

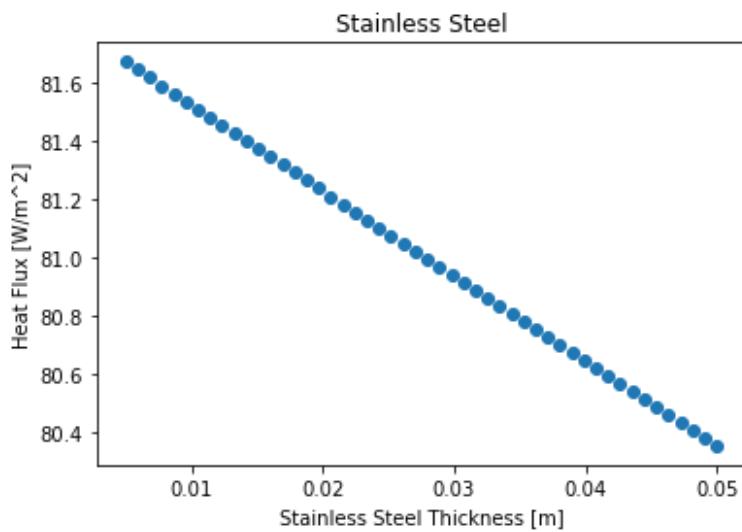
Problem 2

```
In [1]: #Problem 2 Part 2
T_f=-10+273.15
T_r=20+273.15
h_f=10
h_r=10
th_b=1/100
th_w=5/1000
k_b=0.06
k_w=15
R_conv1=1/h_r
R_cond1=th_w/k_w
R_cond2=th_b/k_b
R_cond3=th_w/k_w
R_conv2=1/h_f
R_dprime_tot=R_conv1+R_cond1+R_cond2+R_cond3+R_conv2
q_dprime_net=(T_r-T_f)/(R_dprime_tot)
print('R_tot:', R_dprime_tot, 'q_total: ', q_dprime_net)
```

```
R_tot: 0.367333333333334 q_total:  81.66969147005443
```

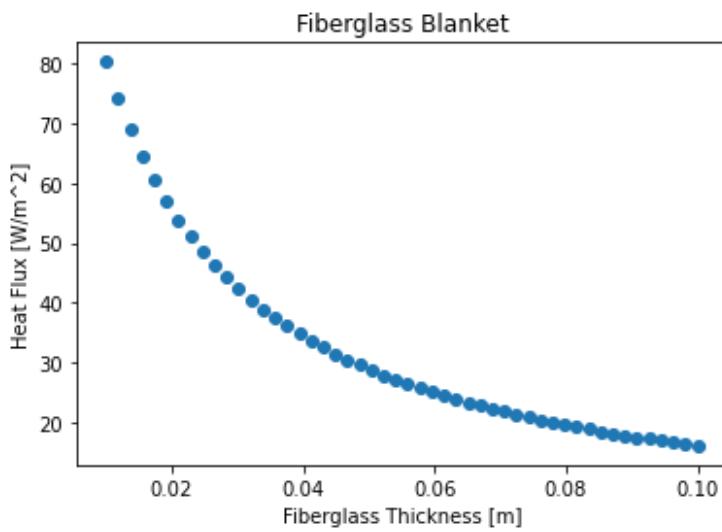
In [2]: #Problem 2 Part 3a

```
import matplotlib.pyplot as plt
import numpy as np
T_f=-10+273.15
T_r=20+273.15
h_f=10
h_r=10
th_b=1/100
th_w=np.linspace(5/1000, 50/1000, 50)
k_b=0.06
k_w=15
R_conv1=1/h_r
R_cond1=th_w/k_w
R_cond2=th_b/k_b
R_cond3=th_w/k_w
R_conv2=1/h_f
R_dprime_tot=R_conv1+R_cond1+R_cond2+R_cond3+R_conv2
q_dprime_net=(T_r-T_f)/(R_dprime_tot)
plt.plot(th_w, q_dprime_net, 'o')
plt.title("Stainless Steel")
plt.xlabel("Stainless Steel Thickness [m]")
plt.ylabel("Heat Flux [W/m^2]")
plt.show()
```



In [3]: #Problem 2 Part 3b

```
import matplotlib.pyplot as plt
import numpy as np
T_f=-10+273.15
T_r=20+273.15
h_f=10
h_r=10
th_b=np.linspace(1/100, 10/100, 50)
th_w=5/100
k_b=0.06
k_w=15
R_conv1=1/h_r
R_cond1=th_w/k_w
R_cond2=th_b/k_b
R_cond3=th_w/k_w
R_conv2=1/h_f
R_dprime_tot=R_conv1+R_cond1+R_cond2+R_cond3+R_conv2
q_dprime_net=(T_r-T_f)/(R_dprime_tot)
plt.plot(th_b, q_dprime_net, 'o')
plt.title("Fiberglass Blanket")
plt.xlabel("Fiberglass Thickness [m]")
plt.ylabel("Heat Flux [W/m^2]")
plt.show()
```



Problem 2c

Increasing the stainless steel thickness will decrease the rate of heat transfer linearly, but increasing the thickness of the fiberglass blanket will decrease the rate of heat transfer at a quicker rate and by more. In relation to the difference in heat flux for the fiberglass blanket, the difference for the stainless steel wall is minimal. Of course you have to consider the cost differences of increasing the thickness of the fiberglass versus the stainless steel.

```
In [4]: #Problem 2 Part 4
```

```
T_f=-10+273.15
T_r=20+273.15
h_f=10
h_r=10
th_b=1/100
th_w=5/1000
k_b=0.06
k_w=15
R_conv1=1/h_r
R_cond1=th_w/k_w
R_cond2=th_b/k_b
R_cond3=th_w/k_w
R_dprime4=R_conv1+R_cond1+R_cond2+R_cond3
q_dprime_net4=81.67
T_freezer_surface=(-(q_dprime_net4*R_conv1-T_r))-273.15
print('T_freezer_surface [°C]:', T_freezer_surface)
```

```
T_freezer_surface [°C]: 11.833000000000027
```

No, the current freezer does not satisfy the design requirement. It is less than 15°C

```
In [5]: #Problem 2 Part 5a
```

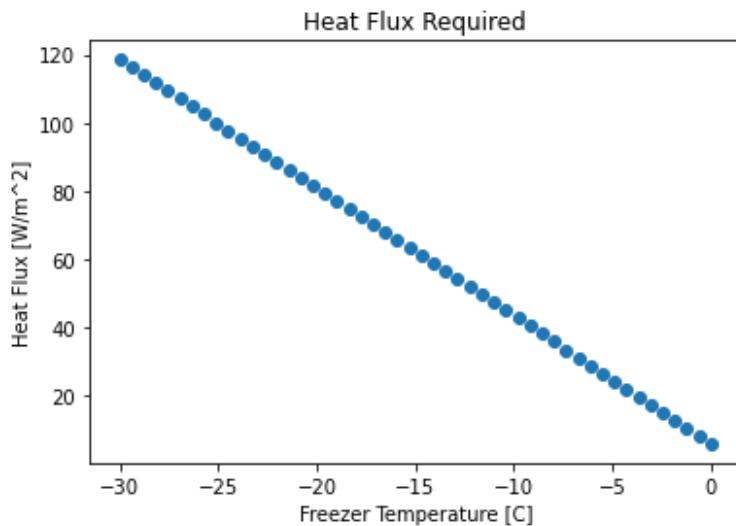
```
T_f=-10+273.15
T_r=20+273.15
h_f=10
h_r=10
th_b=1/100
th_w=5/1000
k_b=0.06
k_w=15
R_conv1=1/h_r
R_cond1=th_w/k_w
R_cond2=th_b/k_b
R_cond3=th_w/k_w
R_conv2=1/h_f
q1_dprime=(T_r-(15+273.15))/R_conv1
T2=-(q1_dprime*R_cond1-(15+273.15))
q2_dprime=(T2-T_f)/(R_cond2+R_cond3+R_conv2)
q_dprime_heater=q2_dprime-q1_dprime
print('Heat required [W/m^2]:', q_dprime_heater)
```

```
Heat required [W/m^2]: 43.57053682896385
```

In [6]: #Problem 2 Part 5b

```
T_f=np.linspace(-30+273.15, 0+273.15, 50)
T_r=20+273.15
h_f=10
h_r=10
th_b=1/100
th_w=5/1000
k_b=0.06
k_w=15
R_conv1=1/h_r
R_cond1=th_w/k_w
R_cond2=th_b/k_b
R_cond3=th_w/k_w
R_conv2=1/h_f
q1_dprime=(T_r-(15+273.15))/R_conv1
T2=- (q1_dprime*R_cond1-(15+273.15))
q2_dprime=(T2-T_f)/(R_cond2+R_cond3+R_conv2)
q_dprime_heater=q2_dprime-q1_dprime

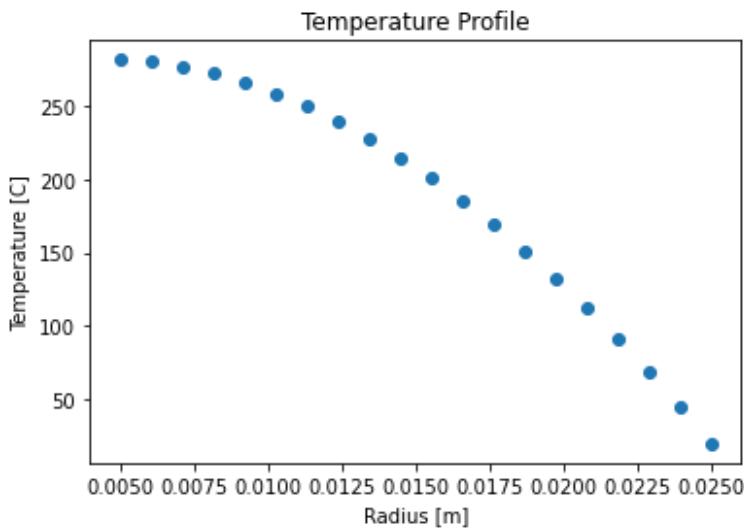
plt.plot(T_f-273.15, q_dprime_heater, 'o')
plt.title("Heat Flux Required")
plt.xlabel("Freezer Temperature [C]")
plt.ylabel("Heat Flux [W/m^2]")
plt.show()
```



Problem 3

In [7]: #Problem 3 Part 5

```
r_in = 5/1000
r_out=25/1000
q_dot=10**6
q_dprime_in = 100
T_out = 20+273.15
k=0.5
r=np.linspace(r_in, r_out, 20)
C1=(-r_in/k)*(q_dprime_in-(q_dot*r_in/2))
C2=T_out+((q_dot*(r_out**2))/(4*k))-C1*np.log(r_out)
T=((q_dot*(r**2))/(4*k))+C1*np.log(r)+C2
plt.plot(r, T-273.15, 'o')
plt.title("Temperature Profile")
plt.xlabel("Radius [m]")
plt.ylabel("Temperature [C]")
plt.show()
```



Problem 4

```
In [8]: #Square
D=1*10**(-3)
h=35
k=2.8
L=10*10**-3
P_square=4*D
A_f_square=P_square*L
A_c_square=D**2
m_square=np.sqrt((h*P_square)/(k*A_c_square))
Efficiency_Square=np.tanh(m_square*L)/(m_square*L)
print("Square Efficiency:", Efficiency_Square)
```

Square Efficiency: 0.43711204016107363

```
In [9]: #Triangle
D=1*10**(-3)
k=2.8
h=35
L=10*10**-3
P_triangle=D*3
A_f_triangle=P_triangle*L
A_c_triangle= (np.sqrt(3)/4)*D**2
m_triangle=np.sqrt((h*P_triangle)/(k*A_c_triangle))
Efficiency_Triangle=np.tanh(m_triangle*L)/(m_triangle*L)
print("Triangle Efficiency:", Efficiency_Triangle)
```

Triangle Efficiency: 0.33792542125981023

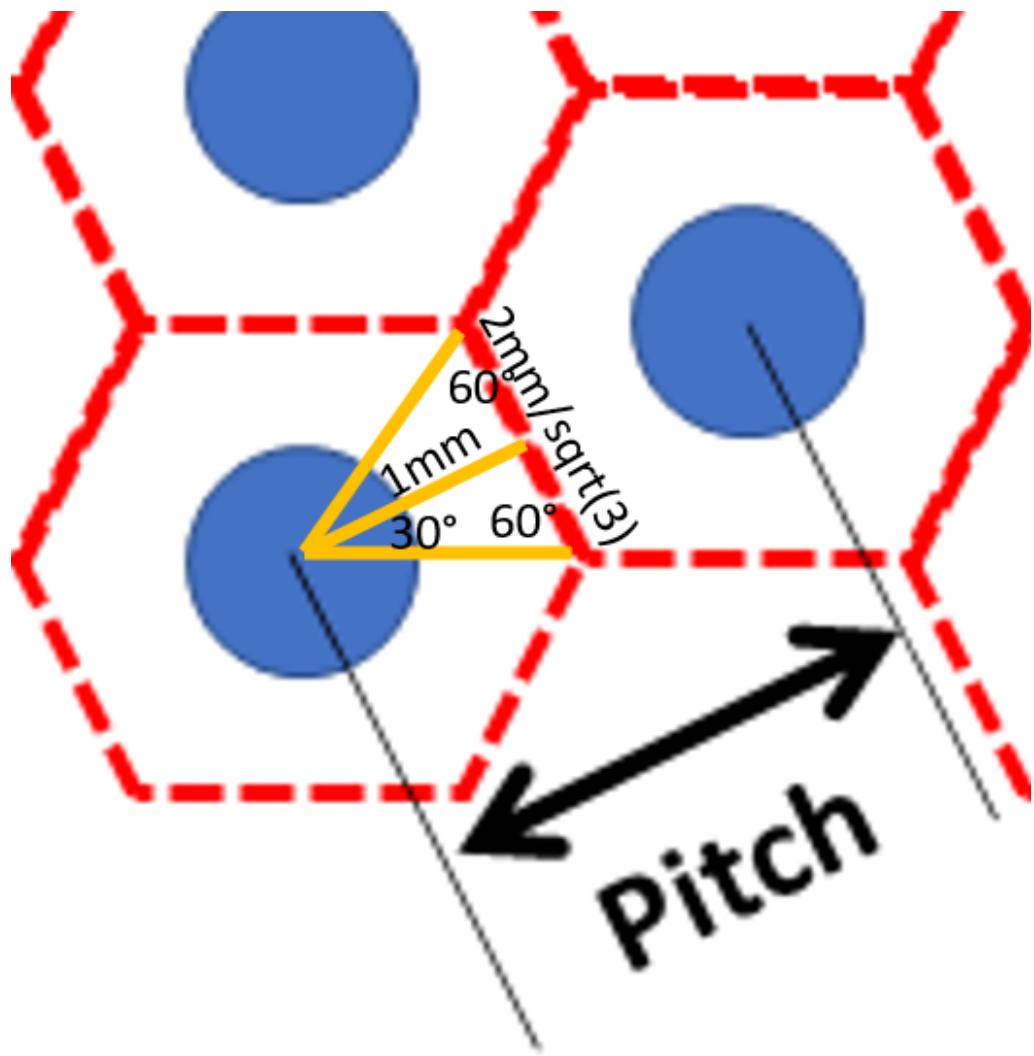
```
In [11]: #Circle
import math # math functions
D=1*10**(-3)
k=2.8
h=35
L=10*10**-3
P_circle=math.pi*D
A_f_circle=P_circle*L
A_c_circle= (math.pi*D**2)/4
m_circle=np.sqrt((h*P_circle)/(k*A_c_circle))
Efficiency_Circle=np.tanh(m_circle*L)/(m_circle*L)
print("Circle Efficiency:", Efficiency_Circle)
```

Circle Efficiency: 0.43711204016107363

The circle and the square have the same efficiencies

```
In [12]: #Number of Fins: 1
side=(2*10**(-3))/np.sqrt(3)
A_Hexagon = (3*np.sqrt(3)/2)*side**2
N=1/A_Hexagon
print(N)
```

288675.1345948129



```
In [13]: #R_unfin: 2 Circle
N=288675
A_b_circle= 1-A_c_circle*N
R_conv_unfin=1/(h*A_b_circle)
print('Circle:', R_conv_unfin)
```

Circle: 0.036948591030671635

```
In [14]: #R_unfin: 2 Square
A_b_square= 1-A_c_square*N
R_conv_unfin=1/(h*A_b_square)
print('Square:', R_conv_unfin)
```

Square: 0.040166490101470595

```
In [15]: #R_unfin: 2 Triangle
A_b_triangle= 1-A_c_triangle*N
R_conv_unfin=1/(h*A_b_triangle)
print('Triangle:', R_conv_unfin)
```

Triangle: 0.03265305904956232

```
In [16]: #R_fin: 3 Circle
R_fin_circle=1/(Efficiency_Circle*h*A_f_circle)
print('Circle:', R_fin_circle)
```

Circle: 2080.6034474201233

```
In [17]: #R_fin: 3 Square  
R_fin_square=1/(Efficiency_Square*h*A_f_square)  
print('Square:', R_fin_square)
```

Square: 1634.1021263621644

```
In [18]: #R_fin: 3 Triangle  
R_fin_triangle=1/(Efficiency_Triangle*h*A_f_triangle)  
print('Square:', R_fin_triangle)
```

Square: 2818.3169790257502

```
In [19]: #Total Resistance and Efficiency Circle  
A_tot_circle=N*A_f_circle+A_b_circle  
Surface_Efficiency_circle= 1-(N*A_f_circle/A_tot_circle)*(1-Efficiency_Circle)  
print("Surface Efficiency Circle:", Surface_Efficiency_circle)  
Total_resistance_circle=1/(Surface_Efficiency_circle*h*A_tot_circle)  
print("Total Resistance Circle:", Total_resistance_circle)
```

Surface Efficiency Circle: 0.48133632883128197

Total Resistance Circle: 0.006030983463979283

```
In [21]: #Total Resistance and Efficiency Square  
A_tot_square=N*A_f_square+A_b_square  
Surface_Efficiency_square= 1-(N*A_f_square/A_tot_square)*(1-Efficiency_Square)  
print("Surface Efficiency Square:", Surface_Efficiency_square)  
Total_resistance_square=1/(Surface_Efficiency_square*h*A_tot_square)  
print("Total Resistance Square:", Total_resistance_square)
```

Surface Efficiency Square: 0.4697752529599205

Total Resistance Square: 0.0049614736492842254

```
In [22]: #Total Resistance and Efficiency Triangle  
A_tot_triangle=N*A_f_triangle+A_b_triangle  
Surface_Efficiency_triangle= 1-(N*A_f_triangle/A_tot_triangle)*(1-Efficiency_Triangle)  
print("Surface Efficiency Triangle:", Surface_Efficiency_triangle)  
Total_resistance_triangle=1/(Surface_Efficiency_triangle*h*A_tot_triangle)  
print("Total Resistance Triangle:", Total_resistance_triangle)
```

Surface Efficiency Triangle: 0.39868054476924353

Total Resistance Triangle: 0.007515793270600793

```
In [23]: #Heat Transfer Rate Circle  
T_gas=35+273.15  
T_base=60+273.15  
Theta=T_base-T_gas  
qt_circle=Theta/Total_resistance_circle  
print("Heat Transfer Rate Circle [W]:", qt_circle)
```

Heat Transfer Rate Circle [W]: 4145.260909653503

```
In [24]: #Heat Transfer Rate Square  
qt_square=Theta/Total_resistance_square  
print("Heat Transfer Rate Square [W]:", qt_square)
```

Heat Transfer Rate Square [W]: 5038.8255117724275

```
In [25]: #Heat Transfer Rate Triangle  
qt_triangle=Theta/Total_resistance_triangle  
print("Heat Transfer Rate Triangle [W]:", qt_triangle)
```

Heat Transfer Rate Triangle [W]: 3326.328851778219

Problem 5

```
In [26]: D=5*10**-2  
u=0.75  
T_in=300  
k=40  
alpha=0.001  
th=0.6*10**-3  
k_g=0.03  
L_c=D/4  
h=k_g/th  
Bi=h*L_c/k  
print(Bi)
```

0.015625

In [27]: # Set up the python script

```
# import required modules

#Numerical Math
import math # math functions
import numpy as np # numerical math
from numpy import *
```

```
# Scientific Math
import scipy # scientific computing functions
import scipy.special as sp # scientific computing functions
import scipy.misc as misc

#Symbolic math
import sympy # symbolic math
from sympy import *
from sympy.abc import x
```

#plotting

```
params = {'legend.fontsize': 'xx-large',
          'figure.figsize': (15, 10),
          'axes.labelsize': 'xx-large',
          'axes.titlesize':'xx-large',
          'xtick.labelsize':'xx-large',
          'ytick.labelsize':'xx-large'}
```

```
import matplotlib.pyplot as plt
plt.rcParams.update(params)
```

```
T = symbols('T', cls=Function)      # define T as a function
a1, a2, Tw0, Tf, Lc, xinf, Tin = symbols('a1 a2 Tw0 Tf Lc xinf Tin', positive = true)    # define
eq = T(x).diff(x,x) - a1*T(x).diff(x) + a2*(T(x)-(Tf - (Tw0-Tf)*exp(-x/Lc)))           # define
Teq=dsolve(eq)                      # symbolically solve the ode
pprint(Teq)
print(Teq)
```

$$T(x) = C_1 \cdot e^{\frac{x}{Lc}} + C_2 \cdot e^{\frac{-x}{Lc}}$$

$$+ \frac{2}{Lc \cdot a_2 +$$

$$- \frac{2}{Lc \cdot a_1 + 1} - \frac{2}{Lc \cdot a_1 + Lc \cdot a_2 + Lc \cdot a_1 + 1}$$

$$\frac{-x}{Lc \cdot a_2 \cdot e^{\frac{x}{Lc}}} + \frac{2}{Lc \cdot Tw_0 \cdot a_2 \cdot e^{\frac{-x}{Lc}}} + \frac{Tf}{Lc \cdot a_1 + 1}$$

$$Eq(T(x), C1*exp(x*(a1 - sqrt(a1**2 - 4*a2))/2) + C2*exp(x*(a1 + sqrt(a1**2 - 4*a2))/2) - Lc**2*Tf*a2*exp(-x/Lc)/(Lc**2*a2 + Lc*a1 + 1) + Lc**2*Tw0*a2*exp(-x/Lc)/(Lc**2*a2 + Lc*a1 + 1) + Tf)$$

```
In [28]: C1, C2 = symbols('C1 C2')      # define these as symbols
constants = sympy.solve([Teq.rhs.subs(x,0)-Tw0, Teq.rhs.subs(x,xinf)-Tf ],[C1,C2])  #Solve for
#pprint(constants)
Teq = Teq.subs(constants)  # Substitute constants C1 and C2 into the equation
pprint(Teq)
print(Teq)
```

$$T(x) = -\frac{\frac{2}{Lc} \cdot \frac{-x}{Tf \cdot a_2 \cdot e}}{\frac{2}{Lc \cdot a_2 + Lc \cdot a_1 + 1}} + \frac{\frac{2}{Lc} \cdot \frac{-x}{Tw_0 \cdot a_2 \cdot e}}{\frac{2}{Lc \cdot a_2 + Lc \cdot a_1 + 1}} + Tf + \frac{\frac{2}{Lc \cdot a_2 \cdot (Tf - Tw_0)} + (}{Lc \cdot a_2 \cdot (Tf - Tw_0) + (}$$

$$\frac{\frac{Lc \cdot Tf \cdot a_1 - Lc \cdot Tw_0 \cdot a_1 + Tf - Tw_0 \cdot e}{2 \cdot Lc} \cdot \frac{xinf \cdot \sqrt{\frac{2}{a_1 - 4 \cdot a_2}}}{1 - e} \cdot \frac{2}{Lc \cdot a_2 + Lc \cdot a_1 + 1} + \frac{1 - \sqrt{\frac{2}{a_1 - 4 \cdot a_2}}}{2} \cdot xinf \cdot \left(-\frac{a_1}{2} + \frac{\sqrt{\frac{2}{a_1 - 4 \cdot a_2}}}{2} - \frac{1}{Lc} \right) \cdot \frac{2}{Lc \cdot a_2 \cdot (Tf - Tw_0)}}{+ \frac{xinf \cdot \sqrt{\frac{2}{a_1 - 4 \cdot a_2}}}{2 \cdot Lc} \cdot e + (-Lc \cdot Tf \cdot a_1 + Lc \cdot Tw_0 \cdot a_1 - Tf + Tw_0) \cdot e} \cdot e$$

$$\frac{xinf \cdot \sqrt{\frac{2}{a_1 - 4 \cdot a_2}}}{2 \cdot Lc} \cdot e + \frac{xinf \cdot (Lc \cdot a_1 + 2)}{2 \cdot Lc} \cdot e + \frac{xinf \cdot \sqrt{\frac{2}{a_1 - 4 \cdot a_2}}}{2 \cdot Lc} \cdot e \cdot e + \frac{(-Lc \cdot Tf \cdot a_1 + Lc \cdot Tw_0 \cdot a_1 - Tf + Tw_0) \cdot e}{2 \cdot Lc} \cdot e + \frac{xinf \cdot \sqrt{\frac{2}{a_1 - 4 \cdot a_2}}}{2 \cdot Lc} \cdot e \cdot e - \frac{a_1 \cdot xinf}{2} - \frac{xinf}{Lc} \cdot e$$

```

Eq(T(x), -Lc**2*Tf*a2*exp(-x/Lc)/(Lc**2*a2 + Lc*a1 + 1) + Lc**2*Tw0*a2*exp(-x/Lc)/(Lc**2*a2 + Lc*a1 + 1) + Tf + (Lc**2*a2*(Tf - Tw0) + (Lc*Tf*a1 - Lc*Tw0*a1 + Tf - Tw0)*exp(xinf*(Lc*a1 + Lc*sqrt(a1**2 - 4*a2) + 2)/(2*Lc)))*exp(x*(a1 - sqrt(a1**2 - 4*a2))/2)*exp(xinf*(-a1/2 + sqrt(a1**2 - 4*a2)/2 - 1/Lc))/((1 - exp(xinf*sqrt(a1**2 - 4*a2)))*(Lc**2*a2 + Lc*a1 + 1)) + (-Lc**2*a2*(Tf - Tw0)*exp(xinf*sqrt(a1**2 - 4*a2)/2) + (-Lc*Tf*a1 + Lc*Tw0*a1 - Tf + Tw0)*exp(xinf*(Lc*a1 + 2)/(2*Lc)))*exp(x*(a1 + sqrt(a1**2 - 4*a2))/2)*exp(-a1*xinf/2 - xinf/Lc)/((1 - exp(xinf*sqrt(a1**2 - 4*a2)))*(Lc**2*a2 + Lc*a1 + 1)))

```

```

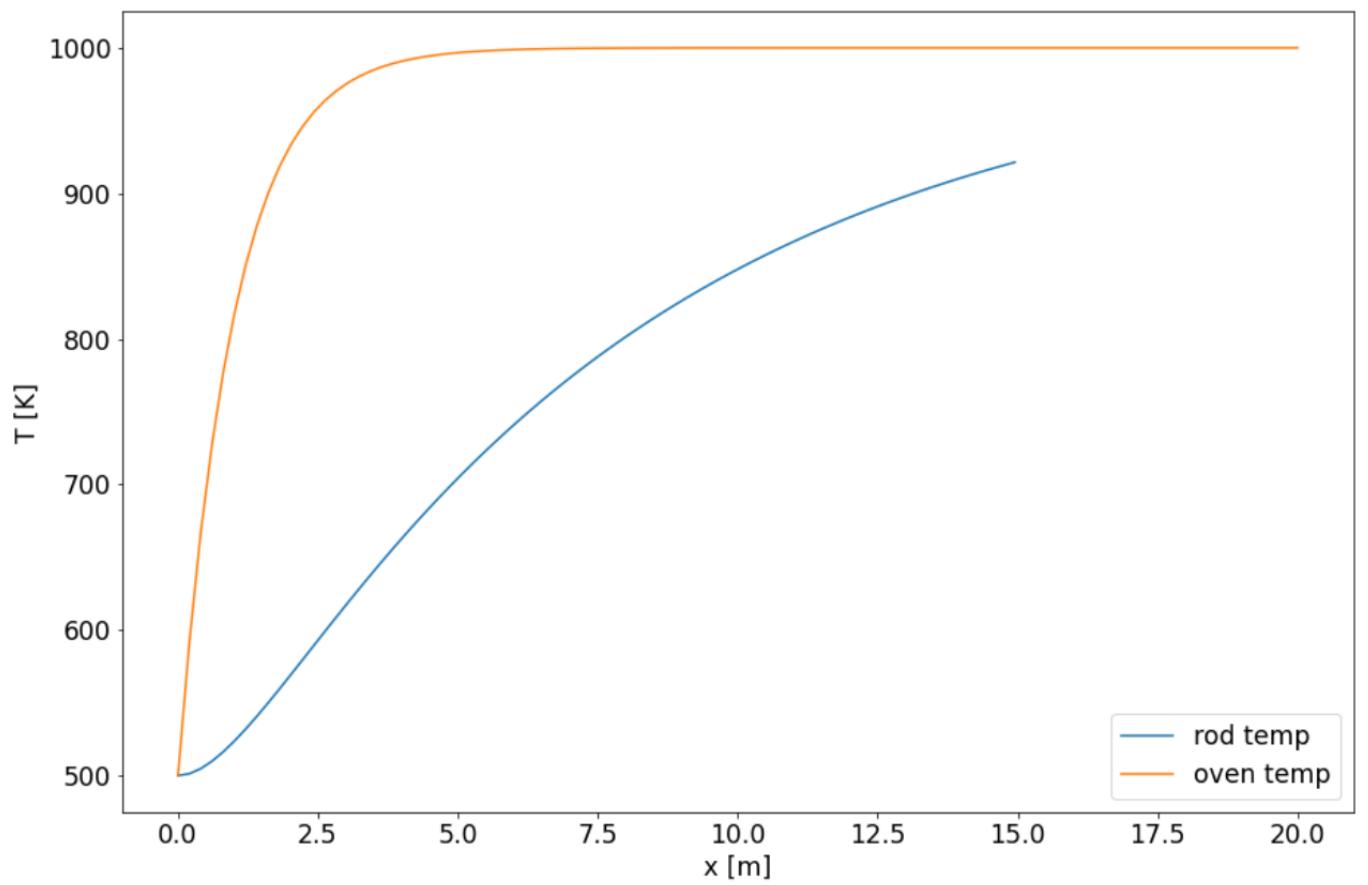
In [ ]: k = 40      #[W/m-K] Thermal conductivity of rod
k_g = 0.03     #[W/m-K] Thermal conductivity of gas
alpha = 0.001   #[m^2/s] diffusivity of rod
u = 0.75       #[m/s] speed of rod
th = 0.6*10**-3 #[m] thickness of gap
D = 5*10**-2    #[m] diameter of rod
Lcs = 1         #[m] decay length for oven temp
Tw0s = 500      #[C] Wall inlet temp
Tfs = 1000      #[C] Wall downstream temp
Tins = 300      #[C] inlet temp
L = 20          #[m] lenght for plotting
xinf = 2000     #[m] a long length to assume x --> infinity

a1s = u/alpha
a2s = -4*k_g/(k*D*th)

Tp = Teq.rhs.subs([(a1,a1s),(a2,a2s),(Tw0,Tw0s),(Tf,Tfs),(Lc,Lcs),(xinf,xinf),(Tin,Tins)]) #
Tp = lambdify(x,Tp,"numpy")
xp = np.linspace(0,L,num=100, dtype=float128)
Tp = Tp(xp)
plt.figure(figsize=(15,10))
plt.plot(xp,Tp,label = 'rod temp')
Tw = (Tfs - (Tfs-Tw0s)*np.exp(-xp/Lcs))
plt.plot(xp,Tw,label='oven temp')
plt.xlabel('x [m]')
plt.ylabel('T [K]')
plt.legend();

```

float128 didn't work on my Jupyter Notebook so I ran this section in Google Colabs using the same code as above



```
In [29]: T_prime=Teq.rhs.diff(x)
pprint(T_prime)
print(T_prime)
```

$$\frac{\frac{-x}{Lc}}{Lc \cdot Tf \cdot a_2 \cdot e} - \frac{\frac{-x}{Lc} \sqrt{\frac{a_1^2 - 4 \cdot a_2}{2}}}{Lc \cdot Tw_0 \cdot a_2 \cdot e} + \frac{\left(\frac{a_1}{Lc} - \frac{\sqrt{\frac{a_1^2 - 4 \cdot a_2}{2}}}{2} \right)^2}{Lc \cdot a_2 \cdot (Tf - Tw_0) \cdot e}$$

$$\frac{2}{Lc \cdot a_2 + Lc \cdot a_1 + 1} - \frac{2}{Lc \cdot a_2 + Lc \cdot a_1 + 1}$$

$$\frac{xinf \cdot \sqrt{\frac{a_1^2 - 4 \cdot a_2}{2}}}{2 \cdot Lc} +$$

$$Tw_0) + (Lc \cdot Tf \cdot a_1 - Lc \cdot Tw_0 \cdot a_1 + Tf - Tw_0) \cdot e$$

$$\frac{\left(1 - e^{xinf \cdot \sqrt{\frac{a_1^2 - 4 \cdot a_2}{2}}} \right) \left(\frac{2}{Lc \cdot a_2 + Lc \cdot a_1 + 1} \right)}{e^{x \cdot \left(a_1 - \sqrt{\frac{a_1^2 - 4 \cdot a_2}{2}} \right)}} \cdot e^{xinf \cdot \left(-\frac{a_1}{2} + \frac{\sqrt{\frac{a_1^2 - 4 \cdot a_2}{2}}}{2} - \frac{1}{Lc} \right)} \cdot \frac{a_1}{2} + \sqrt{\frac{a_1^2 - 4 \cdot a_2}{2}}$$

$$\frac{\frac{2}{a_1^2 - 4 \cdot a_2}}{2} \cdot -Lc \cdot a_2 \cdot (Tf - Tw_0) \cdot e + (-Lc \cdot Tf \cdot a_1 + Lc \cdot Tw_0 \cdot a_1) \cdot e^{\frac{xinf \cdot \sqrt{\frac{a_1^2 - 4 \cdot a_2}{2}}}{2}}$$

$$\frac{\left(1 - e^{xinf \cdot \sqrt{\frac{a_1^2 - 4 \cdot a_2}{2}}} \right)}{2 \cdot Lc} \cdot e^{xinf \cdot (Lc \cdot a_1 + 2)} \cdot \frac{x \cdot \left(a_1 + \sqrt{\frac{a_1^2 - 4 \cdot a_2}{2}} \right)}{2} - \frac{a_1 \cdot xinf}{2} - \frac{xinf}{Lc}$$

$$a_1 - Tf + Tw_0) \cdot e$$

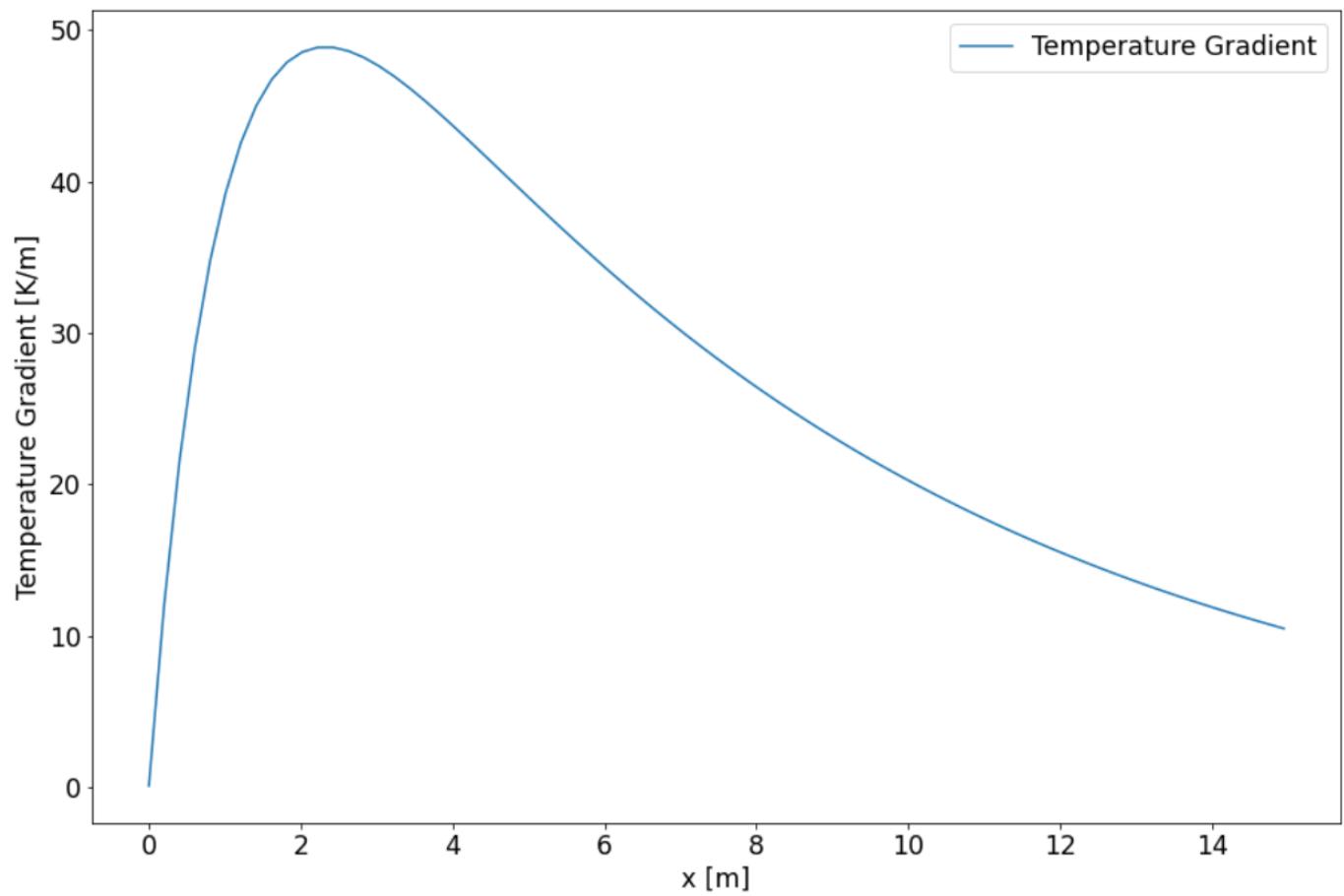
$$\begin{aligned}
& \frac{2}{Lc \cdot a_2 + Lc \cdot a_1 + 1} \\
& Lc^*Tf^*a2^*\exp(-x/Lc)/(Lc^{**2}*a2 + Lc*a1 + 1) - Lc^*Tw0^*a2^*\exp(-x/Lc)/(Lc^{**2}*a2 + Lc*a1 + 1) + \\
& (a1/2 - \sqrt{a1^{**2} - 4*a2}/2)*(Lc^{**2}*a2^*(Tf - Tw0) + (Lc*Tf^*a1 - Lc^*Tw0^*a1 + Tf - Tw0)^*\exp(x \\
& \inf^*(Lc*a1 + Lc^*\sqrt{a1^{**2} - 4*a2}) + 2)/(2*Lc)))*\exp(x*(a1 - \sqrt{a1^{**2} - 4*a2})/2)^*\exp(x \\
& \inf^*(-a1/2 + \sqrt{a1^{**2} - 4*a2}/2 - 1/Lc))/((1 - \exp(x\inf^*\sqrt{a1^{**2} - 4*a2})))^*(Lc^{**2}*a2 + Lc*a \\
& 1 + 1)) + (a1/2 + \sqrt{a1^{**2} - 4*a2}/2)^*(-Lc^{**2}*a2^*(Tf - Tw0)^*\exp(x\inf^*\sqrt{a1^{**2} - 4*a2})/2) \\
& + (-Lc*Tf^*a1 + Lc^*Tw0^*a1 - Tf + Tw0)^*\exp(x\inf^*(Lc*a1 + 2)/(2*Lc)))*\exp(x*(a1 + \sqrt{a1^{**2} - \\
& 4*a2})/2)^*\exp(-a1*x\inf/2 - x\inf/Lc)/((1 - \exp(x\inf^*\sqrt{a1^{**2} - 4*a2})))^*(Lc^{**2}*a2 + Lc*a1 + \\
& 1))
\end{aligned}$$

```
In [ ]: = 40      #[W/m-K] Thermal conductivity of rod
g = 0.03    #[W/m-K] Thermal conductivity of gas
lpha = 0.001  #[m^2/s] diffusivity of rod
= 0.75     #[m/s] speed of rod
h = 0.6*10**-3   #[m] thickness of gap
=5*10**-2    #[m] diameter of rod
cs = 1        #[m] decay Length for oven temp
w0s = 500     #[C] Wall inlet temp
fs = 1000     #[C] Wall downstream temp
ins = 300     #[C] inlet temp
= 20          #[m] Length for plotting
infs = 2000    #[m] a long length to assume x --> infinity

1s = u/alpha
2s = -4*k_g/(k*D*th)

T = T_prime.subs([(a1,a1s),(a2,a2s),(Tw0,Tw0s),(Tf,Tfs),(Lc,Lcs),(xinf,xinfs),(Tin,Tins)]) # :
T = lambdify(x,dT,"numpy")
p = np.linspace(0,L,num=100, dtype=float128)
T = dT(xp)
lt.figure(figsize=(15,10))
lt.plot(xp,dT,label = 'rod temp')
lt.legend();
```

again, float128 did not work in Jupyter so I ran the above code in Google Colab



Problem 1:

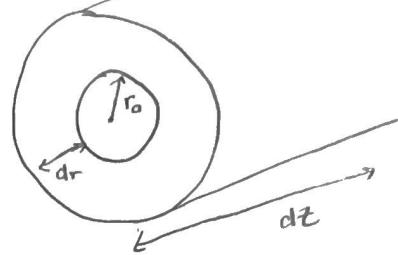
Assumptions: Steady State, 2D (r and z directions), constant k_z and k_r .

Spatially varying heat generation rate \dot{q}

$$\textcircled{1} \quad \rho C_p \frac{\partial T}{\partial t} = \frac{1}{r} \frac{\partial}{\partial r} \left(k_r r \frac{\partial T}{\partial r} \right) + \frac{1}{r^2} \frac{\partial}{\partial \theta} \left(k_\theta \frac{\partial T}{\partial \theta} \right) + \frac{\partial}{\partial z} \left(k_z \frac{\partial T}{\partial z} \right) + \dot{q}$$

Constant k_r 2D in r & z directions Constant k_z

$$0(\text{ss}) \quad D = \frac{k_r}{r} \frac{d}{dr} \left(r \frac{dT}{dr} \right) + k_z \left(\frac{d^2 T}{dz^2} \right) + \dot{q}(r, z)$$



$$\textcircled{2} \quad q_r = q'' A = \boxed{-k_r \frac{\partial T}{\partial r} r_o (2\pi) dz = q_r}$$

$$\textcircled{3} \quad q_{r+dr} = q''_{r+dr} A = q''_r r_o (2\pi) dz + \frac{\partial}{\partial r} (q''_r r_o (2\pi) dz) dr = \boxed{-k_r \frac{\partial T}{\partial r} r_o (2\pi) dz + \frac{\partial}{\partial r} (-k_r \frac{\partial T}{\partial r} r_o (2\pi) dz) dr}$$

$q_{r+dr} + \frac{\partial}{\partial r} (q''_r dr)$

$$\textcircled{4} \quad q_r - q_{r+dr} = \boxed{-k_r \frac{\partial T}{\partial r} r_o (2\pi) dz - (-k_r \frac{\partial T}{\partial r} r_o (2\pi) dz) dr + \frac{\partial}{\partial r} (-k_r \frac{\partial T}{\partial r} r_o (2\pi) dz) dr}$$

constant cancels

$$q_r - q_{r+dr} = \boxed{-\frac{\partial}{\partial r} (-k_r \frac{\partial T}{\partial r} r_o (2\pi) dz) dr}$$

$$q_r - q_{r+dr} = k_r \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) (2\pi) dz dr$$

$2\pi r_o dz dr = \text{volume}$

(5)

$$q_z = q''_z A$$

$$q_z = -k_z \frac{\partial T}{\partial z} r_o (2\pi) dr$$

$$q_{z+dz} = -k_z \frac{\partial T}{\partial z} r_o (2\pi) dr + \frac{\partial}{\partial z} \left(-k_z \frac{\partial T}{\partial z} r_o (2\pi) dr \right) dz$$

$$q_z - q_{z+dz} = -k_z \frac{\partial T}{\partial z} r_o (2\pi) dr - \left(-k_z \frac{\partial T}{\partial z} r_o (2\pi) dr + \frac{\partial}{\partial z} \left(-k_z \frac{\partial T}{\partial z} r_o (2\pi) dr \right) dz \right)$$

$$q_z - q_{z+dz} = \boxed{-\frac{\partial}{\partial z} \left(-k_z \frac{\partial T}{\partial z} r_o (2\pi) dz \right)}$$

constant volume

$$q_z - q_{z+dz} = k_z \frac{\partial}{\partial z} \left(\frac{\partial T}{\partial z} r_o (2\pi) dz \right)$$

→

(5)

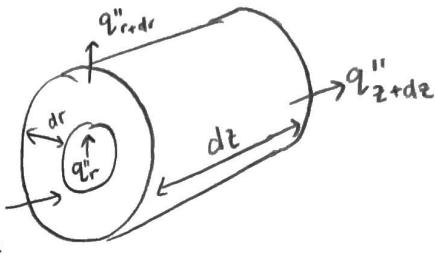
$$\dot{E}_{in} - \dot{E}_{out} + \dot{E}_{gen} = \dot{E}_{st}$$

$$q_r + q_z - q_{r+dr} - q_{z+dz} + \dot{q} \nabla = \rho C_p \frac{dT}{dt} \nabla$$

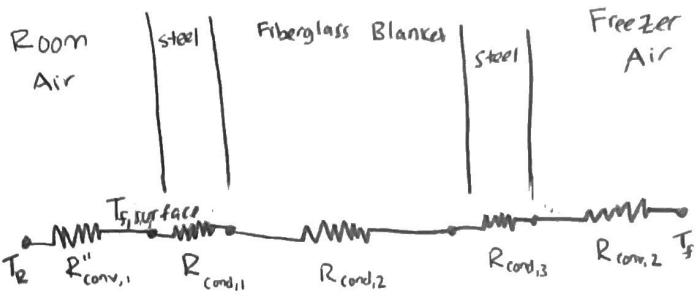
$$(q_r - q_{r+dr}) + (q_z + q_{z+dz}) + \dot{q} r_0 dr (2\pi) dz = \rho C_p \frac{dT}{dt} r_0 dr (2\pi) dz$$

$$\left[\underbrace{\left(k_r \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) \right)}_{\nabla} \underbrace{(2\pi) dz dr}_{\nabla} + \left(k_z \frac{\partial}{\partial z} \left(\frac{\partial T}{\partial z} \right) \right) \underbrace{G(2\pi) dz dr}_{\nabla} + \dot{q} \underbrace{r_0 dr (2\pi) dz}_{\nabla} \right] = \rho C_p \frac{dT}{dt} \text{ für kleine } \nabla$$

$$\boxed{k_r \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) + k_z \frac{\partial}{\partial z} \left(\frac{\partial T}{\partial z} \right) + \dot{q} = \rho C_p \frac{dT}{dt}}$$



Problem 2:
Assumptions



$$(1) R''_{conv,1} = \frac{1}{h_r}$$

$$R''_{cond,1} = \frac{t_w}{k_w}$$

$$R_{cond,2} = \frac{t_w}{k_b}$$

$$R_{cond,3} = \frac{t_w}{k_w}$$

$$R''_{conv,2} = \frac{1}{h_f}$$

$$R''_{tot} = R''_{conv,1} + R''_{cond,1} + R''_{cond,2} + R''_{cond,3} + R''_{conv,2}$$

$$q''_{net} = \frac{(T_R - T_f)}{R''_{tot}}$$

* Jupyter Notebook *

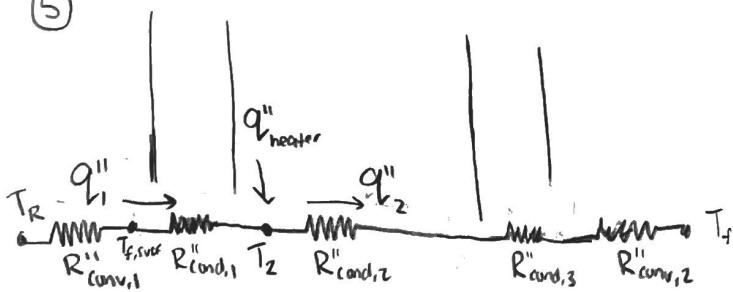
$$(2) R''_{tot} = 0.367$$

$$q''_{tot} = 81.67 \frac{W}{m^2} \quad * \text{Jupyter Notebook} *$$

$$(4) q''_{net} = \frac{(T_R - T_{f,surface})}{R''_{conv,1}} \rightarrow T_{f,surface} = -\left[\left(q''_{net} R''_{conv,1} \right) - T_R \right]$$

$$T_{f,surface} = -11.83^\circ C \quad * \text{Jupyter Notebook} *$$

(5)



$$q''_1 = \frac{T_R - T_{f,surface}}{R''_{conv,1}}$$

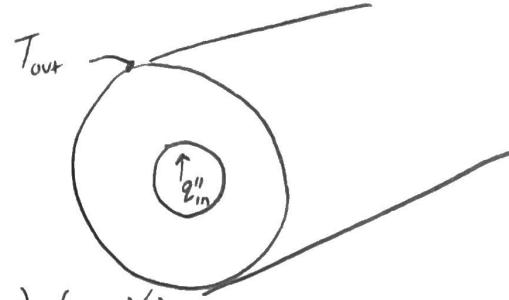
$$\text{Solve for } q''_1 = \frac{T_{f,surface} - T_2}{R''_{cond,1}}$$

$$\text{Solve for } q''_2 \rightarrow q''_2 = \frac{T_2 - T_f}{R''_{cond,2} + R''_{cond,3} + R''_{conv,2}}$$

$$q''_{heater} = q''_2 - q''_1$$

Problem 3

Assumptions: 1D, steady state, constant k



$$\textcircled{1} \quad \cancel{\rho C_p \frac{dT}{dt}} = \underbrace{\frac{1}{r} \frac{\partial}{\partial r} \left(k_r r \frac{\partial T}{\partial r} \right)}_{O(ss)} + \underbrace{\frac{1}{r^2} \frac{\partial}{\partial \theta} \left(k_\theta \frac{\partial T}{\partial \theta} \right)}_{O(1D)} + \underbrace{\frac{\partial}{\partial z} \left(k_z \frac{\partial T}{\partial z} \right)}_{O(1D)} + \dot{q}$$

$$O = \frac{k_r}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) + \dot{q}$$

$$r \frac{dT}{dr} = -\frac{\dot{q}}{2k_r} r^2 + C_1 \rightarrow -k_r \frac{dT}{dr} = \frac{\dot{q} r}{2} - R_r \frac{C_1}{r}$$

\textcircled{2}

$$T(r) = -\frac{\dot{q}}{4k_r} r^2 + C_1 \ln(r) + C_2$$

\textcircled{3} Boundary Conditions

Constant Surface Heat Flux

$$-\left. k \frac{dT}{dr} \right|_{r=r_{in}} = q''_{in} = \frac{\dot{q} r_{in}}{2} - \frac{k_r C_1}{r} \quad -\frac{r_{in}}{k_r} \left[q''_{in} - \frac{\dot{q} r_{in}}{2} \right] = C_1$$

$$T(r=r_{out}) = T_{out} = -\frac{\dot{q}}{4k_r} r_{out}^2 + \left[\left(-\frac{r_{in}}{k_r} \right) \left(q''_{in} - \frac{\dot{q} r_{in}}{2} \right) \right] \ln(r_{out}) + C_2$$

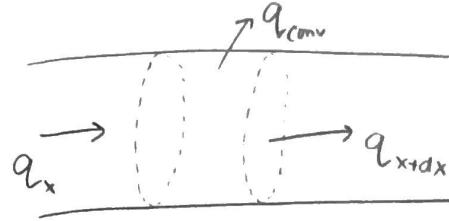
$$\textcircled{4} \quad C_2 = T_{out} + \frac{\dot{q}}{4k_r} r_{out}^2 - \left[\left(-\frac{r_{in}}{k_r} \right) \left(q''_{in} - \frac{\dot{q} r_{in}}{2} \right) \right] \ln(r_{out})$$

$$T(r) = -\frac{\dot{q}}{4k_r} r^2 + \left[\left(-\frac{r_{in}}{k_r} \right) \left(q''_{in} - \frac{\dot{q} r_{in}}{2} \right) \right] \ln(r) + \left[T_{out} + \frac{\dot{q}}{4k_r} r_{out}^2 - \left(\left(-\frac{r_{in}}{k_r} \right) \left(q''_{in} - \frac{\dot{q} r_{in}}{2} \right) \right) \ln(r_{out}) \right]$$

\textcircled{5} * Jupyter Notebook *

Problem 5

$$\textcircled{1} \quad B_i = \frac{h L_c}{k} \quad L_c = \frac{r_o}{2} = \frac{D}{4}$$



$$\textcircled{2} \quad \dot{E}_{in} - \dot{E}_{out} + \dot{E}_{gen}^{\rightarrow 0} = \dot{E}_{sys}$$

$$q_x - q_{x+dx} - q_{conv} = \frac{\partial}{\partial t} (\rho C_p A_c T(x))$$

$$q_x - (q_x + \frac{\partial}{\partial x} (q_x) dx) - h_{conv}(dA_s)(T(x) - T_w(x)) = \rho C_p A_c dx \frac{dx}{dt} \frac{dT}{dx}$$

$$- \frac{\partial}{\partial x} (q_x) dx - h_{conv}(\pi D dx)(T(x) - T_w(x)) = \rho C_p \frac{\pi D^2}{4} dx u \frac{dT}{dx}$$

$$- \frac{\partial}{\partial x} \left(-k \frac{\partial T}{\partial x} \frac{\pi D^2}{4} \right) dx - h_{conv} \left(\frac{\pi D}{4} \frac{\partial T}{\partial x} \right) (T(x) - T_w(x)) = \rho C_p \frac{\pi D^2}{4} dx u \frac{dT}{dx}$$

$$- \frac{\partial}{\partial x} \left(-k \frac{\partial T}{\partial x} \frac{D}{4} \right) - h_{conv} (T(x) - T_w(x)) = \rho C_p \frac{D}{4} u \frac{dT}{dx} \rightarrow \rho C_p = \frac{k}{u}$$

$$\frac{K D}{4} \left(\frac{d^2 T}{dx^2} \right) - h_{conv} (T(x) - T_w(x)) = \frac{k}{u} \frac{D}{4} u \frac{dT}{dx}$$

$$\frac{K D}{4} \left(\frac{d^2 T}{dx^2} \right) + \frac{k}{u} \frac{D}{4} u \frac{dT}{dx} - \frac{k_g}{h} (T(x) - T_w(x)) = 0$$

$$\frac{d^2 T}{dx^2} - \frac{u}{k} \frac{dT}{dx} - \frac{4 k_g}{KD + h} (T(x) - T_w(x)) = 0$$

B.C.
 $T(x=0) - T_{w0} = 0$

$$T(x=\infty) - T_f = 0$$

$$a_1 = \frac{u}{k}$$

$$a_2 = -\frac{4 k_g}{KD + h}$$

* Jupyter Notebook *

In []:

