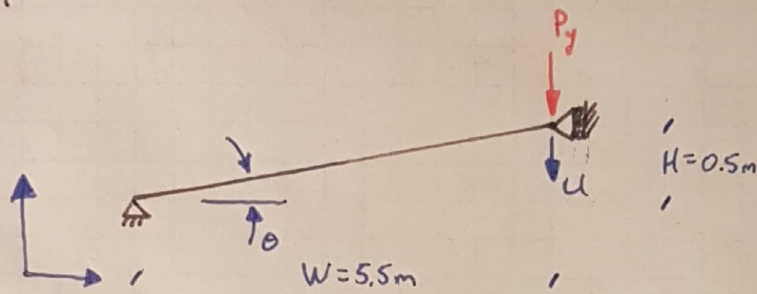


1-1



$$EA = 2100 \text{ kN}$$

$$1a \quad \epsilon = \frac{L-L}{L}$$

$$1b \quad \epsilon = \frac{1}{2} \frac{L^2 - L^2}{L^2}$$

$$1c \quad \epsilon = \frac{1}{2} \frac{L^2 - L^2}{L^2}$$

$$1d \quad \tilde{\epsilon} = \frac{1}{2} \ln\left(\frac{L^2}{L^2}\right)$$

1. Derive force-displacement relation for all possible combinations (8 options) of kinematic relations and equilibrium on the undeformed and the deformed configuration and compare them in a single plot for $0 \leq u \leq 2.5 H$. Include the linear solution in the same plot

$$\underline{L} = \begin{Bmatrix} 5.5 \\ 0.5 \end{Bmatrix}$$

$$\underline{L} = \begin{Bmatrix} 5.5 \\ 0.5 - u \end{Bmatrix}$$

$$L^2 = \underline{L} \cdot \underline{L} = 30.5$$

$$L^2 = \underline{L} \cdot \underline{L} = 30.5 + u^2 - u$$

$$f = EA \cdot \epsilon$$

$$P_y = f \cdot \sin(\theta)$$

$$\sin(\theta) = \frac{H-u}{L}$$

Undeformed

$$1a \quad P_y = EA \cdot \frac{L-L}{L} \cdot \frac{H}{L}$$

$$1b \quad P_y = EA \cdot \frac{L^2 - L^2}{2L^2} \cdot \frac{H}{L}$$

$$1c \quad P_y = EA \cdot \frac{L^2 - L^2}{2L^2} \cdot \frac{H}{L}$$

$$1d \quad P_y = \frac{EA}{2} \ln\left(\frac{L^2}{L^2}\right) \cdot \frac{H}{L}$$

Deformed

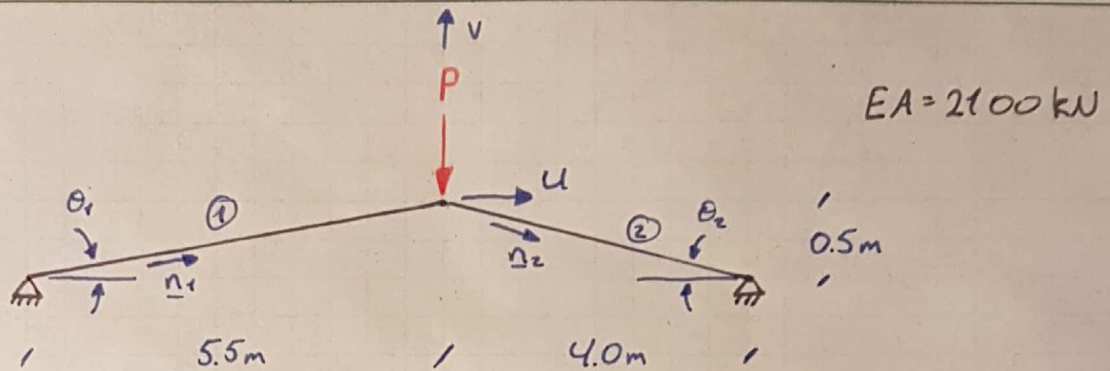
$$P_y = EA \cdot \frac{L-L}{L} \cdot \frac{H-u}{L}$$

$$P_y = EA \cdot \frac{L^2 - L^2}{2L^2} \cdot \frac{H-u}{L}$$

$$P_y = EA \cdot \frac{L^2 - L^2}{2L^2} \cdot \frac{H-u}{L}$$

$$P_y = \frac{EA}{2} \ln\left(\frac{L^2}{L^2}\right) \cdot \frac{H-u}{L}$$

1-2



1. Using Henkey strain, a linear relation $\sigma = E \cdot \epsilon$ $A = \text{const.}$ and equilibrium on the deformed system, derive the relationship between displacement and forces on the free node i.e.

$$\begin{Bmatrix} P_x \\ P_y \end{Bmatrix} = \begin{Bmatrix} F_x(u, v) \\ F_y(u, v) \end{Bmatrix}$$

$$\epsilon = \frac{1}{2} \ln(\lambda^2) = \frac{1}{2} \ln\left(\frac{L^2}{L_0^2}\right) \quad (\text{Henkey strain})$$

$$L_1^2 = 5.5^2 + 0.5^2 = 30.5 \text{ m}^2$$

$$L_2^2 = 4.0^2 + 0.5^2 = 16.25 \text{ m}^2$$

$$L_1^2 = (5.5 + u)^2 + (0.5 + v)^2$$

$$L_2^2 = (4.0 - u)^2 + (0.5 + v)^2$$

$$= 30.5 + u^2 + v^2 + 11u + v$$

$$= 16.25 + u^2 + v^2 - 8u + v$$

$$P = -(f_{1,j} + f_{2,i}) = -(f_1 \cdot \underline{n}_1 + (-f_2 \cdot \underline{n}_2)) = -(f_1 \cdot \underline{n}_1 - f_2 \cdot \underline{n}_2) = f_2 \cdot \underline{n}_2 - f_1 \cdot \underline{n}_1$$

same for both elements

$$P = EA \left(\frac{L_2}{\|L_2\|} \epsilon_2 - \frac{L_1}{\|L_1\|} \epsilon_1 \right)$$

$$\underline{n}_k = \frac{\underline{V}_k}{\|\underline{V}_k\|}$$

$$\underline{L}_1 = \begin{Bmatrix} 5.5 \\ 0.5 \end{Bmatrix} + \begin{Bmatrix} u \\ v \end{Bmatrix}$$

$$\underline{L}_2 = \begin{Bmatrix} 4.0 \\ -0.5 \end{Bmatrix} + \begin{Bmatrix} -u \\ -v \end{Bmatrix} = \begin{Bmatrix} 4.0 \\ -0.5 \end{Bmatrix} - \begin{Bmatrix} u \\ v \end{Bmatrix}$$

$$\|\underline{L}_1\| = L_1$$

$$\|\underline{L}_2\| = L_2$$

$$P = EA \left(\frac{\epsilon_2}{L_2} \begin{Bmatrix} 4.0 - u \\ -0.5 - v \end{Bmatrix} - \frac{\epsilon_1}{L_1} \begin{Bmatrix} 5.5 + u \\ 0.5 + v \end{Bmatrix} \right) = \begin{Bmatrix} P_x \\ P_y \end{Bmatrix}$$

Also written as

$$f_2 \underline{n}_2 - f_1 \underline{n}_1 = P$$

1-2

2. Find the tangent stiffness matrix of the system. Keep it simple and don't substitute long expressions into your answer

Tangent stiffness for element is written as

$$[K^e] = \begin{bmatrix} k^e & -k^e \\ -k^e & k^e \end{bmatrix}$$

where

$$k^e = \frac{EA}{L} \underline{n} \otimes \underline{n} + \frac{\tilde{F}}{L} (1 - \underline{n} \otimes \underline{n}) \quad \text{where } \tilde{F} \text{ is force in element}$$

Our global stiffness matrix is then

$$\begin{matrix} & \begin{matrix} 1 & 2 & 3 \end{matrix} \\ \begin{matrix} 1 \\ 2 \\ 3 \end{matrix} & \begin{bmatrix} k^1 & -k^1 & 0 \\ -k^1 & k^1 + k^2 & -k^2 \\ 0 & -k^2 & k^2 \end{bmatrix} \end{matrix} \quad \begin{array}{l} \text{with nodes 1 \& 3 being supported} \\ \text{node 2 unsupported} \end{array}$$

u_1 & $u_3 = 0$, we are therefor only interested in $K_{ff} = k^1 + k^2$

$$k^1 = \frac{EA}{L_1} \underline{n}_1 \otimes \underline{n}_1 + \frac{\tilde{F}_1}{L_1} (1 - \underline{n}_1 \otimes \underline{n}_1)$$

$$\underline{n}_1 = \begin{Bmatrix} \cos(\theta_1) \\ \sin(\theta_1) \end{Bmatrix} = \begin{Bmatrix} c_1 \\ s_1 \end{Bmatrix} \quad \tilde{F}_1 = EAE_1$$

$$= \frac{EA}{L_1} \begin{bmatrix} c_1^2 & c_1 s_1 \\ c_1 s_1 & s_1^2 \end{bmatrix} + \frac{EAE_1}{L_1} \left(\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} - \begin{bmatrix} c_1^2 & c_1 s_1 \\ c_1 s_1 & s_1^2 \end{bmatrix} \right)$$

$$= \frac{EA(1-E_1)}{L_1} \begin{bmatrix} c_1^2 & c_1 s_1 \\ c_1 s_1 & s_1^2 \end{bmatrix} + \frac{EAE_1}{L_1} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

1-2 2. continued

$$k^2 = \frac{EA}{l_2} \underline{n}_2 \otimes \underline{n}_2 + \frac{\tilde{f}_2}{l_2} \left(\underline{1} - \underline{n}_2 \otimes \underline{n}_2 \right)$$

$$\underline{n}_2 = \begin{Bmatrix} \cos(\theta_2) \\ -\sin(\theta_2) \end{Bmatrix} = \begin{Bmatrix} c_2 \\ -s_2 \end{Bmatrix} \quad \tilde{f}_2 = EA \cdot \epsilon_2$$

$$= \frac{EA}{l_2} \begin{bmatrix} c_1^2 & -c_1 s_1 \\ -c_1 s_1 & s_1^2 \end{bmatrix} + \frac{EA \epsilon_2}{l_2} \left(\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} + \begin{bmatrix} c_1^2 & -c_1 s_1 \\ -c_1 s_1 & s_1^2 \end{bmatrix} \right)$$

$$= \frac{EA(1-\epsilon_2)}{l_2} \begin{bmatrix} c_1^2 & -c_1 s_1 \\ -c_1 s_1 & s_1^2 \end{bmatrix} + \frac{EA \epsilon_2}{l_2} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

K_{ff} then becomes

$$K_{ff} = \begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix}$$

where

$$K_{11} = \frac{EA(1-\epsilon_1)}{l_1} c_1^2 + \frac{EA \epsilon_1}{l_1} + \frac{EA(1-\epsilon_2)}{l_2} c_2^2 + \frac{EA \epsilon_2}{l_2}$$

$$= EA \left(\frac{c_1^2(1-\epsilon_1) + \epsilon_1}{l_1} + \frac{c_2^2(1-\epsilon_2) + \epsilon_2}{l_2} \right)$$

$$K_{21} = K_{12} = \frac{EA(1-\epsilon_1)}{l_1} c_1 s_1 + \frac{EA(1-\epsilon_2)}{l_2} (-c_1 s_2)$$

$$= EA \left(\frac{c_1 s_1(1-\epsilon_1)}{l_1} - \frac{c_1 s_2(1-\epsilon_2)}{l_2} \right)$$

$$K_{22} = \frac{EA(1-\epsilon_1)}{l_1} s_1^2 + \frac{EA \epsilon_1}{l_1} + \frac{EA(1-\epsilon_2)}{l_2} s_2^2 + \frac{EA \epsilon_2}{l_2}$$

$$= EA \left(\frac{s_1^2(1-\epsilon_1) + \epsilon_1}{l_1} + \frac{s_2^2(1-\epsilon_2) + \epsilon_2}{l_2} \right)$$

Terms ϵ, l have been written out on previous pages.

1-2

3. Formulate the condition $P_x = 0$ to the system of equations. Will this allow you to eliminate the horizontal displacement from the system of equations? Why? Why not?

From 1-2.1. we have

$$\frac{EA\epsilon_2}{l_2} \begin{Bmatrix} 4.0 - u \\ -0.5 - v \end{Bmatrix} - \frac{EA\epsilon_1}{l_1} \begin{Bmatrix} 5.5 + u \\ 0.5 + v \end{Bmatrix} = \begin{Bmatrix} P_x \\ P_y \end{Bmatrix}$$

Now setting $P_x = 0$ gives

$$\frac{EA\epsilon_2}{l_2} \begin{Bmatrix} 4.0 - u \\ -0.5 - v \end{Bmatrix} - \frac{EA\epsilon_1}{l_1} \begin{Bmatrix} 5.5 + u \\ 0.5 + v \end{Bmatrix} = \begin{Bmatrix} 0 \\ P_y \end{Bmatrix}$$

Looking only at force in x direction

$$EA \left(\underbrace{\frac{\epsilon_2}{l_2} (4.0 - u) - \frac{\epsilon_1}{l_1} (5.5 + u)}_{= 0 \text{ to fulfill condition}} \right) = 0$$

Solving for u gives

$$u = \frac{5.5 \cdot \frac{\epsilon_1}{l_1} - 4.0 \cdot \frac{\epsilon_2}{l_2}}{-\left(\frac{\epsilon_1}{l_1} + \frac{\epsilon_2}{l_2}\right)}$$

But $l_1, l_2, \epsilon_1, \epsilon_2$ are all functions of u , we can therefore not eliminate u .

Side note, if system was symmetric and $l_1 = \begin{Bmatrix} a \\ b \end{Bmatrix}$ $l_2 = \begin{Bmatrix} a \\ -b \end{Bmatrix}$

we would get

$$\frac{\epsilon_2}{l_2} (a - u) - \frac{\epsilon_1}{l_1} (a + u) \quad \begin{matrix} w/ \epsilon_2 = \epsilon_1 = \epsilon \\ l_2 = l_1 = l \end{matrix}$$

$$\Rightarrow 2u \frac{\epsilon}{l} = P_x = 0$$

which would only be fulfilled at $u = 0$ and we could eliminate u