To: Doctor Dahlke; Brewing Engineer Team

From: Nguyen Khoa Bui

Re: Characterization of heat exchanger for purchase

Dear Doctor Dahlke and Brewing Engineering Team,

A small-scale tube-and-shell heat exchanger was setup according to The Lab Manual to

characterize heat transfer properties for various cold- and hot-side flowrates in co- and

countercurrent flow (Heat Exchanger Experiment). For both flows, the overall heat transfer

coefficient U is not impacted by change in hot-side flowrate but varied with change in cold-side

flowrate. This may be due to hot-side flowrates were two to ten times larger than cold-side

flowrates for many runs, which minimize the hot-side resistance impact on U. This make

determining fouling effects not possible due to disagreement in constant c = 0.2 for

countercurrent and infeasible value c = -1.64 for co-current during parameters fitting. For both

flow conditions, experimentally determined heat transfer coefficient h_i^{Exp} do not behave as

expected when compared to that of Sieder-Tate correlation h_iS-T. The data collected are

considered accurate as all normalized Q_c+Q_h are within the error propagation ranges. We

concluded our data may only be used for countercurrent flow, limited to large hot-side to cold-

side flowrate difference. We strongly recommend the brewing team to reconduct the experiment

for a smaller flowrate difference between both sides and parameters should be re-fit.

Cc: Abdullah Alkazrai, Saeed Alharmoodi, Khalid Alsinan

Encl: 5 figures

Figures:

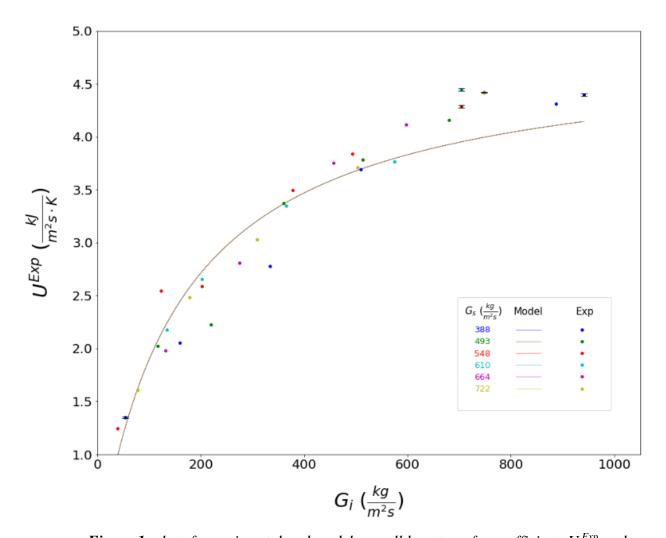


Figure 1. plot of experimental and model overall heat transfer coefficient, U_i^{Exp} and U_i^{Model} versus mass velocity of tube-side G_i for various shell-side mass velocity G_s in countercurrent condition. Here, $U_i^{model} = \frac{1}{\left(\frac{a}{G_i^b} + c + \frac{d}{G_i^e}\right)}$, where $a = 40.09 \frac{s^{2.08} \cdot m^{4.16} \cdot K}{kJ \cdot kg^{1.08}}$, b = 1.08, $c = 0.23 \frac{s \cdot m^2 \cdot K}{kJ}$, $d = 0.44 \frac{s^{6.93} \cdot m^{13.86} \cdot K}{kJ \cdot kg^{5.93}}$, e = 5.93. While b value is close to Sieder-Tate expected value of b = 0.8, e value deviated greatly from Sieder-Tate value e = 0.55. These parameters result in all model trend for various G_s to clumped up into one line. Error bars for elements with repeated runs are presented and small compared to data point.

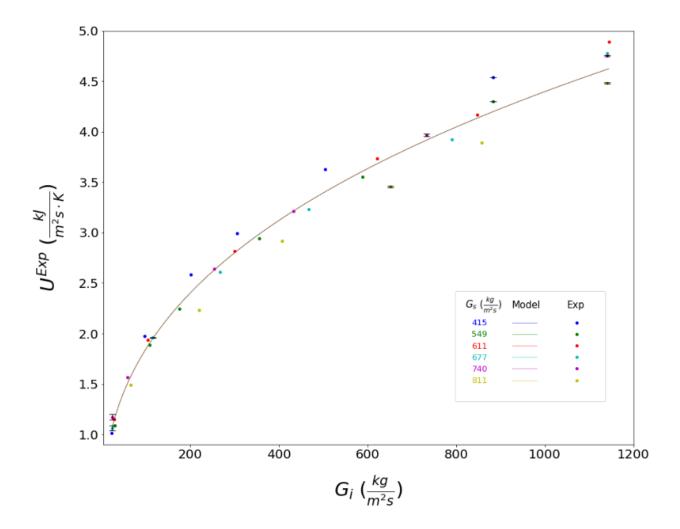


Figure 2. plot of tube-side experimental U_i^{Exp} and model U_i^{Model} overall heat transfer coefficient versus mass velocity of tube-side G_i for various shell-side mass velocity G_s in cocurrent condition. Here, $U_i^{model} = \frac{1}{\left(\frac{a}{c_i^2} + c + \frac{d}{c_i^2}\right)}$, where $a = 2.68 \frac{s^{1.31} \cdot m^{2.62} \cdot K}{kJ \cdot kg^{0.31}}$, b = 0.31, $c = -16.4 \frac{s \cdot m^2 \cdot K}{kJ}$, $d = 16.6 \frac{s^{1.0} \cdot m^{2.0} \cdot K}{kJ \cdot kg^{2.62 \times 10^{-3}}}$, $e = 2.62 \times 10^{-3}$. These parameters result in all model trend for various G_s to clumped up into one line. Both b and e values deviate greatly from expected values from Sieder-Tate where b = 0.8 and e = 0.55. Model yield negative value for c, which is physically impossible despite proper fitting. Error bars for elements with repeated runs are presented and small compared to data point.

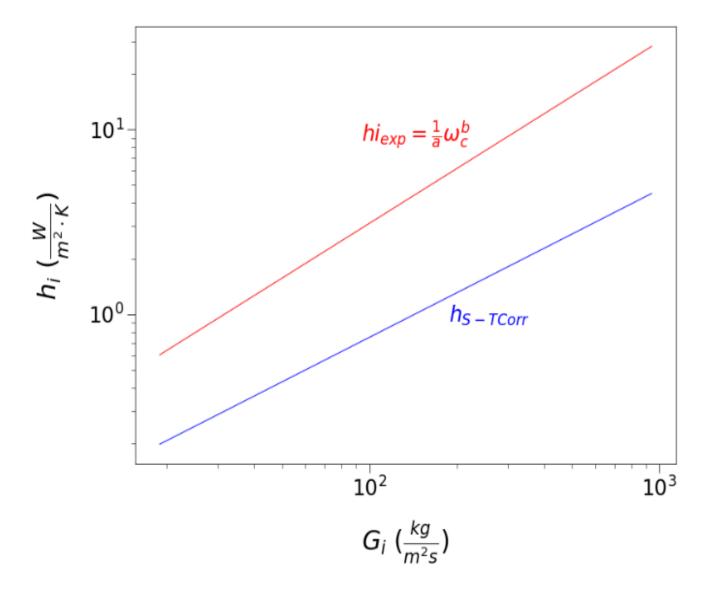


Figure 3. log-log plot of tube-side experimental h_i^{Exp} and Sieder-Tate correlation h_i^{S-T} heat transfer coefficient versus mass velocity G_i for countercurrent condition. Here, $h_i^{Exp} = \frac{1}{a}\omega_c^b$ where b=1.08 and $a=40.09\frac{s^{2.08}\cdot m^{4.16}\cdot K}{kJ\cdot kg^{1.08}}$. Both models portray the same trends on the log-log scale, but h_i^{Exp} values are four to ten magnitudes larger than h_i^{S-T} , scale inversely with G_i .

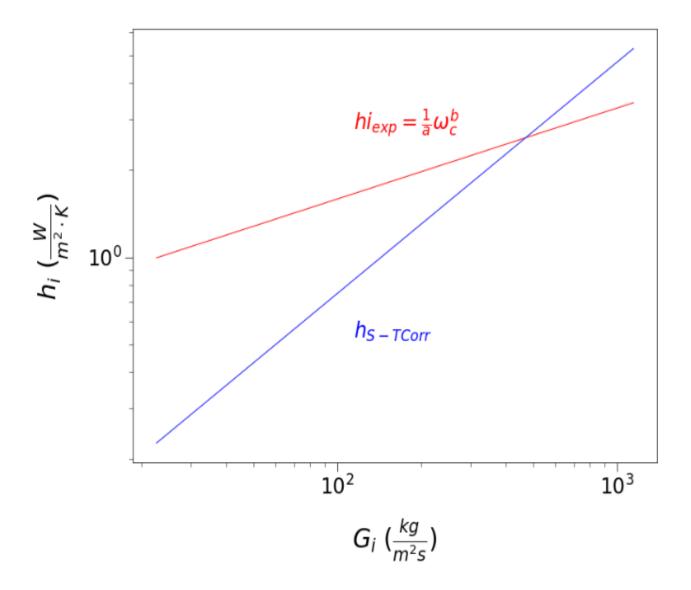


Figure 4. log-log plot of tube-side experimental h_i^{Exp} and Sieder-Tate correlation h_i^{S-T} heat transfer coefficient versus mass velocity G_i . for co-current condition. Here, $h_i^{Exp} = \frac{1}{a} \omega_c^b$ where b = 0.31 and $a = 2.68 \frac{s^{1.31} \cdot m^{2.62} \cdot K}{kJ \cdot kg^{0.31}}$. h_i^{Exp} start off higher than h_i^{S-T} at lower G_i but increase slower. This leads to an intersection point between the two model at $G_i = 420 \frac{kg}{m^2s}$.

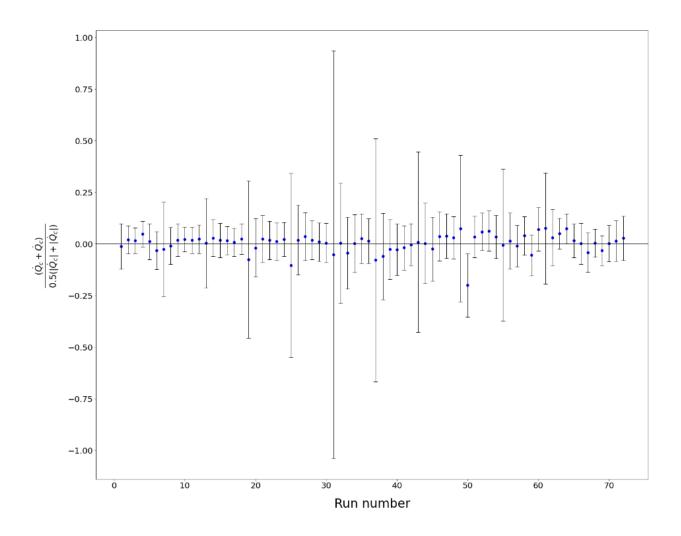


Figure 5. Plot of normalized heat rate versus number of runs. All data point is within error tolerance with the normalized axis. Points deviations are noticed to be relatively small compared to error bars. Points with spiked error bars are of runs where G_i are around 10 times smaller than G_s . Errors are smallest for run with similar G_1 to G_s . This shows that the data may be accurate, but is not precise, which is reflected through the unusual model fitting for co- and countercurrent.

	Ap	pendix:
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References:

(n.d.). CBE 424 Lab Manual: Heat Exchanger Experiment.

Sample calculation:

U, E	2 hy t= 40-1	we, = 0.038 [hg]
	7	5
Avg we	= We, 1 + WC, 2	0.037 +0.038 = 0.0377 (hg)
	2	2 = 0.0377 5
4d w - Tw	-w 1/2 -/w	The property of the second
13	to the stand of the stand of	(0.0377 - 0.37) + (0.037 - 0.
3.0	10 . Why	
11	10. 4 hy	*
(4)	17 ± 0.0003 hr	
WE = 0.0	37 ± 0.0003 hay	
Mary C	= Q _{c,1} +Q _{c,2} =	(·)
544 0	2,1 46,6 =	3.53 KT
We :	= 0.0017 (AT)	
	Ls]	=) Qc = 3.53 ±0,0027 hT
Q = 365	± 0.0135 LJ	3+d Q = 10.077 + 10] = 0.000135 b)
	5	2 = 0.000135 65
世		Std V = 0.0135 h5 1 1
	+000 -1	= 0.00049 kJ 26K
U : 1.25	T 1100 (20 124 1 1 T	1 0.000 13 4.1
U : 1.85	± 0,000 49 / 47 7	> shown error on graph

$$G_{i} = \frac{\omega_{o}}{N_{f} \, \mathcal{R} \cdot \frac{\partial f}{\partial t}} = \frac{0.037 \, \frac{M_{f}}{S}}{31.4 \, \left(\frac{0.91}{89.31}\right)^{2}} = \frac{0.037 \, \frac{M_{f}}{S}}{32.4 \, \frac{M_{g}}{M_{g}}} = \frac{0.037 \, \frac{M_{f}}{S}}{32.37} = \frac{0.042 \, \frac{M_{g}}{M_{g}}}{M_{g}} = \frac{0.022 \, \frac{M_{g}}{M_{g}}}{M_{g}} = \frac{0.024 \, \frac{M_{g}}{M_{g}$$

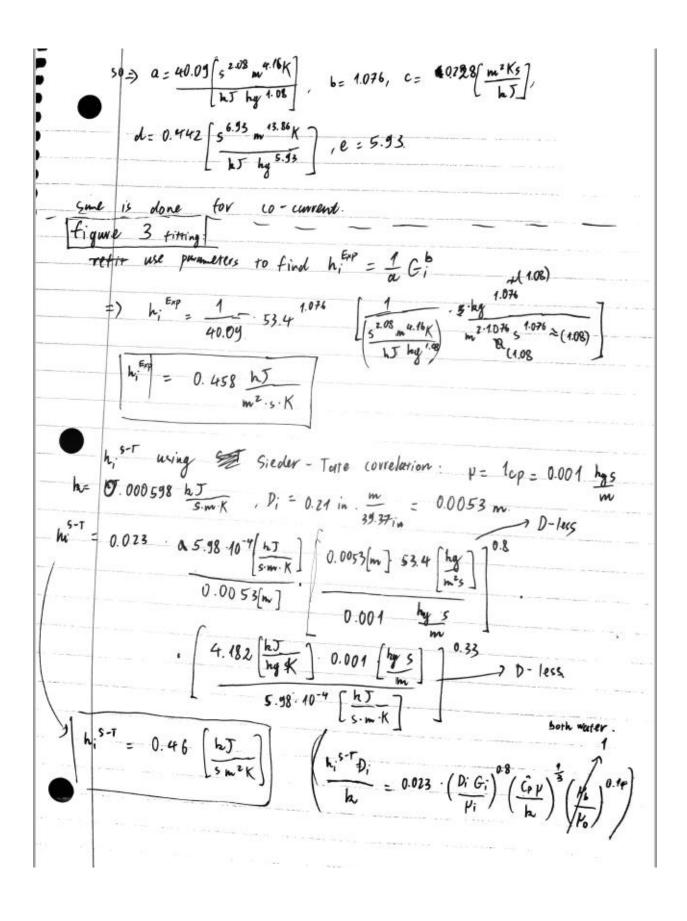


Figure 5. Error Propagation Q = miGrate, QH = mH Cp dIH Normalized desire $Q = |Q_c| + |Q_H|$ $\frac{dQ}{dQ_c} = \frac{1}{2} \cdot \frac{dQ}{dQ_H} = \frac{1}{2}$ dQ = |dQi + |dQi | | |dQ dQc + |dQ DQH | 10 - DQ - \[\frac{1}{2} DQ_c \right|^2 = \$ VAQ12 +AQ12 DQc = \land AQc & me \rangle + \dQc & Te \rangle 2 \ \frac{dQc}{dme} = Cp dT, \frac{dQc}{dTe} = \text{me Cp} DQ = \ [CPE(TE, ORT - TE, in) Dine] + [mie Cp AT]2 # Cpc= 4.182 hJ , Dinc = std mc = 0.000297 hg & Te, our -Te, in = 22.39 K DT = 0.5 (systematic fulcernation) mic = 0.0377 hy ΔQc = \(\langle \lan 0.084 hI DQH derived similar. DQH = 0.39 LT

$$\Delta Q = 2 \sqrt{(0.084)^2 + (0.39)^2} = 0.398$$

Normalised data:
$$\frac{4Q_c \sharp + Q_H}{0.5(|Q_H| + |Q_d|)} = \frac{3.53}{3.65} - 3.78 = -0.0635$$

Done for all aleta point.

Raw data:

Co	Counter Current						
V_{ς}	% 1:						
Pu	mp Spee	1=35	approx.	Nol. Year	Fing CAVR)=5,10	
Ma	55(1)=	8.53 Kg	time	(1) = 20.	05 sec		
Ma	55 (2)=	8.3 D Kg	time	(2)=19	99 50	c	
		_					
_	AVR=	AVR=1.81	AVR=	AVR=	AVR=	AVR=	
100	Mess 1=1.50	M455 1= 5.87	M 455 1= 6.94	Mass 1= 14.15	Mass 1=12.44	Mass 1=9.78	
	time 1= 40.[time 1= 53.02	time 1=30.03	time 1= 40.05	time 1= 20.24	time 1= 15.0	
010	Massz=1,52 Linez=40.0	M9552=	M9552=	M9552=	M9552=	Massz=12.29	
	time 2 = 40.0	timez=	timez=	timez=	timez=	timez= 19.99	
TH,in	55.82	57.58	58.62	58.67	57.00	55.45	
THOUT	53.74	53.69	52.93	51.37	48.17	48.75	
Tc, in	16.27	16.84	16.04	15.27	14.81	14.43	
Tciont	38.66	30.91	26.24	24.25	20.81	20.09	
	RVAl	Rvn 2	Run 3	Run 4	Ru 5	Run 6	
	1/.	1		-			

Co	unter	Current					
	₩2 :						
Pu	mp Spee	1= 45.19	approx.	Nol. Year	Fing CAVR	()=	
	55(1)=			(1) = 19.			
Ma	55 (2)=	10.86	time ((2)= 20	.07		
	AVR=	1.10	1,10	1,10	AVR=	AVR=	
	AVK=	AVR=	AVR=	AVR=	AVK=	AVK=	
	Mess 1= 1,25	Mass 1= 4,85	Mass 1=7.60	Mass 1= 10.08	Mass 1= 7,18	Mass 1=9,48	
	time 1 = 60.15	time 1 = B0.10	time 1 = 50.04	time 1 = 40.6	time 1= 20.18	time 1= 20.10	
	Massz=1.26	M9552=	M9552=	M9552=	Massze	M9552=	
	time 2 = 60.09	timez=	timez=	timez=	timez=	timez=	
TH,in	63.52	64.26	64.30	63.52	62.74	62.00	
THOUT	62.29	60.96	60.19	57.67	56.09	54.66	
$T_{c,in}$	15.17	15.13	15.16	14.99	14.96	(4.93	
Tcioot	47.48	37.33	29.45	28.27	25.50	23-61	
	Run 7 Run 12						

Co	unter	Curred					
	₩3 :						
Pu	mp Spee	1=50.11	approx.	Nol. Year	1:00 CAVR	()=	
Ma	155(1)=	1=50.11	time	(1)= 20	2.07		
	AVR= AVR= AVR= AVR= AVR= AVR= AVR= Mess 1= 0.83 Mess 1= 2.56 Mess 1= 4.19 Mess 1= 6.86 Mess 1= 6.89 Mess 1= 7.4						
	Mess 1= 0-83	M 455 1= 2.56	M455 1=4.19	Mass 1=6.56	Mass 1=6.89	Mass 1= 7.4	

	AVR=	AVR=	AVR=	AVR=	AVK=	AVK=
	Mass 1= 0.83	Mass 1= 2.56	Mass 1=4.19	Mess 1=6.56	Mass 1=6.89	Mass 1= 7.42
	time 1= 30.00	time 1= 30.13	time 1= 29.92	time 1 = 25.0	Hime 1= 20.17	time 1= 5.21
	M9552=	M9552=	M9552=	M9552=	Mass2=	Massz= 7.28
	timez=	timez=	timez=	timez=	timez=	timez= 15.10
TH,in	63.38	64.11	64.08	63.75	63.02	62.10
THOUS	61.98	60.90	60.11	58.27	57.00	55.28
Tc, in	15.26	15.11	15.12	15.17	15.14	15.16
Tcjoot	48.06	38.24	32.71	28.52	26.42	23.86
	D 12				_	Ω

Counter Curred

Vs **4:

Pump speed = \$5.03 approx. Nol. Yeading (AVR) =

mass (1) = 10.04 time (1) = 15.0

mass (2) = time (2) =

	AVR=	AVR=	AVR=	AVR=	AVR=	AVR=
	Mass 1=0.51	M 455 1=1.88	Mess 1=2.81	Mess 1=3.84	Mass 1= 6.02	Mass 1=7.42
	time 1=20,27	time 1= 20.13	time 1= 20.03	time 1= 15.15	time 1= 15,12	time 1= 5.2.
	Massz=0.51	M9552=	M9552=	Massze	M9552=	Massz=7.28
	time 2 = 20.07	timez=	timez=	timez=	timez=	timez=15.10
TH,in	58.49	57,64	57.61	57.73	58.35	60.01
THOUT	S7.52	25.10	54.37	S 3. S3	J3.13	54.05
Tc, in	15.61	15.33	15.28	15.28	15.19	15.12
Tcjoot	3 9.95	33.50	3 o. S8	26.82	23.96	23.50
	Run 19					Run 24

Counter Current

Vs **5:

Pump speed = 60.30 approx. Nol. reading (AVR) =

mass (1) = 10.95 time (1) = 15.04

mass (2) = time (2) =

	AVR=	AVR=	AVR=	AVR=	AVR=	AVR=
	Mess 1 = 0.51	Mess 1=1, 39	M455 1= 2.85	Mass 1= 4.77	Mess 1= 4,14	Mass 1=5.23
	time 1= 20.27	time 1= 15.23	time 1= 14.98	time 1= 15.08	time 1= 10.00	time 1= 10.09
	Massz= 0.51	M9552=	M9552=	M9552=	Mass2=	Massz=5.20
	time 2 = 20.0	timez=	timez=	timez=	timez=	timez = 10.05
TH,in	60.09	60.37	60.37	60.13	59.44	58.59
THOUT	59.27	58.12	57.00	55.61	54.32	53.08
Tc, in	15.70	15.59	15.50	15.56	15.52	15,41
Tcjoot	41.29	34.10	29.14	26.76	24.67	23.16
	P.10 25					Q.1. 20

Counter Current

Vs *6:

Pump speed = 65.08 approx. Nol. reading (AVR) =
mass (1) = 7.97 time (1) = (0.07

mass (2) = 0.09 time (2) = 10.15

	AVR=	AVR=	AVR=	AVR=	AVR=	AVR=
	M 455 1=0.33	M 455 1=0.82	Mass 1= 1.86	Mass 1=2,14	Mass 1=3,50	M 455 1=5.23
	time 1=25.17	time 1= 15.05	time 1= 15.07	time 1 = 9.99	time 1= 10.03	time 1= 10.09
	M9552=	M9552=	M9552=	M9552=	Mass2=	Massz = 5.20
	timez=	timez=	timez=	timez=	timez=	timez = 10.05
TH,in	56.90	56.07	55.81	55.81	55.97	56.84
THOUT	56.47	54.64	53.34	52.68	52.03	10.52
Tc, in	15.65	15.46	15.34	15-73	15.30	15-31
Tcioot	40,51	36.32	30.67	26.92	24.37	22.89
	RU1 31					Run 36

(0-Curred)

Vs *1:

Pump speed = 65.00 approx, Nol. Yeading (AVR) =

mass (1) = 7.97 time (1) = (0.07

mass (2) = 0.09 time (2) = 10.15

	AVR=	AVR=	AVR=	AVR=	AVR=	AVR=
	Mess 1= .47	M 455 1= 1.01	M 955 1=2.(2	Mess 1= 2.16	Mass 1= 3.51	M 455 1=6,14
	time 1= 30.0	time 1= 15.08	time 1= 15,14	time 1= 10.70	time 1= 10.05	time 1= 10.04
	M9552=	M9552=	M9552=	Mass2=	M9552=	Massz=6.18
	Limez=	timez=	timez=	timez=	time2=	timez=10.12
TH,in	61.30	62.26	62.26	62.12	61.69	60.88
THOUT	60.60	60.19	\$9.32	58.51	57.30	55.41
Tc, out	\$2.25	39.38	32. 4 2	28.84	25.76	72.83
Tesin	16.16	15.94	15.95	15.89	15.86	15.71

Run 37 ... Run 42

(0-Curred Vs *2: Pump speed = 60.16 approx. Nol. reading (AVR) = Mass (1) = 7.38 time (1) = 10.15

mass (2) = time (2) =

	AVR=	AVR=	AVR=	AVR=	AVR=	AVR=
	Mass 1= 0-42	M 455 1=1,14	Mess 1= 1.24	M 455 1= 2.51	M 455 1=4,/2	Mass 1=6,14
	time 1=20.04	time 1=15.07	time 1= 10.14	time 1= 1012	time 1= 10.09	time 1= 10.04
	Massz=0.39	M9552=	M9552=	M9552=	M9552=	Massz=6.18
	timez = 20.05	timez=	timez=	timez=	timez=	timez=10.12
TH,in	57.90	57.39	57.11	57.22	57.50	59.58
Hout	57.04	55:43	54.58	53.68	53.09	53,94
Tc, od	46.32	34. 58	30.22	25.61	23.15	22.10
Teiln	15.72	15.57	15.46	15.41	15.44	15.5
	Run 43	?				Run 48

Co-Curred Ve * 3: Pump speed = SS.30 approx. Nol. reading (AVR) = mass (1) = 6.74 time (1) = 10.14 Mass (2)= time (2)= AVR= AVR= AVR= AVR= AVR= AVR= Mass 1 = 0.42 Mass 1 = 1, 10 Mass 1 = 2.09 Mass 1 = 4.38 Mass 1 = 5.92 Mass 1 = 8.03 time 1=20.09 time 1= 15.15 time 1= 10.03 time 1=10.12 time 1=10.09 time 1= 70.13 M9552= M9552= M9552= Massz=7.99 timez = 2005 timez= timez= timez= timez= timez=10.12

> 15.69 Run49 Run St

59.67

54.41

23.65

15.67

58.8Z

53.01

22.03

15.50

57.75

51.03

23.82

15.32

Co-Current

5 9.44

58.46

49.16

12.81

Ve *4:

Pump speed = 50.11 approx. Nol. reading (AVR) = mass (1) = 6.11 time (1) = 10.18

59.99

15.74

57.67 56.15

3 6.50 27.77

time (2)= mass (2)=

60.01

	AVR=	AVR=	AVR=	AVR=	AVR=	AVR=
	Mass 1=0.34	M 455 1= 1.22	Mass 1=1.88	Mess 1= 3.27	M 455 1=5.58	Mass 1=8.03
	time 1=20.0	time 1= 15:13	time 1= (0.15	time 1= 10.10	time 1= 10,19	time 1=10.13
	Massz 2.31	Massz=1.21	M9552=	M9552=	Massz=	Massz=7.99
	time2=2012	timez = 15.12	timez=	timez=	timez=	timez=10.17
TH,in	56.05	55-27	54.91	54.92	55.23	56.59
THOUT	55.20	52.92	51,39	50.43	49.64	49.54
Toool	47.79	33.11	26.41	23.43	21.20	20.42
Terin	15.43	15.28	15.28	15.25	15.23	15.18
	Runs	ζ	,			Rundo

(o-Current Ve \$5: Pump speed = 45.12 approx. Nol. Yeading (AVR) = Mass (1) = 5.66 time (1)=10.50 mass (2) = time (2) = AVR= AVR= AVR= AVR= AVR= AVR= Mess 1 = 0.34 Mess 1 = 0.82 Mess 1=1.96 Mess 1 = 3.01 Mess 1 = 5.16 Mess 1=7.95 time 1 = 20.0 time 1 = 20.14 time 1 = 11.15 time 1 = 10.03 time 1 = (0.17 time 1 = 10.06 Massz=0.31 Massz= Massz = 5.16 Massz = 7.25 M9552= M9552= time2 = 2012 time2 = timez = 10.06 timez = 10.00 timez= timez= 60.44 59.83 TH: 59.69 60.72 60.76 J8.07 THOU! 58.65 58.69 56.29 54.90 52.99 50.16 42,79 28.88 52,21 25,42 22.79 20.77 15.64 15.66 15.64 15.40 15.65 15.59 Run66 Run61 . . .

(0-Cvr-11b	
Vs *6:	
Puma seed = 35.04	approx, Nol. Yeading (AVR)=
masscriptical	approx. Nol. reading (AVR)= time (1)= 15.15
Mass (1) ~ 0.10	TIME (1)= 12.1)
Mass (2)=	time (2)=
1	

	AVR=	AVR=	AVR=	AVR=	AVR=	AVR=
	Mass 1= 0.95	Mass 1=2.31	Mess 1=4.27	Mess 1=4,56	Mass 1= 6.02	M 455 1=7,95
	time 1= 21:00	time 1= 5.15	time 1=15.LS	time 1= 10.11	time 1= 10.13	time 1= 10-00
	M9552=	M9552=	Massze	Massz=4,59	M9552=	Massz= 7,05
	timez=	timez=	timez=	timez = 10.08	timez=	timez=10.00
TH,in	54.19	33.48	53,70	53.74	54.77	22.89
THOUT	51.93	49.35	47.86	47.02	46.91	46.63
Tc,out	37.07	26.48	23.36	21.53	20.71	19.90
Tein	15.60	15.42	15.41	15.47	15.45	15.19
	RUAC	2	,			R11177