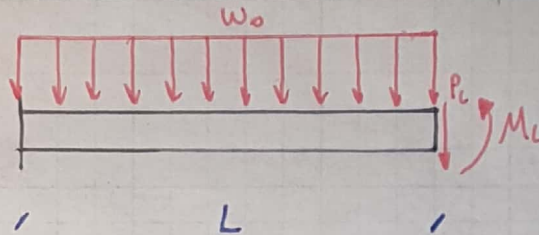


4-1



1. The potential energy stored in the deformed beam is

$$\Pi(v) = \frac{1}{2} \int_L EI \phi^2 dx - \int_L w_0 v dx + \bar{M}_L \theta(L) - \bar{P}_L v(L)$$

$$w/ \quad \theta(x) = v'(x) \quad \& \quad \phi(x) = -\theta'(x) = -v''(x)$$

Find the Euler equations i.e. strong form represented by  $\Pi(v) \rightarrow \min$   
 Use  $M(x) = EI \phi(x)$  &  $V(x) = M'(x)$  to simplify your expressions

$$\delta \Pi(v, \delta v) = \underbrace{\int_L EI \phi \delta \phi}_{M(x)} - \int_L w_0 \delta v dx + \bar{M}_L \delta \theta(L) - \bar{P}_L \delta v(L) = 0$$

$$= -M \delta \theta \Big|_0^L - \int_L \frac{dM}{dx} \delta \theta dx - \int_L w_0 \delta v dx + \bar{M}_L \delta \theta(L) - \bar{P}_L \delta v(L) = 0$$

$$= -M \delta \theta \Big|_0^L + V \delta v \Big|_0^L - \int_L \frac{dV}{dx} \delta v dx - \int_L w_0 \delta v dx + \bar{M}_L \delta \theta(L) - \bar{P}_L \delta v(L) = 0$$

$$= - \int_L \left( \frac{dV}{dx} + w_0 \right) \delta v dx - (M(L) \delta \theta(L) - M(0) \delta \theta(0)) + (V(L) \delta v(L) - V(0) \delta v(0)) \dots$$

$$\dots + \bar{M}_L \delta \theta(L) - \bar{P}_L \delta v(L) = 0$$

$$= - \underbrace{\int_L (V' + w_0) \delta v dx}_{=0 \text{ in } \mathcal{A}, 0 \leq x \leq L} + \underbrace{(M_L - M(L)) \delta \theta(L)}_{=0} + \underbrace{M(0) \delta \theta(0)}_{=0} + \underbrace{(V(L) - \bar{P}_L) \delta v(L)}_{=0} - \underbrace{V(0) \delta v(0)}_{=0} = 0$$

$$\Rightarrow V'(x) + w_0 = M''(x) + w_0 = EI \phi''(x) + w_0 = -EI \theta'''(x) + w_0$$

$$-EI v''''(x) + w_0 = 0$$

$$\underline{\underline{EI v''''(x) = w_0}}$$

$$v(0) = 0 \quad v'(0) = 0$$

$$\underline{\underline{M(L) = \bar{M}_L \quad V(L) = \bar{P}_L}}$$

4-1 continued

$$EI v''(x) = w_0$$

$$w/ \quad v(0) = 0$$

$$M(L) = -EI v''(L) = \bar{M}_L$$

$$v'(0) = 0$$

$$V(L) = -EI v'''(L) = \bar{P}_L$$



4-1  
2.

$$\tilde{v}(x) = a + bx + cx^2 + dx^3$$

$$\tilde{v}'(x) = b + 2cx + 3dx^2$$

we are interested in a function spanning  $0 \leq x \leq L$  which scales proportionately to  $L$ . Change  $\tilde{v}$  to:

$$\tilde{v}(\xi) = a + b\xi + c\xi^2 + d\xi^3 \quad \text{with} \quad \xi = \frac{x}{L} \quad d\xi = \frac{dx}{L} \Rightarrow dx = Ld\xi$$

$$\frac{d}{dx} \tilde{v}(\xi) = L \cdot \tilde{v}'(\xi) = b + 2c\xi + 3d\xi^2 \quad 0 \leq \xi \leq 1$$

$$\tilde{v}(0) = a = v_i \quad \Rightarrow \quad a = v_i$$

$$\tilde{v}'(0) = b/L = \theta_i \quad \Rightarrow \quad b = L\theta_i$$

$$\tilde{v}(1) = v_i + L\theta_i + c + d = v_j \quad \Rightarrow \quad c = v_j - v_i - L\theta_i - d \quad (1)$$

$$\tilde{v}'(1) = L\theta_i + 2c + 3d = L\theta_j \quad (2)$$

insert (1) into (2)

$$L\theta_i + 2(v_j - v_i - L\theta_i - d) + 3d = L\theta_j$$

$$-L\theta_i + 2v_j - 2v_i + d = L\theta_j \quad \Rightarrow \quad d = L(\theta_j + \theta_i) + 2(v_i - v_j) \quad (3)$$

insert (3) into (1)

$$c = v_j - v_i - L\theta_i - (L(\theta_j + \theta_i) + 2(v_i - v_j))$$

$$= 3(v_j - v_i) - 2L\theta_i - L\theta_j$$

Rewrite  $\tilde{v}$

$$\tilde{v}(\xi) = v_i + L\theta_i \xi + (3(v_j - v_i) - 2L\theta_i - L\theta_j)\xi^2 + (L(\theta_j + \theta_i) + 2(v_i - v_j))\xi^3$$

Re organize in terms of  $v_i, v_j, \theta_i, \theta_j$

$$\tilde{v}(\xi) = \underbrace{v_i(1 - 3\xi^2 + 2\xi^3)}_{N_1} + \underbrace{\theta_i L(\xi - 2\xi^2 + \xi^3)}_{N_2} + \underbrace{v_j(3\xi^2 - 2\xi^3)}_{N_3} + \underbrace{\theta_j L(\xi^3 - \xi^2)}_{N_4}$$

Shape functions match those of beams

4-7

2. continued

$$\tilde{v}(x) = v_i N_i(x) + \theta_i N_2(x) + v_j N_3(x) + \theta_j N_4(x)$$

$$\delta \tilde{v}(x) = \delta v_i N_i(x) + \delta \theta_i N_2(x) + \delta v_j N_3(x) + \delta \theta_j N_4(x)$$

$$\tilde{v}'(x) = v_i N_i'(x) + \theta_i N_2'(x) + v_j N_3'(x) + \theta_j N_4'(x)$$

$$\delta \tilde{v}'(x) = \delta v_i N_i'(x) + \delta \theta_i N_2'(x) + \delta v_j N_3'(x) + \delta \theta_j N_4'(x)$$

$$\tilde{v}''(x) = v_i N_i''(x) + \theta_i N_2''(x) + v_j N_3''(x) + \theta_j N_4''(x)$$

$$\delta \tilde{v}''(x) = \delta v_i N_i''(x) + \delta \theta_i N_2''(x) + \delta v_j N_3''(x) + \delta \theta_j N_4''(x)$$

$$\tilde{\pi}(v_i, \theta_i, v_j, \theta_j) = \pi(\tilde{v}) = \frac{1}{2} \int_L EI \tilde{\phi}^2 dx - \int_L \omega_0 \tilde{v} dx + \bar{M}_L \theta_j - \bar{P}_L v_j$$

with:

$$\tilde{\phi} = -\tilde{v}''$$

and B.C.

$$v_i = 0$$

$$\theta_i = 0$$

$$\Rightarrow \tilde{\pi}(0, 0, v_j, \theta_j) = -\frac{1}{2} \int_L EI \tilde{v}''^2 dx - \int_L \omega_0 \tilde{v} dx + \bar{M}_L \theta_j - \bar{P}_L v_j$$

$$= -\frac{1}{2} \int_L EI (v_j N_3''(x) + \theta_j N_4''(x))^2 dx - \int_L \omega_0 (v_j N_3(x) + \theta_j N_4(x)) dx \dots$$

$$\dots + \bar{M}_L \theta_j - \bar{P}_L v_j$$



4-1  
3.

$$\begin{aligned}\delta \pi(\tilde{v}, \delta \tilde{v}) &= \int_L EI \tilde{\phi} \delta \tilde{\phi} dx - \int_L w_0 \delta \tilde{v} dx + \bar{M}_L \delta \theta_j - \bar{P}_L \delta v_j = 0 \\ &= \int_L EI (v_j N_3'' + \theta_j N_4'') (\delta v_j N_3'' + \delta \theta_j N_4'') dx - \int_L w_0 (\delta v_j N_3 + \delta \theta_j N_4) dx \dots \\ &\dots + \bar{M}_L \delta \theta_j - \bar{P}_L \delta v_j = 0\end{aligned}$$

separate in terms of  $\delta v_j$  &  $\delta \theta_j$

$$\begin{aligned}&= \delta v_j \left( \int_L EI (N_3'' N_3'' v_j + N_4'' N_3'' \theta_j) dx - \int_L w_0 N_3 dx - \bar{P}_L \right) \dots \\ &\dots \delta \theta_j \left( \int_L EI (N_3'' N_4'' v_j + N_4'' N_4'' \theta_j) dx - \int_L w_0 N_4 dx + \bar{M}_L \right) = 0\end{aligned}$$

or written as

$$\begin{Bmatrix} \delta v_j \\ \delta \theta_j \end{Bmatrix} \begin{Bmatrix} v_j \int_L EI N_3'' N_3'' dx + \theta_j \int_L EI N_4'' N_3'' dx - \int_L w_0 N_3 dx - \bar{P}_L \\ v_j \int_L EI N_3'' N_4'' dx + \theta_j \int_L EI N_4'' N_4'' dx - \int_L w_0 N_4 dx + \bar{M}_L \end{Bmatrix} = 0$$

$\delta v_j$  &  $\delta \theta_j$  are both arbitrary, therefore

$$v_j \int_L EI N_3'' N_3'' dx + \theta_j \int_L EI N_4'' N_3'' dx - \int_L w_0 N_3 dx - \bar{P}_L = 0$$

&

$$v_j \int_L EI N_3'' N_4'' dx + \theta_j \int_L EI N_4'' N_4'' dx - \int_L w_0 N_4 dx + \bar{M}_L = 0$$

using Mathematica to calculate integrals we get

$$v_j \frac{12EI}{L^3} - \theta_j \frac{6EI}{L^2} - \frac{w_0 \cdot L}{2} - \bar{P}_L = 0 \quad (1)$$

&

$$-v_j \frac{6EI}{L^2} + \theta_j \frac{4EI}{L} + \frac{w_0 \cdot L^2}{12} + \bar{M}_L = 0 \quad (2)$$

4-1

3. continued

Solving  $v_j$  &  $\theta_j$ to ① we do  $\times \frac{L}{2}$  to get:

$$v_j \frac{6EI}{L^2} - \theta_j \frac{3EI}{L} - \frac{w_0 L^2}{4} - \frac{\bar{P}_L \cdot L}{2} = 0 \quad (3)$$

② + ③:

$$v_j \left( \frac{6EI}{L^2} - \frac{6EI}{L^2} \right) + \theta_j \left( \frac{4EI}{L} - \frac{3EI}{L} \right) + \frac{w_0 L^2}{12} - \frac{w_0 L^2}{4} - \frac{\bar{P}_L \cdot L}{2} + \bar{M}_L = 0$$

$$\Rightarrow \theta_j = \left( \frac{w_0 L^2}{6} + \frac{\bar{P}_L \cdot L}{2} - \bar{M}_L \right) \frac{L}{EI} = \frac{w_0 L^3}{6EI} + \frac{\bar{P}_L L^2}{2EI} - \frac{\bar{M}_L L}{EI}$$

$$\boxed{\theta_j = \frac{w_0 L^3}{6EI} + \frac{\bar{P}_L L^2}{2EI} - \frac{\bar{M}_L L}{EI}} \quad (4)$$

insert ④ into ①

$$v_j \left( \frac{12EI}{L^3} \right) - \left( \frac{w_0 L^3}{6EI} + \frac{\bar{P}_L L^2}{2EI} - \frac{\bar{M}_L L}{EI} \right) \frac{6EI}{L^2} - \frac{w_0 L}{2} - \bar{P}_L = 0$$

$$v_j \left( \frac{12EI}{L^3} \right) = w_0 L - \frac{w_0 L}{2} + 3\bar{P}_L - \frac{6\bar{M}_L}{L} + \bar{P}_L = \frac{3w_0 L}{2} + 4\bar{P}_L - \frac{6\bar{M}_L}{L}$$

$$\boxed{v_j = \frac{w_0 L^4}{8EI} + \frac{\bar{P}_L L^3}{3EI} - \frac{\bar{M}_L L^2}{2EI}}$$



4-1  
4.

$$\tilde{V}(\xi) = \left( \frac{W_0 L^4}{8EI} + \frac{\bar{P}_i L^3}{3EI} - \frac{\bar{M}_i L^2}{2EI} \right) (3\xi^2 - 2\xi^3) + \left( \frac{W_0 L^3}{6EI} + \frac{\bar{P}_i L^2}{2EI} - \bar{M}_i \right) L (\xi^3 - \xi^2)$$

with  $\xi = \frac{x}{L}$  it can be written as

$$\tilde{V}(x) = \left( \frac{W_0 L^4}{8EI} + \frac{\bar{P}_i L^3}{3EI} - \frac{\bar{M}_i L^2}{2EI} \right) \left( 3\left(\frac{x}{L}\right)^2 - 2\left(\frac{x}{L}\right)^3 \right) + \left( \frac{W_0 L^3}{6EI} + \frac{\bar{P}_i L^2}{2EI} - \bar{M}_i \right) L \left( \left(\frac{x}{L}\right)^3 - \left(\frac{x}{L}\right)^2 \right)$$

4-2

1.

$$G(u, \delta u) = - \int_L M(x) \delta \phi(x) + \int_L w_0 \delta v(x) dx - \bar{M}_L \delta \theta(L) + \bar{P}_L \delta v(L) = 0$$

where

$$M(x) = EI \phi(x), \quad \theta(x) = v'(x), \quad \phi(x) = -\theta'(x) = -v''(x)$$

$$V(x) = M'(x) \quad \delta \theta(x) = \delta v'(x), \quad \delta \phi(x) = -\delta \theta'(x) = -\delta v''(x)$$

Find strong form (Euler equations) represented by  $G(u, \delta u) = 0 \quad \forall \delta v(x)$ 

$$G(u, \delta v) = - \int_L M(x) (-\delta v''(x)) dx + \int_L w_0 \delta v(x) dx - \bar{M}_L \delta v'(L) + \bar{P}_L \delta v(L) = 0$$

IBP

$$= M(x) \delta v'(x) \Big|_0^L - \int_L \frac{dM}{dx} \delta v'(x) dx + \int_L w_0 \delta v(x) dx - \bar{M}_L \delta v'(L) + \bar{P}_L \delta v(L) = 0$$

IBP

$$= M(x) \delta v'(x) \Big|_0^L - V(x) \delta v(x) \Big|_0^L + \int_L \frac{dV}{dx} \delta v(x) dx + \int_L w_0 \delta v(x) dx - \bar{M}_L \delta v'(L) + \bar{P}_L \delta v(L) = 0$$

collect by  $\delta v$  &  $\delta v' = \delta \theta$ 

$$= \int_L (V' + w_0) \delta v(x) dx + (M(L) - \bar{M}_L) \delta \theta(L) - M(0) \delta \theta(0) + (\bar{P}_L - V(L)) \delta v(L) + V(0) \delta v(0) = 0$$

$$EI v''''(x) = w_0 \quad \text{on } \Omega \quad 0 \leq x \leq L$$

$$v(0) = v'(0) = 0$$

$$V(L) = \bar{P}_L$$

$$M(L) = \bar{M}_L$$



4-2

2. Use the adjusted cubic polynomial from P4-1(2), build a similar function for the virtual displacement,  $\delta v(x)$ , and solve for all remaining degrees of freedom.

Same process as in 4-1(3) but now we start from

$$G(v, \delta v) = -\int_L M(x) \delta v(x) dx + \int_L w_0 \delta v(x) dx - \bar{M}_L \delta \theta(L) + \bar{P}_L \delta v(L) = 0$$

instead of potential energy and linear relation of  $M = EI \phi''(x)$   
to find min potential energy

otherwise the same process.

4-2

$$3. \quad \hat{v}(x) = C_0 + C_1 \sin\left(\frac{\pi x}{2L}\right) + C_2 \cos\left(\frac{\pi x}{2L}\right)$$

Use trig. series and find all remaining degrees of freedom using RVD

$$\hat{v}'(x) = 0 + \frac{C_1 \pi}{2L} \cos\left(\frac{\pi x}{2L}\right) - \frac{C_2 \pi}{2L} \sin\left(\frac{\pi x}{2L}\right)$$

Fulfill B.Cs.

$$\hat{v}(0) = C_0 + C_2 = v_i = 0 \Rightarrow C_0 = -C_2$$

$$\hat{v}'(0) = \frac{C_1 \pi}{2L} = \theta_i = 0 \Rightarrow C_1 = 0$$

$$\hat{v}(x) = C_0 + (-C_0) \cos\left(\frac{\pi x}{2L}\right) = C_0 \left(1 - \cos\left(\frac{\pi x}{2L}\right)\right)$$

$$\delta \hat{v}(x) = \delta C_0 \left(1 - \cos\left(\frac{\pi x}{2L}\right)\right)$$

$$\hat{v}'(x) = \frac{C_0 \pi}{2L} \sin\left(\frac{\pi x}{2L}\right)$$

$$\delta \hat{v}'(x) = \frac{\delta C_0 \pi}{2L} \sin\left(\frac{\pi x}{2L}\right)$$

$$\hat{v}''(x) = \frac{C_0 \pi^2}{4L^2} \cos\left(\frac{\pi x}{2L}\right)$$

$$\delta \hat{v}''(x) = \frac{\delta C_0 \pi^2}{4L^2} \cos\left(\frac{\pi x}{2L}\right)$$

$$-\int_L EI (-\hat{v}'') (-\delta \hat{v}'') dx + \int_L w_0 \delta \hat{v} dx - \bar{M}_L \delta \hat{v}'(L) + \bar{P}_L \delta \hat{v}(L) = 0$$

$$-\int_L EI C_0 \frac{\pi^2}{4L^2} \cos\left(\frac{\pi x}{2L}\right) \delta C_0 \frac{\pi^2}{4L^2} \cos\left(\frac{\pi x}{2L}\right) dx + \int_L w_0 \delta C_0 \left(1 - \cos\left(\frac{\pi x}{2L}\right)\right) dx \dots$$

$$\dots - \bar{M}_L \delta C_0 \frac{\pi}{2L} + \bar{P}_L \delta C_0 = 0$$

Collect by  $\delta C_0$

$$\delta C_0 \left( -\frac{EI \pi^4}{32 L^3} C_0 + \frac{(\pi-2)L}{\pi} w_0 - \frac{\bar{M}_L \pi}{2L} + \bar{P}_L \right) = 0 \quad \forall \delta C_0$$

We can now solve for  $C_0$

$$C_0 = \left( \frac{\bar{M}_L \pi}{2L} - \bar{P}_L - \frac{(\pi-2)L w_0}{\pi} \right) \frac{-32 L^3}{EI \pi^4} = \frac{32 L^3 \bar{P}_L}{EI \pi^4} + \frac{32 \left(1 - \frac{2}{\pi}\right) L^4 w_0}{EI \pi^4} - \frac{16 \bar{M}_L L^2}{EI \pi^3}$$

$$C_0 = \frac{32 \left(1 - \frac{2}{\pi}\right) L^4 w_0}{EI \pi^4} + \frac{32 L^3 \bar{P}_L}{EI \pi^4} - \frac{16 \bar{M}_L L^2}{EI \pi^3}$$



4-2

3. continued

$$\hat{v}_j = \hat{v}(L) = \frac{32(1 - \frac{2}{\pi})L^4 w_0}{EI \pi^4} + \frac{32L^4 \bar{p}_L}{EI \pi^4} - \frac{16 \bar{M}_L L^2}{EI \pi^3}$$

$$\hat{\theta}_j = \hat{v}'(L) = C_0 \cdot \frac{\pi}{2L} = \frac{32(1 - \frac{2}{\pi})L^3 w_0}{2EI \pi^3} + \frac{16L^3 \bar{p}_L}{EI \pi^3} - \frac{8 \bar{M}_L L}{EI \pi^2}$$

4-3

1. Compare solutions from 4-1 and 4-2 to exact solution at  $x=L$  and  $x=\frac{1}{2}$

For exact solution solve

$$EI v''''(x) = w_0 \quad \text{or} \quad v''''(x) = \frac{w_0}{EI}$$

$$V(0) = V'(0) = 0$$

$$V(L) = -EI v''''(x) = \bar{P}_L$$

$$M(L) = -EI v'''(x) = \bar{M}_L$$

$$V(x) = \frac{w_0}{EI} x^4 + C_1 x^3 + C_2 x^2 + C_3 x + C_4$$

$$V'(x) = \frac{w_0}{6EI} x^3 + 2C_1 x^2 + C_2 x + C_3$$

$$V(x) = \frac{w_0}{24EI} x^4 + \frac{1}{6} C_1 x^3 + \frac{1}{2} C_2 x^2 + C_3 x + C_4$$

$$V(0) = C_4 = 0 \Rightarrow C_4 = 0$$

$$V'(0) = C_3 = 0 \Rightarrow C_3 = 0$$

$$V(L) = -EI \left( \frac{w_0}{EI} L^4 + C_1 \right) = \bar{P}_L$$

$$\Rightarrow C_1 = \frac{-\bar{P}_L}{EI} - \frac{w_0 L^4}{EI}$$

$$M(L) = -EI \left( \frac{w_0}{2EI} L^3 + L \left( \frac{-\bar{P}_L}{EI} - \frac{w_0 L^4}{EI} \right) + C_2 \right) = \bar{M}_L$$

$$\Rightarrow C_2 = -\frac{\bar{M}_L}{EI} - \frac{w_0 L^3}{2EI} + \frac{\bar{P}_L L}{EI} + \frac{w_0 L^5}{EI} = \frac{w_0 L^5}{2EI} + \frac{\bar{P}_L L}{EI} - \frac{\bar{M}_L}{EI}$$

$$V(x) = \frac{w_0}{24EI} x^4 + \frac{1}{6} \left( \frac{-\bar{P}_L}{EI} - \frac{w_0 L^4}{EI} \right) x^3 + \frac{1}{2} \left( \frac{w_0 L^5}{2EI} + \frac{\bar{P}_L L}{EI} - \frac{\bar{M}_L}{EI} \right) x^2$$

$$V(x) = \frac{w_0 (x^4 - 4Lx^3 + 6L^2x^2)}{24EI} + \frac{\bar{P}_L (3Lx^2 - x^3)}{6EI} - \frac{\bar{M}_L x^2}{2EI}$$

$$V'(x) = \frac{w_0 (x^3 - 3Lx^2 + 3L^2x)}{6EI} + \frac{\bar{P}_L (2Lx - x^2)}{2EI} - \frac{\bar{M}_L x}{EI}$$



4-3

1. continued 1

Comparing results

at  $x = L$ 

$$\text{Exact: } V(L) = \frac{w_0 L^4}{8EI} + \frac{\bar{P}_L L^3}{3EI} - \frac{\bar{M}_L L^2}{2EI}$$

$$\theta(L) = \frac{w_0 L^3}{6EI} + \frac{\bar{P}_L L^2}{2EI} - \frac{\bar{M}_L L}{EI}$$

$$\text{Cubic: } V(L) = \frac{w_0 L^4}{8EI} + \frac{\bar{P}_L L^3}{3EI} - \frac{\bar{M}_L L^2}{2EI}$$

$$\theta(L) = \frac{w_0 L^3}{6EI} + \frac{\bar{P}_L L^2}{2EI} - \frac{\bar{M}_L L}{EI}$$

$$\text{Trig: } V(L) = \frac{32(1 - \frac{2}{\pi}) w_0 L^4}{EI \pi^4} + \frac{32 L^3 \bar{P}_L}{EI \pi^4} - \frac{16 \bar{M}_L L^2}{EI \pi^3}$$

$$= 0.11938 \frac{w_0 L^4}{EI} + 0.32851 \frac{\bar{P}_L L^3}{EI} - 0.51603 \frac{\bar{M}_L L^2}{EI}$$

$$\theta(L) = \frac{16(1 - \frac{2}{\pi}) w_0 L^3}{EI \pi^3} + \frac{16 L^2 \bar{P}_L}{EI \pi^3} - \frac{8 \bar{M}_L L}{EI \pi^2}$$

$$= 0.18751 \frac{w_0 L^3}{EI} + 0.51603 \frac{\bar{P}_L L^2}{EI} - 0.81057 \frac{\bar{M}_L L}{EI}$$

4-3

1. continued 2

at  $x = \frac{L}{2}$ 

$$\text{Exact: } V(\frac{L}{2}) = \frac{17 W_0 L^4}{384 EI} + \frac{5 \bar{P}_L L^3}{48 EI} - \frac{\bar{M}_L L^2}{8 EI}$$

$$\theta(\frac{L}{2}) = \frac{7 W_0 L^3}{48 EI} + \frac{3 \bar{P}_L L^2}{8 EI} - \frac{\bar{M}_L L}{2 EI}$$

$$\text{Cubic: } V(\frac{L}{2}) = \frac{W_0 L^4}{24 EI} + \frac{5 \bar{P}_L L^3}{48 EI} - \frac{\bar{M}_L L^2}{8 EI}$$

$$\theta(\frac{L}{2}) = \frac{7 W_0 L^3}{48 EI} + \frac{3 \bar{P}_L L^2}{8 EI} - \frac{\bar{M}_L L}{2 EI}$$

$$\text{Trig: } V(\frac{L}{2}) = 0.034964 \frac{W_0 L^4}{EI} + 0.0962188 \frac{\bar{P}_L L^3}{EI} - 0.15114 \frac{\bar{M}_L L^2}{EI}$$

$$\theta(\frac{L}{2}) = 0.132592 \frac{W_0 L^3}{EI} + 0.364884 \frac{\bar{P}_L L^2}{EI} - 0.573159 \frac{\bar{M}_L L}{EI}$$



4-4

1. with  $M(\phi) = A \cdot \arctan(B\phi)$ Find the coefficients  $A$  &  $B$  such that

a)  $\frac{dM}{d\phi} \Big|_{\phi=0} = EI$

b)  $\lim_{\phi \rightarrow \infty} M(\phi) = M_y$

$$\frac{dM}{d\phi} = \frac{A \cdot B}{B^2 \cdot \phi^2 + 1}$$

$$\frac{dM}{d\phi} \Big|_{\phi=0} = A \cdot B = EI \quad (1)$$

$$\lim_{\phi \rightarrow \infty} M(\phi) = A \cdot \frac{\pi}{2} = M_y$$

$$\Rightarrow A = \frac{2M_y}{\pi} \quad (2)$$

Insert (2) into (1)

$$\frac{2M_y}{\pi} \cdot B = EI$$

$$\Rightarrow B = \frac{EI \cdot \pi}{2M_y}$$

$$\underline{\underline{M(\phi) = \frac{2M_y}{\pi} \tan^{-1}\left(\frac{EI \pi}{2M_y} \phi\right)}}$$

4-4

2. Formulate the weak form equilibrium (PVD) for the nonlinear material model and a general approximation function

$$\tilde{v}(x) = \sum_{i=1}^N N_i(x) q_i$$

With  $N_i(x)$  as the  $i$ -th (given) shape function and  $q_i$  as the respective unknown degree of freedom. Assume that the given function already satisfies all essential boundary conditions.

We have

$$\tilde{v}(x) = \sum_{i=1}^N N_i(x) q_i$$

$$\delta \tilde{v}(x) = \sum_{i=1}^N N_i(x) \delta q_i$$

$$\tilde{v}'(x) = \sum_{i=1}^N N_i'(x) q_i$$

$$\delta \tilde{v}'(x) = \sum_{i=1}^N N_i'(x) \delta q_i$$

$$\tilde{v}''(x) = \sum_{i=1}^N N_i''(x) q_i$$

$$\delta \tilde{v}''(x) = \sum_{i=1}^N N_i''(x) \delta q_i$$

Moment is now described with

$$M(x) = \tilde{M}(\tilde{v}'')$$

$$\text{with } \tilde{v}''(x, q_1, q_2, \dots, q_N)$$

Create new description of moment as a function of  $q$ 's

$$\bar{M}(q_1, q_2, q_3, \dots, q_N) \text{ or short hand } \bar{M}(q)$$

$$G(\tilde{v}, \delta \tilde{v}) = \int_L \bar{M}(q) \delta \tilde{v}'' dx + \int_L w_0 \delta \tilde{v} dx = 0$$

$$\Rightarrow \int_L \bar{M}(q) \sum_{i=1}^N N_i''(x) \delta q_i dx + \int_L w_0 \sum_{i=1}^N N_i(x) \delta q_i dx = 0$$

$$\Rightarrow \sum_{i=1}^N \delta q_i \left( \int_L \bar{M}(q) N_i''(x) dx + \int_L w_0 N_i(x) dx \right) = 0$$

4-4.3

$\delta q_i$  is arbitrary and therefore

$$R_i(q) = \int_L \bar{M}(q) N_i''(x) dx + \int_L w_0 N_i(x) dx = 0$$

which gives

$$G(v, \delta v) =: -\{\delta q_1, \dots, \delta q_N\} \cdot \{R\}$$