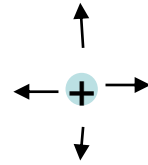


# Panel Methods

# Source and Vortex

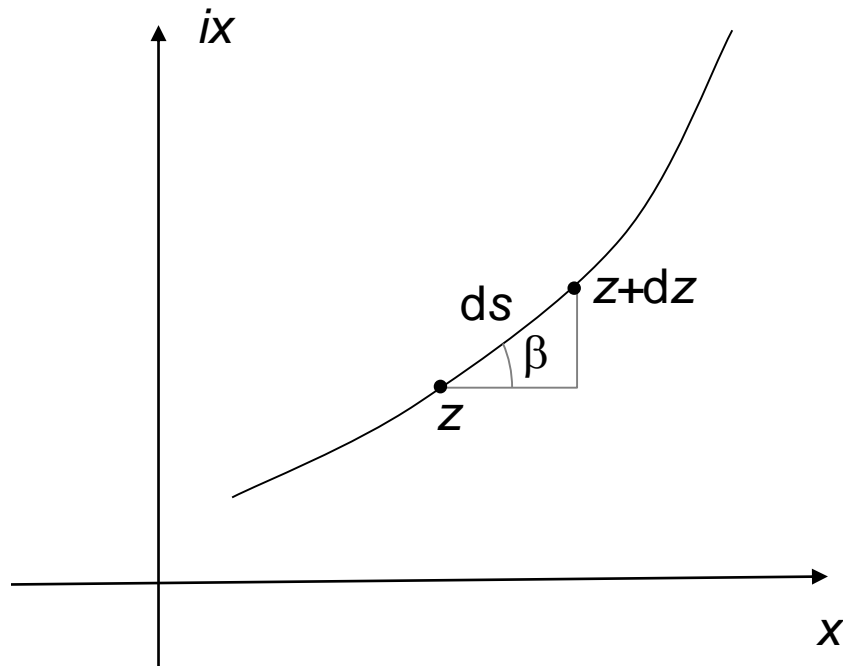
- Point Source



- Point Vortex



# $dz$ in Polar Form



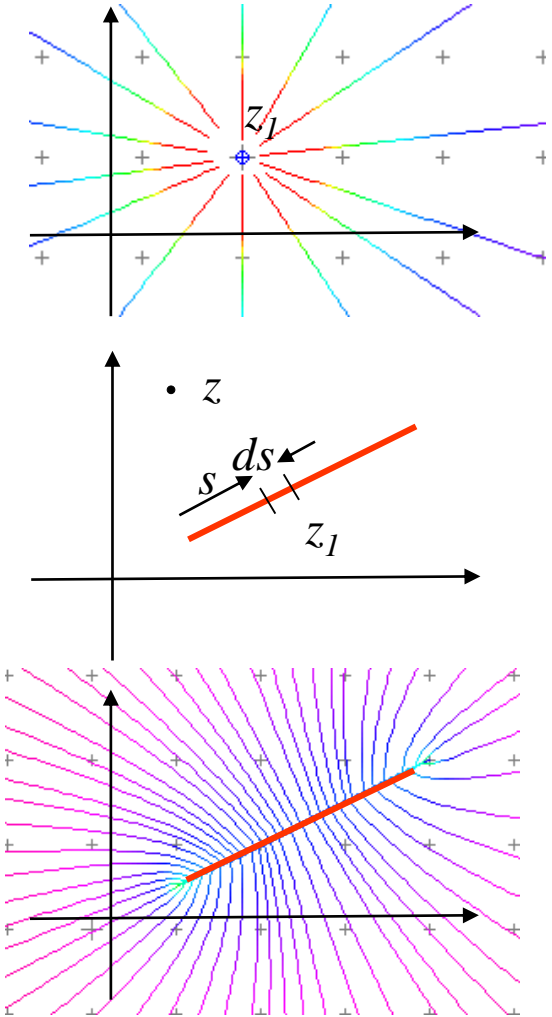
# Panels

Singularity distributed along a line

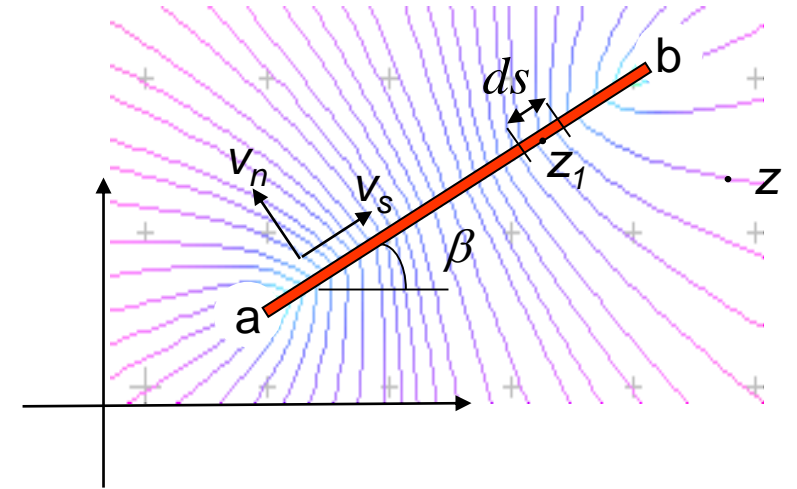
## Example: The Source Panel (or Sheet)

Consider a point source  $\oplus$   $W(z) = \frac{q}{2\pi(z - z_1)}$

Imagine spreading the source along a line. We would then end up with a certain strength per unit length  $q(s)$  that could vary with distance  $s$  along the line.



# Constant Strength Source Panel



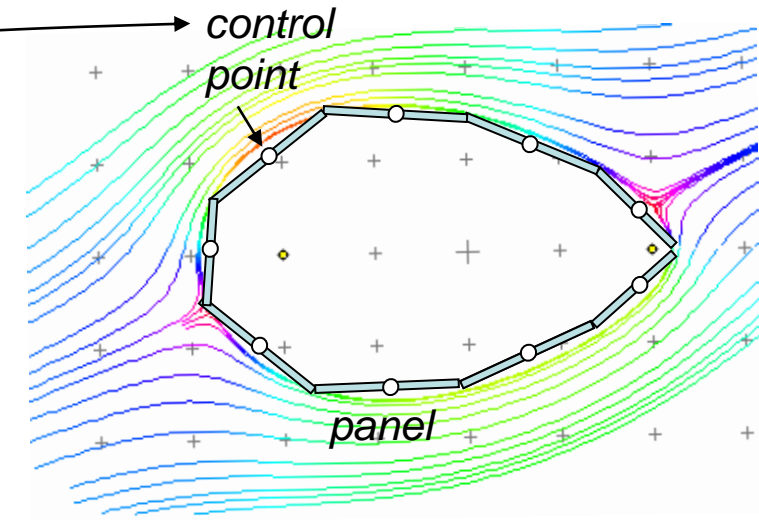
The panel is not a solid boundary to the flow. To make it behave like one you would set the strength  $q$  so that the total  $v_n$  (due to the panel and the flow) is zero

Vortex?

# A Simple Source Panel Method

*For flow past an arbitrary body*

- Break up the body surface into  $N$  straight panels.
- Write an expression for the normal component of velocity at the **middle of the panel** from the sum of all the velocities produced by the panels and the free stream. Gives  $N$  expressions.
- Given that each expression must be equal to zero, solve the  $N$  equations for the  $N$  strengths



# Defining the $N$ Panels

- Number the panels anticlockwise, 1 to  $N$
- Define  $N$  coordinates  $z_a$  that identify the start of every panel (going counter clockwise), and  $z_b$  that identify the end of every panel.

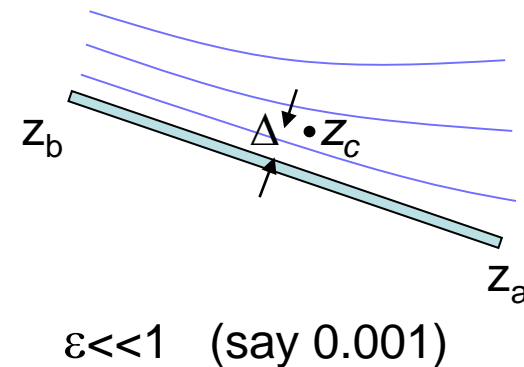
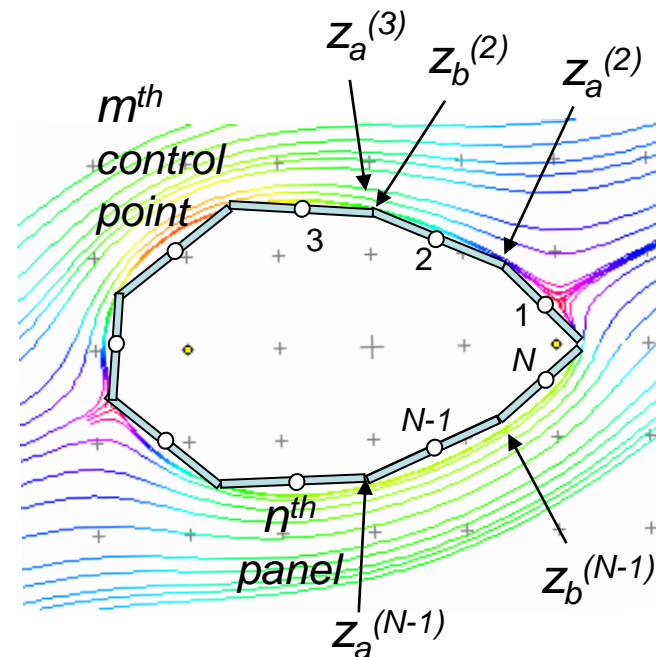
- Each panel has a slope  $\frac{dz}{ds} = e^{i\beta} = \frac{z_b - z_a}{|z_b - z_a|}$   
So, if  $W(z)$  is the velocity of the whole flow,

$-\text{Im}\left\{W(z)\frac{dz}{ds}\right\}$  is the component normal to the panel

- We pick a control point very close to the center of the panel at

$$z_c = \frac{1}{2}(z_a + z_b) - i\varepsilon(z_b - z_a)$$

Center point      Displacement  $\Delta$



# Completing the Method

Velocity produced by whole flow is

$$W(z) = W_\infty + \sum_{n=1}^N q^{(n)} \frac{1}{2\pi} \log_e \left( \frac{z - z_a^{(n)}}{z - z_b^{(n)}} \right) \frac{ds}{dz_1} \Big|^{(n)}$$

Velocity at the control point of the  $m^{\text{th}}$  panel  $z_c^{(m)}$  in panel aligned components is

$$= W_\infty \frac{dz_1}{ds} \Big|^{(m)} + \sum_{n=1}^N q^{(n)} \frac{1}{2\pi} \log_e \left( \frac{z_c^{(m)} - z_a^{(n)}}{z_c^{(m)} - z_b^{(n)}} \right) \frac{ds}{dz_1} \Big|^{(n)} \frac{dz_1}{ds} \Big|^{(m)}$$

So, velocity normal to the  $m^{\text{th}}$  panel is

$$= \text{Im} \left\{ \frac{dz_1}{ds} \Big|^{(m)} W_\infty \right\} + \sum_{n=1}^N q^{(n)} \text{Im} \{ C^{(m,n)} \}$$

Velocity parallel to the  $m^{\text{th}}$  panel is

$$= \text{Re} \left\{ \frac{dz_1}{ds} \Big|^{(m)} W_\infty \right\} + \sum_{n=1}^N q^{(n)} \text{Re} \{ C^{(m,n)} \}$$

We want the normal velocity to be zero, so this is what we use to get the  $q$ 's

We write

$$- \text{Im} \left\{ \frac{dz_1}{ds} \Big|^{(m)} W_\infty \right\} = \sum_{n=1}^N q^{(n)} \text{Im} \{ C^{(m,n)} \}$$

Or

$$\begin{matrix} 1 \times N \text{ result matrix} \\ \text{(known)} \end{matrix} = \begin{matrix} 1 \times N \text{ matrix} \\ \text{of strengths} \\ \text{(unknown)} \end{matrix} \times \begin{matrix} N \times N \text{ matrix of} \\ \text{ceoffs (known)} \end{matrix}$$

Once we have solved this for the  $q$ 's we can use eqn. 2 to get the velocities along the body surface, or eqn. 1 to get them anywhere else

1

2



# Computational Steps

- Define coordinates of start and end of panels  $z_a$  and  $z_b$   $z_a^{(n)}, z_b^{(n)}$
- Compute the panel slopes  $\frac{dz}{ds} = e^{i\beta} = \frac{z_b - z_a}{|z_b - z_a|}$
- Put the control points next to the panel centers  $z_c = \frac{1}{2}(z_a + z_b) - i\varepsilon(z_b - z_a)$
- Determine the component of  $W_\infty$  normal to each panel  $-\text{Im}\left\{\left.\frac{dz_1}{ds}\right|^{(m)} W_\infty\right\}$
- Determine the influence coefficients  $C^{(m,n)} = \frac{1}{2\pi} \log_e \left( \frac{z_c^{(m)} - z_a^{(n)}}{z_c^{(m)} - z_b^{(n)}} \right) \frac{ds}{dz_1} \bigg|^{(n)} \frac{dz_1}{ds} \bigg|^{(m)}$
- Solve the matrix problem, i.e. matrix divide  $\text{Im}\{C^{(m,n)}\}$  by  $-\text{Im}\left\{\left.\frac{dz_1}{ds}\right|^{(m)} W_\infty\right\}$
- Compute the flow velocities and pressures

# Matlab Code

```

clear all;
%Circular cylinder example, radius 2, 35 panels
npanels=35;r=2;winf=1;

$$z_a^{(n)}, z_b^{(n)}, \left. \frac{dz_1}{ds} \right|^{(n)}$$

{
    z=r*exp(i*[2*pi/npanels:2*pi/npanels:2*pi]);
    a=[1:npanels];b=[2:npanels 1];
    dzds=(z(b)-z(a))./abs(z(b)-z(a));

    
$$z_c^{(n)}$$

    {
        eps=0.0001;
        zc=(z(a)+z(b))/2-i*eps*(z(b)-z(a)); %control points

        
$$C^{(m,n)}$$

        {
            cm=zeros(npanels);
            for m=1:npanels
                cm(:,m)=log((zc(m)-z(a))./(zc(m)-z(b)))/2/pi./dzds(a)*dzds(m);
            end
            res=imag(-winf*dzds);
            q=res/imag(cm);

            
$$-\operatorname{Im}\left\{\left.\frac{dz_1}{ds}\right|^{(m)} W_\infty\right\}$$

            Result matrix

            Matrix div. →

            ut=real(q*cm+winf*dzds);
            cp=1-ut.^2/abs(winf).^2;
            figure
            plot(angle(zc)*180/pi,cp);

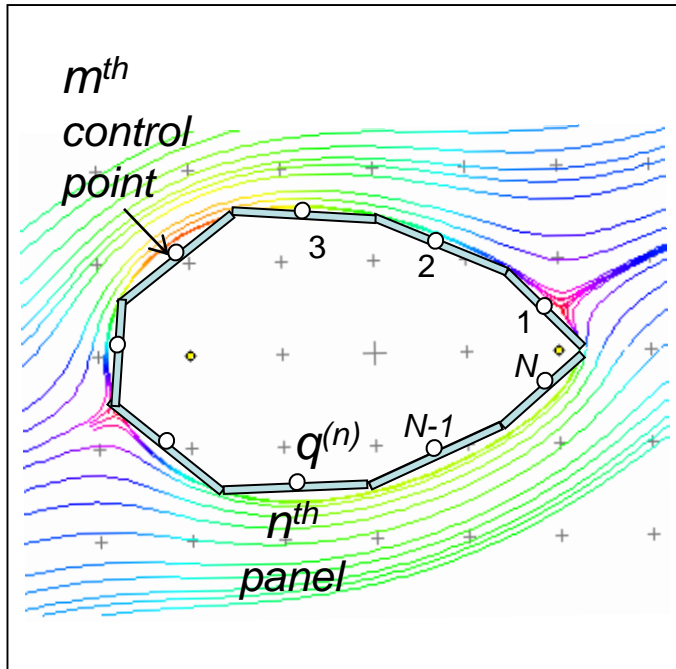
            
$$\operatorname{Re}\left\{\left.\frac{dz_1}{ds}\right|^{(m)} W_\infty\right\} + \sum_{n=1}^N q^{(n)} \operatorname{Re}\{C^{(m,n)}\}$$

            Velocities along body surface
        }
    }
}

```

$$-\operatorname{Im}\left\{\left.\frac{dz_1}{ds}\right|^{(m)} W_\infty\right\} = \sum_{n=1}^N q^{(n)} \operatorname{Im}\{C^{(m,n)}\}$$

$$\begin{pmatrix} \text{res}(1) \\ \text{res}(2) \\ \vdots \\ \text{res}(m) \\ \vdots \\ \text{res}(N) \end{pmatrix} = \begin{pmatrix} \operatorname{Im}\{C^{(1,1)}\} & \operatorname{Im}\{C^{(1,2)}\} & \cdots & \operatorname{Im}\{C^{(1,n)}\} & \cdots & \operatorname{Im}\{C^{(1,N)}\} \\ \operatorname{Im}\{C^{(2,1)}\} & . & & & & \\ \vdots & & . & & & \\ \operatorname{Im}\{C^{(m,1)}\} & & & \operatorname{Im}\{C^{(m,n)}\} & & \\ \vdots & & & & . & \\ \operatorname{Im}\{C^{(N,1)}\} & & & & & \operatorname{Im}\{C^{(N,N)}\} \end{pmatrix} \begin{pmatrix} q^{(1)} \\ q^{(2)} \\ \vdots \\ q^{(n)} \\ \vdots \\ q^{(N)} \end{pmatrix}$$



```
%panel
zc=(z(a)+z(b))/2-i*eps*(z(b)-z(a)); %control points

cm=zeros(npanels);
for m=1:npanels
    cm(:,m)=log((zc(m)-z(a))/(zc(m)-z(b)))/2/pi./dzds(a)*dzds(m);
end
res=imag(-winf*dzds);
q=res/imag(cm);

ut=real(q*cm+winf*dzds);
cp=1-ut.^2/abs(winf).^2;
figure
```

## Matlab Code Ideas:

## 1. Non-Uniform Free Stream

E.g. Suppose free stream includes, say a doublet outside the body at a location  $x=5$ , so

$$W_{\infty} = 1 + \frac{10}{(z-5)^2}$$

```
clear all;
%Circular cylinder example, radius 2, 35 panels
npanels=35;r=2;winf=1;
z=r*exp(i*[2*pi/npanels:2*pi/npanels:2*pi]);
a=[1:npanels];b=[2:npanels 1];
dzds=(z(b)-z(a))./abs(z(b)-z(a));

eps=0.0001;
zc=(z(a)+z(b))/2-i*eps*(z(b)-z(a)); %control points

cm=zeros(npanels);
for m=1:npanels
    cm(:,m)=log((zc(m)-z(a))./(zc(m)-z(b)))/2/pi./dzds(a)*dzds(m);
end
res=imag(-winf*dzds);
q=res/imag(cm);

ut=real(q*cm+winf*dzds);
cp=1-ut.^2/abs(winf).^2;
figure
plot(angle(zc)*180/pi,cp);
```

# Matlab Code Ideas:

## 2. More than one body

E.g. Suppose  
we have two  
circles

```
clear all;
%Circular cylinder example, radius 2, 35 panels
npanels=35;r=2;winf=1;
z=r*exp(i*[2*pi/npanels:2*pi/npanels:2*pi]);
a=[1:npanels];b=[2:npanels 1];
dzds=(z(b)-z(a))./abs(z(b)-z(a));

eps=0.0001;
zc=(z(a)+z(b))/2-i*eps*(z(b)-z(a)); %control points

cm=zeros(npanels);
for m=1:npanels
    cm(:,m)=log((zc(m)-z(a))./(zc(m)-z(b)))/2/pi./dzds(a)*dzds(m);
end
res=imag(-winf*dzds);
q=res/imag(cm);

ut=real(q*cm+winf*dzds);
cp=1-ut.^2/abs(winf).^2;
figure
plot(angle(zc)*180/pi,cp);
```

# Matlab Code Ideas:

## 3. Use more sophisticated panels

E.g. Panels with linearly varying strength

```
clear all;
%Circular cylinder example, radius 2, 35 panels
npanels=35;r=2;winf=1;
z=r*exp(i*[2*pi/npanels:2*pi/npanels:2*pi]);
a=[1:npanels];b=[2:npanels 1];
dzds=(z(b)-z(a))./abs(z(b)-z(a));

eps=0.0001;
zc=(z(a)+z(b))/2-i*eps*(z(b)-z(a)); %control points

cm=zeros(npanels);
for m=1:npanels
    cm(:,m)=log((zc(m)-z(a))./(zc(m)-z(b)))/2/pi./dzds(a)*dzds(m);
end
res=imag(-winf*dzds);
q=res/imag(cm);

ut=real(q*cm+winf*dzds);
cp=1-ut.^2/abs(winf).^2;
figure
plot(angle(zc)*180/pi,cp);
```

# 3. Linear Source Panel Method

E.g. Panels with linearly varying strength

```
clear all;
%Circular cylinder example, radius 2, 35 panels
npanels=35;r=2;winf=1;
z=r*exp(i*[2*pi/npanels:2*pi/npanels:2*pi]);
a=[1:npanels];b=[2:npanels 1];c=[3:npanels 1 2];
dzds=(z(b)-z(a))./abs(z(b)-z(a));

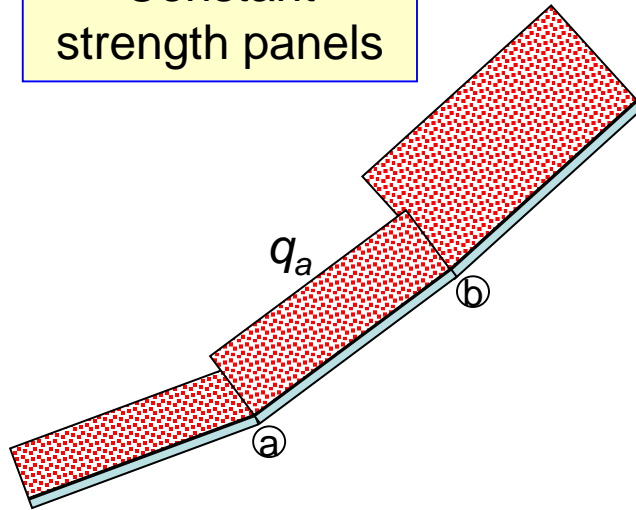
eps=0.0001;
zc=(z(a)+z(b))/2-i*eps*(z(b)-z(a)); %control points

cm=zeros(npanels);
for m=1:npanels
cm(:,m)=((zc(m)-z(a))./(z(b)-z(a)).*log((zc(m)-z(a))./(zc(m)-z(b))))
        -((zc(m)-z(c))./(z(b)-z(c)).*log((zc(m)-z(c))./(zc(m)-z(b))))
end
res=imag(-winf*dzds);
q=res/imag(cm);

ut=real(q*cm+winf*dzds);
cp=1-ut.^2/abs(winf).^2;
figure
plot(angle(zc)*180/pi,cp);
```

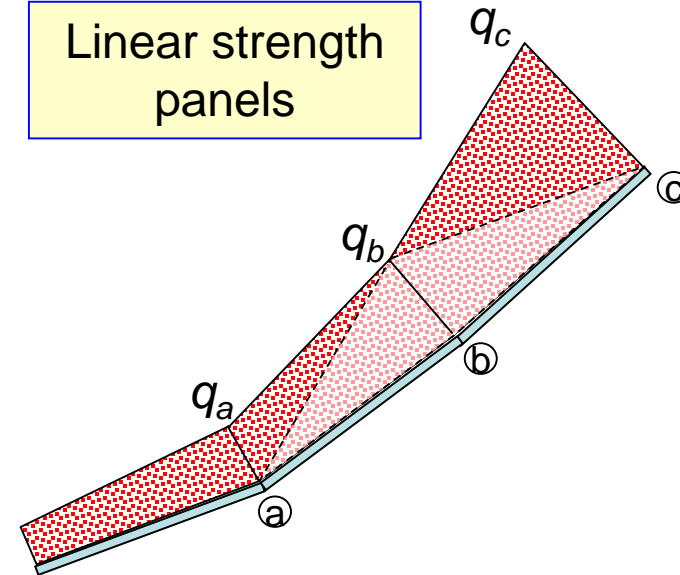
### 3. Linear Source Panels

Constant  
strength panels



*Influence of  $q_a$   
depends only  
panel ab*

Linear strength  
panels



*Influence of  $q_b$   
depends on panel  
ab and panel bc*



# 3. Linear Source Panel Method

E.g. Panels with linearly varying strength

```
clear all;
%Circular cylinder example, radius 2, 35 panels
npanels=35;r=2;winf=1;
z=r*exp(i*[2*pi/npanels:2*pi/npanels:2*pi]);
a=[1:npanels];b=[2:npanels 1];c=[3:npanels 1 2];
dzds=(z(b)-z(a))./abs(z(b)-z(a));

eps=0.0001;
zc=(z(a)+z(b))/2-i*eps*(z(b)-z(a)); %control points

cm=zeros(npanels);
for m=1:npanels
cm(:,m)=( ((zc(m)-z(a))./(z(b)-z(a)).*log((zc(m)-z(a))./(zc(m)-z(b))))
          - ((zc(m)-z(c))./(z(b)-z(c)).*log((zc(m)-z(c))./(zc(m)-z(b))))
end
res=imag(-winf*dzds);
q=res/imag(cm);

ut=real(q*cm+winf*dzds);
cp=1-ut.^2/abs(winf).^2;
figure
plot(angle(zc)*180/pi,cp);
```

# Matlab Code Ideas:

## 4.Change to vortex panel method

$$W(z) = \frac{q}{2\pi(z - z_1)}$$

$$W(z) = \frac{-i\Gamma}{2\pi(z - z_1)}$$

```
clear all;
%Circular cylinder example, radius 2, 35 panels
npanels=35;r=2;winf=1;
z=r*exp(i*[2*pi/npanels:2*pi/npanels:2*pi]);
a=[1:npanels];b=[2:npanels 1];c=[3:npanels 1 2];
dzds=(z(b)-z(a))./abs(z(b)-z(a));

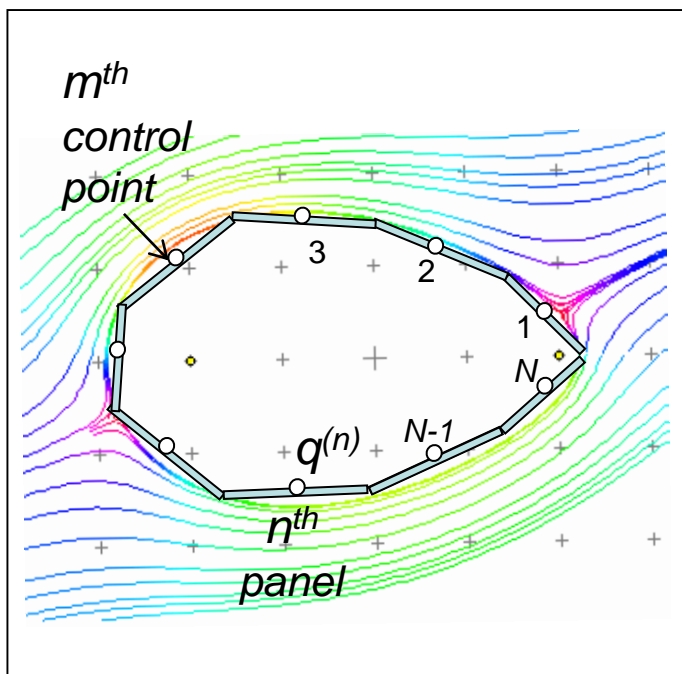
eps=0.0001;
zc=(z(a)+z(b))/2-i*eps*(z(b)-z(a)); %control points

cm=zeros(npanels);
for m=1:npanels
cm(:,m)=( ( (zc(m)-z(a))./(z(b)-z(a)).*log((zc(m)-z(a))./(zc(m)-z(b)))
          - ( (zc(m)-z(c))./(z(b)-z(c)).*log((zc(m)-z(c))./(zc(m)-z(b)))
end
res=imag(-winf*dzds);
q=res/imag(cm);

ut=real(q*cm+winf*dzds);
cp=1-ut.^2/abs(winf).^2;
figure
plot(angle(zc)*180/pi,cp);
```

$$-\operatorname{Im}\left\{\left.\frac{dz_1}{ds}\right|^{(m)}W_\infty\right\}=\sum_{n=1}^Nq^{(n)}\operatorname{Im}\{C^{(m,n)}\}$$

$$\begin{pmatrix} res(1) \\ res(2) \\ \vdots \\ res(m) \\ \vdots \\ res(N) \end{pmatrix} = \begin{pmatrix} \operatorname{Im}\{C^{(1,1)}\} & \operatorname{Im}\{C^{(1,2)}\} & \cdots & \operatorname{Im}\{C^{(1,n)}\} & \cdots & \operatorname{Im}\{C^{(1,N)}\} \\ \operatorname{Im}\{C^{(2,1)}\} & . & & & & \\ \vdots & & . & & & \\ \operatorname{Im}\{C^{(m,1)}\} & & & \operatorname{Im}\{C^{(m,n)}\} & & \\ \vdots & & & & . & \\ \operatorname{Im}\{C^{(N,1)}\} & & & & & \operatorname{Im}\{C^{(N,N)}\} \end{pmatrix} \begin{pmatrix} q^{(1)} \\ q^{(2)} \\ \vdots \\ q^{(n)} \\ \vdots \\ q^{(N)} \end{pmatrix}$$



LinearVortexPanel.m  
(see also  
ConstantVortexPanel.m)

# Matlab Code Ideas:

## 4. Vortex panel method

```
clear all;
%Circular cylinder example, radius 2, 35 panels
npanels=35;r=2;winf=1;gamma=-10;
z=r*exp(i*[2*pi/npanels:2*pi/npanels:2*pi]);
a=[1:npanels];b=[2:npanels 1];c=[3:npanels 1 2];
dzds=(z(b)-z(a))./abs(z(b)-z(a));

eps=0.0001;
zc=(z(a)+z(b))/2-i*eps*(z(b)-z(a)); %control points

cm=zeros(npanels);
for m=1:npanels
cm(:,m)=-i*((zc(m)-z(a))./(z(b)-z(a)).*log((zc(m)-z(a))./(zc(m)-z(b)
        -((zc(m)-z(c))./(z(b)-z(c)).*log((zc(m)-z(c))./(zc(m)-z(b)
end
res=imag(-winf*dzds);
cm1=imag(cm);cm1(:,end)=0.5*(abs(z(b)-z(a))+abs(z(c)-z(b)));
res(end)=gamma;
q=res/cm1;

ut=real(q*cm+winf*dzds);
cp=1-ut.^2/abs(winf).^2;
figure
```

LinearVortexPanel.m  
(see also  
ConstantVortexPanel.m)

# Matlab Code Ideas:

## 5. Set a Kutta Condition

Kutta condition  
requires that  
surface vorticity  
at trailing edge is  
zero.

```
clear all;
%Circular cylinder example, radius 2, 35 panels
npanels=35;r=2;winf=1;gamma=-10;
z=r*exp(i*[2*pi/npanels:2*pi/npanels:2*pi]);
a=[1:npanels];b=[2:npanels 1];c=[3:npanels 1 2];
dzds=(z(b)-z(a))./abs(z(b)-z(a));

eps=0.0001;
zc=(z(a)+z(b))/2-i*eps*(z(b)-z(a)); %control points

cm=zeros(npanels);
for m=1:npanels
cm(:,m)=-i*((zc(m)-z(a))./(z(b)-z(a)).*log((zc(m)-z(a))./(zc(m)-z(b)
-((zc(m)-z(c))./(z(b)-z(c)).*log((zc(m)-z(c))./(zc(m)-z(b)
end
res=imag(-winf*dzds);
cm1=imag(cm);cm1(:,end)=0.5*(abs(z(b)-z(a))+abs(z(c)-z(b)));
res(end)=gamma;
q=res/cm1;

ut=real(q*cm+winf*dzds);
cp=1-ut.^2/abs(winf).^2;
figure
```

# Matlab Code Ideas:

## 5. Kutta Condition Code

Kutta condition requires that surface vorticity at trailing edge is zero.

```
clear all;
%Circular cylinder example, radius 2, 35 panels
npanels=35;r=2;winf=1;k=npanels-1;
z=r*exp(i*[2*pi/npanels:2*pi/npanels:2*pi]);
a=[1:npanels];b=[2:npanels 1];c=[3:npanels 1 2];
dzds=(z(b)-z(a))./abs(z(b)-z(a));

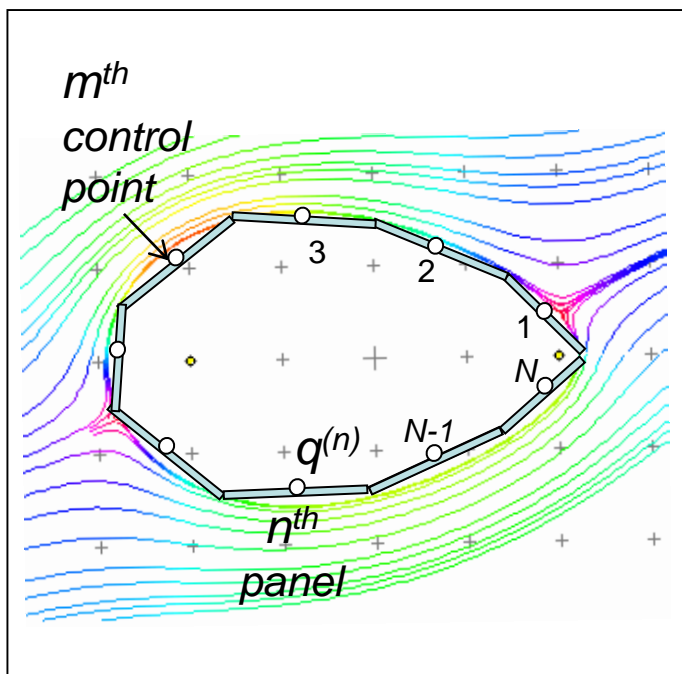
eps=0.0001;
zc=(z(a)+z(b))/2-i*eps*(z(b)-z(a)); %control points

cm=zeros(npanels);
for m=1:npanels
cm(:,m)=-i*((zc(m)-z(a))./(z(b)-z(a)).*log((zc(m)-z(a))./(zc(m)-z(k)
-(zc(m)-z(c))./(z(b)-z(c)).*log((zc(m)-z(c))./(zc(m)-z(k)
end
res=imag(-winf*dzds);
cm1=imag(cm);cm1(:,end)=0;cm1(k,end)=1;
res(end)=0;
q=res/cm1;

ut=real(q*cm+winf*dzds);
cp=1-ut.^2/abs(winf).^2;
figure
```

$$-\operatorname{Im}\left\{\left.\frac{dz_1}{ds}\right|^{(m)}W_\infty\right\}=\sum_{n=1}^Nq^{(n)}\operatorname{Im}\{C^{(m,n)}\}$$

$$\begin{pmatrix} res(1) \\ res(2) \\ \vdots \\ res(m) \\ \vdots \\ res(N) \end{pmatrix} = \begin{pmatrix} \operatorname{Im}\{C^{(1,1)}\} & \operatorname{Im}\{C^{(1,2)}\} & \cdots & \operatorname{Im}\{C^{(1,n)}\} & \cdots & \operatorname{Im}\{C^{(1,N)}\} \\ \operatorname{Im}\{C^{(2,1)}\} & \cdot & & & & \\ \vdots & & \cdot & & & \\ \operatorname{Im}\{C^{(m,1)}\} & & & \operatorname{Im}\{C^{(m,n)}\} & & \\ \vdots & & & & \cdot & \\ \operatorname{Im}\{C^{(N,1)}\} & & & & & \operatorname{Im}\{C^{(N,N)}\} \end{pmatrix} \begin{pmatrix} q^{(1)} \\ q^{(2)} \\ \vdots \\ q^{(n)} \\ \vdots \\ q^{(N)} \end{pmatrix}$$



# Something to watch out for...

- The control-point equation

$$z_c = \frac{1}{2}(z_a + z_b) - i\epsilon(z_b - z_a)$$

*Center point      Displacement  $\Delta$*

assumes that as you move from  $a$  to  $b$  you are progressing counter-clockwise around the body surface. (For clockwise you need to reverse the sign before  $i$ ).