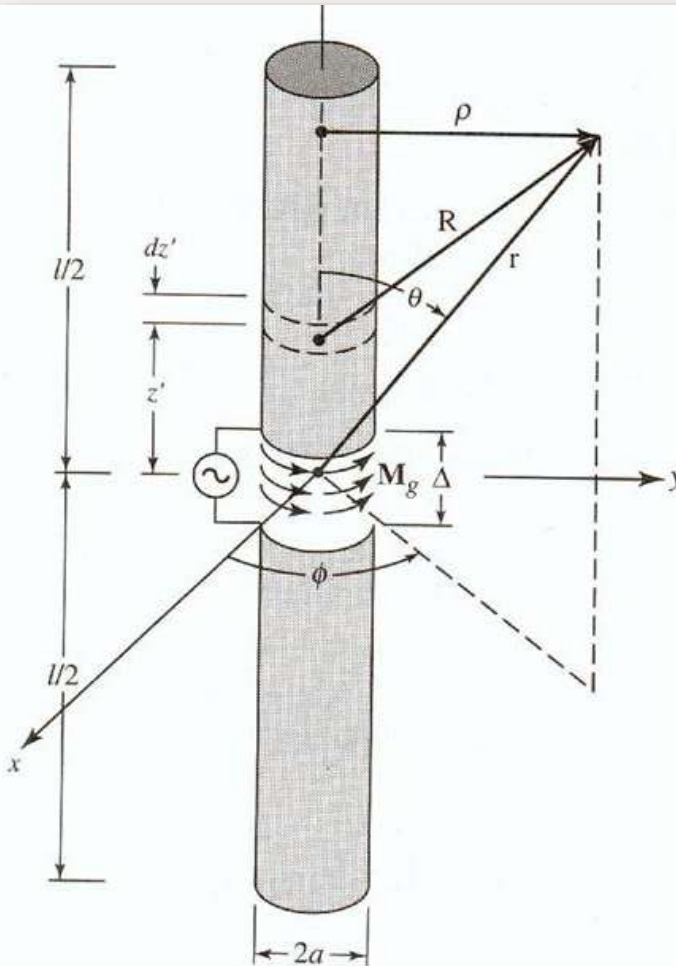
Context and Objectives

CONTEXT :

- APPLICATION OF THE METHOD OF MOMENTS TO SOLVE INTEGRAL EQUATIONS
- ANTENNA MODELING AND NUMERICAL SIMULATIONS

OBJECTIVES :

- USE THE METHOD OF MOMENTS TO ANALYZE THE CURRENT DISTRIBUTION ON A THIN-WIRE ANTENNA
- SOLVE THE INTEGRAL EQUATION USING TWO CONFIGURATION AND COMPARE THE RESULTS WITH THOSE OBTAINED FROM NEC



Key Principles Of the Method of Moments

Discretization

Divide the structure into small segments and
Approximate the current distribution with basis
functions

```
N = [7, 17, 27];
nb_of_segments = N(m);
Zmn = zeros(nb_of_segments, nb_of_segments);
delta = 1 / nb_of_segments;
```

Impedance Matrix Z_{mn}

Rows: Observation points (testing functions).
Columns: Current contributions (basis functions).

$$\begin{pmatrix} Z_{11} & \cdots & Z_{1N} \\ \vdots & \ddots & \vdots \\ Z_{N1} & \cdots & Z_{NN} \end{pmatrix}$$

Integral Equation

Formulate the integral equation using Green's
function.

$$Z_{mn} = \frac{j}{\omega \varepsilon} \int_{(n-1)\Delta}^{n\Delta} \left(k^2 + \frac{\partial^2}{\partial z'^2} \right) G(R) dz'$$

$$\frac{j}{\omega \varepsilon_0} \frac{k}{\sin(k\Delta)} \int_{z_m - \Delta/2}^{z_m + \Delta/2} [G(R_{n+1}) + G(R_{n-1}) - 2G(R_n) \cos(k\Delta)] dz$$

Testing Functions

Apply **test functions** to convert the integral
equation into a set of linear algebraic
equations

$$\delta(z - z_a)$$

$$g_n(z) = u \left[z - \left(z_n - \frac{\Delta}{2} \right) \right] - u \left[z - \left(z_n + \frac{\Delta}{2} \right) \right]$$

Solution

$$I = Z^{-1} \times V$$

$$I_n = Z_{mn} \setminus V_m;$$

First using piecewise continuous basis functions and point-matching testing

```
figure;
hold on;
for m = 1:3

    nb_of_segments = N(m); % Select number of basis functions (segments)
    Zmn = zeros(nb_of_segments, nb_of_segments); % Initialize impedance matrix
    delta = 1 / nb_of_segments; % Length of each segment
    legend_labels{m} = ['Segments: ', num2str(nb_of_segments)];
    % Fill impedance matrix Zmn
    for j = 1:nb_of_segments
        for i = 1:nb_of_segments
            zm = (i - 0.5) * delta; % Midpoint of the segment
            R = sqrt(a^2 + (zm - z).^2); % Distance between observation and source points

            % Define integrand for impedance calculation using point-matching

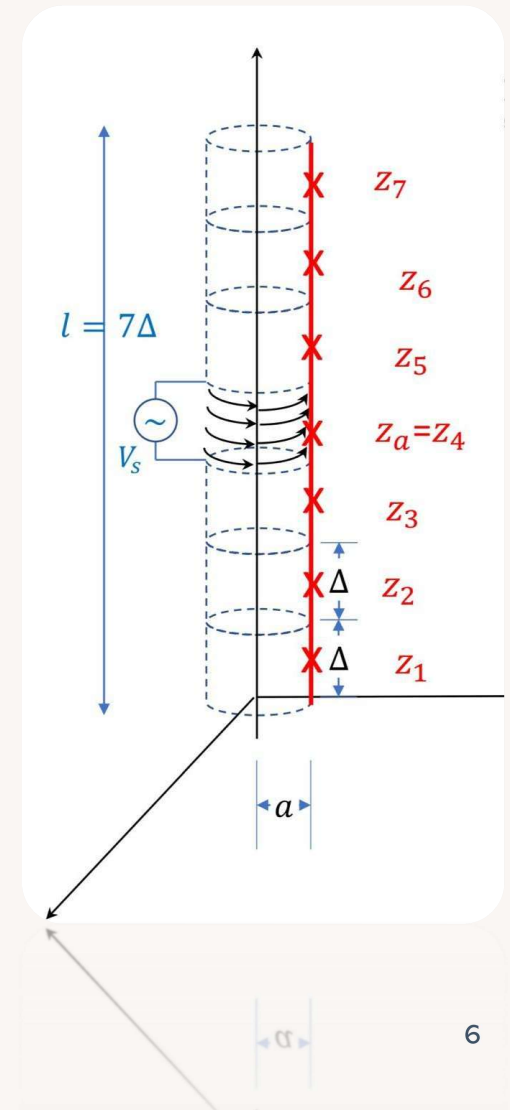
            func = inline((1j / (2 * pi * frq * e0)) * ...
                (exp(-1i * k * R) / (4 * pi * R^5) * (-R^2 * (1 + 1i * k * R) - ...
                (1i * k * R * (zm - z).^2 - (1 + 1i * k * R) * (3 + 1i * k * R) * (zm - z).^2)) + ...
                k^2 * exp(-1i * k * R) / (4 * pi * R)));

            Zmn(j, i) = quad(func, (j-1) * delta, j * delta); % Numerical integration over segment
        end
    end

    % Define excitation voltage vector and solve for current distribution I_n
    V_m = zeros(nb_of_segments, 1); % Initialize voltage vector
    V_m((nb_of_segments + 1) / 2) = 1 / delta; % Excitation at the center segment

    I_n = Zmn \ V_m; % Solve for current distribution I_n
    z_N = linspace(delta / 2, 1 - delta / 2, nb_of_segments); % Segment midpoints for plotting

    % Store total impedance by taking the reciprocal of center segment current
    impedance_values(m) = 1 / I_n((nb_of_segments + 1) / 2);
end
```



Second using piecewise sinusoidal basis functions and piecewise continuous test functions

```
figure;
hold on;
for m = 1:3
    nb_of_segments = N(m); % Number of segments
    Zmn2 = zeros(nb_of_segments, nb_of_segments); % Initialize impedance matrix
    delta = 1 / (nb_of_segments + 1); % Segment length with sinusoidal basis
    legend_labels{m} = ['Segments: ', num2str(nb_of_segments)];
    % Fill impedance matrix Zmn2
    for j = 1:nb_of_segments
        for i = 1:nb_of_segments
            zm = i * delta; % Center of each segment
            zm_1 = zm - delta;
            zm_2 = zm + delta;

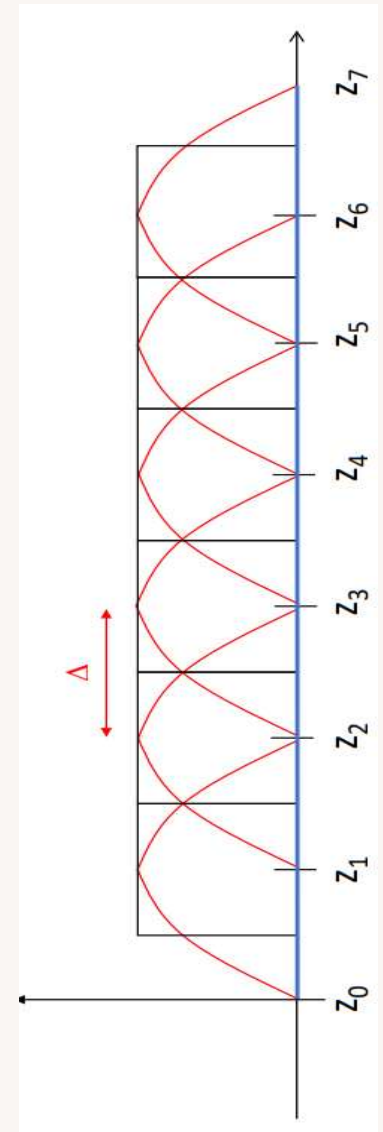
            % Calculate distances for sinusoidal basis function points
            R = sqrt(a^2 + (zm - z).^2);
            R_1 = sqrt(a^2 + (zm_1 - z).^2);
            R_2 = sqrt(a^2 + (zm_2 - z).^2);

            % Define integrand for sinusoidal basis function configuration
            func2 = inline((1j / (2 * pi * frq * e0)) * (k / sin(delta * k)) * (...
                (exp(-1j * k * R_2) / (4 * pi * R_2)) + ...
                (exp(-1j * k * R_1) / (4 * pi * R_1)) - ...
                (2 * (exp(-1j * k * R) / (4 * pi * R)) * cos(k * delta))));

            Zmn2(j, i) = quad(func2, (j - 0.5) * delta, (j + 0.5) * delta); % Numerical integration over segment
        end
    end

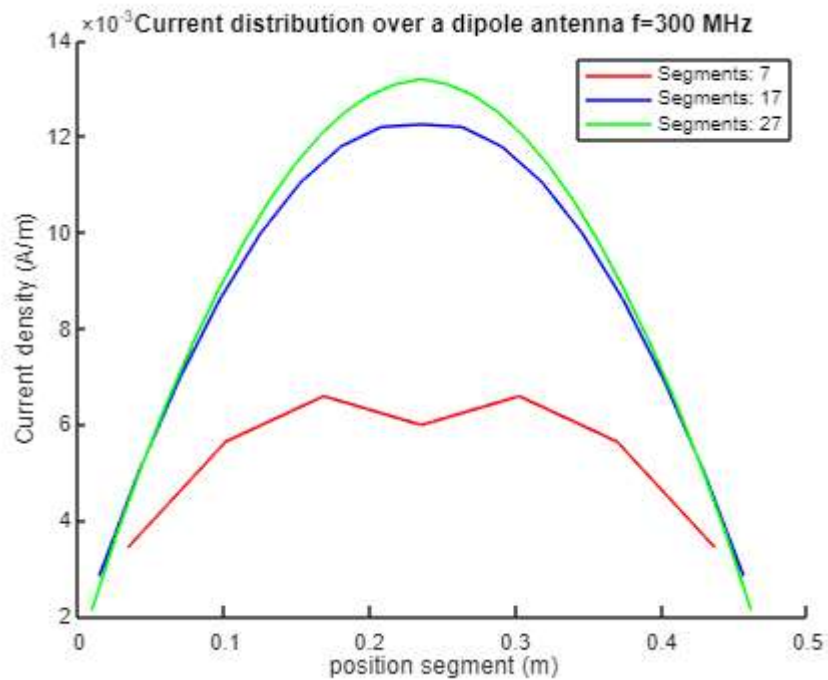
    % Define excitation vector and solve for current distribution I_n2
    V_m2 = zeros(nb_of_segments, 1);
    V_m2((nb_of_segments + 1) / 2) = 1; % Center excitation

    I_n2 = Zmn2 \ V_m2; % Solve for current distribution
    z_N = linspace(delta, 1 - delta, nb_of_segments); % Segment midpoints for plotting
end
```

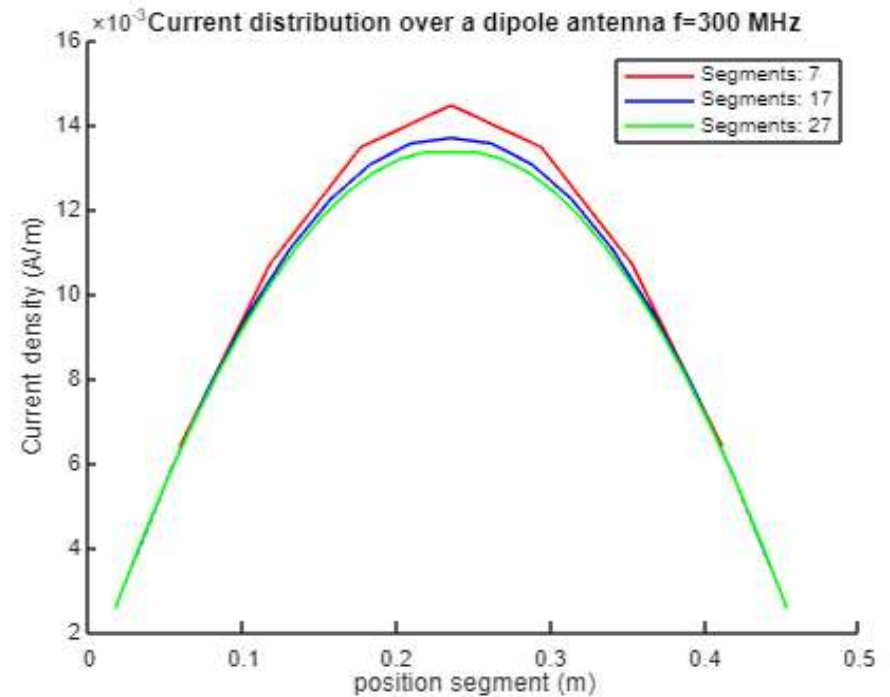


Output results

First Method

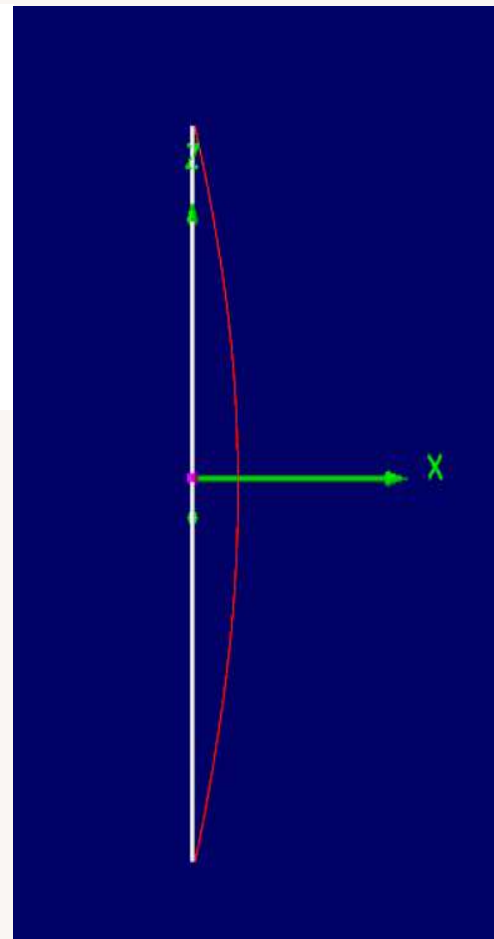


Second Method



Comparison using nec software

Number_of_Segments	Impedance_Value	Method
"7"	"122.6052-113.6914i"	"Method 1"
"17"	"81.08956-10.11419i"	"Method 1"
"27"	"75.50314+6.395627i"	"Method 1"
"_ _"	"_ _ _ _ _ _ _ _"	"_ _ _ _ _"
"7"	"68.9659+5.56679i"	"Method 2"
"17"	"73.12-1.0705i"	"Method 2"
"27"	"74.8893-3.44255i"	"Method 2"



Main [V5.9.3] (F2)

File Edit Settings Calculate Window Show Run Help

Filename: EXAMPLE1.out

Frequency: 300 Mhz
Wavelength: 0.999 mtr

Voltage: 103 + j0 V
Current: 0.97 - j0.56 A

Impedance: 80 + j46.2
Parallel form: 107 // j185

S.W.R.50: 2.33
Efficiency: 100 %
Radiat-eff: 99.92 %
RDF [dB]: 2.17

Series comp.: 11.48 pF
Parallel comp.: 2.875 pF
Input power: 100 W
Structure loss: 0 uW
Network loss: 0 uW
Radiat-power: 100 W

Environment: ☐ Loads ☐ Polar
FREE SPACE

Comment: Example 1 : Dipole in free space
See GetStarted.txt

Seg's/patches: 27
Pattern lines: 5329
Freq/Eval steps: 1
Calculation time: 0.063 s

Theta: start -180 stop 180 count 73 step 5
Phi: start 0 stop 360 count 73 step 5