

$$1a) S = \frac{1800}{0.85} = 2117.6 \text{ kVA}$$

$$\text{Voltage} = 22 \text{ kV}$$

$$\text{Phases} = 3\text{-phase}$$

$$\text{No. of wires} = 3\text{-wire}$$

$$\text{Earthing System} = \text{TNS}$$

$$I_{\max} = \frac{1800 \times 10^3}{0.85 \times 22 \times 10^3 \times \sqrt{3}} = 55.57 \text{ A}$$

1b) Isolating Transformer.

The neutral of the secondary side of the isolating transformer is not earthed.
It is the separation of neutral from earth.

2. Purpose of SOA

The basic purpose is to move the construction industry towards a more systematic approach in setting up of temporary electrical installation. This also applies to festive lighting, trade-fairs, mini-fairs and exhibition sites.

The SOA must be totally enclosed with all the live parts totally protected from direct contact.

Socket outlets must be equipped with MCB, RCCB. Fuses are not allowed.

110V - yellow.

230V - blue

400V - red

Daily for night market.

Q 3a)

A person can receive an electric shock in two ways, firstly by coming into contact with live parts and secondly by touching metallic parts that have become live due to a fault.

Direct contact is by coming into contact with live parts.

Indirect contact is by touching metallic parts that have become live due to a fault.

Indirect contact

- Earthed Equipotential Bonding and Automatic Disconnection of Supply
- Double Insulation

b) $I_1 = I_2$

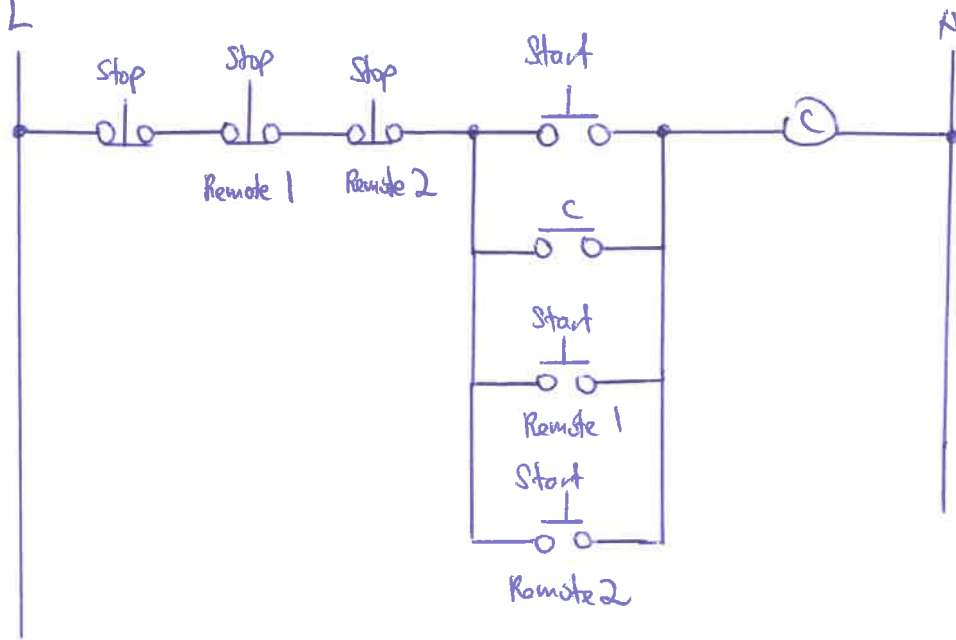
$$I_1 = \frac{230 \text{ V}}{23 \Omega} = 10 \text{ A}$$

$$I_2 = 10 \text{ A}$$

$$\begin{aligned} \text{Since } V_L &= 400 \text{ V, } V_R = 400 - (I_2 \times 25) \\ &= 400 - (10 \times 25) \\ &= 150 \text{ V} // \end{aligned}$$

$$\begin{aligned} R_X &= \frac{V_R}{I_R} = \frac{150}{10} \\ &= 15 \Omega // \end{aligned}$$

Q4.



Q5.i) 20s

Yes, discrimination is achieved since the tripping time of the 40A Type C MCB is 60s for overload current of 100A.

ii) 15s.

40A Type C MCB (a) 165A \rightarrow 33s.

Yes, discrimination is achieved.

iii) 0.1s.

40A Type C MCB (a) 320A \rightarrow 7s.

Yes, discrimination is achieved.

6a) Minimum acceptable reading according to 55638 is $1.0 \text{ m}\Omega$.

The reading of $0.4 \text{ m}\Omega$ for 500 points is acceptable if the 500 points are split into about 5 sections of each 100 points, which will result in $0.4 \times 5 = 2 \text{ m}\Omega$ for each of the phases.

b) Continuity of protective conductors

Continuity of Ring final circuit conductors.

Polarity check

Earth Fault Loop Impedance.

Earth electrode Resistance

Functional test of RCB.

BI:

Description	Connected Load	D.F.	Current Demand
30 nos. 2x32 W Fluorescent lamps	$\frac{30 \times 2 \times 32 \times 1.8}{230} = 15.03 \text{ A}$	90%	13.53 A
13A SSD (Largest ckt)	$\frac{4 \times 10^3}{230} = 17.39 \text{ A}$	100%	17.39 A
13A SSD (Remainding ckt)	$\frac{3 \times 4 \times 10^3}{230} = 52.17 \text{ A}$	50%	26.09 A
1st storage water heater	$\frac{1.2 \times 10^3}{230} = 5.217 \text{ A}$	100%	5.217 A
1st instantaneous water heater	$\frac{2.5 \times 10^3}{230} = 10.87 \text{ A}$	100%	10.87 A
			<hr/> 73.097 A (1- ϕ)
Multi-split air- conditioning, 15kW 3 phase, 92% eff, pf=0.85	$\frac{15 \times 10^3}{\sqrt{3} \times 400 \times 0.92 \times 0.85} = 23.21 \text{ A}$	100%	23.21 A (3- ϕ)

i) Three phase max demand = $\frac{73.097}{3} + 23.21 = 47.58 \text{ A}$

ii) $47.58 \times 1.25 = 59.47 \text{ A}$

\therefore We can choose 63A TPN MCB.

iii) For motor, $I_N \geq 2 \times I_B$

$$I_N \geq 2 \times 23.21 \text{ A}$$

$$I_N \geq 46.42 \text{ A}$$

\therefore We can choose 50A TPN MCB. Type B.

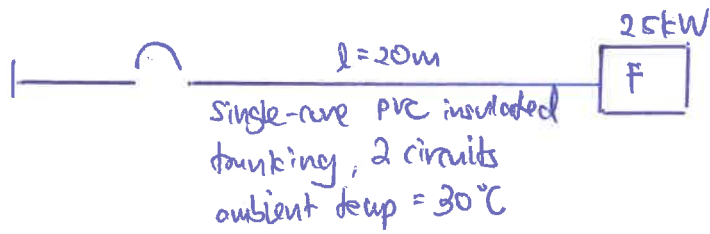
Automatic disconnection of supply and Earthed equipotential bonding.

B2 a)

$$i) I_B = \frac{25 \times 10^3}{400 \times 15 \times 1} = 36.08 \text{ A}$$

Since $I_A \geq I_B$, we can choose 40A TPN MCB.

ii)



From Table 4C1, $C_a = 1.0$

From Table 4B1, $C_g = 0.8$

$$C_i = 1$$

$$I_t \geq \frac{I_A}{C_a \times C_g \times C_i}$$

$$I_t \geq \frac{40}{1.0 \times 0.8 \times 1.0}$$

$$I_t \geq 50 \text{ A}$$

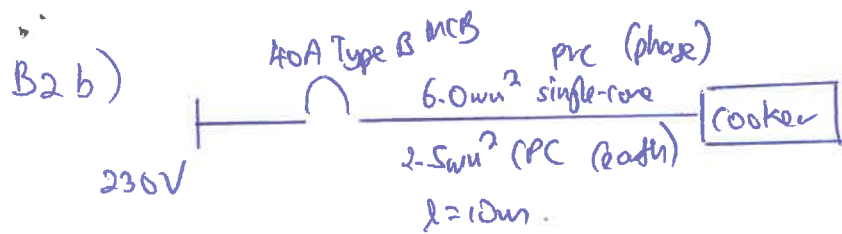
From Table 4D1A, we can choose 10 mm^2 single-core PVC insulated cables with a current carrying capacity of 50A.

$$iii) V_{drop} = \frac{V_{cc} \times I_B \times l}{1000}$$

$$V_{cc} = 3.8 \text{ mV/A/m (from table 4D1B)}$$

$$\therefore V_{drop} = \frac{3.8 \times 36.08 \times 20}{1000} = 2.74 \text{ V} < 4\% \text{ of } 400 \text{ V}$$

$\therefore 10 \text{ mm}^2$ single-core PVC insulated cable can meet SS638 requirement of 4% voltage drop.



$$Z_E = 0.65 \Omega$$

$$Z_S = Z_E + (R_1 + R_2)$$

From Table 17A, $R_1 + R_2 = 10.49 \text{ m}\Omega/\text{m}$

$$\therefore Z_S = 0.65 + 1.38 \left(\frac{10.49 \times 10}{1000} \right)$$

$$= 0.65 + 0.14476$$

$$= 0.795 \Omega$$

From Table 41B2 (L),

Max earth fault loop Impedance for 40A Type B MCB = 1.15Ω

$$Z_S (\text{max}) \geq Z_S (\text{cal})$$

\therefore CPC meets both shock protection requirement.

$$k^2 S^2 \geq I^2 t$$

$$(115^2)(S^2) \geq (289^2)(0.1)$$

$$S \geq 0.6315 \text{ mm}^2$$

$$I_F = \frac{230}{0.795} = 289.3 \text{ A}$$

For 289.3 A, $t = 0.1 \text{ s}$,
(40A Type B MCB)

\therefore Size of 2.5mm² meet thermal constraint requirement.