

## Radiation of Accelerating Charges:

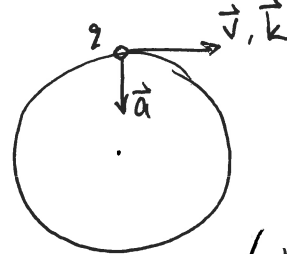
### I) The Point Charge

Stationary:  $\vec{E} = \frac{1}{4\pi\epsilon_0} \frac{q}{r^2} \hat{r}$

Accelerating:  $\vec{E} = \frac{1}{4\pi\epsilon_0} \frac{a}{c^2} \sin\theta \frac{q}{r} \hat{\theta}$

- radiation is always emitted perpendicular to  $\vec{a}$  ( $\vec{k} \perp \vec{a}$ )

Ex: Synchrotron radiation  
- the strong forward emission from circulating charges



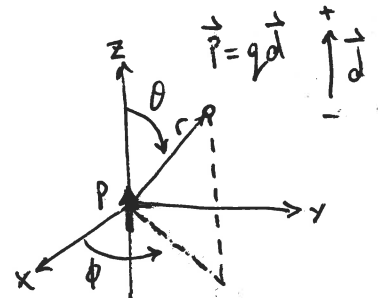
radiated power is  

$$P = \frac{1}{4\pi\epsilon_0} \cdot \frac{2}{3} \cdot \frac{q^2 a^2}{c^3} \gamma^4$$
 (where  $\gamma = 1/\sqrt{1-v^2/c^2}$ )

### II) The Electric Dipole

Stationary:  $\vec{E} = \frac{p}{4\pi\epsilon_0 r^3} (2\cos\theta \hat{r} + \sin\theta \hat{\theta})$

Oscillating:  $\vec{E} = \frac{p_0 k^2}{4\pi\epsilon_0} \sin\theta \frac{e^{i(kr-\omega t)}}{r} \hat{\theta}$



when  $p = p_0 e^{i(kr-\omega t)}$ , no radiation emitted in  $\vec{a}$  direction

Note: for both the point charge and dipole, acceleration/oscillation leads to radiated field with  $E \propto 1/r$  in direction  $k \perp \vec{a}, \vec{d}$

## Atomic Absorption & Emission of Radiation

- atoms are built of charges in a bound state
- lowest energy state = "ground state", but many higher energy "excited states"

Quantum Picture:  $\begin{matrix} |1\rangle \\ \uparrow \\ \omega = \frac{E_1 - E_0}{\hbar} \\ \downarrow \\ |0\rangle \end{matrix}$  | Lorentz Oscillator Model: (Works surprisingly well in many cases)

The Driven Oscillator:

$$\vec{F}_{\text{spring}} = -m\omega_0^2 \vec{x} \quad \& \quad \vec{F}_{\text{E-field}} = q\vec{E}(t) = q\vec{E}_0 e^{i\omega t}$$

then the (undamped) equation of motion is:

$$m \frac{d^2 \vec{x}}{dt^2} + m\omega_0^2 \vec{x} = q\vec{E}_0 e^{i\omega t} \quad [\text{remember: } \text{Re}(e^{i\omega t}) = \cos \omega t]$$

has the solution  $x(t) = x_0 e^{i\omega t}$

$$\Rightarrow x(t) = \frac{q/m}{(\omega_0^2 - \omega^2)} E_0 e^{i\omega t} = \frac{q/m}{(\omega_0^2 - \omega^2)} E(t)$$

so the oscillator just follows the field

now add a damping term:  $\vec{F}_{\text{damp}} = -\gamma \frac{d\vec{x}}{dt}$

$$\Rightarrow \frac{d^2 x}{dt^2} + \gamma \frac{dx}{dt} + \omega_0^2 x = \frac{qE_0}{m} e^{i\omega t}$$

$$\Rightarrow -\omega^2 x(t) + i\gamma x(t) + \omega_0^2 x(t) = \frac{q}{m} E_0 e^{i\omega t}$$

$$\Rightarrow x(t) = \frac{q/m}{(\omega_0^2 - \omega^2 + i\gamma\omega)} E(t)$$

in the context of bound charges of an atom, this relates to Polarization

$$P(t) = q x(t) = \frac{q^2/m}{(\omega_0^2 - \omega^2 + i\gamma\omega)} E_0 e^{i\omega t} \quad \left[ \text{same as Hecht eq 3.68, but with damping - see Hecht eq 3.72} \right]$$

and for  $N$  atoms

$$P(t) = q N x(t) = \frac{q^2 N/m}{(\omega_0^2 - \omega^2 + i\gamma\omega)} E_0 e^{i\omega t}$$

Note: this is complex valued, so get a phase shift from complex part

$$|z| = \sqrt{\tilde{z} \tilde{z}^*} = a^2 + b^2 \quad \& \quad \phi = \tan^{-1} \left( \frac{\tilde{z} - \tilde{z}^*}{\tilde{z} + \tilde{z}^*} \right) = \tan^{-1}(b/a)$$

When light interacts with matter it

[2-3]

- 1) causes charges in the matter to oscillate at the same frequency, but with a magnitude and phase that depends on  $\omega - \omega_0$
- 2) the oscillating charges re-radiate (scattering)
- 3) the incident and scattered waves both continue to propagate

## Light in Bulk Matter

What is the primary difference to our previous vacuum?

electric permittivity & magnetic permeability constants

$$\epsilon_0, \mu_0 \xrightarrow{\text{in matter}} \epsilon = \underset{\substack{| \\ \text{relative permittivity}}}{K_E} \epsilon_0, \quad \mu = \underset{\substack{| \\ \text{relative permeability}}}{K_M} \mu_0, \quad v = 1/\sqrt{\epsilon\mu}$$

index of refraction:  $n \equiv c/v = \sqrt{\frac{\epsilon\mu}{\epsilon_0\mu_0}}$  (this root is negative for only very special cases)

unless dealing with magnetic materials,  $\frac{\mu}{\mu_0} \sim 1$

$$\Rightarrow n \approx \sqrt{\epsilon/\epsilon_0} = \sqrt{K_E}$$

Now, given the formula for the polarization of a single dipole, let's connect to the macroscopic properties of a material (ie:  $\epsilon$  and  $n$ )

$$\vec{P}(t) = \frac{q^2 N/m}{(\omega_0^2 - \omega^2 + i\delta\omega)} \vec{E}(t)$$

- have  $N$  oscillators of charge  $q$  per unit volume
- we're pretending there's only 1 resonance freq and no interactions

Assume our bulk matter is a linear dielectric

[2-4]

$$\vec{P} = \epsilon_0 \chi_E \vec{E}$$

$\chi_E$ : electric susceptibility

$$= \epsilon_0 (K_E - 1) \vec{E}$$

$K_E$ : relative permittivity

$$= \epsilon_0 \left( \frac{\epsilon}{\epsilon_0} - 1 \right) \vec{E}$$

(or dielectric constant)

$$= (\epsilon - \epsilon_0) \vec{E}$$

$$\text{then } \epsilon = \epsilon_0 + \frac{\vec{P}}{\vec{E}} = \frac{q^2 N/m}{(\omega_0^2 - \omega^2 + i\delta\omega)} + \epsilon_0$$

[Caveat: changes to a sum for multiple resonances and modified if the oscillators interact] (see Hecht eqn 3.73)

now remembering the connection between  $\epsilon$  and the speed of the wave

$$n = \frac{c}{v} = \sqrt{\frac{\epsilon\mu}{\epsilon_0\mu_0}} = \sqrt{K_E K_M}, \text{ but } K_M \approx 1 \text{ for almost all transparent materials}$$

$$n^2 = K_E = \epsilon/\epsilon_0 = 1 + \frac{Nq^2}{\epsilon_0 m} \left( \frac{1}{\omega_0^2 - \omega^2 + i\delta\omega} \right)$$

It bears repeating: this is overly simple  $\rightarrow$  usually have multiple resonances

$$\Rightarrow n^2 = 1 + \frac{Nq^2}{\epsilon_0 m} \sum_n \frac{f_n}{\omega_n^2 - \omega^2 + i\delta\omega} \quad (\text{Hecht eqn 3.72})$$

Also, there may be interactions between oscillators in a dense medium, so that they're not independent (Hecht eqn 3.73)

Limiting cases are worth considering

A)  $\omega_0^2 - \omega^2 \gg \delta\omega$  [negligible absorption]

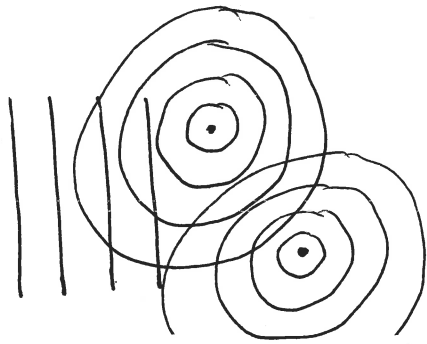
B)  $\epsilon/\epsilon_0 \ll 1$  [very small index, dilute gas]

C)  $\omega \approx \omega_0$  [near resonance]

# Microscopic - Macroscopic Connection

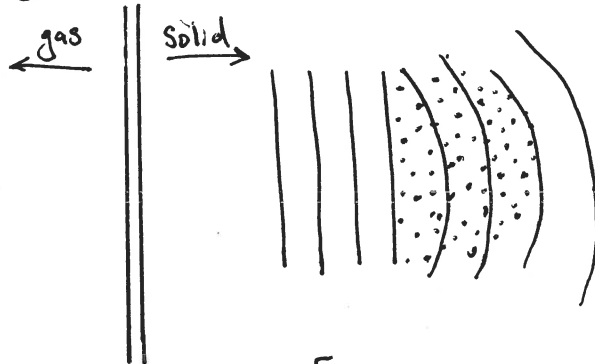
[2-5]

What effect does the  $N$  charged oscillators have on the EM wave when the density of  $N$  changes?



[dilute medium]

- essentially independent scattered waves
- lots of lateral scattering



[dense medium]

- constructive interference going forward
- destructive interference on sides (very little lateral scattering)

The scattered waves experience a phase lag  $\rightarrow$  interferes with incident wave  
~ this is why light travels slower when  $n > 1$

Velocity of light in a medium:  $v = c/n$

Velocity of light "between" atoms:  $v = c$

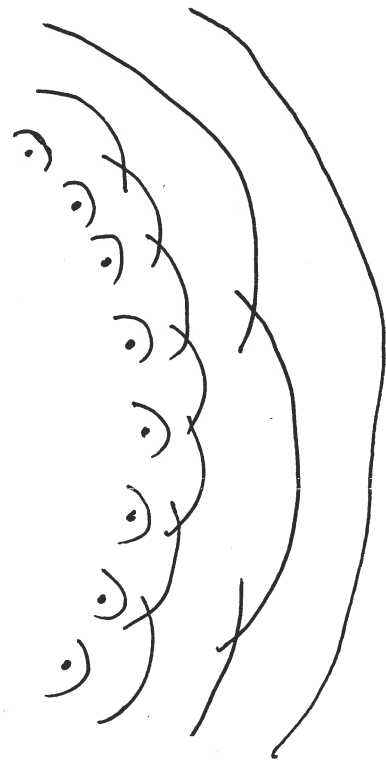
$n > 1 \rightarrow$  scattered phase lags (velocity slower than  $c$ )

$n < 1 \rightarrow$  scattered phase leads (velocity faster than  $c$ ?!)

Remember: these are phase velocities, which motivates other definitions of velocity

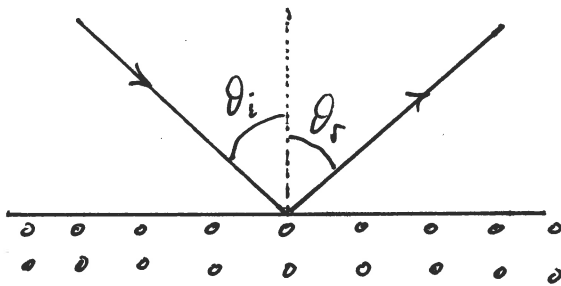
## Huygens' Principle

Propagation modeled as emission of a bunch of "wavelets" from each point on a surface of equal phase



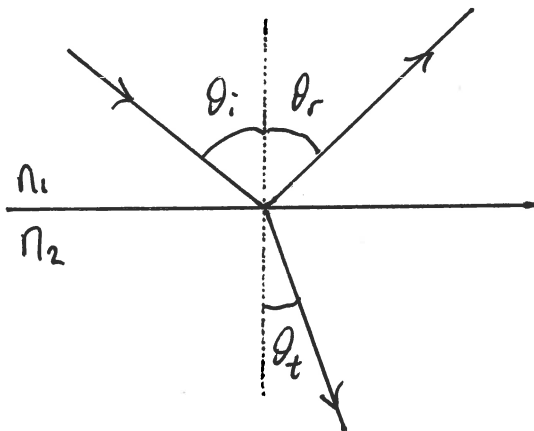
[2-6]

## Law of Reflection



$$\theta_i = \theta_r$$

## Law of Refraction



Snell's Law

$$n_1 \sin \theta_i = n_2 \sin \theta_t$$

# Reflection / Refraction at an Interface

What happens when a plane wave passes from one medium to another

First, consider case of normal incidence

In most general case, have complex vector wave equations

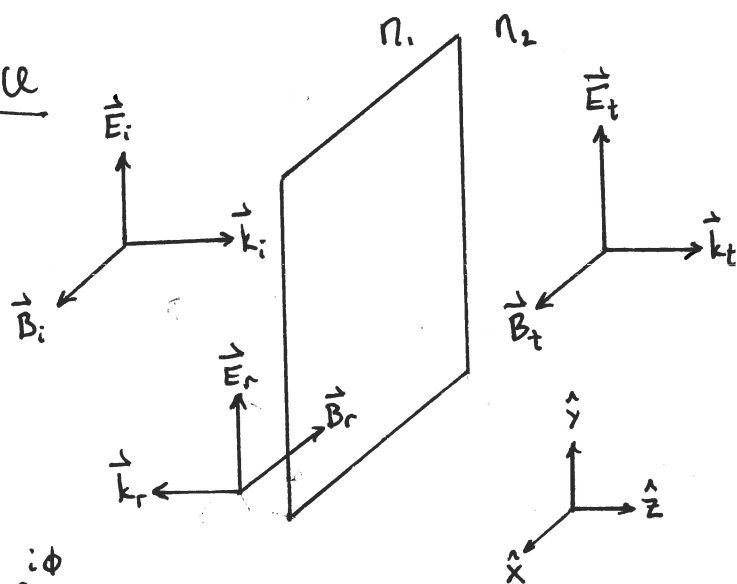
$$\tilde{\mathbf{E}}(\vec{r}, t) = \tilde{\mathbf{E}}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)} \hat{u}$$

$$\tilde{\mathbf{B}}(\vec{r}, t) = \tilde{\mathbf{B}}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)} (\hat{k} \times \hat{u})$$

where the phase has been absorbed:  $\tilde{A}_0 = A_0 e^{i\phi}$

and remembering that  $|E_0| = c|B_0|$  in vacuum  $\rightarrow |E_0| = v|B_0|$  in matter

$$\tilde{\mathbf{B}}(\vec{r}, t) = \frac{n}{c} \tilde{\mathbf{E}}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)} (\hat{k} \times \hat{u}) \quad [\text{Note: drop the } \sim \text{ notation to simplify}]$$



incident

reflected

transmitted

$$\vec{E}_i(z, t) = E_{0i} e^{i(k_i z - \omega t)} \hat{y}$$

$$\vec{B}_i(z, t) = B_{0i} e^{i(k_i z - \omega t)} \hat{x}$$

$$(B_{0i} = \frac{n_1}{c} E_{0i})$$

$$E_{0r} e^{i(-k_r z - \omega t)} \hat{y}$$

$$-\frac{n_1}{c} E_{0r} e^{i(-k_r z - \omega t)} \hat{x}$$

(note the minus signs)

$$E_{0t} e^{i(k_t z - \omega t)} \hat{y}$$

$$\frac{n_2}{c} E_{0t} e^{i(k_t z - \omega t)} \hat{x}$$

for continuity at the material interface, enforce EM boundary conditions

fields // to interface

fields  $\perp$  to interface

$$i) E_{||}^{(1)} = E_{||}^{(2)}$$

$$iii) \epsilon_1 E_{\perp}^{(1)} = \epsilon_2 E_{\perp}^{(2)}$$

(assuming bound charges, no surface charge density  $\sigma_f$ )

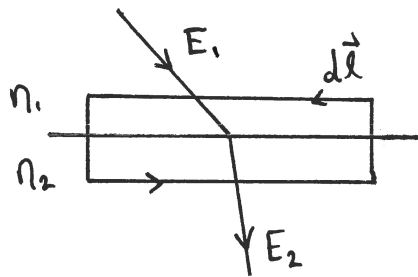
$$ii) \frac{1}{\mu_1} B_{||}^{(1)} = \frac{1}{\mu_2} B_{||}^{(2)}$$

$$iv) B_{\perp}^{(1)} = B_{\perp}^{(2)}$$

$$(B_{||}^{(1)} \approx B_{||}^{(2)})$$

Where do these boundary conditions come from? [2-8]

[We won't rigorously derive these, but it's easy to explain  
 Since we only care about the case for linear media with no free surface charge or current  
 (see Griffiths 7.3.6) Charge or current]



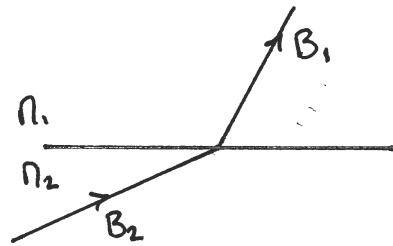
Faraday's Law (integral form)

$$\oint_C \vec{E} \cdot d\vec{l} = -\frac{d}{dt} \int_A \vec{B} \cdot d\vec{A}$$

take the area (flux) to zero

$$\oint_C \vec{E} \cdot d\vec{l} = 0$$

$$E_{||}^{(1)} - E_{||}^{(2)} = 0$$



Ampere's Law

$$\oint_C \vec{B} \cdot d\vec{l} = \mu_0 I_{enc} + \frac{d}{dt} \int_A \epsilon \vec{E} \cdot d\vec{A}$$

(same trick:  $A \rightarrow 0$ )

$$\oint_C \vec{B} \cdot d\vec{l} = 0$$

$$B_{||}^{(1)} - B_{||}^{(2)} = 0$$

So the fields  $\parallel$  to the interface must be equal to be continuous

How do the  $\perp$  fields change at dielectric interface?

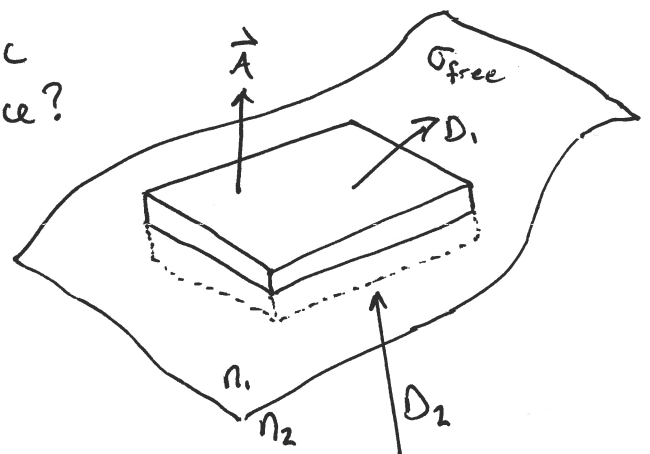
Gauss' Law

$$\oint_A \vec{D} \cdot d\vec{A} = Q_{free}^{enc} \quad (\vec{D}_i = \epsilon_i \vec{E}_i)$$

$$\vec{D}_1 \cdot \vec{A} - \vec{D}_2 \cdot \vec{A} = \cancel{Q_{free}^{enc}} A$$

$$\epsilon_1 E_{\perp}^{(1)} = \epsilon_2 E_{\perp}^{(2)}$$

(and similar for  $\oint_A \vec{B} \cdot d\vec{A} = 0 : B_{\perp}^{(1)} = B_{\perp}^{(2)}$ )





Now, given these BC's and the field definitions, have [2-9]

$$E_{||}^{(1)} = E_{||}^{(2)}$$

$$B_{||}^{(1)} = B_{||}^{(2)}$$

$$E_{oi} + E_{or} = E_{ot}$$

$$n_1 (E_{oi} - E_{or}) = n_2 E_{ot} \quad (E = \frac{c}{n} B)$$

and can solve for  $E_{ot}$  &  $E_{or}$  in terms of  $E_{oi}$

Amplitude Reflection Coefficient:  $r = E_{or}/E_{oi} = \left( \frac{n_1 - n_2}{n_1 + n_2} \right)$

Amplitude Transmission Coefficient:  $t = E_{ot}/E_{oi} = \left( \frac{2n_1}{n_1 + n_2} \right)$

What about powers involved? ( $I \propto E^2$ )

Reflectance:  $R = I_r/I_i = r^2 = \left( \frac{n_1 - n_2}{n_1 + n_2} \right)^2$

Transmittance:  $T = I_t/I_i = \frac{n_2}{n_1} t^2 = \frac{n_2}{n_1} \left( \frac{2n_1}{n_1 + n_2} \right)^2$

Conservation requires:

$$R + T = 1$$

↑ [needed since velocity changes between media  $\rightarrow$  changes energy delivered per unit time and area]

A few comments:

- the above amplitude and power ratios are for normal incidence; we'll expand these to the general Fresnel Eqn's for arb. angle incidence
- the sign of  $r$  changes from  $n_1 > n_2$  to  $n_1 < n_2$  ( $180^\circ$  phase change)
- $r$  gets larger when  $n_1/n_2$  is very different from 1
- $t$  gets smaller when " " " " " "

## A digression to discuss polarization

[2-10]

imagine a plane wave  $\vec{E} = \vec{E}_0 \cos(kz - \omega t)$

assume  $\vec{E}_0$  is constant in time: "linear" polarization

could even write  $\vec{E}_0$  as a superposition of two orthogonal components

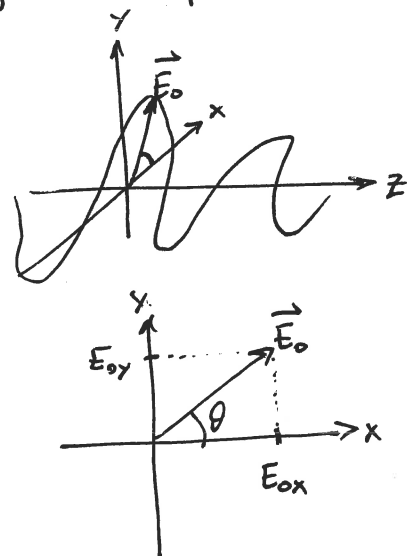
$$\vec{E}_0 = E_{0x} \hat{i} + E_{0y} \hat{j}$$

where it's easy to see that

$$E_0^2 = E_{0x}^2 + E_{0y}^2$$

$$E_{0x} = E_0 \cos \theta$$

$$E_{0y} = E_0 \sin \theta$$



and can simply write  $\vec{E}(z, t) = (E_{0x} \hat{i} + E_{0y} \hat{j}) \cos(kz - \omega t)$

Linear polarization means the E-field is oscillating along a line (or plane), and the angle is variable

Note: the B-field is still there, orthogonal to E all the time, we're just not concerned with it at the moment

★ In general, the phase of the x & y components don't have to be equal

Ex:  $\vec{E}(z, t) = \hat{i} E_{0x} \cos(kz - \omega t + \phi_x) + \hat{j} E_{0y} \cos(kz - \omega t + \phi_y)$

- magnitude and phase of E become time-dependent
- for now, it's sufficient to know we can decompose any polarization into a sum of orthogonal linear polarizations

# EM Waves at Interface for Arbitrary Angle

[2-11]

Remember, in general have wave functions of the form

$$\vec{E}_i(\vec{r}, t) = \vec{E}_{oi} e^{i(\vec{k}_i \cdot \vec{r} - \omega t)} \quad \& \quad \vec{B}_i(\vec{r}, t) = \frac{\eta_i}{c} (\vec{k}_i \times \vec{E}_i)$$

(and similarly for  $\vec{E}_r$  &  $\vec{E}_t$ , just with different polarization and  $\vec{k}$  - see above)

Before, the fields were always  $\parallel$  to the interface; now we have to consider components  $\perp$  to interface, too

How to define polarization with respect to the interface?

S-polarized/Transvers Electric:  $\vec{E} \perp$  plane of incidence

P-polarized/Transverse Magnetic:  $\vec{E} \parallel$  plane of incidence

Each polarization state (S and P) have separate calculations for reflection & transmission coefficients

Can add the polarization components back up at the end to get general result for total transmitted and reflected waves

Same prescription as for normal incidence case, just more to keep track of

1) develop expressions for i, r, t fields of form:  $\vec{E}(r, t) = \vec{E}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}$

2) apply EM boundary conditions to get expressions of the form:

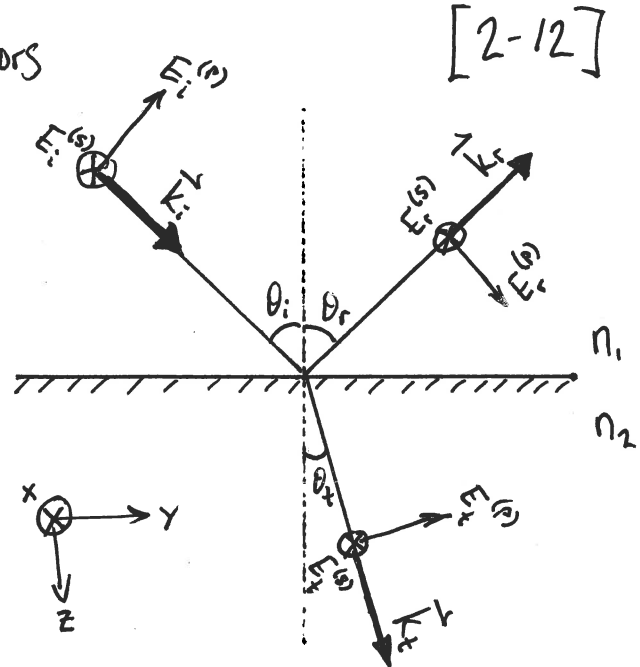
$$\left( \right) e^{i(\vec{k}_i \cdot \vec{r} - \omega t)} + \left( \right) e^{i(\vec{k}_r \cdot \vec{r} - \omega t)} = \left( \right) e^{i(\vec{k}_t \cdot \vec{r} - \omega t)}$$

First, let's look at constraints on propagation vectors

incident:  $\vec{k}_i \cdot \vec{r} = k_i(y \sin \theta_i + z \cos \theta_i)$

reflected:  $\vec{k}_r \cdot \vec{r} = k_r(y \sin \theta_r - z \cos \theta_r)$

transmitted:  $\vec{k}_t \cdot \vec{r} = k_t(y \sin \theta_t + z \cos \theta_t)$



All of the BC's, defined at  $z=0$ , have the form:

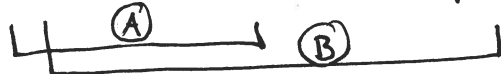
$$\left( \right) e^{i(k_i y \sin \theta_i - \omega t)} + \left( \right) e^{i(k_r y \sin \theta_r - \omega t)} = \left( \right) e^{i(k_t y \sin \theta_t - \omega t)}$$

To be satisfied at all possible values of  $y$  &  $t$ , must have

I)  $\omega_i = \omega_r = \omega_t = \omega$

II)  $k_i \sin \theta_i = k_r \sin \theta_r = k_t \sin \theta_t$  (remember:  $k = \frac{\omega}{v} = \frac{n\omega}{c}$ )

$$\Rightarrow n_i \sin \theta_i = n_r \sin \theta_r = n_t \sin \theta_t$$



Ⓐ Since  $n_i = n_r$ , then  $\theta_i = \theta_r \rightarrow$  Law of Reflection

Ⓑ  $n_i \sin \theta_i = n_t \sin \theta_t \rightarrow$  Snell's Law

So with the exponential parts of the BC's being equal, we can solve for the field amplitudes

Break the fields down into vector components

$\vec{E} = \vec{E}^{(s)} + \vec{E}^{(p)}$  (orthogonal linear polarization states)

$$\vec{E}_i = E_i^{(p)} (\hat{y} \cos \theta_i - \hat{z} \sin \theta_i) + \hat{x} E_i^{(s)}$$

[2-13]

$$\vec{E}_r = E_r^{(p)} (\hat{y} \cos \theta_r + \hat{z} \sin \theta_r) + \hat{x} E_r^{(s)}$$

$$\vec{E}_t = E_t^{(p)} (\hat{y} \cos \theta_t + \hat{z} \sin \theta_t) + \hat{x} E_t^{(s)}$$

$$\vec{B} = \vec{B}^{(s)} + \vec{B}^{(p)}$$

$$\vec{B}_i = \frac{n_i}{c} \left[ -\hat{x} E_i^{(p)} + E_i^{(s)} (-\hat{z} \sin \theta_i + \hat{y} \cos \theta_i) \right]$$

$$\vec{B}_r = \frac{n_r}{c} \left[ \hat{x} E_r^{(p)} + E_r^{(s)} (-\hat{z} \sin \theta_r - \hat{y} \cos \theta_r) \right]$$

$$\vec{B}_t = \frac{n_t}{c} \left[ -\hat{x} E_t^{(p)} + E_t^{(s)} (-\hat{z} \sin \theta_t + \hat{y} \cos \theta_t) \right]$$

Now we can solve the transmission/reflection problem separately for the two orthogonal linear polarization states (s and p, or  $\perp$  and  $\parallel$ )

Simplify the problem: S-polarized component only

notations may be used interchangeably along with TE and TM

$$\vec{E}_i = E_i^{(s)} \hat{x}$$

$$\vec{B}_i = \frac{n_i}{c} E_i^{(s)} (-\hat{z} \sin \theta_i + \hat{y} \cos \theta_i)$$

$$\vec{E}_r = E_r^{(s)} \hat{x}$$

$$\vec{B}_r = \frac{n_r}{c} E_r^{(s)} (-\hat{z} \sin \theta_r - \hat{y} \cos \theta_r)$$

$$\vec{E}_t = E_t^{(s)} \hat{x}$$

$$\vec{B}_t = \frac{n_t}{c} E_t^{(s)} (-\hat{z} \sin \theta_t + \hat{y} \cos \theta_t)$$

Apply boundary conditions:

$$i) E_{\parallel}^{(1)} = E_{\parallel}^{(2)} \implies \boxed{\vec{E}_i^{(s)} + \vec{E}_r^{(s)} = \vec{E}_t^{(s)}} \quad (\text{just } \hat{x}\text{-components... easy!})$$

$$ii) B_{\parallel}^{(1)} = B_{\parallel}^{(2)} \implies \vec{B}_i^{(s)} + \vec{B}_r^{(s)} = \vec{B}_t^{(s)} \quad (\text{only } \hat{y}\text{-components } \parallel \text{ to surface, } \hat{z} \text{ gives redundant set of constraints})$$

$$\implies \frac{n_i}{c} E_i^{(s)} \cos \theta_i - \frac{n_r}{c} E_r^{(s)} \cos \theta_r = \frac{n_t}{c} E_t^{(s)} \cos \theta_t$$

$$\implies n_i \cos \theta_i (E_i^{(s)} - E_r^{(s)}) = n_t E_t^{(s)} \cos \theta_t \implies \boxed{E_i^{(s)} - E_r^{(s)} = \frac{n_t \cos \theta_t}{n_i \cos \theta_i} E_t^{(s)}} \quad \left( \begin{array}{l} \theta_i = \theta_r \\ n_i = n_r \end{array} \right)$$

So have 2 equations and 3 unknowns

[2-14]

Can eliminate 1 of the 3 fields and calculate the ratio for the remaining two (same as we did for normal coincidence)

$$r_s = E_r^{(s)} / E_i^{(s)} \quad \& \quad t_s = E_t^{(s)} / E_i^{(s)}$$

Usually have to do some work to express these relations in a form that's convenient for a given problem

Simple Substitution gives  $r_s = \frac{n_i \cos \theta_i - n_t \cos \theta_t}{n_i \cos \theta_i + n_t \cos \theta_t}$  ( $n_i, n_t, \theta_i, \theta_t$  are not independent  $\rightarrow$  Snell's Law)

1) Want to eliminate  $n_i$  &  $n_t$ ?

$$\Rightarrow r_s = - \frac{\sin(\theta_i - \theta_t)}{\sin(\theta_i + \theta_t)}$$

(by using Snell's law and product-to-sum trig identities)

2) eliminate  $\theta_t$  instead?

rewrite Snell's law:  $\theta_t = \sin^{-1}\left(\frac{n_i}{n_t} \sin \theta_i\right)$

then  $\cos \theta_t = \sqrt{1 - \left(\frac{n_i}{n_t} \sin \theta_i\right)^2}$

$$\Rightarrow r_s = \frac{\frac{n_i}{n_t} \cos \theta_i - \sqrt{1 - \left(\frac{n_i}{n_t} \sin \theta_i\right)^2}}{\frac{n_i}{n_t} \cos \theta_i + \sqrt{1 - \left(\frac{n_i}{n_t} \sin \theta_i\right)^2}}$$

Similar (simple) Substitution gives amplitude transmission coefficient

$$t_s = \frac{2 n_i \cos \theta_i}{n_i \cos \theta_i + n_t \cos \theta_t}$$

The same algorithm can be applied to get  $r_p$  &  $t_p$  [2-15]

- consider only P-polarized components of  $i$ ,  $r$ , and  $t$  EM fields
- apply boundary conditions: iii)  $\epsilon_1 E_{\perp}^{(1)} = \epsilon_2 E_{\perp}^{(2)}$ , iv)  $B_{\perp}^{(1)} = B_{\perp}^{(2)}$
- obtain 2 equations of 3 unknowns (field amplitudes)
- eliminate 1 of these 3 fields and calculate ratio of remaining two
- apply Snell's Law & Law of Reflection throughout, as needed

$$r_p = \frac{n_t \cos \theta_i - n_i \cos \theta_t}{n_i \cos \theta_t + n_t \cos \theta_i}$$

$$t_p = \frac{2 n_i \cos \theta_i}{n_i \cos \theta_t + n_t \cos \theta_i}$$

## Reflectance/Transmittance for Arbitrary Angle of Incidence

We still have  $R = |r|^2$ , but there are two effects to account for in the transmitted beam

- 1) change in velocity of propagation
- 2) change in cross-sectional area

$$R = \frac{I_r A \cos \theta_r}{I_i A \cos \theta_i} = \frac{I_r}{I_i} = |r|^2$$

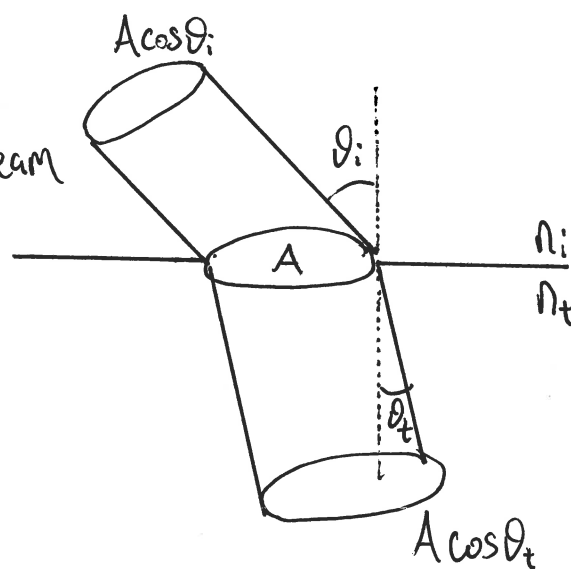
(can be  $r_{||}$  or  $r_{\perp}$ )

$$T = \frac{I_t A \cos \theta_t}{I_i A \cos \theta_i} = \frac{I_t \cos \theta_t}{I_i \cos \theta_i} = \frac{n_t \cos \theta_t}{n_i \cos \theta_i} \left( \frac{E_{ot}}{E_{oi}} \right)^2 = \frac{n_t \cos \theta_t}{n_i \cos \theta_i} t^2$$

( $t_{||}$  or  $t_{\perp}$ )

$$R + T = 1, \quad R_{||} + T_{||} = 1, \quad R_{\perp} + T_{\perp} = 1, \quad R = \frac{1}{2} (R_{||} + R_{\perp})$$

[P  $\leftrightarrow$  ||]                      [S  $\leftrightarrow$   $\perp$ ]



[See plots of  $r, t, R, T$  in Unit 2 Class slides]

[2-16]

## Phase Shift at the Interface

the phase of a wave can change upon interacting with an interface

$$\Delta\phi_{ti} = \phi_t - \phi_i \quad \Delta\phi_{ri} = \phi_r - \phi_i$$

these phase differences aren't necessarily zero

## Normal Incidence

$$\Delta\phi_{ti} = 0$$

$$t = \frac{2n_i}{n_i + n_t} \quad (\text{always positive})$$

$$\Delta\phi_{ri} = \begin{cases} 0 & \text{if } n_i > n_t \\ \pi & \text{if } n_i < n_t \end{cases}$$

$$r = \frac{n_t - n_i}{n_t + n_i} \quad (\text{can change sign})$$

## Arbitrary Incidence

Two new issues appear:  $\theta_i = \theta_{\text{Brewster}}$   $\theta_i > \theta_{\text{crit}}$

1) for s-polarized ( $\perp$ ) light, phase flips  $180^\circ$  when

$\theta_i$  goes through  $\theta_{\text{Brewster}}$  (projection of dipole oscillation changes)

2) when  $\theta_i > \theta_{\text{crit}}$ , the phases of reflected and "transmitted" (actually evanescent) waves will vary with angle ( $\theta_i$ )

$$\text{Generally: } [0 < \Delta\phi_{ri} < \pi] \quad \& \quad [0 < \Delta\phi_{ti} < \pi/2]$$



# Total Internal Reflection (TIR)

[2-17]

Now, for the case where  $n_i > n_t$ , can see in plot of reflection amplitude coefficients that, as  $\theta_i$  increases, there is a  $\theta_{crit}$  beyond which  $r_{||} = r_{\perp} = 1$ .

What is this angle,  $\theta_{crit}$ ? (Ans: the  $\theta_i$  which causes  $\theta_t = 90^\circ$ )

$$\text{Snell's Law: } n_i \sin \theta_i = n_t \sin \theta_t$$

$$\Rightarrow \sin \theta_i = \frac{n_t}{n_i} \sin \theta_t = \frac{n_t}{n_i} \sin \frac{\pi}{2}$$

$$\Rightarrow \theta_{crit} = \theta_i|_{\theta_t = \pi/2} = \sin^{-1}(n_t/n_i)$$

So, for  $\theta_i \geq \theta_{crit}$ , get perfect reflection ( $I_r = I_i$  and  $I_t = 0$ )

## Evanescent Waves

What does it mean to have no transmitted wave at interface?

BC's still need to be met! ( $E_{||}^{(1)} = E_{||}^{(2)}$  &  $\epsilon_1 E^{(1)} = \epsilon_2 E^{(2)}$ )

Note: The full treatment here is a bit involved, so we'll just take a peak!

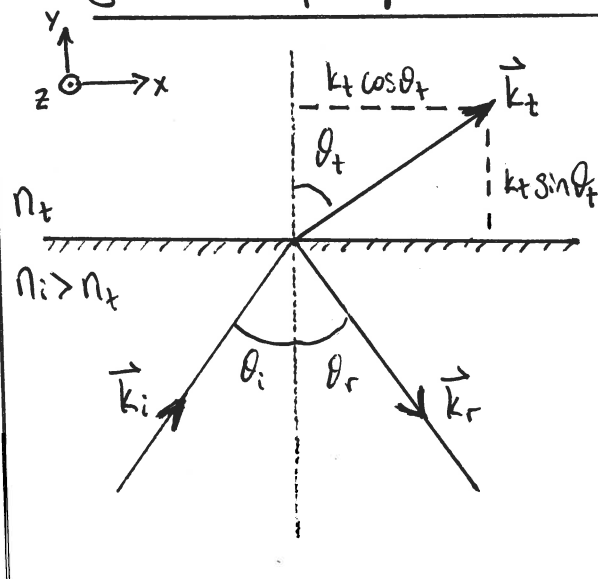
Assume a wavefunction for the transmitted wave

$$\vec{E}_t = \vec{E}_{0t} e^{i(\vec{k}_t \cdot \vec{r} - \omega t)}$$

$$\text{where } \vec{k}_t \cdot \vec{r} = k_{tx}x + k_{ty}y$$

$$\text{and } k_{tx} = k_t \sin \theta_t$$

$$k_{ty} = k_t \cos \theta_t$$



use Snell's law to rewrite in terms of  $\theta_i$  ( $n_i \sin \theta_i = n_t \sin \theta_t$ ) [2-18]

$$k_{tx} = k_t \sin \theta_t = k_t \frac{n_i}{n_t} \sin \theta_i$$

$$k_{ty} = k_t \cos \theta_t = \pm k_t \sqrt{1 - \sin^2 \theta_t} = \pm k_t \sqrt{1 - \left(\frac{n_i}{n_t}\right)^2 \sin^2 \theta_i}$$

but at  $\theta_{crit}$  have  $\sin \theta_{crit} = n_t/n_i$ , so when  $\theta_i > \theta_{crit}$ , then  $\sin \theta_i > n_t/n_i$

$$\Rightarrow k_{ty} = \pm i k_t \sqrt{\left(\frac{n_i}{n_t}\right)^2 \sin^2 \theta_i - 1} \equiv \pm i \beta \quad (\beta: \text{"attenuation coefficient"})$$

Now  $\vec{E}_t = \vec{E}_{ot} e^{\mp \beta y} e^{i(k_{tx} \frac{n_i}{n_t} \sin \theta_i - \omega t)}$  (Note:  $+\beta$  solution is nonphysical)

And have a surface (evanescent) wave traveling on the interface (x-direction),  
BUT decays exponentially in the y-direction across the interface

So, how far does the evanescent field penetrate into  $n_t$ ?

Can use  $\beta$  as a metric since  $k = 2\pi/\lambda$

$$\left[ \begin{array}{l} \text{Note: Remember for free-space } v=c \text{ and } c=v\lambda, \\ \text{while for dielectrics } v=c/n, \text{ so } \lambda = c/nv = \lambda_0/n \quad (\lambda_0: \text{vacuum wavelength}) \end{array} \right]$$

$$\Rightarrow \beta = \frac{2\pi n_t}{\lambda_0} \sqrt{\left(\frac{n_i}{n_t}\right)^2 \sin^2 \theta_i - 1}$$

Define a penetration depth to be where field drops off by  $1/e$  ( $\sim 65\%$ )

$$\delta = 1/\beta$$

# Optical Properties of Metals

[2-19]

What's the key difference between a conductor and an insulator?

Mobile charges! ( $\vec{J}$ ) [Note: these are in addition to the bound charges]

Previously only considered bound charges in a polarizable medium, but now with free charges we can drive actual currents in the material

So, what changes?  $\rightarrow$  Maxwell's Eqn's!

$$i) \vec{\nabla} \cdot \vec{E} = \frac{1}{\epsilon} \rho_{\text{free}} \quad iii) \vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$ii) \vec{\nabla} \cdot \vec{B} = 0 \quad iv) \vec{\nabla} \times \vec{B} = \mu_0 \epsilon \frac{\partial \vec{E}}{\partial t} + \mu_0 \vec{J}_{\text{free}} \quad (\vec{J} = \sigma \vec{E})$$

Have to now consider  $\rho$  (free charge density) and  $\vec{J}$  (free current density)

First, use the continuity eqn. to make a sanity check

$$\frac{\partial \rho}{\partial t} = -\vec{\nabla} \cdot \vec{J} = -\frac{\sigma}{\epsilon} \rho \Rightarrow \text{soln of form } \rho(t) = \rho(0) e^{-(\sigma t / \epsilon)}$$

and see that initial density,  $\rho(0)$ , dissipates within time  $\tau = \epsilon / \sigma$

So we'll limit ourselves to very good conductors:  $\sigma \rightarrow \infty$  &  $\tau \rightarrow 0$

then  $i) \vec{\nabla} \cdot \vec{E} = 0$ , and we only take care for terms with  $\vec{J}$  (Ampere's law)

Just as before, to get wave eqn's for  $\vec{E}$  &  $\vec{B}$ :  $\nabla \times (\nabla \times \vec{E})$  &  $\nabla \times (\nabla \times \vec{B})$

$$\nabla^2 \vec{E} = \mu_0 \epsilon \frac{\partial^2 \vec{E}}{\partial t^2} + \mu_0 \sigma \frac{\partial \vec{E}}{\partial t} \quad \& \quad \nabla^2 \vec{B} = \mu_0 \epsilon \frac{\partial^2 \vec{B}}{\partial t^2} + \mu_0 \sigma \frac{\partial \vec{B}}{\partial t}$$

$$\text{where } \vec{E}(z, t) = \tilde{E}_0 e^{i(\tilde{k}z - \omega t)} \quad \& \quad \vec{B}(z, t) = \tilde{B}_0 e^{i(\tilde{k}z - \omega t)}$$

Why write the wavefunctions in a fully complex form?

[2-20]

Let's check by plugging the wavefunctions into the wave equation

$$\Rightarrow -k^2 \tilde{\vec{E}}(z,t) = -\mu_0 \epsilon \omega^2 \tilde{\vec{E}}(z,t) - i\mu_0 \sigma \omega \tilde{\vec{E}}(z,t)$$

$$\Rightarrow k = \pm \sqrt{\mu_0 \epsilon \omega^2 + i\mu_0 \sigma \omega} = \pm \omega \sqrt{\mu_0 \epsilon} \sqrt{1 + i\sigma/\epsilon\omega}$$

So see that  $k$  is complex here and can separate into real/imag components

$$\tilde{k} = k + iK, \quad |\tilde{k}|^2 = k^2 + K^2$$

Where the expressions for  $k$  and  $K$  get a bit messy

$$\text{Re}(\tilde{k}) = k = \omega \sqrt{\frac{\mu_0 \epsilon}{2}} \left[ \sqrt{\frac{\sigma^2}{\epsilon \omega} + 1} + 1 \right]^{1/2}$$

$$\text{Im}(\tilde{k}) = K = \omega \sqrt{\frac{\mu_0 \epsilon}{2}} \left[ \sqrt{\frac{\sigma^2}{\epsilon \omega} + 1} - 1 \right]^{1/2}$$

then the wavefunctions become: (after choosing a polarization, applying BCs,  $B_0 \rightarrow \frac{k}{\omega} E_0$ )

$$\tilde{\vec{E}}(z,t) = \tilde{E}_0 e^{-Kz} e^{i(kz - \omega t)} \hat{x}, \quad \tilde{\vec{B}}(z,t) = \frac{\tilde{k}}{\omega} \tilde{E}_0 e^{-Kz} e^{i(kz - \omega t)} \hat{y}$$

A few important points here:

- Waves continue to propagate into the metal!

- BUT decay exponentially

- the characteristic depth here, where amplitude decays by  $1/e$ , is called the skin depth (or penetration depth):  $d = 1/K$

- Since  $\tilde{k}$  is complex, also implies other quantities have real/imag component

- $\tilde{k} = \frac{\tilde{n}\omega}{c} \rightarrow \tilde{n} = n_R - i n_I$

- $\tilde{n} = \sqrt{\tilde{\epsilon}/\epsilon_0} \rightarrow \tilde{\epsilon} = \epsilon_R - i\epsilon_I$

Okay, now let's figure out the amplitudes

[2-21]

Start by representing  $\tilde{\mathbf{k}}$  as:  $\tilde{\mathbf{k}} = |\tilde{\mathbf{k}}| e^{i\phi}$

$$\text{where } |\tilde{\mathbf{k}}| = \sqrt{k^2 + \kappa^2} \quad \& \quad \phi = \tan^{-1}(\kappa/k)$$

and remember that the complex amplitudes  $\tilde{\mathbf{E}}_0$ ,  $\tilde{\mathbf{B}}_0$  can absorb phase offset

$$\tilde{\mathbf{E}}_0 = \mathbf{E}_0 e^{i\delta_E}, \quad \tilde{\mathbf{B}}_0 = \mathbf{B}_0 e^{i\delta_B}$$

$$\text{but } \tilde{\mathbf{B}}_0 \text{ also equals: } \tilde{\mathbf{B}}_0 = \frac{\tilde{\mathbf{k}}}{\omega} \tilde{\mathbf{E}}_0 = \frac{|\tilde{\mathbf{k}}| e^{i\phi}}{\omega} \mathbf{E}_0 e^{i\delta_E}$$

$$\Rightarrow \mathbf{B}_0 e^{i\delta_B} = \frac{|\tilde{\mathbf{k}}| e^{i\phi}}{\omega} \mathbf{E}_0 e^{i\delta_E} = \frac{|\tilde{\mathbf{k}}|}{\omega} \mathbf{E}_0 e^{i(\phi + \delta_E)}$$

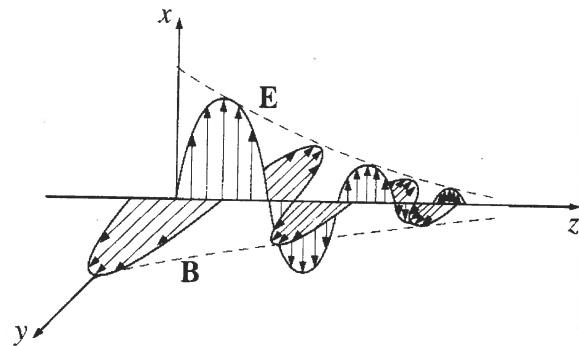
$$\Rightarrow \delta_B - \delta_E = \phi (!)$$

Wow! So  $\vec{\mathbf{E}}$  and  $\vec{\mathbf{B}}$  are no longer in phase ( $\vec{\mathbf{B}}$  lags  $\vec{\mathbf{E}}$ )

This was impossible for EM waves in free space and linear dielectrics.

## Dispersion in Metals

Remember: defined metals as a collection of both free and bound charges



Have already seen derivation of  $n(\omega)$  for

bound charges as following from driven-damped oscillator

$$F_{\text{tot}} = F_{\text{drive}} - F_{\text{damp}} - F_{\text{restore}} \Rightarrow \frac{d^2 x}{dt^2} = \frac{q \tilde{\mathbf{E}}_0}{m} e^{i\omega t} - \gamma_b \frac{dx}{dt} - \omega_0^2 x$$

$$\text{where } x(t) = \frac{q^2/m}{(\omega_0^2 - \omega^2 + i\gamma_b \omega)} \tilde{\mathbf{E}}(t)$$

$$\text{and since } \mathbf{P}(t) = qN x(t) \quad \text{and} \quad \epsilon = \epsilon_0 + \frac{\vec{\mathbf{P}}}{\vec{\mathbf{E}}} = \epsilon_0 + \frac{q^2 N/m}{(\omega_0^2 - \omega^2 + i\gamma_b \omega)}$$

$$\text{then } n_{\text{bound}}^2 = \frac{\epsilon}{\epsilon_0} = 1 + \frac{Nq^2}{\epsilon_0 m} \left( \frac{1}{\omega_0^2 - \omega^2 + i\gamma_b \omega} \right) \quad [2-22]$$

but the free  $e^-$  gas of a metal has no restoring force ( $\omega_0 \rightarrow 0$ )

$$\Rightarrow n_{\text{free}}^2 = 1 + \frac{Nq^2}{\epsilon_0 m} \left( \frac{1}{-\omega^2 + i\gamma_e \omega} \right) = 1 - \frac{Nq^2}{\epsilon_0 m} \left( \frac{1}{\omega^2 - i\gamma_e \omega} \right)$$

two items of note here: 1) pick up a phase change (180° out of phase)

2)  $\gamma_e$  is damping within  $e^-$  gas ( $e^-e^-$  collisions, etc)

assume for a moment that EM freq.  $\omega$  is large compared to collision rate

$$\Rightarrow n_{\text{plasma}}^2 = 1 - \frac{Nq^2}{\epsilon_0 m \omega^2} = 1 - \frac{\omega_p^2}{\omega^2} \quad (\omega^2 \gg \gamma \omega)$$

where  $\omega_p = \sqrt{\frac{Nq^2}{\epsilon_0 m}}$  is called the Plasma frequency

can see for  $\omega < \omega_p$ :  $n$  is complex valued (material reflects)

$\omega > \omega_p$ :  $n$  is real valued (material is transparent)

for metals, in general, though

$$\epsilon_{\text{Tot}} = \epsilon_{\text{vac}} + \epsilon_{\text{bound}} + \epsilon_{\text{free}} \quad (\epsilon_{\text{vac}} = \epsilon_0)$$

$$\Rightarrow n_{\text{metal}}^2 = \frac{\epsilon}{\epsilon_0} = 1 + \frac{Nq^2}{\epsilon_0 m} \left[ \frac{1}{-\omega^2 + i\gamma_e \omega} + \frac{1}{\omega_0^2 - \omega^2 + i\gamma_b \omega} \right]$$

$$= 1 - \frac{\omega_p}{\omega^2 - i\gamma_e \omega} + \frac{\omega_p}{\omega_0^2 - \omega^2 + i\gamma_b \omega}$$