Fourier Optics

Diffraction Recap

- · general integral: \(\vec{E}(\vec{F}) = C \) \(\vec{E}(\vec{x}', \vec{y}', \vec{o}) \vec{U}(\vec{k}, \vec{R}) \) dx'dy'
- · Scalar approximation: È -> E
- · Fresnel Kirchoff: E(r) = -i][E(x', y', o) eikR [1+cos(r,z)]dx'dy
- · Fresnel: ") 0' is small 2) 22 >> (x-x')2+ (y-y')2

$$\Rightarrow R = Z \sqrt{1 + \frac{(x-x')^2 + (y-y')^2}{Z^2}} \approx Z \left(1 + \frac{(x-x')^2 + (y-y')^2}{2Z^2}\right)$$

$$\Rightarrow \frac{1}{R} \approx \frac{1}{2} \quad \text{de ikR} \quad \text{ikz ik} \frac{(x-x')^2 + (y-y')^2}{12}$$

$$\implies E(x,y,z) = \frac{-i}{\lambda^2} e^{ikz} e^{i\frac{kz}{2z}(x^2+y^2)} \iint E(x',y') e^{-i\frac{kz}{2z}(x'^2+y'^2) - i\frac{kz}{2}(xx'+yy')} dx'dy'$$

• Frankofer: $z = \frac{a^2}{\lambda}$ (far-field)

$$\Rightarrow E(x,y,z) = \phi(x,y,z) \iint E(x',y') e^{-i\frac{k}{2}(xx'+yy')} dx'dy'$$

Array Theorem: a very nice way to calculate the diffraction pattern caused by N identical apertures with Eaperture (x', y', 0)

· assume each aperture has a center-of-mass located at (Xn, Yn')

$$E(x|x,z) = \frac{-i}{hz} e^{ikz} e^{i\frac{kz}{2z}(x^2+y^2)} \sum_{n=1}^{N} \iint_{Eap} (x'-x_n,y'-y_n')$$

$$= \frac{-i}{hz} e^{ikz} e^{i\frac{kz}{2z}(x^2+y^2)} \sum_{n=1}^{N} \iint_{Eap} (x'-x_n,y'-y_n')$$

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$$= \frac{-i}{hz} e^{ikz} e^{i\frac{kz}{2z}(x^2+y^2)} \sum_{n=1}^{N} \iint_{Eap} (x'-x_n,y'-y_n')$$

· and then make a change of variables

$$= x' - x'_{n}$$
 $= y' - y'_{n}$

$$E(x,y,z) = \frac{-1}{\lambda z} e^{ikz} e^{i\frac{kz}{\lambda z}(x^2+y^2)} \sum_{n=1}^{N} \iint E_{ap}(x'',y'') e^{-i\frac{kz}{\lambda z}[x(x''+x'_n)+y(y''+y'_n)]} dx'' dy''$$

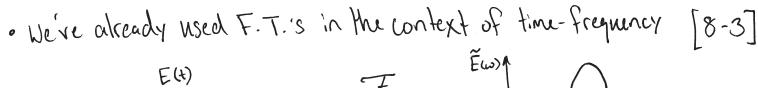
· now parts involving xn & yn can be pulled out

$$E(x,y,z) = \left[\sum_{n=1}^{N} e^{-i\frac{k}{2}(xx_n'+yy_n')}\right] \left[\sum_{n=1}^{-1} e^{ikz} e^{i\frac{kz}{2}(x^2+y^2)}\right] \left[\sum_{n=1}^{-1} e^{i\frac{kz}{2}(x^2+y^2)}\right] \left[\sum_{n=1}^{-1} e^{ikz} e^{i\frac{k$$

$$\sim \left[\frac{\sin N\alpha}{\sin \alpha}\right] \left[\frac{\sin \beta}{\beta}\right]$$
 (mutiple slit interference)

Fourier Optics

- · Fourier Analysis gives a powerful way of describing optical fields passing through a system
 - describes optical field in real space as for of position, f(x,y)
 - OR describe the field in terms of spacial frequency, which is related to the so-called angular spectrum of the field



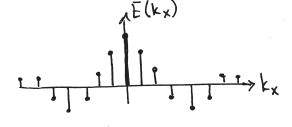
$$= \underbrace{F(t)}_{\text{Wo}} + \underbrace{F(w)}_{\text{Wo}}$$

$$\mathcal{F}[E(t)] = \tilde{E}(\omega)$$

- · E(w) and E(t) both contain the Same information about the field. just written in terms of different (conjugate) variables
- · Now, consider signals in space, not time.

I magne a series of slits along &, illuminated by a plane wave





- · What does the spatial freg tell us, practically? A: How much light is propagating in a certain direction after the aperture I grating.
- · So, this gives exactly what the intensity pattern at the screen will be for the far-field
- · The far-field E-field is the 2D F. T. of the E-field at the aperture

$$E(x',y',0)$$

$$E(x,ky,0)$$

$$\frac{k_{x}}{k} \sim \theta_{x} \sim \frac{x}{z}$$

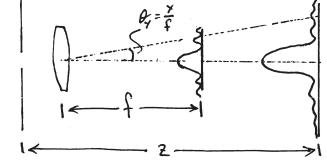
$$\frac{k_{y}}{k} \sim \theta_{y} \sim \frac{y}{z}$$

$$E(x,y,z) = \frac{-i}{\lambda z} e^{ikz} e^{i\frac{kz}{2z}(x^2+y^2)} \iint E(x',y',o) e^{-i\frac{kz}{2z}(xx'+yy')} dx'dy'$$

- · Where the Spatial freq. components corresponding to a given kx represent plane waves propagating at an angle
 - 8-4]

Ex: $\alpha = 2mm$ >= 500 nm 7 = 8 m

- · however, place a lens immediately after the aperture
- and get image at infinity brought to focal plane of lens
- · Why is this a useful thing?
 - F.T. is comparatively simple
 - F.T. is linear, so can build up complicated functions from simple ones



· rather than writing out the full integral expression for F.T. each time, is more convenient to write as operators: F[...] & F'[...] $\Rightarrow f(x) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{ikx} \left[\frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} f(x') e^{ikx'} dx' \right] dk$ (its inverse)

$$= \mathcal{F}^{-1}[\mathcal{F}[f(x)]]$$

$$=f(x)$$

Examples:
$$f(x) = rect(x) \qquad \boxed{\begin{cases} 8-5 \end{cases}}$$

$$f(x) = rect(x) \qquad \boxed{\begin{cases} x = 5 \end{cases}}$$

$$\mathcal{F}[\text{rect}(x)] = \text{Sinc}(\frac{k_x}{2}) = \text{Fik}_x$$

$$e^{-x^{2}/2}$$

•
$$f(x) = e^{-x^2/2}$$
 $f(e^{-x^2/2}) = e^{-kx^2/2} = f(kx)$

- no aperture:
$$\mathcal{F}[C] = \frac{c}{2\pi} J(k_x - k_o)$$

$$free delta function:$$

$$S(x) = \begin{cases} 0 & x \neq 0 \\ \infty & x = 0 \end{cases}$$

 $\int_{-\infty}^{\infty} \delta(x) dx = 1$

$$\delta(x-x_0) = \begin{cases} 0 & x \neq x_0 \\ \infty & x = x_0 \end{cases}$$

• the delta function here is kind of special and very useful as a sifting function
$$f(x) = \int_{-\infty}^{\infty} f(x') \delta(x-x') dx'$$

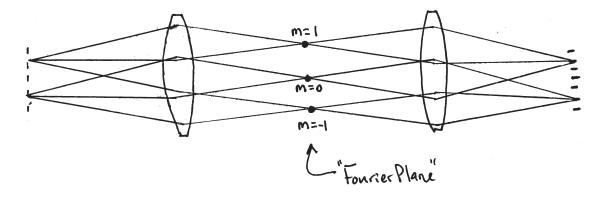
$$f(x) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{ikx} \left[\frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} f(x') e^{ikx'} dx' \right] dx$$

$$= \int_{-\infty}^{\infty} f(x') \left[\frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{ik(x-x')} dx \right] dx'$$

$$\Longrightarrow \delta(x-x') = \sqrt{\frac{1}{2\pi}} \int_{-\infty}^{\infty} ik(x-x') dk$$

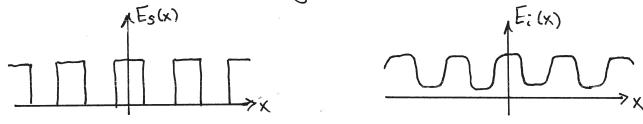
which is a very interesting result - the only way the d-function can be infinitely sharp is to be a uniform superposition of all freq. components!

- · We've discussed the idea of spatial frequency content within an image, now let's consider this concept in real applications
- · Ex: Difficution by a grating, reformsed by a lens



- · what happens when the lens is too small?
 - get fewer orders at the Fourier plane
- " What happens if the grating period is increased?
 - spots move further apart (so would need larger diameter lens)
- · What happens when the first lens is placed closer and closer to the
 - Still get diffraction orders at a distance of behind the lens, but the overall pattern is <u>diverging</u>
 - So if we want to re-image the diffraction pattern with another lens, it's most convenient to place the first lens f away from grating -> leads to so-called "4-f" imaging setup

• if the leases of the 4-f setup are finite diameter, the higher diffraction orders are lost → the pattern at the image plane is not as sharp as the original (loss of contrast)



so, the more diffraction orders retained, the sharper edges will be

- a Similar (but not identical) effect occurs if we obstruct the beam in the Fourier plane closing down an iris in that plane cuts off information about higher spatial frequencies [essentially forming] a bw-pass filter]
- Ex: have a laser with a "messy" non-uniform intensity profile across its beam cross-section. Can "clean" the beam by focusing it through a pinhole (of carefully chosen diameter) to reject high spatial freq's
- · this is all very qualitative so far, need to formalize these ideas

- · What we want is a formalism which specifies how different spatial frequencies will be handled by an optical system
- · imagine a plane wave incident on some real, physical, non-ideal optical element (eg. a lens with defects & smudges)

-> results in a modifical amplitude and phase

Escan) E: (x,y)

-> can write this as a transfer function

 $A(x,y) = A_0(x,y) e$ omplifule phase

Aperture Function
Pupil Function

 $\Rightarrow E_A = E_o A_o(x_1y) e^{i\phi(x_1y)}$

· Why does this matter? Many optical instruments have A non-trivial aperture function (Ex. Cassegrain telescope)

Point Spread Function:

A(p) = \$1 Eq.

A(p) = { 1 Eq Lp Lq o elsewhere

- . a point at the source plane will always result in a characteristic diffraction pattern at the imaging plane
- · We've seen that diffraction from some aperture is related by a Fourier Transform as the transfer function, which here we call the "Point Spread Function" of diffracted intensities

$$S(x,y) = \left| \mathcal{F} \left[A_{o}(x,y) e^{i\phi(x,y)} \right] \right|^2$$

• We'll only consider <u>real-valued</u> aperture functions, for simplicity $S(x,y) = \mathcal{F}[A_0(x,y)]^2$

· We've Solved for diffraction of fairly simple apertures (circular, square),
but what about more complicated (i.e. realistic) ones like
the annular aperture of a reflecting telescope -> Babinet's
Principle.

Exisimple Circular aperture:

$$\mathcal{J}[A_{\epsilon=0}] = 2\pi a^2 \frac{\mathcal{J}_{\epsilon}(ap)}{ap}$$

annular aperture:

$$\mathcal{F}[A_{\epsilon}] = 2\pi a^{2} \left(\frac{J_{i}(ap)}{ap} - 2\pi \epsilon^{2} a^{2} \left(\frac{J_{i}(ap)}{\epsilon ap} \right) \right)$$

$$= 2\pi a^{2} \left[\frac{J_{i}(ap)}{ap} - \epsilon^{2} \frac{J_{i}(\epsilon ap)}{\epsilon ap} \right]$$

using Babinet's principle

then the point spread function is the modulus squared

$$S(x,y) = \mathcal{F}\left[A_{\varepsilon}\right]^{2} = \left(2\pi a^{2}\right)^{2} \left[\left(\frac{J_{\varepsilon}(ap)}{ap}\right) - \varepsilon^{2}\left(\frac{J_{\varepsilon}(\varepsilon ap)}{\varepsilon ap}\right)\right]^{2}$$

· Note: you can't do this with the intensities, just the fields. the cross terms are important

- · Okay, so how to treat more complicated images?
 - -> Simply add up a collection of points describing the image
- · the image of an extended, non-point object is the convolution of the ideal image with the point-spread function

$$I(x,y) = \iint I_{o}(x',y') S(x-x',y-y') dx' dy'$$

$$= I_{o}(x',y') S(x-x',y-y')$$
Object convolution Point-spread function

- So, the main idea of convolution is that it's a special "product" of function' $g(x) = \int_{-\infty}^{\infty} f(x') h(x-x') dx'$
- o important property of convolution is that if commutes $g(x) = \int_{-\infty}^{\infty} f(x')h(x-x')dx' = \int_{-\infty}^{\infty} f(x-x')h(x')dx' \quad \begin{cases} change & chan$

- another important property is that convolution in spatial representation is the same as simple multiplication in freq. representation

$$\mathcal{F}[f \otimes h] = \mathcal{F}[f] \cdot \mathcal{F}[h]$$

Proof:

$$\widetilde{g}(k) = \mathcal{F}[f \circ h] = \mathcal{F}\left[\int_{-\infty}^{\infty} f(x')h(x-x')dx'\right]
= \int_{-\infty}^{\infty} \left[\int_{-\infty}^{\infty} f(x)h(x-x')dx'\right] e^{ikx} dx$$

Since the limits are at infinity, makes no difference whether we integrate over x or x' first

$$\Rightarrow g(x) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h(x-x') e^{ikx} dx \int_{-\infty}^{\infty} f(x') dx'$$

then introduce the multiplicative factor $e^{ikx'}$ $e^{ikx'} = 1$ $= \iint_{-\infty} \left[\int_{-\infty}^{\infty} h(x-x')e^{ikx} e^{ikx'} dx \right] f(x') e^{ikx'} dx'$

integrals are now independent

=
$$\iint \int_{-\infty}^{\infty} \int_{-\infty$$

$$= \mathcal{F}[f(x)] \cdot \mathcal{F}[h(x)] = \tilde{f}(k) \cdot \tilde{h}(k)$$

· the idea of convolution can be extended

$$g(x) = \int_{-\infty}^{\infty} f(x')h(x-x')dx' = f(x) \otimes h(x)$$
 [convolution]

• a related integral transform operation is called <u>Cross-Correlation</u> $C(x) = \iint_{-\infty}^{\infty} f(x') h(x+x') dx' = f(x) \circ h(x)$

- * the cross-correlation is a way of comparing two (possibly complex-valued) functions to see how similar they are to one another
 - also known as a "sliding dot product" since it measures Simularity as a function of relative displacement between fix of hix
- · Some important properties of coss-correlation

- if f*(x) = f(-x) (ie. f is Hermetian), then foh = f⊗h
- if both f and h are Hermetian, than foh = h of
- -in general, though: $(f \circ h) \circ (f \circ h) = (f \circ f) \circ (h \circ h)$ $g \circ (f \circ h) = (g \circ f) \circ h \qquad (cross-correl.)$ ulitself?

- and similar to the convolution theorem: F[foh] = F[f] . F[h]

of a function with itself
$$\rightarrow$$
 called autocorrelation [8-13] $a(x) = \int_{-\infty}^{\infty} f(x') f(x+x') = f(x) \circ f(x)$

· why would you do this? it's really useful for finding periodic, repeating patterns in a complicated Signal Wavefunction

Back to Optical Transfer Functions

· Okay, so we saw that the image formed by an (imperfect) imaging system with a given point-spread function, S(x,y), is [Convolution] $\overline{I}(x,y) = \overline{I}_{o}(x,y) \otimes S(x,y)$

· by using the convolution theorem here, we have

$$\mathcal{F}[I(x,y)] = \mathcal{F}[I_0(x,y)] \cdot \mathcal{F}[S(x,y)]$$

=> T(kx, ky) = To(kx, ky). T(kx, ky)

[Spatial freq. | Spatial freq. | Spatial freq. | transfer function]

[image spectrum] = [Object spectrum]. [transfer function]

Phase Transfer Modulation Function Transfer Fn.

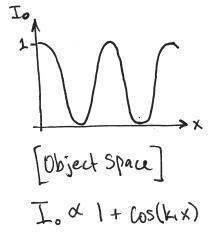
the part that's actually called

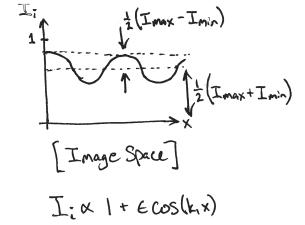
Optical Transfer

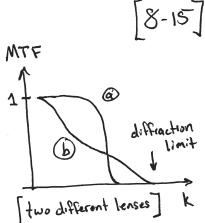
Function

- · So, what does the OTF, T, tell us about the system? [8-14]
 - if the source contains information at some spatial freq (kx, kx), then T(kx, kx) gives how much of that information is transferred from the source to the image
- · again, we will simplify by not concerning ourselves with the phase transfer function (commonly called just PTF')
- · However, the MTF (modulation transfer function) is very important, as it defines the loss in contrast from object to image vs. frequency
 - -> M = ratio of image modulation to object modulation at all spatial frequencies
- O a Simple example to illustrate this: Sinusoidal amplitude transmission mask

 k, o k,
- · for a finite aperture lens, the larger k, is, the less light will go through
- · Since it's the interference of light at ± k, that gives the modulation:







· Modulation transfer function normally just called "modulation" or "contrast"

$$M = \frac{I_{\text{max}} - I_{\text{min}}}{I_{\text{max}} + I_{\text{min}}}$$

Note: if there was a phase offset between I. & I:, then would be due to effects from Phase Transfer Function

· Contrast always falls of at higher spatial frequencies -> Diffraction Limit!

· as indicated above, MTF is related to PSF (and, hence, aperture)

$$M(k_{x},k_{y}) = \mathcal{F}[S(x,y)]$$

$$= \mathcal{F}[|\mathcal{F}[A(x,y)]|^{2}]$$

autocorrelation of the aperture fr. ... obviously.

o Okay, I'm glossing over details like coherent vs. in coherent illumination. The proof of this last step requires wrangling of integrals, variable substitutions, and an interesting observation that $\mathcal{F}[\mathcal{F}[f(x,y)]] = f(-x,-y)$, which is HW8-A1. Also note that $A(x,y) \otimes A(x,y) = A(x,y) \otimes A(x,y)$, iff A(x,y) is even / Hermetian

• Cach of these transfer functions is usually normalized
$$S(x,y) = \frac{S(x,y)}{\iint S(x,y) dxdy}$$
 [Aren = 1]

[8-16]

$$S_{n}(x,y) = \frac{S(x,y)}{\iint S(x,y) dxdy}$$

· two common apertures:

