

ECE381V HW1 - Mingyo Seo (EID: ms84662)

Question 1

Let \dot{i}_k be the slew rate at time t_k . Then, the equations of linear time-invariant system is given as,

$$\dot{x}_{k+1} = A_k \dot{x}_k + B_k u_k$$

$$u_{k+1} = u_k + \Delta t \dot{i}_k$$

Let define new variables as

$$\bar{x}_k = \begin{cases} \begin{bmatrix} x_k \\ u_k \end{bmatrix}^{\top} & \text{for } k < N \\ \begin{bmatrix} 0 \\ i_k \end{bmatrix}^{\top} & \text{for } k = N \end{cases}$$

Then, the above equations are formulated as,

$$\bar{x}_{k+1} = \bar{A}_k \bar{x}_k + \bar{B}_k \bar{u}_k,$$

where

$$\bar{A}_k = \begin{bmatrix} A_k & B_k \\ 0 & I \end{bmatrix}, \bar{B}_k = \Delta t \begin{bmatrix} 0 & 0 \\ 0 & I \end{bmatrix}.$$

From the above formulation, we can apply a quadratic cost with respect to \bar{x}_k and \bar{u}_k . To regulate \dot{i}_k , u_k and x_k to the zero point, the quadratic cost can be given as,

$$J = \frac{1}{2} \bar{x}_N^{\top} Q_N \bar{x}_N + \sum_{k=1}^{N-1} \left(\frac{1}{2} \bar{u}_k^{\top} R_k \bar{u}_k + \frac{1}{2} \bar{x}_k^{\top} Q_k \bar{x}_k \right)$$

Here, we consider Q_k , R_k and P_N to be positive definite.

By plugging these results into the LQR formulation of an LTI system, the optimal sequence of $\{\bar{u}_k\}_{k=1}^N$ is given as,

$$\bar{u}_k^* = L_k \bar{x}_k \text{ for } k \leq N - 1,$$

where

$$L_k = - \left(R_k + \bar{B}_k^{\top} K_{k+1} \bar{B}_k \right)^{-1} \left(\bar{B}_k^{\top} K_{k+1} \bar{B}_k \right) \text{ for } k \leq N - 1,$$
$$K_k = \begin{cases} Q_k + L_k^{\top} R_k L_k + \left(\bar{A}_k + \bar{B}_k L_k \right)^{\top} K_{k+1} \left(\bar{A}_k + \bar{B}_k L_k \right) & \text{for } k \leq N - 1 \\ P_N & \text{for } k = N \end{cases}.$$

\bar{u}_k^* can be computed backward from $k = N - 1$ to $k = 1$.

Then, the optimal control sequence u_k^* can be computed forward from $k = 1$ to $k = N - 1$, by the equation

$$\bar{x}_{k+1} = \bar{A}_k \bar{x}_k + \bar{B}_k \bar{u}_k^*.$$

Question 2

Define a new variable, as

$\bar{x}_k = \begin{cases} \begin{bmatrix} x_k \\ u_k \end{bmatrix}^{\top} & \text{for } k < N \\ \begin{bmatrix} 0 \\ i_k \end{bmatrix}^{\top} & \text{for } k = N \end{cases}$ Then, we can re-write the formulations of the given dynamics and the quadratic cost with respect \bar{x}_k , as

$$\bar{x}_{k+1} = \bar{A}_k \bar{x}_k, \\ c(\bar{x}_k) = \frac{1}{2} \bar{x}_k^\top \bar{Q}_k \bar{x}_k + \bar{q}_k^\top \bar{x}_k + h_k,$$

where

$$\bar{A}_k = \begin{bmatrix} A_k & B_k \\ O & O \end{bmatrix}, \bar{Q}_k = \begin{bmatrix} Q_k & H \\ H^\top & R_k \end{bmatrix}, \bar{q}_k = \begin{bmatrix} q_k \\ r_k \end{bmatrix}.$$

Let J_k be the cost-to-go at k -th step. Then, J_{N-1} is given as,

$$J_{N-1} = \frac{1}{2} \bar{x}_{N-1}^\top \bar{Q}_{N-1} \bar{x}_{N-1} + \bar{q}_{N-1}^\top \bar{x}_{N-1} + h_{N-1} + J_N$$

By using the equation $\bar{x}_{k+1} = \bar{A}_k \bar{x}_k$ we can get

$$\begin{aligned} J_{N-1} &= \frac{1}{2} \bar{x}_{N-1}^\top [\bar{Q}_{N-1} A_N^\top \bar{Q}_N] \bar{x}_{N-1} + [\bar{q}_{N-1}^\top + 2d_{N-1}^\top \bar{Q}_N A_{N-1} + \bar{q}_N A_{N-1}] \bar{x}_{N-1} + h_{N-1} + h_N \\ &\quad - \bar{q}_N d_{N-1} + d_{N-1}^\top d_{N-1} \\ &= \frac{1}{2} \bar{x}_{N-1}^\top V_{N-1} \bar{x}_{N-1} + v_{N-1}^\top \bar{x}_{N-1} + w_{N-1} \end{aligned}$$

,

where

$$\begin{aligned} V_N &= \bar{Q}_{N-1} A_N^\top \bar{Q}_N, \\ v_N &= [\bar{q}_{N-1}^\top + 2d_{N-1}^\top \bar{Q}_N A_{N-1} + \bar{q}_N A_{N-1}]^\top, \\ w_N &= h_{N-1} + h_N - \bar{q}_N d_{N-1} + d_{N-1}^\top d_{N-1}. \end{aligned}$$

Likewise, by computing backward from $k = N - 1$, J_k is given as,

$$\begin{aligned} J_k &= \frac{1}{2} \bar{x}_k^\top \bar{Q}_k \bar{x}_k + \bar{q}_k^\top \bar{x}_k + h_k + J_{k+1} \\ &= \frac{1}{2} \bar{x}_k^\top [\bar{Q}_k A_{k+1}^\top \bar{Q}_{k+1}] \bar{x}_k + [\bar{q}_k^\top + 2d_k^\top \bar{Q}_{k+1} A_k + \bar{q}_{k+1} A_k] \bar{x}_k + h_k + h_{k+1} - \bar{q}_{k+1} d_k + d_k^\top d_k \\ &= \frac{1}{2} \bar{x}_k^\top V_k \bar{x}_k + v_k^\top \bar{x}_k + w_k \end{aligned}$$

,

where

$$\begin{aligned} V_k &= \bar{Q}_k A_N^\top \bar{Q}_{k+1}, \\ v_k &= [\bar{q}_k^\top + 2d_k^\top \bar{Q}_{k+1} A_k + \bar{q}_{k+1} A_k]^\top, \\ w_k &= h_k + h_{k+1} - \bar{q}_{k+1} d_k + d_k^\top d_k. \end{aligned}$$

Thus, for all $k \leq N$, the above cost-to-go can be written as,

$$c(\bar{x}_k) = \frac{1}{2} (\bar{x}_k - \bar{b}_k)^\top V_k (\bar{x}_k - \bar{b}_k) + h_k.$$

where

$$\bar{b}_k = 2(V_k + V_k^\top)^{-1} v^\top,$$

which is minimized at $\bar{x}_k = -\bar{b}_k$.

From the above results, the optimal sequence of $\{\bar{x}_k\}_{k=1}^N$ can be computed backward from $k = N$, as

$$\begin{aligned} \bar{x}_k^* &= -2(V_k + V_k^\top)^{-1} v^\top. V_k = \bar{Q}_k A_N^\top \bar{Q}_{k+1}, \\ v_k &= [\bar{q}_k^\top + 2d_k^\top \bar{Q}_{k+1} A_k + \bar{q}_{k+1} A_k]^\top, \\ w_k &= h_k + h_{k+1} - \bar{q}_{k+1} d_k + d_k^\top d_k. \end{aligned}$$

Then, the optimal control sequence u_k^* can be found at $\{\bar{x}_k^*\}_{k=1}^{N-1}$.

Question 3

The differential equation of the dynamics are given as

$$\begin{bmatrix} F \\ 0 \end{bmatrix} = \begin{bmatrix} M_t & -ml \cos \theta \\ -ml \cos \theta & J_t \end{bmatrix} \begin{bmatrix} \ddot{q} \\ \ddot{\theta} \end{bmatrix} + \begin{bmatrix} c & 0 \\ 0 & \gamma \end{bmatrix} \begin{bmatrix} \dot{q} \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} ml\theta^2 \sin \theta \\ -mgl \sin \theta \end{bmatrix}.$$

We can linearize the equation as,

$$\begin{bmatrix} F \\ 0 \end{bmatrix} \approx \begin{bmatrix} M_t & -ml \cos \theta \\ -ml \cos \theta & J_t \end{bmatrix} \begin{bmatrix} \ddot{q} \\ \ddot{\theta} \end{bmatrix} + \begin{bmatrix} c & 0 \\ 0 & \gamma \end{bmatrix} \begin{bmatrix} \dot{q} \\ \dot{\theta} \end{bmatrix} + \dot{\theta} \begin{bmatrix} ml(2\theta \sin \theta + \theta^2 \cos \theta) \\ -mgl \cos \theta \end{bmatrix} \quad (6)$$

$$= C(q, \theta) \begin{bmatrix} \ddot{q} \\ \ddot{\theta} \end{bmatrix} + D(\theta) \begin{bmatrix} \dot{q} \\ \dot{\theta} \end{bmatrix} \quad (7)$$

where

$$C(q, \theta) = \begin{bmatrix} M_t & -ml \cos \theta \\ -ml \cos \theta & J_t \end{bmatrix}, D(\theta) = \begin{bmatrix} c & ml(2\theta \sin \theta + \theta^2 \cos \theta) \\ 0 & \gamma - mgl \cos \theta \end{bmatrix}.$$

Define the states of the discrete-time system at t_k as $x_t = [q(t_k), \theta(t_k), \dot{q}(t_k), \dot{\theta}(t_k)]^\top$ and the control inputs $u_k = [F_k, 0, 0, 0]^\top$.

Then, by using the linearized equation derived above, the dynamics of x_t is linearized as,

$$x_{k+1} \approx A_k x_k + B_k u_k,$$

where

$$A_k = \begin{bmatrix} I & \delta t I \\ O & -\Delta t C_k^{-1}(q_k, \theta) D(\theta_k) \end{bmatrix}, B_k = \begin{bmatrix} O & O \\ \Delta t C_k^{-1} & O \end{bmatrix}.$$

Here, I and O are the unit, and zero matrices, respectively, and Δt is the time step.

We can also apply the below quadratic cost. Here Q_k , R_k and P_N are positive semi-definite.

$$J = \frac{1}{2} \sum_{k=0}^{N-1} x_k^\top Q_k x_k + \frac{1}{2} u_k^\top R_k u_k + \frac{1}{2} x_N^\top P_N x_N$$

With the above formulations, we can control the cart-pole system. The code are presented below.

```
In [23]: import numpy as np
import scipy as sp
import cvxpy as cp

# Parameters
DYNAMIC_PARAMETERS = {
    'Gravity': -9.8,
    'Cart mass': 10,
    'Cart inertia': 100,
    'Pendulum mass': 80,
    'Pole length': 1.0,
    'Viscosity': 0.1,
    'Damping': 0.01,
    'Time step': 0.05
}
```

```

N = 100

MAT_R = 0.1*np.eye(4)
MAT_Q = np.eye(4)
MAT_Q[:2, :2] = 100*np.eye(2)

```

In this simulation, we set up a consistent time step $\Delta t = 0.1\text{sec}$, and used a finite time horizon $N = 100$ (in simulation time, 10sec). For the quadratic cost, we used positive definite diagonal matrices.

```

In [19]: # Discrete LQR
def solve_dlqr(A,B,Q,R):

    X = np.array(sp.linalg.solve_discrete_are(A, B, Q, R))
    K = np.linalg.inv(B.T@X@B+R) @ (B.T@X@A)
    eig_vals, eig_vecs = np.linalg.eig(A-B@K)

    return K, X, eig_vals

```

In `solve_dlqr` function, we solve the LQR of the discrete-time system of

$$x_{k+1} = Ax_k + Bu_k,$$

$$Cost = \sum_{k=1}^{N-1} (x_k^\top Q x_k + u_k^\top R u_k) + x_N^\top Q x_N.$$

A, B, Q, R are given as the inputs of the function.

```

In [28]: # Define the cart-pole dynamics
class CartPole(object):

    def __init__(self, parameters):

        self._dt = parameters['Time step']
        self._c = parameters['Viscosity']
        self._r = parameters['Damping']
        self._l = parameters['Pole length']
        self._m = parameters['Pendulum mass']
        self._g = parameters['Gravity']
        self._M_t = parameters['Cart mass'] + parameters['Pendulum mass']
        self._J_t = parameters['Cart inertia'] + (self._m * self._l**2)

    def reset(self, init_state):
        # state = [Cart pos, Pendulum ang, Cart vel, Pendulum angvl]

        self._state = np.array(init_state)

    def _get_mat_C(self, state):

        theta = state[1]
        mat_C = np.array([[self._M_t, - self._m * self._l * np.cos(theta)],
                          [- self._m * self._l * np.cos(theta), self._J_t]])

        return mat_C

    def _get_mat_D(self, state):

```

```

        theta = state[1]
        mat_D = np.array([[self._c, self._m * self._l * (2 * theta * np.sin(theta) + (t
                                [0, self._r - self._m * self._g * np.cos(theta)])])

    return mat_D

def linearize(self, state):

    mat_C = self._get_mat_C(state)
    mat_D = self._get_mat_D(state)
    mat_inv_C = np.linalg.inv(mat_C)

    mat_A = np.zeros((4, 4))
    mat_A[:2, :2] = np.eye(2)
    mat_A[:2, 2:] = self._dt * np.eye(2)
    mat_A[2:, 2:] = self._dt * mat_inv_C @ mat_D

    mat_B = np.zeros((4, 4))
    mat_B[:2, 2:] = self._dt * mat_inv_C

    return mat_A, mat_B

def step(self, u):

    mat_C = self._get_mat_C(self._state)
    mat_inv_C = np.linalg.inv(mat_C)

    dq = self._state[2]
    dtheta = self._state[3]
    theta = self._state[1]

    vec_nonlin = - self._m * self._l * np.sin(theta) * np.array([theta**2, - self._
    vec_lin = - np.array([self._c * dq, self._r * dtheta])
    vec_ctrl = np.array(u[2:])

    self._state[:2] += self._dt * self._state[2:]
    self._state[2:] += self._dt * mat_inv_C @ (vec_ctrl + vec_lin + vec_nonlin)

    return np.copy(self._state)

@property
def state(self):

    return np.copy(self._state)

```

In `CartPole`, we define the cart-pole system. Every simulation, `reset` initiate the system with the given initial states. For computing iLQR, `linearize` computes the linearized dynamic matrices. For evaluation, `step` computes the forward dynamics.

```
In [56]: target_state = np.array([0,0.5,0,0.0])
```

```

env = CartPole(DYNAMIC_PARAMETERS)
env.reset(init_state)
A, B = env.linearize(target_state)
K,_,_ = solve_dlqr(A,B,MAT_Q,MAT_R)

print("K", K)

```

```

print("A", A)
print("B", B)

init_state = np.array([0, 10./180.*np.pi, 0., 0.])

U = cp.Variable((N, 4))
X = cp.Variable((N+1,4))

control = np.zeros((N, 4))
states = np.zeros((N+1,4))

for attempt in range(100):

    const = []
    const.append( X[0,:] == np.zeros((4)))

    env.reset(init_state)
    states[0,:] = env.state

    for i in range(N):
        A, B = env.linearize(env.state)
        env.step(control[i])
        states[i+1,:] = env.state
        const.append( X[i+1,:] == A @ X[i,:] + B @ U[i,:] )

    X_p = X + states
    U_p = U + control

    cost = 100*cp.sum((X_p[:,0] - target_state[0])**2) + \
          100*cp.sum((X_p[:,1] - target_state[1])**2) + \
          1*cp.sum((X_p[:,2] - target_state[2])**2) + \
          1*cp.sum((X_p[:,3] - target_state[3])**2) + \
          0.1* cp.sum((U_p[:,2]
                      )**2)

    prob = cp.Problem(cp.Minimize(cost), const)
    prob.solve()

    print(attempt)
    for a,b in zip(U.value+control, X.value+states):
        print("angle", b[1], "vel", b[1], "act", a[2])
    control += U.value

```

K [[0.00000000e+00 0.00000000e+00 0.00000000e+00 0.00000000e+00]
[0.00000000e+00 0.00000000e+00 0.00000000e+00 0.00000000e+00]
[3.12264267e+01 -1.54249067e-01 1.56145841e+00 5.31834070e-01]
[-1.54249067e-01 3.14241633e+01 -7.64682592e-03 2.19783423e+00]]

A [[1.00000000e+00 0.00000000e+00 5.00000000e-02 0.00000000e+00]
[0.00000000e+00 1.00000000e+00 0.00000000e+00 5.00000000e-02]
[0.00000000e+00 0.00000000e+00 7.98507138e-05 2.58927506e-01]
[0.00000000e+00 0.00000000e+00 3.11447084e-05 2.92111986e-01]]

B [[0. 0. 0.00079851 0.00031145]
[0. 0. 0.00031145 0.00039925]
[0. 0. 0. 0.]
[0. 0. 0. 0.]]

0

angle 0.17453292468499115 vel 0.17453292468499115 act -5.829039422084705
angle 0.3604030658856764 vel 0.3604030658856764 act -5.740445395933394
angle 0.3646983113004555 vel 0.3646983113004555 act -5.65154106559572
angle 0.36870290012573353 vel 0.36870290012573353 act -5.562443443601401
angle 0.3722439926450606 vel 0.3722439926450606 act -5.473350148390723
angle 0.3751778610433935 vel 0.3751778610433935 act -5.38452418392933
angle 0.37740018224381056 vel 0.37740018224381056 act -5.296274450761857
angle 0.3788541212386233 vel 0.3788541212386233 act -5.208933582431083
angle 0.37953500435741666 vel 0.37953500435741666 act -5.122834424467315
angle 0.3794907208240517 vel 0.3794907208240517 act -5.038286218901435
angle 0.3788184789174676 vel 0.3788184789174676 act -4.955552034485579
angle 0.3776597143291267 vel 0.3776597143291267 act -4.874829968054945
angle 0.37618938906550475 vel 0.37618938906550475 act -4.79623792280449
angle 0.3746049022478797 vel 0.3746049022478797 act -4.719804445831617
angle 0.37311158958061996 vel 0.37311158958061996 act -4.6454653847777365
angle 0.37190738605611257 vel 0.37190738605611257 act -4.57306670081976
angle 0.3711703293674813 vel 0.3711703293674813 act -4.502374903263605
angle 0.37104291400991446 vel 0.37104291400991446 act -4.433091609384823
angle 0.3716234587628824 vel 0.3716234587628824 act -4.364873968132962
angle 0.37295724571046873 vel 0.37295724571046873 act -4.297357232670627
angle 0.37503456079267006 vel 0.37503456079267006 act -4.230179643878591
angle 0.3777902119774554 vel 0.3777902119774554 act -4.163006137575587
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angle 0.3848366854621776 vel 0.3848366854621776 act -4.02759481326438
angle 0.3887880879526001 vel 0.3887880879526001 act -3.9590033194776537
angle 0.39276458269100717 vel 0.39276458269100717 act -3.8897320391878947
angle 0.39656662440260776 vel 0.39656662440260776 act -3.8198315130871388
angle 0.4000090314508007 vel 0.4000090314508007 act -3.7494439236803228
angle 0.4029338376013303 vel 0.4029338376013303 act -3.6787940178886975
angle 0.4052205956648739 vel 0.4052205956648739 act -3.6081741632805837
angle 0.40679358913466657 vel 0.40679358913466657 act -3.537924293303992
angle 0.4076266265591841 vel 0.4076266265591841 act -3.468408525643293
angle 0.4077431724696559 vel 0.4077431724696559 act -3.399989191159889
angle 0.40721305178069034 vel 0.40721305178069034 act -3.33299995499916
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angle 0.40468948819609285 vel 0.40468948819609285 act -3.204354760947998
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angle 0.39839643095044397 vel 0.39839643095044397 act -2.970698339752156
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angle 0.3972992985751173 vel 0.3972992985751173 act -2.863469395170207
angle 0.39768720489414716 vel 0.39768720489414716 act -2.8111487129007973
angle 0.3987594146425893 vel 0.3987594146425893 act -2.7591731105606527
angle 0.4005014724426812 vel 0.4005014724426812 act -2.7071713888982685
angle 0.4028514294442844 vel 0.4028514294442844 act -2.654817797481824
angle 0.40570330717273345 vel 0.40570330717273345 act -2.601853677355404
angle 0.4089133406411683 vel 0.4089133406411683 act -2.548102616655366
angle 0.4123105288601387 vel 0.4123105288601387 act -2.4934791856323217

angle 0.41570821663755103 vel 0.41570821663755103 act -2.437990344984219
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angle 0.4267151278244511 vel 0.4267151278244511 act -2.1531664847529006
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angle 0.42640926313709726 vel 0.42640926313709726 act -2.040618883135048
angle 0.42524223033166686 vel 0.42524223033166686 act -1.9857158866158708
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angle 0.42147153921898284 vel 0.42147153921898284 act -1.879543344565329
angle 0.4192120135020778 vel 0.4192120135020778 act -1.8284344691625638
angle 0.416964336808442 vel 0.416964336808442 act -1.7786301860879687
angle 0.4149262761629203 vel 0.4149262761629203 act -1.7300319870884977
angle 0.4132777330070129 vel 0.4132777330070129 act -1.6824793736176888
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angle 0.41636680692900757 vel 0.41636680692900757 act -1.405900774927606
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angle 0.43294195267085567 vel 0.43294195267085567 act -0.9133830266907946
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5

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43

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46
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84
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