

**B1.**

(a) Either one of the following:

[2 marks]

- (1) Full-wave centre-tapped transformer rectifier
- (2) Full-wave bridge rectifier
- (3) Full-wave rectifier

(b) The frequency of the output voltage is twice that of the input ac voltage:  $f_o = 2 \times 200 \text{ Hz} = \underline{400 \text{ Hz}}$

[2 marks]

(c) Capacitor (RC filter)

[2 marks]

(d) To reduce the large fluctuations in the output of the rectifier

[2 marks]

(e) Peak-to-peak voltage of ripple:  
 $V_{r(p-p)} = 2 \text{ V}$

RMS value of Ripple voltage:

$$V_{r(rms)} = \frac{V_{r(p-p)}}{2\sqrt{3}} = \frac{2}{2\sqrt{3}} = 0.5773 \text{ V} \quad [2 \text{ marks}]$$

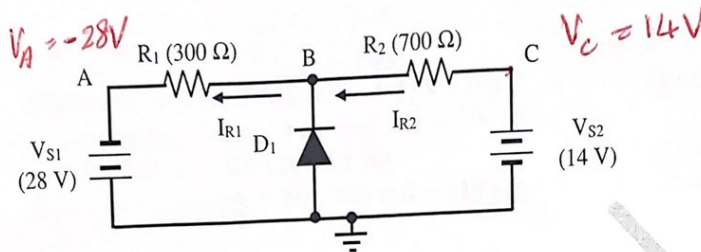
$$\begin{aligned} \text{Average output, } V_{DC} &= V_p - \frac{1}{2} V_{r(p-p)} \\ &= 101 \text{ V} - \frac{1}{2} (2 \text{ V}) = 100 \text{ V} \end{aligned} \quad [2 \text{ marks}]$$

Ripple factor,  $r$ :

$$r = \frac{V_{r(rms)}}{V_{DC}} = \frac{0.5773 \text{ V}}{100 \text{ V}} = 0.005773 = \underline{0.5773 \%} \quad [2 \text{ marks}]$$

**Total: [14 marks]**

B2.



- (a) Applying voltage divider rule to the circuit ABC comprising  $R_1$  and  $R_2$  with diode  $D_1$  removed:

$$V_{BA} = (V_C - V_A) \frac{R_1}{R_1 + R_2}$$

$$V_{BA} = (14 - (-28)) \frac{300}{300 + 700} = 12.6V$$

$$V_B = V_{BA} + V_A = 12.6V + (-28V) = -15.4V$$

[2 marks]

[2 marks]

{ Alternatively,

$$\text{Total current} = (V_{S1} + V_{S2}) / (R_1 + R_2) = (28V + 14V) / 1000\Omega$$

$$= 0.042 \text{ A} = 42 \text{ mA}$$

$$V_{BA} = 0.042 \text{ A} \times 300\Omega = 12.6 \text{ V}$$

$$V_B = V_{BA} + V_A = 12.6 \text{ V} + (-28V) = -15.4 \text{ V}$$

Since  $V_B$  is more negative than  $-0.7 \text{ V}$ ,  $D_1$  will be forward biased when it is connected between node B and Ground  
Diode is **forward biased** ✖

[2 marks]

- (b) Since the diode is forward biased,  $V_B = -0.7 \text{ V}$  ✖

[2 marks]

- (c) Current flowing through  $R_1$ ,  $I_{R1} = (V_B - V_A) / R_1$   
 $I_{R1} = (-0.7V - (-28V)) / 300\Omega = 0.091 \text{ A} = 91 \text{ mA}$  ✖  
 In the direction from **node B to node A** ✖

[1 mark]

[1 mark]

Current flowing through  $R_2$ ,  $I_{R2} = (V_C - V_B) / R_2$   
 $I_{R2} = (14V - (-0.7V)) / 700\Omega = 0.021 \text{ A} = 21 \text{ mA}$  ✖  
 In the direction from **node C to node B** ✖

[1 mark]

[1 mark]

- (d) Applying KCL at node B:

$$\text{Diode current, } I_D = I_{R1} - I_{R2}$$

$$I_D = (91 - 21) \text{ mA} = 70 \text{ mA} \text{ ✖}$$

[2 marks]

Total: [14 marks]

B3.

$$\text{or } Z_Z = \frac{V_{Z_{\max}} - V_{Z_T}}{I_{Z_{\max}} - I_{Z_T}} \Rightarrow 12 = \frac{6.8 - 6.2}{I_{Z_{\max}} - 60\text{mA}} \Rightarrow I_{Z_{\max}} = 110\text{mA}$$

(a)

Change of voltage:  $\Delta V = (6.8 - 6.2) \text{ V} = 0.6 \text{ V}$ Corresponding change of current:  $\Delta I = \Delta V / Z_Z$ 

$$\Delta I = 0.6 / 12 = 0.05 \text{ A} = 50 \text{ mA}$$

$$I_{ZM} = (I_{ZT} + \Delta I) \text{ mA} = (60 + 50) \text{ mA} = 110 \text{ mA}$$

[1 mark]

[1 mark]

[2 marks]

(b)

(i)

The total current that flows through R ( $33\Omega$ ) is

$$I_{33\Omega} = \frac{V_{IN} - V_{ZM}}{R} = \frac{12 - 6.8}{33} = 157.6 \text{ mA}$$

[2 marks]

(ii)

Since  $I_{ZM}$  is flowing through the Zener diode:

$$I_L = I_{33\Omega} - I_{ZM} = (157.6 - 110) \text{ mA} = 47.6 \text{ mA}$$

[4 marks]

(c)

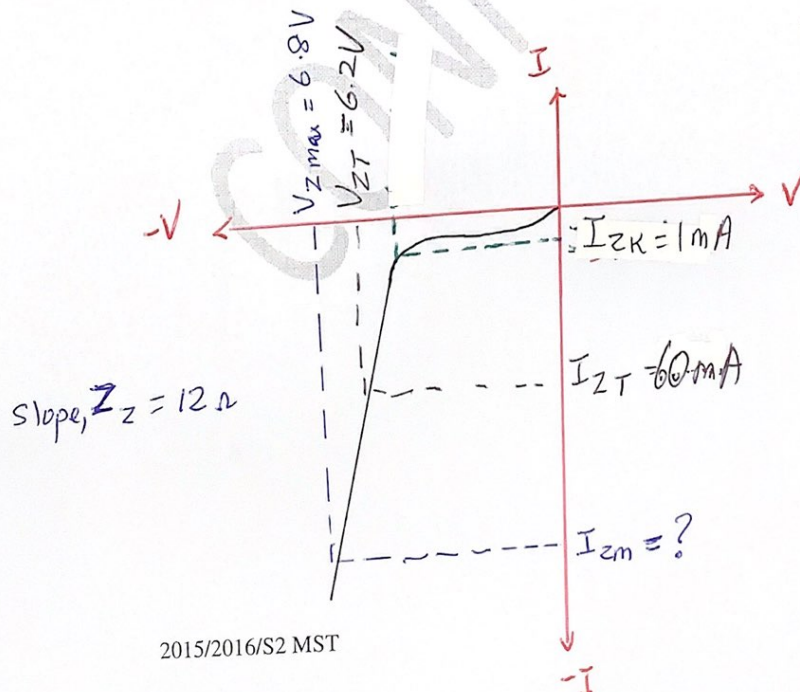
$$\begin{aligned} \text{Power } P_{33\Omega} &= I_{33\Omega}^2 R = (157.6 \text{ mA})^2 \times 33\Omega \\ &= 0.1576^2 \times 33 \text{ W} \\ &= 0.82 \text{ W} \end{aligned}$$

[2 marks]

Select resistor with power rating of 1W $(R > 0.82 \text{ W})$ 

[2 marks]

Total: [14 marks]





B4.

(a)

$$I_B = (4 - 0.7)/10 \text{ k} = 0.33 \text{ mA} \quad [1 \text{ mark}]$$

$$I_C = 180 \times 0.33 = 59.4 \text{ mA} \quad [1 \text{ mark}]$$

$$I_E = 0.33 + 59.4 = \underline{59.73 \text{ mA}} \quad [2 \text{ marks}]$$

$$I_E = I_B + I_C$$

$$I_C R_C = 59.4 \text{ mA} \times 150 \Omega = 8.91 \text{ V} \quad [2 \text{ marks}]$$

$$V_{CE} = 12 - 8.91 = \underline{3.09 \text{ V}} \quad [2 \text{ marks}]$$

$$V_{CE} = V_{CC} - I_C R_C$$

(b)

Active modeReason:  $V_{CE}$  is not less than 0.2 V

(Alternatively,

$$I_C (\text{sat}) = (V_{CC} - V_{CE(\text{sat})})/R_C = (12 - 0.2)/150 = 78.67 \text{ mA}$$

 $I_C$  is less than  $I_{C(\text{sat})}$ )

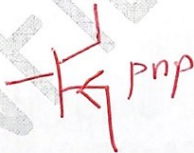
(c)

An NPN transistor

[2 marks]

Total: [14 marks]

If PNP transistor,



B5.

- (a) (i) light dependent resistor  
(ii) thermistor  
(iii) moisture sensor

[1 mark]  
[1 mark]  
[1 mark]

- (b) (i) The voltage across LDR is given by:

$$V_{LDR} = \frac{R_{LDR}}{R_{LDR} + R_1} \times V_{CC}$$

$$R_1 = 10 \text{ k}\Omega$$

When the light bulb is in the OFF state:

$$V_{LDR} = 0.6 \text{ V}$$

$$0.6 \text{ V} = \frac{R_{LDR}}{R_{LDR} + 10 \text{ k}} \times 9 \text{ V}$$

[1 mark]

$$(9 - 0.6)R_{LDR} = 0.6 \times 10 \text{ k}$$

[1 mark]

$$\rightarrow R_{LDR} = (6000/8.4) \Omega = 714.3 \Omega$$

[1 mark]

When the light bulb is in the ON state:

$$V_{LDR} = 4.2 \text{ V}$$

$$4.2 \text{ V} = \frac{R_{LDR}}{R_{LDR} + 10 \text{ k}} \times 9 \text{ V}$$

[1 mark]

$$(9 - 4.2)R_{LDR} = 4.2 \times 10 \text{ k}$$

[1 mark]

$$\rightarrow R_{LDR} = (42000/4.8) \Omega = 8750 \Omega = 8.75 \text{ k}\Omega$$

[1 mark]

$$\text{Range of } R_{LDR} = 714.3 \Omega \text{ to } 8.75 \text{ k}\Omega$$

(ii)

When the light bulb is in the OFF state:  $I_B = 0 \text{ A}$

$$I_C = 0 \text{ A}$$

$$V_{CE} = 9 \text{ V}$$

[1 mark]

$$V_{CC} = V_{CE} = 9 \text{ V}$$

[1 mark]

When the light bulb is in the ON state:

$$V_{CE} = 0.2 \text{ V}$$

$$V_{CC} = V_{BULB} + V_{CE}$$

[1 mark]

$$V_{BULB} = \text{Supply voltage} - V_{CE} = 9 \text{ V} - 0.2 \text{ V} = 8.8 \text{ V}$$

[1 mark]

$$I_C = V_{BULB} / R_{BULB} = 8.8 \text{ V} / 200 \Omega = 0.044 \text{ A} = 44 \text{ mA}$$

[1 mark]

Total: [14 marks]