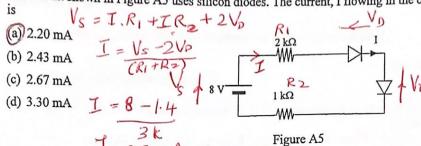
SINGAPORE POLYTECHNIC

ET1006

The circuit shown in Figure A5 uses silicon diodes. The current, I flowing in the diode



- Which one of the following sequences can be a correct order of a DC power supply? A6.
 - Step-up transformer, filter, rectifier and voltage regulator
 - Step-up transformer, voltage regulator, filter and rectifier
 - Step-down transformer, rectifier, filter and voltage regulator
 - (d) Step-down transformer, filter, rectifier and voltage regulator
- Which one of the following IC voltage regulators gives a DC output voltage of 24 V? A7.
 - 7918
 - (b) 7924
 - 7818 (c)
 - 7824
- In a PNP transistor which of the following layers have holes as the majority carrier? A8.
 - Emitter and base layers (a)
 - Collector and base layers (b)
 - Emitter and collector layers (0)
 - Emitter, collector and base layers
- The collector current of a NPN transistor is approximately proportional to the base A9. current when it is operating in the _____ region.
 - saturation
 - avalanche breakdown (b)
 - 0 active
 - cut-off
- Which one of the following devices is NOT a transducer?
 - Photodiode (a)
 - Zener diode (b)
 - Moisture sensor (c)
 - Light dependent resistor (d)

SECTION B (14 marks each)

2016/2017/S2 MST

- B1. (a) Explain the process of doping in producing n-type semiconductors.
 - (b) For the circuit shown in Figure B1,

[2 marks]

Page 4 of 7

- (i) state with reason whether the LED is reverse-biased or forward biased.
 [2 marks]
- (ii) calculate the currents flowing through resistors R₁ and R₂. Indicate the direction of both currents. [9 marks]
- (iii) calculate the current flowing through the LED. [1 mark]

Assume the LED used in the circuit has a forward voltage drop of 1.9 V.

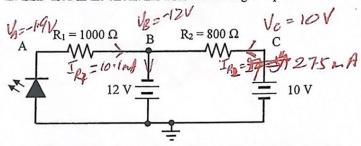
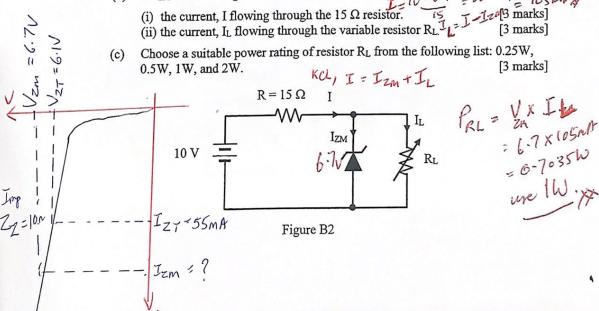


Figure B1

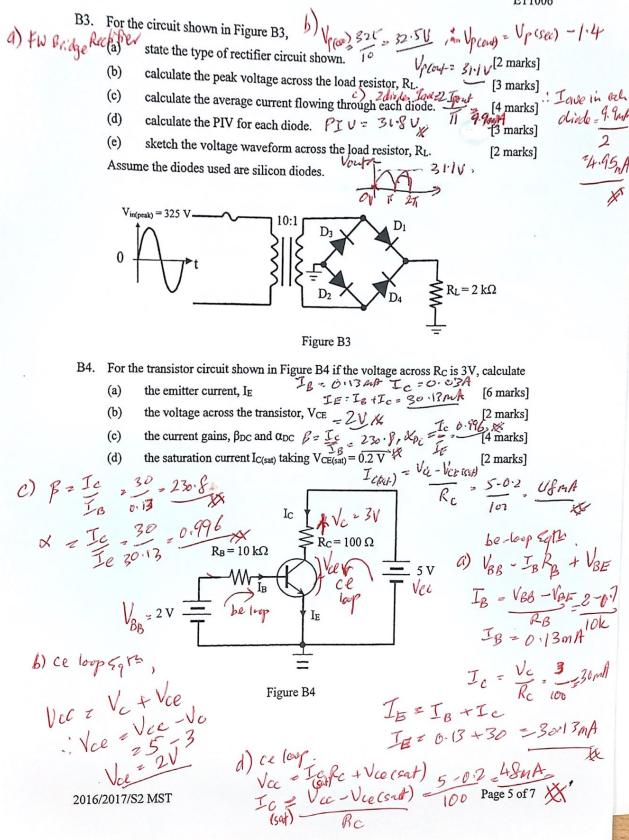
- B2. The circuit shown in Figure B2 is a Zener diode regulator circuit. Given $V_{ZT} = 6.1 \text{ V}$ at $I_{ZT} = 55 \text{ mA}$; $Z_Z = 10 \Omega$; and $V_{ZM} = 6.7 \text{ V}$.
 - (a) Find I_{ZM} of the Zener diode.

 2 = I_{ZM} I_{ZT} [5 marks
 - (b) If I_{ZM} flows through the Zener diode, determine: 10-6-7 = 220 mg to 105 mg to 10



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The moisture sensor circuit shown in Figure B5 is used to detect rain drops. The LED will light up when the circuit shown in Figure B5 is used to detect rain drops. The LED will light up when the sensor gets wet. The circuit has the following parameters:

Resistance of the moisture sensor when it is wet, $R_{M(wet)} = 0 \Omega$ (close-circuited) Resistance of the moisture sensor when it is dry, $R_{M(dry)} = \infty \Omega$ (open-circuited) $V_{LED} = 2.1 \text{ V}$ when it is forward biased and conducting The current gain of the transistor, $\beta_{DC} = 180$ and $V_{CE(sat)} = 0.2V$

- OV (a) What is the voltage across R₂ when the moisture sensor is dry? [2 marks]
- When the moisture sensor is wet, calculate
 - (i) the voltage across R_2 . $V_{F2} = \frac{P_L}{R_1 + R_2} \times V_{CC} = \frac{7 \cdot 13 \text{ V}}{7 \cdot 13 \text{ V}}$. [4 marks] (ii) the base current, $I_{B.} = V_{CL} 0.7 = 0.238 \text{ m/h}$ (iii) the saturated collector current, $I_{C(sat)} = V_{CC} V_{CC} = \frac{278 \text{ m/h}}{120 \text{ marks}}$ [3 marks]
- State with reason whether the transistor is operating in the saturation or active IB(min) > IBCSUF) | IRCSUF = ICOUP[3 marks] 0.238mb > 0.1296mb | 180 region.

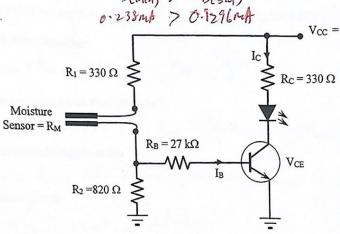


Figure B5

- End of Paper -

Page 6 of 7

SECTION B $(5 \times 14 = 70 \text{ marks})$

No.	SECTION B (5 \times 14 = 70 marks)	MARKS	TOTAL MARKS
B1			
(a)	To produce n-type semiconductors pentavalent impurities are added to pure semiconductor materials. This will result in more free electrons.	2	
(b)	With the LED removed from the circuit	1	
(i)	$V_A = V_B = -12 \text{ V}$ Since V_A is less than -1.9V the LED will be forward biased.	1	à
	Since VA is less than	1	
(ii)	With the LED in the circuit.	1	
	$V_A = -1.9 \text{ V}$	1	
	$V_B = -12 \text{ V}$		
	$I_{AB} = I_{R1} = \frac{(-1.9 - (-12))}{1000} = 10.1 \text{ mA}$	2	
	$V_C = 10 \text{ V}$	2	
	$I_{\text{CB}} = I_{\text{R2}} = \frac{(10 - (-12))}{800} = 27.5 \text{ mA}$	1	
	Direction of I _{R1} from A to B	1	
	Direction of I _{R2} from C to B	1	
(iii)	$I_{\text{LED}} = I_{\text{R1}} = 10.1 mA$		14
			-



		Engineering II (E11006)		MIDI
(a) Change of voltage: $\triangle V = (6.7 - 6.1) \ V = 0.6 \ V$ Corresponding change of current: $\triangle I = \triangle V \ / Z_Z$ $\triangle I = 0.6 \ / \ 10 = 0.06 \ A = 60 \ \text{mA}$ $I_{ZM} = (I_{ZT} + \triangle I) \ \text{mA} = (55 + 60) \ \text{mA} = 115 \ \text{mA}$ (b) (i) The total current that flows through R is $I = \frac{V_{IN} - V_Z}{R} = \frac{10 - 6.7}{15} = 220 \ \text{mA}$ 3 (ii) Since I_{ZM} is flowing through the Zener diode, load current I_L $I_L = I - I_{ZM} = 220 - 115 \ \text{mA} = 105 \ \text{mA}$ (c) Power $P_L = I_L V_L = 105 \text{m} \times 6.7$ $= 703.5 \ \text{mW} = 0.7035 \ \text{W}$ Select resistor with power rating of 1 W 14 B3 (a) Full wave bridge rectifier (b) $V_{sec(p)} = \frac{325}{10} = 32.5 \ V$ $V_{out(p)} = V_{sec(p)} - 1.4$ $= 32.5 - 1.4 = 31.1 \ \text{V}$ (c) $I_{out(p)} = \frac{31.1}{2k} = 15.55 \ \text{mA}$ $I_{out(m)} = \frac{31.1}{2k} = 15.55 \ \text{mA}$ $I_{out(m)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \ \text{mA}$ I_{Lvg} in each diode = $9.9/2 = 4.95 \ \text{mA}$ 1 1 1 1 1 1 1 1 1 1 1 1 1	No.	SOLUTION	MARKS	TOTAL
Corresponding change of current: $\Delta I = \Delta V / Z_Z$ $\Delta I = 0.6 / 10 = 0.06 \text{ A} = 60 \text{ mA}$ $I_{ZM} = (I_{ZT} + \Delta I) \text{ mA} = (55 + 60) \text{ mA} = 115 \text{ mA}$ (b) (i) The total current that flows through R is $I = \frac{V_{IN} - V_Z}{R} = \frac{10 - 6.7}{15} = 220 \text{ mA}$ 3 (ii) Since I_{ZM} is flowing through the Zener diode, load current I_L $I_L = I - I_{ZM} = 220 - 115 \text{ mA} = 105 \text{ mA}$ 3 (c) Power $P_L = I_L V_L = 105 \text{m} \times 6.7$ $= 703.5 \text{ mW} = 0.7035 \text{ W}$ Select resistor with power rating of 1 W 14 B3 (a) Full wave bridge rectifier (b) $V_{sec(p)} = \frac{325}{10} = 32.5 V$ $V_{out(p)} = V_{sec(p)} - 1.4$ $= 32.5 - 1.4 = 31.1 \text{ V}$ 2 (c) $I_{out(p)} = \frac{31.1}{2k} = 15.55 \text{ mA}$ $I_{out(mg)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \text{ mA}$ $I_{svg} \text{ in each diode} = 9.9/2 = 4.95 \text{ mA}$ 1 1 1 1 1 1 1 1 1 1 1 1 1	32.			
(i) The total current that flows through R is $I = \frac{V_{IN} - V_Z}{R} = \frac{10 - 6.7}{15} = 220 \text{ mA}$ (ii) Since I_{ZM} is flowing through the Zener diode, load current I_L $I_L = I - I_{ZM} = 220 - 115 \text{ mA} = 105 \text{ mA}$ (c) Power $P_L = I_L V_L = 105 \text{m} \times 6.7$ $= 703.5 \text{ mW} = 0.7035 \text{ W}$ Select resistor with power rating of 1 W 14 B3 (a) Full wave bridge rectifier (b) $V_{sec(p)} = \frac{325}{10} = 32.5 V$ $V_{out(p)} = V_{sec(p)} - 1.4$ $= 32.5 - 1.4 = 31.1 \text{ V}$ 2 (c) $I_{out(p)} = \frac{31.1}{2k} = 15.55 \text{ mA}$ $I_{out(avg)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \text{ mA}$ $I_{avg} \text{ in each diode} = 9.9/2 = 4.95 \text{ mA}$ 1 1 4	a)	Corresponding change of current: $\triangle I = \triangle V / Z_Z$ $\triangle I = 0.6 / 10 = 0.06 A = 60 \text{ mA}$	10000	
I = $\frac{V_{IN} - V_Z}{R}$ = $\frac{10 - 6.7}{15}$ = 220 mA 3 3 3 3 3 3 3 3 3	(b)	Car		
(ii) Since I_{ZM} is flowing through the Zener diode, load current I_L $I_L = I - I_{ZM} = 220 - 115 \text{ mA} = 105 \text{ mA}$ (c) Power $P_L = I_L V_L = 105 \text{m} \times 6.7$ $= 703.5 \text{ mW} = 0.7035 \text{ W}$ Select resistor with power rating of 1 W 14 B3 (a) Full wave bridge rectifier 2 (b) $V_{sec(p)} = \frac{325}{10} = 32.5 V$ $V_{out(p)} = V_{sec(p)} - 1.4$ $= 32.5 - 1.4 = 31.1 \text{ V}$ 2 (c) $I_{out(p)} = \frac{31.1}{2k} = 15.55 \text{ mA}$ $I_{out(avg)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \text{ mA}$ $I_{svg} \text{ in each diode} = 9.9/2 = 4.95 \text{ mA}$ 1 4	(i)	The total current that flows through R is		
I _L = I - I _{ZM} = 220 - 115 mA = 105 mA 3		$I = \frac{V_{IN} - V_Z}{R} = \frac{10 - 6.7}{15} = 220 \text{ mA}$	3	
Select resistor with power rating of 1 W 14 B3 (a) Full wave bridge rectifier (b) $V_{sec(p)} = \frac{325}{10} = 32.5 V$ $V_{out(p)} = V_{sec(p)} - 1.4$ $= 32.5 - 1.4 = 31.1 V$ 2 (c) $I_{out(p)} = \frac{31.1}{2k} = 15.55 \text{ mA}$ $I_{out(avg)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \text{ mA}$ I_{avg} in each diode = $9.9/2 = 4.95 \text{ mA}$ 1 1 14 15 16 17 18 19 10 10 10 11 11 11 12 13 14	(ii)		3	
B3 (a) Full wave bridge rectifier (b) $V_{sec(p)} = \frac{325}{10} = 32.5 V$ $V_{out(p)} = V_{sec(p)} - 1.4$ $= 32.5 - 1.4 = 31.1 \text{ V}$ 2 (c) $I_{out(p)} = \frac{31.1}{2k} = 15.55 \text{ mA}$ $I_{out(avg)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \text{ mA}$ I avg in each diode = $9.9/2 = 4.95 \text{ mA}$ 1 1 1 1 1 1 1 1 1 1 1 1 1	(c)	= 703.5 mW = 0.7035 W		
(a) Full wave bridge rectifier 2 (b) $V_{sec(p)} = \frac{325}{10} = 32.5 V$ $V_{out(p)} = V_{sec(p)} - 1.4$ $= 32.5 - 1.4 = 31.1 \text{ V}$ 2 (c) $I_{out(p)} = \frac{31.1}{2k} = 15.55 \text{ mA}$ $I_{out(avg)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \text{ mA}$ I_{avg} in each diode = $9.9/2 = 4.95$ mA 1 4				14
(b) $V_{sec(p)} = \frac{325}{10} = 32.5 V$ 1 $V_{out(p)} = V_{sec(p)} - 1.4$ 2 (c) $I_{out(p)} = \frac{31.1}{2k} = 15.55 \text{ mA}$ 2 $I_{out(avg)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \text{ mA}$ 1 $I_{avg} \text{ in each diode} = 9.9/2 = 4.95 \text{ mA}$ 1 4	В3			
$V_{sec(p)} = \frac{1}{10} = 32.3 V$ $V_{out(p)} = V_{sec(p)} - 1.4$ $= 32.5 - 1.4 = 31.1 \text{ V}$ $I_{out(p)} = \frac{31.1}{2k} = 15.55 \text{ mA}$ $I_{out(avg)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \text{ mA}$ $I_{avg} \text{ in each diode} = 9.9/2 = 4.95 \text{ mA}$ $1 = 4$	(a)	Full wave bridge rectifier	2	
$= 32.5 - 1.4 = 31.1 \text{ V}$ (c) $I_{out(p)} = \frac{31.1}{2k} = 15.55 \text{ mA}$ $I_{out(avg)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \text{ mA}$ $I_{avg} \text{ in each diode} = 9.9/2 = 4.95 \text{ mA}$ 1 4	(b)		1	
$I_{out(p)} = \frac{1}{2k} = 13.35 \text{ mA}$ $I_{out(avg)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \text{ mA}$ $I_{avg} \text{ in each diode} = 9.9/2 = 4.95 \text{ mA}$ 1			2	
I_{avg} in each diode = 9.9/2 = 4.95 mA 1 4	(c)	$I_{out(p)} = \frac{31.1}{2k} = 15.55 \text{ mA}$	2	
		$I_{out(avg)} = \frac{2I_{out(p)}}{\pi} = \frac{2x15.55}{\pi} = 9.9 \text{ mA}$	1	
(d) $PIV = V_{out(p)} + 0.7 = 31.1 + 0.7 = 31.8 \text{ V}$ 3		I_{avg} in each diode = $9.9/2 = 4.95$ mA	1	4
	(d)	$PIV = V_{out(p)} + 0.7 = 31.1 + 0.7 = 31.8 \text{ V}$	3	

No.	SOLUTION	MARKS	TOTAL MARKS
(e)	31.1 V 0 V	2	14
B4		2	
(a) I ₁	$_{\rm B} = \frac{\rm V_{BB} - 0.7}{\rm R_B} = \frac{\rm 2 - 0.7}{\rm 10} = 0.13 \text{ mA}$	2	
	$I_{C} = \frac{V_{C}}{R_{C}} = \frac{3}{100} = 0.03 \text{ A}$ $I_{E} = I_{B} + I_{C} = 0.13 + 30 \text{ mA} = 30.13 \text{ mA}$	2	-
(b) X	$V_{CC} = V_{CE} + I_{C}R_{C}$ $5 = V_{CE} + 3$ $V_{CE} = 5 - 3 = 2 V$	2	
1 1		2	
(c)	$\beta_{DC} = \frac{I_C}{I_B} = \frac{30}{0.13} = 230.8$ $\alpha_{DC} = \frac{I_C}{I_E} = \frac{30}{30.13} = 0.996$	2	
(1)	$V_{\text{CC}} = \frac{V_{\text{CC}} - V_{\text{CE(sat)}}}{R_{\text{C}}} = \frac{5 - 0.2}{100} = 0.048 A = 48 mA$	2	
(d)	$I_{C(sat)} = R_C$		14
			+
			Page 4 of

No.	SOLUTION	MA	RKS	TOT
B5				
(a)	V _{R2} = 0		2	
(b)	When wet R _m = 0			
(i)	$V_{R2} = \frac{V_{cc}R_2}{R_1 + R_2}$		2	
	$V_{R2} = \frac{10X820}{330 + 820} = 7.13 \text{ V}$	2		4
(ii)	$I_{B} = \frac{V_{R2} - 0.7}{R_{B}} = \frac{7.13 - 0.7}{27k} = 0.238 \text{ mA}$	2		
(iii)	$V_{CC} = V_{CE} + I_{C(sat)}R_C + V_{LED}$	1		
	$I_{C(sat)}R_{C} = V_{CC} - V_{CE} - V_{LED}$			
	$I_{C(sat)} = (10 - 0.2 - 2.1)/330$	1		
	= 23.33 mA	1		
				3
(c)	$\beta_{DC} = \frac{I_{C(sat)}}{I_{B(r-i)}}$	1		
	$I_{B(\min)} = \frac{I_{C(sat)}}{\beta_{DC}} = \frac{23.33}{180} = 0.1296 mA$	1		
	Since $I_B = 0.238$ mA is more than the minimum base current, 0.1296 mA for saturation to occur, the transistor is operating in the saturation region.	1		3
	Alternative solutions for (c)			
	$\beta_{DC} = \frac{I_C}{I_B}$			
	$I_C = \beta_{DC} I_B = 0.238 \ mX \ 180 = 42.84 \ mA$	1		
	Since I _C is greater than I _{C(sat)} the transistor is operating in the saturation region.	1		
	Alternative solutions for (c)	1	3	_
	$V_{CE} = Vcc - IcRc - V_{LED}$	2		
	$= 10 - 42.84 \text{m} \cdot 330 - 2.1 = -6.24 \text{ V}$	1		
	Since V_{CE} is less than $V_{CE(sat)}$ the transistor is operating in the saturation region.	1	3	
016/2	017/S2 MST		14	