

Suleman Ahmed

Taguchi Quality Design

Taguchi Method Implemented on Tire Wear

One of the most important parts on a car is the tire. It is possibly the only part of a car that actually touches the floor, so its importance is heavily emphasized. Tire wear depends on many different factors and has been researched quite extensively. For the sake of simplicity, our design takes in one tire wear formula that has been derived from previous literature. The formula can be seen in figure 1.

$$A = \left(\frac{E}{\sigma}\right) \mu^{0.45} \left(\frac{\theta a^{2.45}}{2.45}\right)$$

(Figure 1)

In this formula, we take in slip angle, tension strength, coefficient of friction of tire to the floor, the length of the contact area of the tire with the floor, and the modulus of elasticity to calculate A, tire wear.

The Taguchi method allows us to test the quality in the design process and made into the final product, not inspected into it. Our process objective in this experiment is tire wear rate and with our formula we can inspect 5 different factors that influence tire wear rate, with 3 levels acting on 3 factors. Of course, there are many other different factors that can affect tire wear rate, such as pressure, but pressure can influence the contact area of the tire to the floor, and that is well included in our design parameters. The following are the values of our design parameters, where the first value is the average of a regular tire:

θ : [0.1, 0.2, 0.3] degrees

σ : [16.5, 16.6, 16.7] MPA

E : [0.9, 1, 1.1] MPA

μ : [0.68, 0.8, 0.15] concrete, asphalt, ice

a: [83.1, 83.2, 83.3] mm

We also want to create a robust design by adding in factors for noise. In our experiment, we add noise for slip angle, tension strength, and length of contact area, each with 2 levels. These values can be seen below:

θ : [-0.02 ; +0.02]

σ : [-0.03 ; +0.03]

a: [-0.03 ; +0.03]

Following the Taguchi method, we created an inner orthogonal array of $L_{27} 3^5$ (Figure 2) and also combined our noise orthogonal array $L_4 2^3$ (Figure 3) to create our final outer array with our tire wear rate results. Figure 4 shows the tire wear results as well as mean square error and signal to noise ratio. The whole process can also be seen in the excel sheet attachment.

| theata | stress | Modulus | friction | area | |
|--------|--------|---------|----------|------|---|
| 1 | 1 | 1 | 1 | 1 | 1 |
| 1 | 1 | 1 | 1 | 1 | 2 |
| 1 | 1 | 1 | 1 | 1 | 3 |
| 1 | 2 | 2 | 2 | 2 | 1 |
| 1 | 2 | 2 | 2 | 2 | 2 |
| 1 | 2 | 2 | 2 | 2 | 3 |
| 1 | 3 | 3 | 3 | 3 | 1 |
| 1 | 3 | 3 | 3 | 3 | 2 |
| 1 | 3 | 3 | 3 | 3 | 3 |
| 2 | 1 | 1 | 2 | 3 | 1 |
| 2 | 1 | 1 | 2 | 3 | 2 |
| 2 | 1 | 1 | 2 | 3 | 3 |
| 2 | 2 | 2 | 3 | 1 | 1 |
| 2 | 2 | 2 | 3 | 1 | 2 |
| 2 | 2 | 2 | 3 | 1 | 3 |
| 2 | 3 | 3 | 1 | 2 | 1 |
| 2 | 3 | 3 | 1 | 2 | 2 |
| 2 | 3 | 3 | 1 | 2 | 3 |
| 3 | 1 | 1 | 3 | 2 | 1 |
| 3 | 1 | 1 | 3 | 2 | 2 |
| 3 | 1 | 1 | 3 | 2 | 3 |
| 3 | 2 | 2 | 1 | 3 | 1 |
| 3 | 2 | 2 | 1 | 3 | 2 |
| 3 | 2 | 2 | 1 | 3 | 3 |
| 3 | 3 | 3 | 2 | 1 | 1 |
| 3 | 3 | 3 | 2 | 1 | 2 |
| 3 | 3 | 3 | 2 | 1 | 3 |

Figure 2.a; Orthogonal $L_{27} 3^5$ array

| theata | stress | area |
|--------|--------|------|
| 1 | 1 | 1 |
| 1 | 2 | 2 |
| 2 | 1 | 2 |
| 2 | 2 | 1 |

Figure 3.a; Orthogonal $L_4 2^3$ array

| theata | stress | Mod | friction | area |
|---------------|---------------|------------|-----------------|-------------|
| 0.1 | 16.5 | 0.9 | 0.67 | 83.1 |
| 0.1 | 16.5 | 0.9 | 0.67 | 83.2 |
| 0.1 | 16.5 | 0.9 | 0.67 | 83.3 |
| 0.1 | 16.6 | 1 | 0.8 | 83.1 |
| 0.1 | 16.6 | 1 | 0.8 | 83.2 |
| 0.1 | 16.6 | 1 | 0.8 | 83.3 |
| 0.1 | 16.7 | 1.1 | 0.15 | 83.1 |
| 0.1 | 16.7 | 1.1 | 0.15 | 83.2 |
| 0.1 | 16.7 | 1.1 | 0.15 | 83.3 |
| 0.2 | 16.5 | 1 | 0.15 | 83.1 |
| 0.2 | 16.5 | 1 | 0.15 | 83.2 |
| 0.2 | 16.5 | 1 | 0.15 | 83.3 |
| 0.2 | 16.6 | 1.1 | 0.67 | 83.1 |
| 0.2 | 16.6 | 1.1 | 0.67 | 83.2 |
| 0.2 | 16.6 | 1.1 | 0.67 | 83.3 |
| 0.2 | 16.7 | 0.9 | 0.8 | 83.1 |
| 0.2 | 16.7 | 0.9 | 0.8 | 83.2 |
| 0.2 | 16.7 | 0.9 | 0.8 | 83.3 |
| 0.3 | 16.5 | 1.1 | 0.8 | 83.1 |
| 0.3 | 16.5 | 1.1 | 0.8 | 83.2 |
| 0.3 | 16.5 | 1.1 | 0.8 | 83.3 |
| 0.3 | 16.6 | 0.9 | 0.15 | 83.1 |
| 0.3 | 16.6 | 0.9 | 0.15 | 83.2 |
| 0.3 | 16.6 | 0.9 | 0.15 | 83.3 |
| 0.3 | 16.7 | 1 | 0.67 | 83.1 |
| 0.3 | 16.7 | 1 | 0.67 | 83.2 |
| 0.3 | 16.7 | 1 | 0.67 | 83.3 |

Figure 2.b; inner array

| theata | stress | area |
|---------------|---------------|-------------|
| -0.02 | -0.03 | -0.03 |
| -0.02 | 0.03 | 0.03 |
| 0.02 | -0.03 | 0.03 |
| 0.02 | 0.03 | -0.03 |

Figure 3.b; noise array

| Trial 1 | Trial 2 | Trial 3 | Trial 4 | MSE | SN |
|----------------|----------------|----------------|----------------|-------------|--------------|
| 1.928969101 | 1.925370277 | 5.218156525 | 5.190026809 | 15.39837707 | -11.8747495 |
| 1.934663214 | 1.931049661 | 5.233548845 | 5.20534722 | 15.48938693 | -11.90034229 |
| 1.940367262 | 1.936738948 | 5.248968003 | 5.220694364 | 15.5808244 | -11.92590433 |
| 2.307335166 | 2.303080886 | 6.241694617 | 6.208183269 | 22.03206708 | -13.43055245 |
| 2.314146175 | 2.309874426 | 6.26010613 | 6.22650917 | 22.1622844 | -13.45614524 |
| 2.32096907 | 2.316679812 | 6.278549747 | 6.244867048 | 22.29311354 | -13.48170728 |
| 1.187793246 | 1.185628845 | 3.213162447 | 3.195980309 | 5.838817899 | -7.663249307 |
| 1.191299486 | 1.189126168 | 3.222640511 | 3.205414505 | 5.87332738 | -7.688842092 |
| 1.194811844 | 1.192629589 | 3.232135102 | 3.214865163 | 5.907999004 | -7.714404134 |
| 7.969614897 | 7.95474621 | 13.053396 | 12.98302856 | 116.4357316 | -20.66086276 |
| 7.993140358 | 7.978210818 | 13.09190041 | 13.02135308 | 117.1239083 | -20.68645556 |
| 8.01670687 | 8.00171634 | 13.13047196 | 13.05974449 | 117.8153183 | -20.71201761 |
| 17.08809724 | 17.05659009 | 27.98851676 | 27.83824781 | 535.3138611 | -27.28608489 |
| 17.1385395 | 17.10690297 | 28.07107622 | 27.92042337 | 538.4777568 | -27.31167768 |
| 17.18906978 | 17.15730358 | 28.15377964 | 28.00274233 | 541.656518 | -27.33723974 |
| 15.05175957 | 15.02433221 | 24.65320855 | 24.52137743 | 415.3411669 | -26.18404979 |
| 15.09619078 | 15.06865042 | 24.72592965 | 24.59376194 | 417.7959812 | -26.20964258 |
| 15.14069951 | 15.1130459 | 24.79877755 | 24.66627276 | 420.2623295 | -26.23520463 |
| 54.96661443 | 54.86406476 | 76.37434609 | 75.96263198 | 4408.689125 | -36.44309476 |
| 55.12887007 | 55.02590069 | 76.59963223 | 76.18686564 | 4434.746054 | -36.46868756 |
| 55.29140883 | 55.18801881 | 76.8253112 | 76.41149058 | 4460.925411 | -36.49424962 |
| 21.04604408 | 21.00723924 | 29.24280258 | 29.08579943 | 646.3413258 | -28.10461925 |
| 21.10816978 | 21.0692056 | 29.32906189 | 29.17165764 | 650.1614341 | -28.13021205 |
| 21.17040388 | 21.13128 | 29.4154716 | 29.25766566 | 653.9994911 | -28.1557741 |
| 45.58347914 | 45.50041679 | 63.33678084 | 62.9980923 | 3032.112235 | -34.81745273 |
| 45.71803675 | 45.63463219 | 63.52360927 | 63.18405601 | 3050.033102 | -34.84304553 |
| 45.85282916 | 45.76908162 | 63.71076346 | 63.37034422 | 3068.038171 | -34.86860759 |

Figure 4; outer array, with the addition of mean square error and signal to noise ratio

From Figure 4, we see the 4 trails ran from each experiment number (all the way to 27). The 4 trails stem from the L_4 noise array. The next part of experiment requires us to calculate the signal to noise ratio. In our experiment, we want the tire wear rate to be low as possible, so we use the formula for MSE:

$$MSE = \frac{1}{n} \sum_1^n y_i^2$$

And use the MSE to calculate the S/N ratio which is:

$$S/N = -10\log_{10}MSE$$

Figure 4 has all these values already collected for each experiment. The first trail contains the optimal levels and factors for tire wear, 1.9%.

After calculating the S/N ratio for each experiment, we calculate the average S/N value for each factor and level. This is done to observe which parameter has the most effect to the design. We use Minitab software to tabulate our results, and also analyze them graphically, shown below.

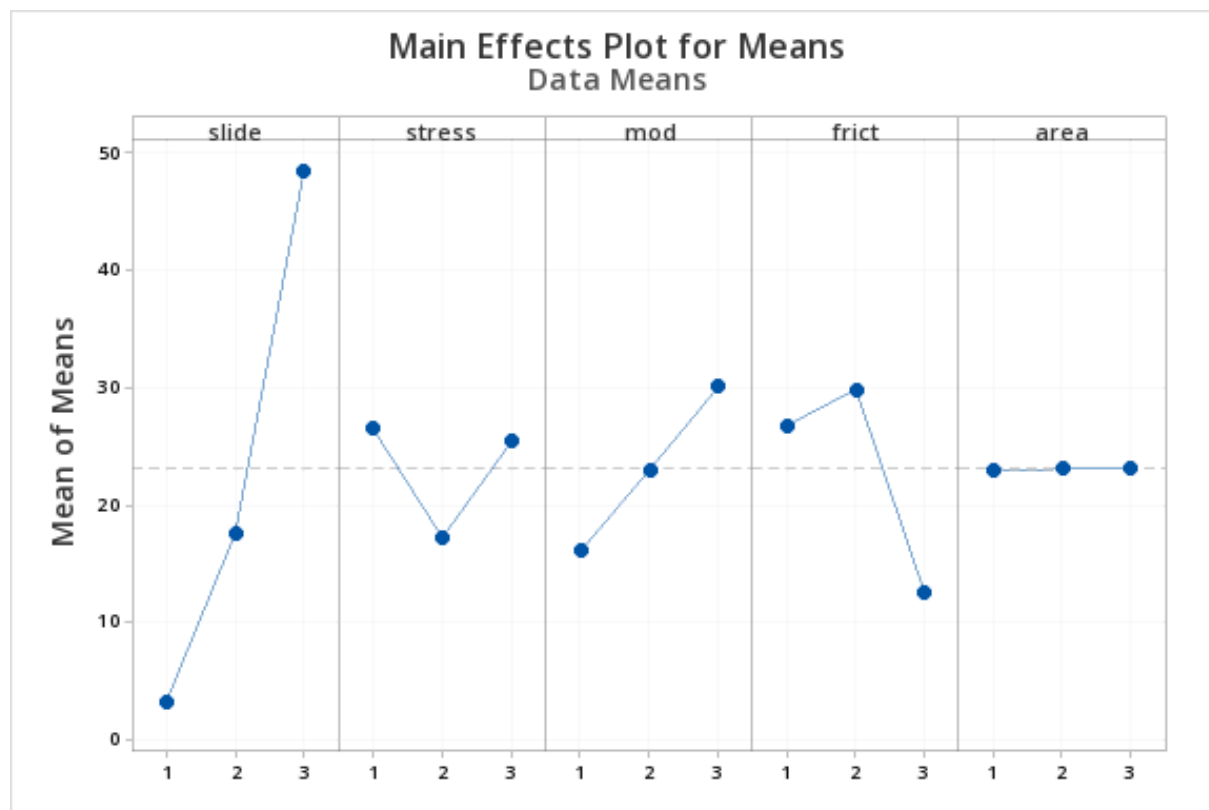
Response Table for Signal to Noise Ratios

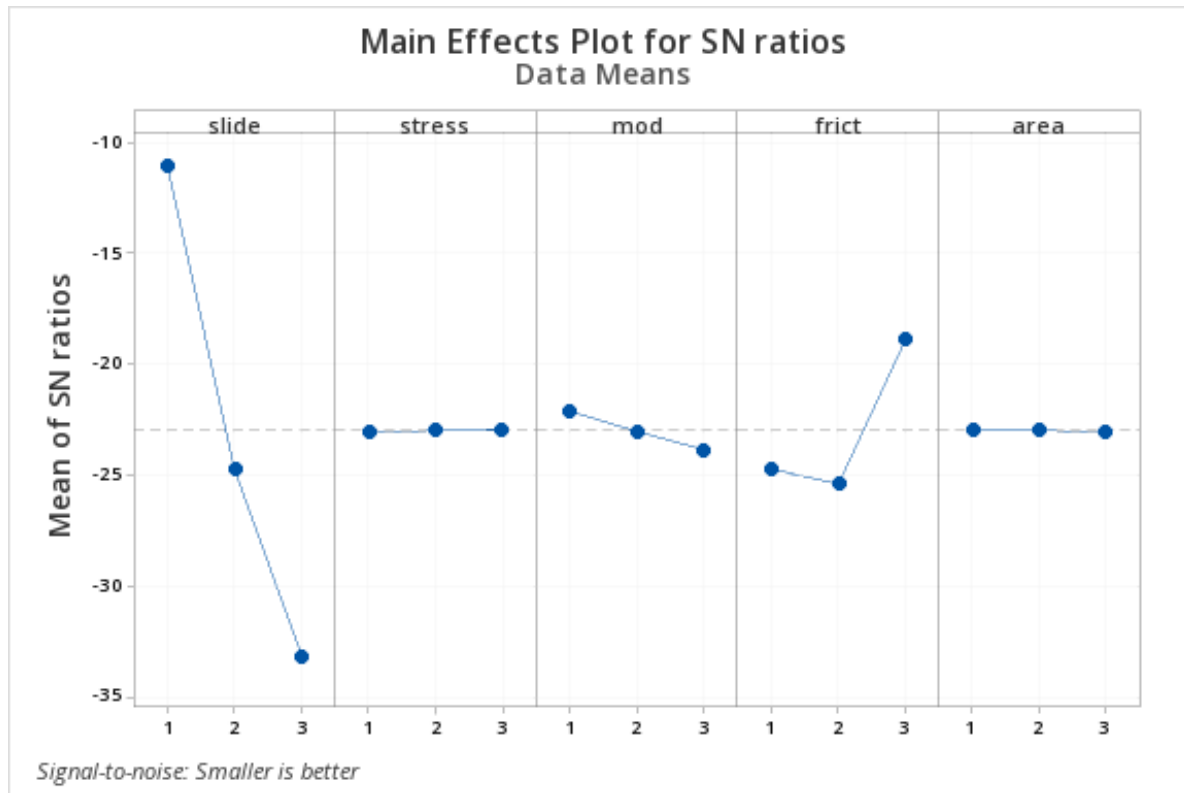
Smaller is better

| Level | slide | stress | mod | frict | area |
|--------------|--------------|---------------|------------|--------------|-------------|
| 1 | -11.02 | -23.02 | -22.08 | -24.69 | -22.94 |
| 2 | -24.74 | -22.97 | -23.00 | -25.38 | -22.97 |
| 3 | -33.15 | -22.91 | -23.82 | -18.84 | -22.99 |
| Delta | 22.13 | 0.10 | 1.74 | 6.54 | 0.05 |
| Rank | 1 | 4 | 3 | 2 | 5 |

Response Table for Means

| Level | slide | stress | mod | frict | area |
|-------|--------|--------|--------|--------|--------|
| 1 | 3.352 | 26.611 | 16.206 | 26.884 | 23.090 |
| 2 | 17.651 | 17.336 | 23.105 | 29.961 | 23.159 |
| 3 | 48.473 | 25.529 | 30.166 | 12.631 | 23.227 |
| Delta | 45.121 | 9.275 | 13.960 | 17.330 | 0.136 |
| Rank | 1 | 4 | 3 | 2 | 5 |





We can see from the charts above that slip angle had the biggest effect on tire wear. If we were to rank, it would be slip angle, coefficient of friction, modulus of elasticity, tension stress, and length of contact area, in that order. From our S/N ratio being low, it can be concluded that the noise play a very big role on the overall quality characteristic variable, tire wear. This experiment can further help us create a tire that allocates for these defects.

Reference:

- Saibel and Tsai, "Tire wear Model", Department of Mechanical Engineering
Carnegie-Mellon University, 1969
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- Rao, "Reliability Engineering", Pearson, 2015