Recall Stokes' Theorem:

Stokes' Theorem Let S be an oriented piecewise-smooth surface that is bounded by a simple, closed, piecewise-smooth boundary curve C with positive orientation. Let F be a vector field whose components have continuous partial derivatives on an open region in \mathbb{R}^3 that contains S. Then

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \iint_S \text{curl } \mathbf{F} \cdot d\mathbf{S}$$

Since

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \int_C \mathbf{F} \cdot \mathbf{T} \, ds \quad \text{and} \quad \iint_S \text{curl } \mathbf{F} \cdot d\mathbf{S} = \iint_S \text{curl } \mathbf{F} \cdot \mathbf{n} \, dS$$

Stokes' Theorem says that the line integral around the boundary curve of S of the tangential component of **F** is equal to the surface integral over S of the normal component of the curl of **F**.

The positively oriented boundary curve of the oriented surface S is often written as ∂S , so Stokes' Theorem can be expressed as

$$\iint_{S} \operatorname{curl} \mathbf{F} \cdot d\mathbf{S} = \int_{\partial S} \mathbf{F} \cdot d\mathbf{r}$$

There is an analogy among Stokes' Theorem, Green's Theorem, and the Fundamental Theorem of Calculus.

As before, there is an integral involving derivatives on the left side of Equation 1 (recall that curl **F** is a sort of derivative of **F**) and the right side involves the values of **F** only on the *boundary* of *S*.

In fact, in the special case where the surface *S* is flat and lies in the *xy*-plane with upward orientation, the unit normal is **k**, the surface integral becomes a double integral, and Stokes' Theorem becomes

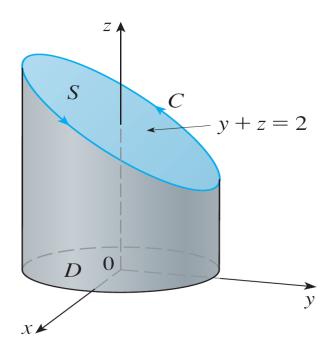
$$\int_C \mathbf{F} \cdot d\mathbf{r} = \iint_S \text{curl } \mathbf{F} \cdot d\mathbf{S} = \iint_S (\text{curl } \mathbf{F}) \cdot \mathbf{k} \ dA$$

This is precisely the vector form of Green's Theorem.

Thus, we see that Green's Theorem is really a special case of Stokes' Theorem.

Example 1

Evaluate $\int_C \mathbf{F} \cdot d\mathbf{r}$, where $\mathbf{F}(x, y, z) = -y^2 \mathbf{i} + x \mathbf{j} + z^2 \mathbf{k}$ and C is the curve of intersection of the plane y + z = 2 and the cylinder $x^2 + y^2 = 1$. (Orient C to be counterclockwise when viewed from above.)



In general, if S_1 and S_2 are oriented surfaces with the same oriented boundary curve C and both satisfy the hypotheses of Stokes' Theorem, then

$$\iint_{S_1} \operatorname{curl} \mathbf{F} \cdot d\mathbf{S} = \int_C \mathbf{F} \cdot d\mathbf{r} = \iint_{S_2} \operatorname{curl} \mathbf{F} \cdot d\mathbf{S}$$

This fact is useful when it is difficult to integrate over one surface but easy to integrate over the other.

Example 2. Use Stokes' Theorem to compute the integral $\iint_S \text{curl } \mathbf{F} \cdot d\mathbf{S}$, where $\mathbf{F}(x, y, z) = xz \mathbf{i} + yz \mathbf{j} + xy \mathbf{k}$ and and S is the part of the sphere $x^2 + y^2 + z^2 = 4$ that lies inside the cylinder $x^2 + y^2 = 1$ and above the xy - plane.

6

We now use Stokes' Theorem to throw some light on the meaning of the curl vector.

Suppose that *C* is an oriented closed curve and **v** represents the velocity field in fluid flow.

Consider the line integral

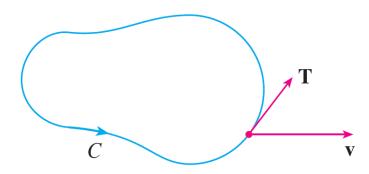
$$\int_C \mathbf{v} \cdot d\mathbf{r} = \int_C \mathbf{v} \cdot \mathbf{T} \, ds$$

and recall that $\mathbf{v} \cdot \mathbf{T}$ is the component of \mathbf{v} in the direction of the unit tangent vector \mathbf{T} .

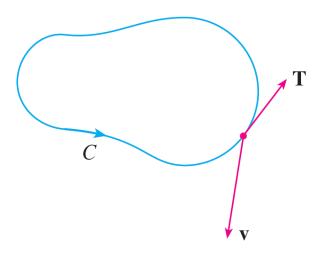
This means that the closer the direction of \mathbf{v} is to the direction of \mathbf{T} , the larger the value of $\mathbf{v} \cdot \mathbf{T}$.

Thus $\int_C \mathbf{v} \cdot d\mathbf{r}$ is a measure of the tendency of the fluid to move around C and is called the **circulation** of \mathbf{v} around C.

(See Figure 5.)



(a) $\int_C \mathbf{v} \cdot d\mathbf{r} > 0$, positive circulation



(b) $\int_C \mathbf{v} \cdot d\mathbf{r} < 0$, negative circulation

Figure 5

Now let $P_0(x_0, y_0, z_0)$ be a point in the fluid and let S_a be a small disk with radius a, center P_0 , unit normal vector \mathbf{n} .

Then $(\text{curl }\mathbf{F})(P)\approx (\text{curl }\mathbf{F})(P_0)$ and $\mathbf{n}(P)\approx \mathbf{n}(P_0)$ for all points P on S_a because curl \mathbf{F} and \mathbf{n} are continuous.

Thus, by Stokes' Theorem, we get the following approximation to the circulation around the boundary circle C_a :

$$\int_{C_a} \mathbf{v} \cdot d\mathbf{r} = \iint_{S_a} \operatorname{curl} \mathbf{v} \cdot d\mathbf{S} = \iint_{S_a} \operatorname{curl} \mathbf{v} \cdot \mathbf{n} \, dS$$

$$\approx \iint_{S_a} \operatorname{curl} \mathbf{v}(P_0) \cdot \mathbf{n}(P_0) \, dS = \operatorname{curl} \mathbf{v}(P_0) \cdot \mathbf{n}(P_0) \pi a^2$$

This approximation becomes better as $a \rightarrow 0$ and we have

$$\operatorname{curl} \mathbf{v}(P_0) \cdot \mathbf{n}(P_0) = \lim_{a \to 0} \frac{1}{\pi a^2} \int_{C_a} \mathbf{v} \cdot d\mathbf{r}$$

Equation 4 gives the relationship between the curl and the circulation.

It shows that curl $\mathbf{v} \cdot \mathbf{n}$ is a measure of the rotating effect of the fluid about the axis \mathbf{n} .

The curling effect is greatest about the axis parallel to curl **v**.

Sketch of proof of Theorem 16.5.4

Theorem If **F** is a vector field defined on all of \mathbb{R}^3 whose component functions have continuous partial derivatives and curl $\mathbf{F} = \mathbf{0}$, then **F** is a conservative vector field.

Given C simple closed curve, suppose we can find an orientable surface S whose boundary is C (this is nontrivial). Then Stokes' Theorem gives

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \iint_S \text{curl } \mathbf{F} \cdot d\mathbf{S} = \iint_S \mathbf{0} \cdot d\mathbf{S} = 0$$

A curve that is not simple can be broken into a number of simple curves, and the integrals around these simple curves are all 0. Adding these integrals, we obtain $\int_C \mathbf{F} \cdot d\mathbf{r} = 0$ for any closed curve C and hence \mathbf{F} is conservative.

16.9

We write Green's Theorem in a vector version as

$$\int_C \mathbf{F} \cdot \mathbf{n} \, ds = \iint_D \operatorname{div} \mathbf{F}(x, y) \, dA$$

where *C* is the positively oriented boundary curve of the plane region *D*.

If we were seeking to extend this theorem to vector fields on \mathbb{R}^3 , we might make the guess that

$$\iint_{S} \mathbf{F} \cdot \mathbf{n} \, dS = \iiint_{E} \operatorname{div} \mathbf{F}(x, y, z) \, dV$$

where S is the boundary surface of the solid region E.

It turns out that Equation 1 is true, under appropriate hypotheses, and is called the Divergence Theorem.

Notice its similarity to Green's Theorem and Stokes' Theorem in that it relates the integral of a derivative of a function (div **F** in this case) over a region to the integral of the original function **F** over the boundary of the region.

We state the Divergence Theorem for regions *E* that are simultaneously of types 1, 2, and 3 and we call such regions **simple solid regions**. (For instance, regions bounded by ellipsoids or rectangles are simple solid regions.)

The boundary of *E* is a closed surface, and we use the convention, that the positive orientation is outward; that is, the unit normal vector **n** is directed outward from *E*.

The Divergence Theorem Let E be a simple solid region and let S be the boundary surface of E, given with positive (outward) orientation. Let F be a vector field whose component functions have continuous partial derivatives on an open region that contains E. Then

$$\iint\limits_{S} \mathbf{F} \cdot d\mathbf{S} = \iiint\limits_{E} \operatorname{div} \mathbf{F} \, dV$$

Thus the Divergence Theorem states that, under the given conditions, the flux of **F** across the boundary surface of *E* is equal to the triple integral of the divergence of **F** over *E*.

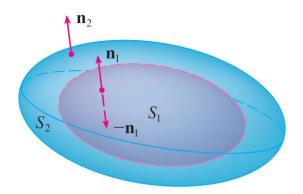
Example 1

Find the flux of the vector field $\mathbf{F}(x, y, z) = z \mathbf{i} + y \mathbf{j} + x \mathbf{k}$ over the unit sphere $x^2 + y^2 + z^2 = 1$.

The divergence theorem can be applied to more general regions being a finite union of simple regions (The procedure is similar to the one we used in Section 16.4 to extend Green's Theorem).

For example, it holds for the region E that lies between the closed surfaces S_1 and S_2 , where S_1 lies inside S_2 . Let \mathbf{n}_1 and \mathbf{n}_2 be outward normals of S_1 and S_2 .

Then the boundary surface of E is $S = S_1 \cup S_2$ and its outward normal \mathbf{n} is given by $\mathbf{n} = -\mathbf{n}_1$ on S_1 and $\mathbf{n} = \mathbf{n}_2$ on S_2 .



Applying the Divergence Theorem to S, we get

$$\iint_{E} \operatorname{div} \mathbf{F} \, dV = \iint_{S} \mathbf{F} \cdot d\mathbf{S}$$

$$= \iint_{S} \mathbf{F} \cdot \mathbf{n} \, dS$$

$$= \iint_{S_{1}} \mathbf{F} \cdot (-\mathbf{n}_{1}) \, dS + \iint_{S_{2}} \mathbf{F} \cdot \mathbf{n}_{2} \, dS$$

$$= -\iint_{S_{1}} \mathbf{F} \cdot d\mathbf{S} + \iint_{S_{2}} \mathbf{F} \cdot d\mathbf{S}$$

Example 3

We considered the electric field:

$$\mathbf{E}(\mathbf{x}) = \frac{\varepsilon Q}{|\mathbf{x}|^3} \mathbf{x}$$

where the electric charge Q is located at the origin and $\mathbf{x} = \langle x, y, z \rangle$ is a position vector.

Use the Divergence Theorem to show that the electric flux of \mathbf{E} through any closed surface S_2 that encloses the origin is

$$\iint\limits_{S_2} \mathbf{E} \cdot d\mathbf{S} = 4\pi \varepsilon Q$$

Another application of the Divergence Theorem occurs in fluid flow. Let $\mathbf{v}(x, y, z)$ be the velocity field of a fluid with constant density ρ . Then $\mathbf{F} = \rho \mathbf{v}$ is the rate of flow per unit area.

If $P_0(x_0, y_0, z_0)$ is a point in the fluid and B_a is a ball with center P_0 and very small radius a, then div $\mathbf{F}(P) \approx \text{div } \mathbf{F}(P_0)$ for all points in B_a since div \mathbf{F} is continuous. We approximate the flux over the boundary sphere S_a as follows:

$$\iint\limits_{S_a} \mathbf{F} \cdot d\mathbf{S} = \iint\limits_{B_a} \operatorname{div} \mathbf{F} \, dV \approx \iint\limits_{B_a} \operatorname{div} \mathbf{F}(P_0) \, dV = \operatorname{div} \mathbf{F}(P_0) V(B_a)$$

This approximation becomes better as $a \rightarrow 0$ and suggests that

$$\operatorname{div} \mathbf{F}(P_0) = \lim_{a \to 0} \frac{1}{V(B_a)} \iint_{S_a} \mathbf{F} \cdot d\mathbf{S}$$

Equation 8 says that div $F(P_0)$ is the net rate of outward flux per unit volume at P_0 . (This is the reason for the name *divergence*.)

If div F(P) > 0, the net flow is outward near P and P is called a **source**.

If div F(P) < 0, the net flow is inward near P and P is called a **sink**.

For the vector field in Figure 4, it appears that the vectors that end near P_1 are shorter than the vectors that start near P_1 .

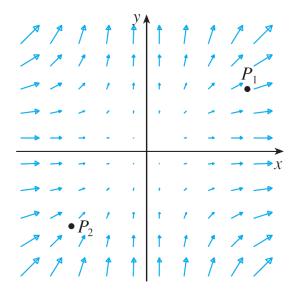


Figure 4

The vector field $\mathbf{F} = x^2 \mathbf{i} + y^2 \mathbf{j}$

Thus the net flow is outward near P_1 , so div $\mathbf{F}(P_1) > 0$ and P_1 is a source. Near P_2 , on the other hand, the incoming arrows are longer than the outgoing arrows.

Here the net flow is inward, so div $\mathbf{F}(P_2)$ < 0 and P_2 is a sink.

We can use the formula for **F** to confirm this impression. Since $\mathbf{F} = x^2 \mathbf{i} + y^2 \mathbf{j}$, we have div $\mathbf{F} = 2x + 2y$, which is positive when y > -x. So the points above the line y = -x are sources and those below are sinks.