

Diffraction

[7-1]

Essentially, there's no real distinction between interference and diffraction

- "interference" : normally when considering only a few waves (and phase shifts)
- "diffraction" : when considering many waves and/or amplitude effects

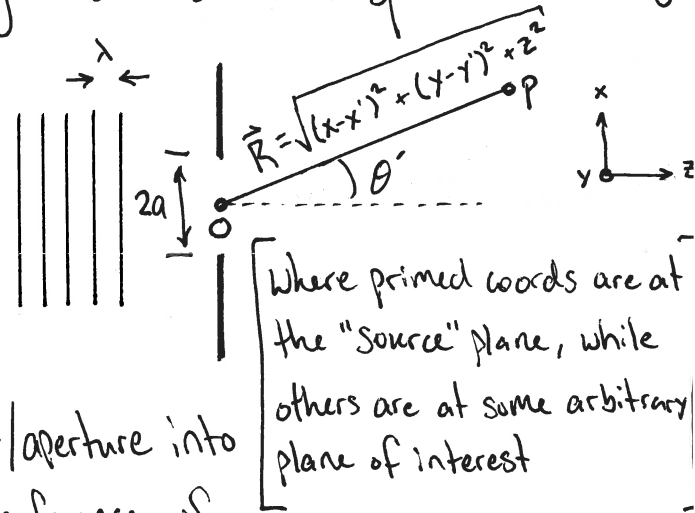
Ex: a) multiple-beam interference in Fabry-Pérot } Physically & mathematically
b) diffraction from a grating } essentially the same thing

Huygens-Fresnel Principle:

- Remember Huygens model of re-radiating "wavelets" making up wavefronts?
- We can model the propagation of light as a sum of spherical wavelets

$$E(r) = C \iint \vec{E}(x', y', z=0) \vec{U}(k, \vec{R}) dx' dy'$$

↑ incident light ↑ diffracted wavelet



Qualitative Diffraction:

- light bends around edges of physical object/aperture into region of geometric shadow due to interference of wavelets making up the wavefront
- if the "source" (object/aperture) is small compared to $\lambda \rightarrow$ plane waves spread out a lot
- if the source is large compared to $\lambda \rightarrow$ light spreads out (comparatively) little

- the full details of diffraction theory can get very complicated [7-2]
 - vector vs scalar fields (include polarization or not)
 - appropriate modeling of the spherical wavelets
 - near-field vs. far-field effects (Fraunhofer vs Fresnel) $R > \frac{a^2}{\lambda}$

Single Slit Diffraction

- take the scenario pictured above with the slit
 - reduce this to a 1D problem \rightarrow slit ∞ long in \hat{x} , ∞ short in \hat{z}
 - then by Huygens-Fresnel, each point w/in the aperture ($z=0$, along $2a$) can be considered a set of pt. emitters of spherical waves that add up
 - by now have: $E(x, y, z) = C \iint E(x', y', z=0) U(k, R) dx' dy'$
- $$(1D) \Rightarrow E(x, z) = C \int_{-a}^a E(x', z=0) U(k, R) dx'$$

where the outgoing wavelets are: $U(k, R) = \underbrace{\frac{E_0}{R}} e^{i k R} \underbrace{\left[\frac{1 + \cos(\theta')}{2} \right]}$

- We recognize the first factor from spherical emitters, but where does that second factor come from?
 - "Oblliquity" factor basically placed by hand (by Huygens & Fresnel anyway) to limit spread in \hat{x} and negate backwards propagation in \hat{z}
 - this general integral is very difficult to solve \rightarrow let's simplify!
- \rightarrow called Fresnel-Kirchoff Diffraction

Simplification 1: $\boxed{\theta' \text{ is small}}$ (Paraxial approx. \rightarrow Fresnel Diffraction) [7-3]

- now $\cos \theta' \approx 1$ and the obliquity factor disappears

$$\Rightarrow E(x, z) = C \int_{-a}^a E(x', z=0) \frac{e^{ikR}}{R} dx' \quad \left| \begin{array}{l} \theta' \approx 0 \\ R = \sqrt{(x-x')^2 + z^2} \end{array} \right.$$

Simplification 2: $\boxed{z^2 \gg (x-x')^2}$

- now the R in the factor $1/R$ can be expanded to the approximation

$$\Rightarrow R = \sqrt{z^2 + (x-x')^2} = z \sqrt{1 + \frac{(x-x')^2}{z^2}} \approx z \left(1 + \frac{(x-x')^2}{2z^2} \right) \approx z$$

\uparrow
 small factors

last step

- BUT this won't work in the exponent (too sensitive to phase) since differences of λ are important even if z is large

$$\begin{aligned} \Rightarrow E(x, z) &= C \int_{-a}^a E(x', z=0) \frac{1}{z} e^{ikz} e^{ik \left(\frac{(x-x')^2}{2z} \right)} dx' \\ &= C \underbrace{\frac{e^{ikz}}{z} e^{ik \frac{x^2}{2z}}}_{\text{pull out}} \int_{-a}^a E(x', z=0) e^{ik \frac{x'^2}{2z}} e^{-ik \frac{xx'}{z}} dx' \end{aligned}$$

- have pulled out the overall phase factors that don't depend on x' .

but what is this?

Δ phase is not uniform over span of "screen"

Δ phase increases with z

Δ phase increases quadratically with x

(important for multiple apertures, stay tuned...)

- what about the constant C ? $\Rightarrow C = -i/\lambda$

Δ spherical wave amplitudes are scaled by $1/\lambda$

Δ if $a \rightarrow \infty$, then must get back our plane wave, so phase must match.

not shown, but Huygens' wavelets are 90° out-of-phase with plane waves $\rightarrow -i$

Simplification 3: $\boxed{z \gg \frac{k}{2} a^2} \Rightarrow e^{ik \frac{x'^2}{2z}} \approx 1$ [7-4]

- in words, if the screen is far enough away from aperture, then the change in phase across the aperture isn't too large an effect

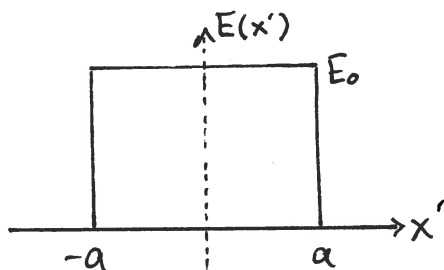
Fraunhofer
or
Far-Field
Limit

$$\Rightarrow E(x, z) = \frac{C}{z} e^{ikz} e^{ik \frac{x^2}{2z}} \int_{-a}^a E(x', z=0) e^{-ik \frac{xx'}{z}} dx'$$

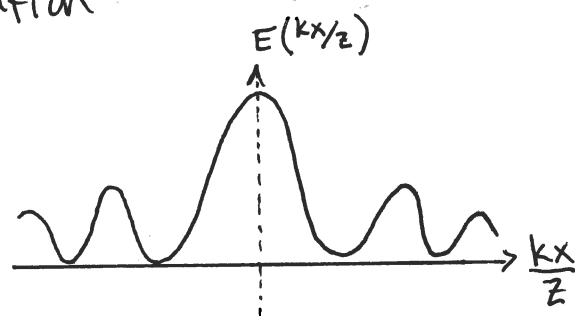
$$= \frac{C}{z} e^{i\phi(x, z)} \int_{-a}^a E(x', z=0) e^{-i(\frac{kx}{z})x'} dx'$$

- here's where the magic comes in: Looks like a Fourier Transform!
(but the transform variables look a bit different \rightarrow more on that later)

- for now, let's look at the solution



[at the slit]



[at the screen]

$$\Rightarrow E(x, z) = \frac{C}{z} e^{i\phi(x, z)} \cdot \frac{\sin(\frac{kax}{z})}{kax/z} = \frac{C}{z} e^{i\phi(x, z)} \frac{\sin \beta}{\beta}$$

where $\beta = \frac{kax}{z} = ka \sin \theta$

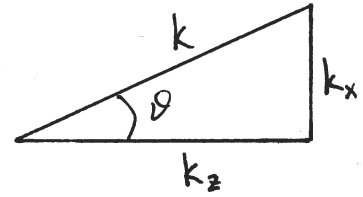
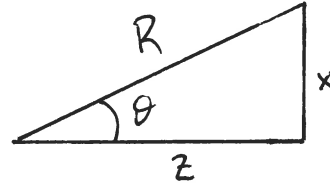
look! sinc!

and in general $E(r) = C \frac{(\text{phase})}{r} \text{sinc } \beta$

$I(r) \propto \frac{1}{r^2} \text{sinc}^2 \beta$

- is sometimes useful to recast this answer as a function of θ , or of x

- Can use $\beta = \frac{kx}{z} = k \sin \theta$ in the paraxial limit for coordinate interchangeability



$$\Rightarrow \theta = \frac{x}{z} = \frac{k_x}{k} \Rightarrow E_z(x) = \tilde{E}\left(k \frac{x}{z}\right) \quad \left[\begin{array}{c} \text{spatial} \\ \text{frequency} \end{array} \right]$$

(can replace k_x with $k \frac{x}{z}$)

- just like when dealing with temporal signals, a short square pulse is composed of a broader spectrum of frequencies.

Here, a narrow slit results in a transmitted field having a lot of different spatial frequencies

- Okay, let's extend this to 2D.

The Square Aperture:

- essentially, there's no difference from 1D, just more coords.

Fresnel - Kirchhoff:

$$E(x, y, z) = \frac{-i}{\lambda} \iint_{\text{aperture}} E(x', y', z=0) \frac{e^{ikr}}{r} \left[\frac{1 + \cos \theta}{2} \right] dx' dy'$$

Fresnel:

$$E(x, y, z) = \frac{-i}{\lambda z} e^{ikz} e^{i \frac{k}{2z}(x^2 + y^2)} \iint E(x', y', 0) e^{i \frac{k}{2z}(x'^2 + y'^2)} e^{-i \frac{k}{z}(xx' + yy')} dx' dy'$$

Fraunhofer:

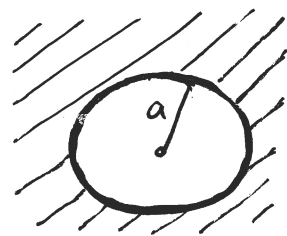
[7-6]

$$E(x, y, z) = \frac{-i}{\lambda z} e^{ikz} e^{i\frac{k}{2z}(x^2+y^2)} \iint E(x', y', 0) e^{-i\frac{k}{2}(xx' + yy')} dx' dy'$$

$$\begin{aligned} \text{if } E_0 = E(x', y', 0) &= \frac{-iE_0}{\lambda z} e^{ikz} \left[e^{i\frac{k}{2z}x^2} \int e^{-i\frac{k}{2}xx'} dx' \right] \left[e^{i\frac{k}{2z}y^2} \int e^{-i\frac{k}{2}yy'} dy' \right] \\ &= \frac{-iE_0}{\lambda z} e^{ikz} \left[e^{i\frac{k}{2z}x^2} \int_{-a_x}^{a_x} e^{-ik_x x'} dx' \right] \left[e^{i\frac{k}{2z}y^2} \int_{-a_y}^{a_y} e^{-ik_y y'} dy' \right] \\ &= \frac{-iE}{\lambda z} e^{ikz} e^{i\frac{k}{2z}(x^2+y^2)} \text{sinc}\left(\frac{ka_x x}{z}\right) \text{sinc}\left(\frac{ka_y y}{z}\right) \end{aligned}$$

and then $I \propto I_{\max} \text{sinc}^2(\beta_x) \text{sinc}^2(\beta_y)$

[just the product of
1D results in \hat{x}, \hat{y} dirs]



The Circular Aperture:

- end up going through exactly the same steps as above, except convert to cylindrical coords.

$$\begin{aligned} \Rightarrow E(\rho, z) &= \frac{-i}{\lambda z} e^{ikz} e^{i\frac{k\rho^2}{2z}} \int_0^{2\pi} \int_0^a E(\rho', 0) e^{i\frac{k\rho'^2}{2z}} e^{-i\frac{k\rho\rho'}{z} \cos(\phi - \phi')} \rho' d\rho' d\phi' \\ &= \frac{-i}{\lambda z} 2\pi e^{ikz} e^{i\frac{k\rho^2}{2z}} \int_0^a J_0\left(\frac{k\rho\rho'}{z}\right) \rho' d\rho' \end{aligned}$$

- where J_0 is a Bessel function (order 0) and integral has form of Hankel Transform

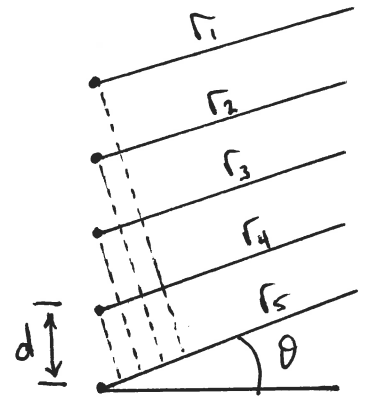
$\Rightarrow I(\rho, z) = I_0 \left(\frac{\pi a^2}{\lambda z}\right)^2 \left[2 \frac{J_1(k\rho/z)}{k\rho/z} \right]^2$ [Airy disk or Airy rings]

Array Theorem:

- Consider case of several coherent oscillators

$$E = E_0(r) \left[e^{i(kr_1 - \omega t)} + e^{i(kr_2 - \omega t)} + \dots + e^{i(kr_N - \omega t)} \right]$$

$$= E_0(r) e^{i\omega t} e^{ikr_1} \left[1 + e^{ik(r_2 - r_1)} + e^{ik(r_3 - r_1)} + \dots \right]$$

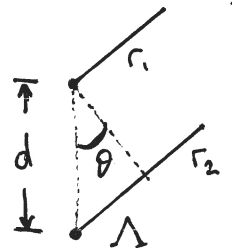


- this array of oscillators has many physically equivalent representations

[linear array of in-phase coherent oscillators]

- plane wave incident on N slits (transmission grating)

- plane wave incident on N mirrors (reflection grating)



- Any regularly-spaced dispersive element which introduces a fixed phase offset between oscillators

- the phase difference between individual waves is

$$\delta = k \cdot \Lambda = k_0 n d \sin \theta$$

$$\Rightarrow E = E_0(r) e^{-i\omega t} e^{ikr_1} \left[1 + e^{i\delta} + e^{2i\delta} + \dots + e^{i(N-1)\delta} \right]$$

$$= E_0(r) e^{-i\omega t} e^{ikr_1} \left(\frac{e^{i\delta N} - 1}{e^{i\delta} - 1} \right)$$

$$\text{where } \left(\frac{e^{i\delta N} - 1}{e^{i\delta} - 1} \right) = \frac{e^{i\delta N/2} (e^{i\delta N/2} - e^{-i\delta N/2})}{e^{i\delta/2} (e^{i\delta/2} - e^{-i\delta/2})} = e^{i\frac{(N-1)}{2}\delta} \left(\frac{\sin N\delta/2}{\sin \delta/2} \right)$$

$$\Rightarrow E = E_0(r) e^{-i\omega t} e^{i[kr_1 + \frac{(N-1)}{2}\delta]} \frac{\sin(N\delta/2)}{\sin(\delta/2)}$$

and can say the "average" distance to our point of interest is $[7-8]$

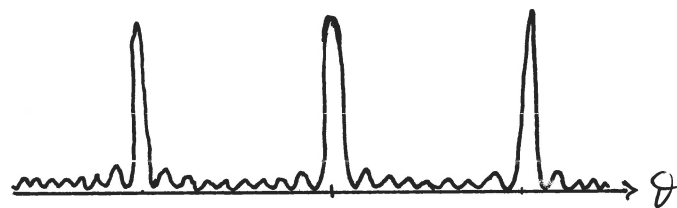
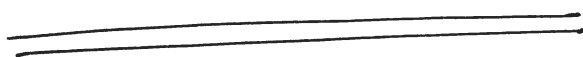
$$R = \frac{1}{2}(N-1)d \sin \theta$$

$$\Rightarrow E = E_0(r) e^{i(kR - \omega t)} \frac{\sin N\delta/2}{\sin \delta/2}$$

$$\Rightarrow I \propto EE^* \Rightarrow I = I_0 \frac{\sin^2(N\delta/2)}{\sin^2(\delta/2)}$$

then go back and explicitly write in $\delta = knd \sin \theta$

$$\Rightarrow I = I_0 \frac{\sin^2[N(kd/2) \sin \theta]}{\sin^2[kd/2 \sin \theta]} \quad \begin{array}{l} \leftarrow \text{Varies rapidly} \\ \leftarrow \text{Varies slowly} \end{array}$$



- Maxima in intensity occur

where $\delta = 2m\pi = kd \sin \theta \Rightarrow \boxed{d \sin \theta_m = m \lambda}$

the "grating" equation

- m is the order parameter
(integer \rightarrow 1st Order, 2nd Order, etc.)

- there are $N-1$ minima between each maxima

- represents a very important tool for spectroscopy since the diffraction angle can be made strongly dependent on λ

- need to be more realistic, though \rightarrow slits are not infinitesimally narrow

- define a re-scaled angle to account for center-to-center [7-9] spacing of slits with finite width, b .

$$\Rightarrow \alpha = \frac{kd}{2} \sin \theta \quad \Rightarrow \quad I(\alpha) = I_0 \left(\frac{\sin(N\alpha)}{\sin \alpha} \right)^2$$

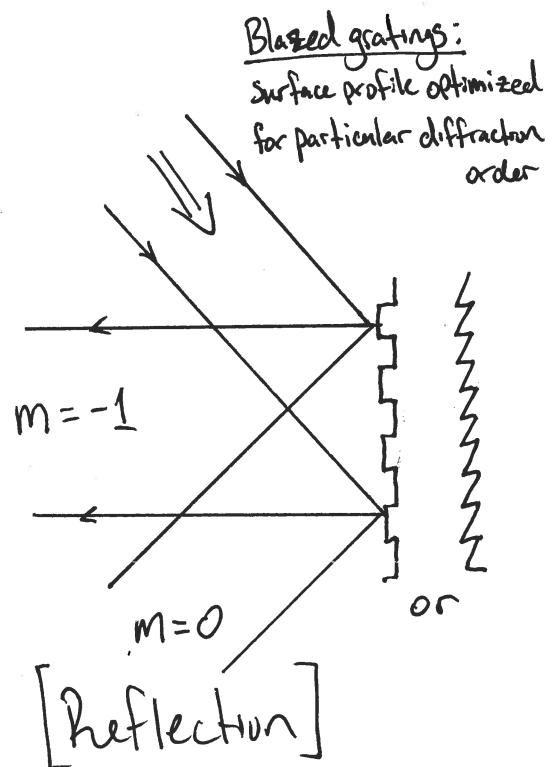
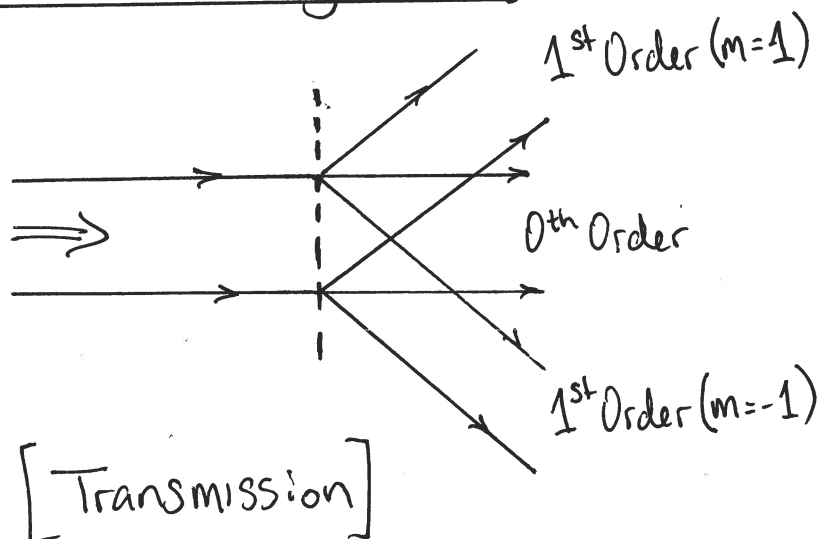
maxima at:
 $\alpha = m\pi$
 minima at:
 $\alpha = \pm \frac{\pi}{N}, \pm \frac{2\pi}{N} \dots$

- as we saw before for the single slit of finite width, b , the intensity distribution at the screen follows an envelope

$$\Rightarrow I(\alpha, \beta) = \frac{I_0}{N^2} \left(\frac{\sin \beta}{\beta} \right)^2 \left(\frac{\sin N\alpha}{\sin \alpha} \right)^2, \quad \beta = \frac{kb}{2} \sin \theta$$

$$= \frac{I_0}{N^2} \text{sinc}^2 \beta \left(\frac{\sin N\alpha}{\sin \alpha} \right)^2$$

Different Grating Types:



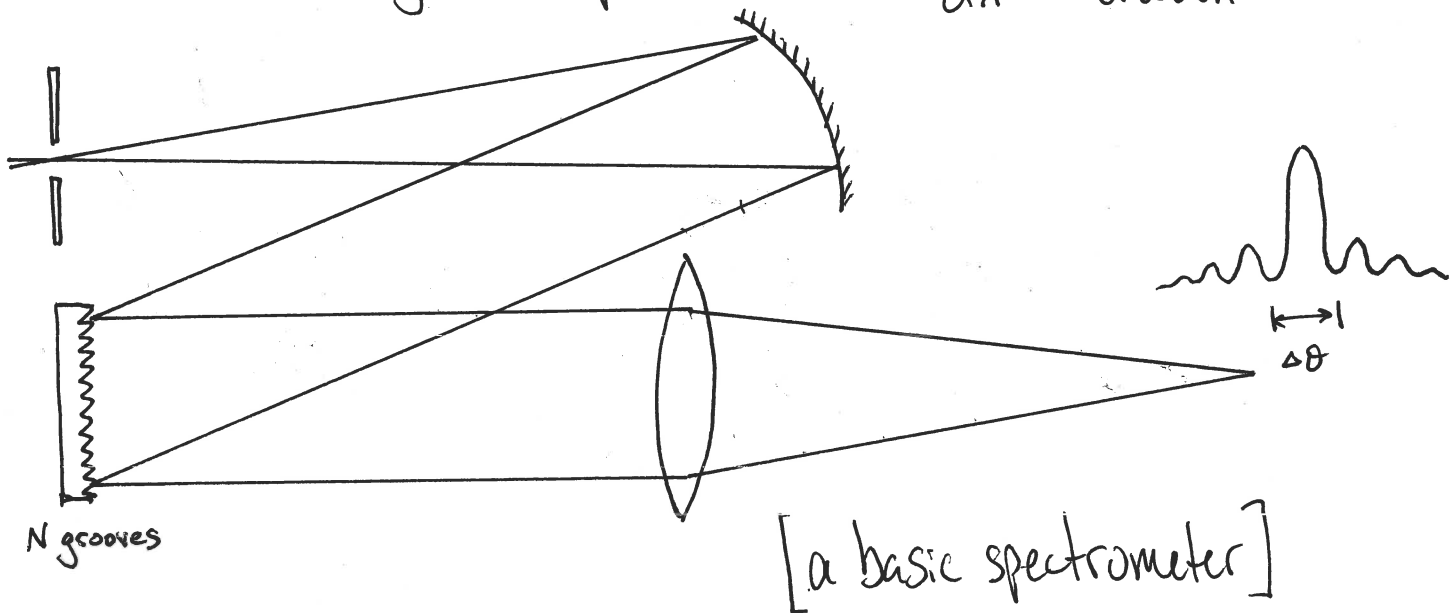
- can also make gratings acting only on amplitude or phase across wavefront

Grating Spectroscopy:

[7-10]

- saw above that θ depends on λ ($d \sin \theta = m\lambda$) for a dispersive grating

- can define an angular dispersion: $D = \frac{d\theta}{d\lambda} = \frac{m}{d \cos \theta_m}$



- for a given λ , the angular width of a diffracted beam will be

$$\Delta\theta = \frac{2\lambda}{Nd \cos \theta_m}$$

[where Nd is the grating width]

Babinet's Principle:

$E_1(x', y', z=0)$



[aperture]

$E_1(x, y, z)$



$E_2(x', y', z=0)$



[obstacle]

$E_2(x, y, z)$



- Consider these 2 different diffraction problems, with plane waves $E_0 e^{i(kz - \omega t)}$ incident from the left side
- What diffraction patterns do we observe at the screens?

- as a consequence of wavefunction linearity and the linearity of the Fourier transform operator, they are complimentary!

- after looking at the problem for a moment it becomes obvious
→ the sum of radiation patterns from each scenario must equal the radiation pattern of the unobstructed beam
- Caveat: these two fields are not necessarily equal in amplitude!
Except, wherever the original beam would not have reached, then the radiated fields are equal amplitude, just opposite phase.
- So, the fields after the apertures add up so that (neglecting time dep.),

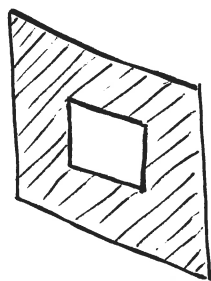
$$E_1(x', y', z=0) + E_2(x', y', z=0) = E_0$$

and the diffraction operation, which is just a Fourier transform, is also linear, so

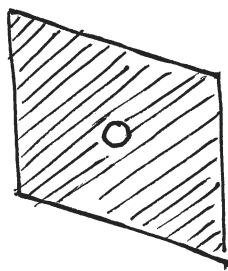
$$\mathcal{D}[E_1(x', y')] + \mathcal{D}[E_2(x', y')] = E_0$$

where, in general, have: $E_1(x, y, z) + E_2(x, y, z) = E_0$

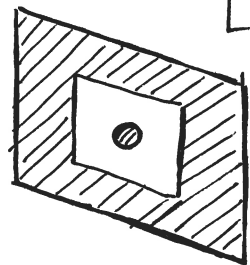
- Result: if you solve the diffraction problem for an aperture, you automatically earn the solution for its conjugate obstruction
- also, get to build-up more complicated apertures from simple ones!



-



=



[7-12]

Note: Babinet's Principle only applies to the electric fields, not the intensities. (Phase is lost when you take $E E^*$!)

~~Ex~~ Let's reconsider the diffraction pattern of a circular aperture
 → there's a pretty neat effect here!



• in 2D cartesian we'll have:

$$E(\mathbf{R}) = C \iint E(x', y', z=0) U(\mathbf{k}, \mathbf{R}) dx' dy' , \text{ with } R = \sqrt{(x-x')^2 + (y-y')^2 + z^2}$$

• but makes much more sense to convert to cylindrical symmetry

$$\Rightarrow x = \rho \cos \phi, y = \rho \sin \phi \quad \& \quad x' = \rho' \cos \phi', y' = \rho' \sin \phi'$$

$$E(\rho, z) = \frac{-i}{\lambda z} e^{ikz} e^{i \frac{k \rho^2}{2z}} \int_0^{2\pi} \int_0^{1/2} E(\rho', 0) e^{i \frac{k \rho'^2}{2z}} e^{-i \frac{k}{z} (\rho \rho' \cos \phi \cos \phi' + \rho \rho' \sin \phi \sin \phi')} \rho' d\rho' d\phi'$$

• trig: use $\rho \rho' (\cos \phi \cos \phi' + \sin \phi \sin \phi') = \rho \rho' \cos(\phi' - \phi)$

$$E(\rho, z) = \frac{-i}{\lambda z} e^{ikz} e^{i \frac{k \rho^2}{2z}} \int_0^{1/2} E(\rho', 0) e^{i \frac{k \rho'^2}{2z}} \left[\int_0^{2\pi} e^{-i \frac{k \rho \rho'}{z} \cos(\phi' - \phi)} d\phi' \right] \rho' d\rho'$$

where the bracketed portion happens to be a zeroth-order Bessel function of first kind

$$E(\rho, z) = \frac{-2\pi i}{\lambda z} e^{ikz} e^{i \frac{k \rho^2}{2z}} \int_0^{1/2} E(\rho', 0) e^{i \frac{k \rho'^2}{2z}} J_0\left(\frac{k \rho \rho'}{z}\right) \rho' d\rho'$$

- in the Fraunhofer limit (far-field), we take $e^{i\frac{k\rho'^2}{2z}} = 1$ [7-13]

$$E(\rho, z) = -\frac{2\pi i}{\lambda z} e^{ikz} e^{i\frac{k\rho^2}{2z}} \int_0^{\rho/2} E(\rho', 0) J_0\left(\frac{k\rho\rho'}{z}\right) \rho' d\rho'$$

- this kind of looks like a Fourier transform \rightarrow it's not! [Hankel transform of order 0]

$$F_\nu(k) = \int f(\rho) J_\nu(k\rho) \rho d\rho$$

Bessel functions are the sine/cosine of cylindrical geometry (beyond the scope of this course, but kind of neat.)

- what's important here is that the integral has an analytical solution

$$E(\rho, z) = -E_0 \left(\frac{\pi \ell^2}{4\lambda z}\right) e^{i\frac{k\rho^2}{2z}} \cdot \frac{2 J_1\left(\frac{k\rho\ell}{2z}\right)}{\left(k\rho\ell/2z\right)} \quad \left[\begin{array}{l} \text{Airy function} \\ \text{(cylindrical generalization} \\ \text{of the sinc function)} \end{array} \right]$$

- remember, this is the far-field limit solution. What if instead, we are close to the circular aperture? (Fresnel limit)

\rightarrow the general solution would need to be computed numerically,

but we can analytically solve for the on-axis field!

which is just solving the above for $\rho=0$

\rightarrow Also, where's the "neat effect"?

An Historical Aside

- 1818 - Ongoing debate between wave & corpuscular theory of light [7-14]
 - Corpuscular (particle) theory of light winning popularity polls
 - it's hard to discount Newton's double prism experiments
 - diffraction is still an outstanding problem, though
 - enter: The French Academy of Science
 - organized a contest to overcome this last obstacle
 - many minor contributions submitted... one major contribution by Fresnel on the wave nature of light (extending Huygens' work)
 - two people on judges' panel: Siméon Poisson & François Arago
 - Poisson (staunch believer in corpuscular theory), took Fresnel's work, applied it to the shadow cast by a circular disk, and showed that it predicted a bright spot generated in exact center of shadow!
 - attempted logical fallacy: reductio ad absurdum
 - Arago saw Poisson's argument, set up the experiment, observed the spot!
 - Fresnel wins the prize
 - few years later, corpuscular theory nearly totally abandoned
-

• okay, back to the on-axis solution

[7-15]

$$E(\rho=0, z) = \frac{-i}{\lambda} \int_0^{l/2} \int_0^{2\pi} E(\rho', 0) \frac{e^{ik\sqrt{\rho'^2 + z^2}}}{\sqrt{\rho'^2 + z^2}} \rho' d\rho' d\phi'$$

$$= -\frac{2\pi i E_0}{\lambda} \cdot \frac{e^{ik\sqrt{\rho'^2 + z^2}}}{ik} \Big|_0^{l/2}$$

$$= -E_0 \left(e^{ik\sqrt{(l/2)^2 + z^2}} - e^{ikz} \right)$$

$$[e^{-i\pi/2} = -i]$$

$$I(\rho=0, z) = 2|E_0|^2 \left[1 - \cos(k\sqrt{(l/2)^2 + z^2} - kz) \right]$$

★ see plot on slide

• So what does this have to do with Babinet's Principle?

→ We actually solved for an open aperture, but

remember: Aperture + Obstacle = Plane Wave

$$\Rightarrow E_0 e^{ikz} = E^{ap}(z) + E^{ob}(z)$$

$$\Rightarrow E^{ob}(z) = E_0 e^{ikz} - E^{ap}(z)$$

$$= E_0 e^{ikz} - (-E_0 (e^{ik\sqrt{(l/2)^2 + z^2}} - e^{ikz}))$$

$$= E_0 e^{ik\sqrt{(l/2)^2 + z^2}}$$

$$\Rightarrow \underline{\underline{I^{ob}(z) = E_z E_z^* = |E_0|^2}}$$

[the intensity at the center of the spot will be the same as if the obstacle wasn't even there]

Note: You would get the wrong answer if you had [7-11e]
 tried to apply Babinet's Principle to the intensities instead

$$\Rightarrow I^{ob}(z) \neq I_0 - I^{ap}(z)$$

• notice that this formula predicts constant intensity on-axis
 right up to the point behind the circular obstacle

→ not actually true! what's wrong? omitted obliquity factor

$$U(k, R) = \frac{1}{R} e^{ikR} \left[\frac{1 - \cos \theta}{2} \right]$$

• a more realistic calculation with \uparrow
 gives a more physical answer

$$\rightarrow I(p=0, z) = \frac{z^2}{z^2 + (\lambda/2)^2} I_0$$

