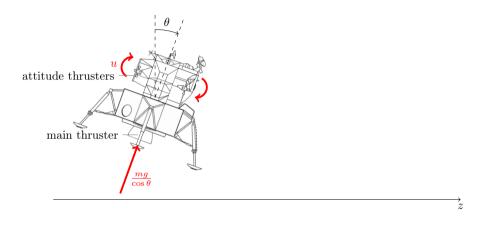
State feedback with observer

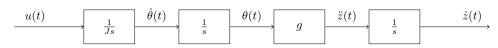
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October 18, 2022

State feedback with reconstructed states

State feedback with reconstructed states





State feedback

Given

$$\dot{x} = Ax + Bu
y = Cx$$
(1)

and measurements (or estimates) of the state vector x.

Linear state feedback is the control law

$$u = f((x, u_c)) = -l_1x_1 - l_2x_2 - \dots - l_nx_n + l_0u_c$$

= $-Lx + l_0u_c$,

where

$$L = \begin{bmatrix} I_1 & I_2 & \cdots & I_n \end{bmatrix}.$$

Substituting the control law in the state space model (5) gives

$$\dot{x} = (A - BL)x + l_0Br$$

$$v(k) = Cx$$
(2)

Observer design

Given model

$$\dot{x} = Ax + Bu$$
$$y = Cx$$

and measurements of the output signal y.

The observer is given by

$$\dot{\hat{x}} = \underbrace{A\hat{x} + Bu}_{\text{simulation}} + \underbrace{K(y - C\hat{x})}_{\text{correction}} = (A - KC)\hat{x} + Bu + Ky$$

with poles given by the eigenvalues of the matrix $A_o = A - KC$

Rule-of-thumb Choose the poles of the observer (eigenvalues of A - KC) at least twice as fast as the poles (eigenvalues) of A - BL.

Control by feedback from reconstructed states

The design problem can be separated into two problems

1. Determine the gain vector L and the gain l_0 of the control law

$$u = -L\hat{x} + I_0 r$$

so that the closed-loop system has good reference tracking.

2. Determine the gain vector **K** of the observer

$$\dot{\hat{x}} = A\hat{x} + Bu + \frac{K}{K}(y - C\hat{x})$$

to get a good balance between disturbance rejection and noise attenuation.

Computing the observer gain

A matrix M and its transpose M^{T} have the same eigenvalues. Hence, the problem of determining the gain K to obtain desired eigenvalues of

$$A - KC$$

is equivalent to determining the gain K in

$$(A - KC)^{\mathrm{T}} = A^{\mathrm{T}} - C^{\mathrm{T}}K^{\mathrm{T}}.$$

The last problem has the exact same form as the problem of determining L to obtain desired eigenvalues of

$$A - BL$$

So, the same matlab function can be used for both problems.

Computing the state feedback and observer gains

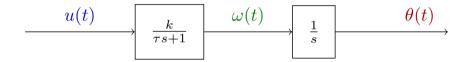
1. Ackerman's method

```
L = acker(A, B, pd)
K = acker(A', C', po)'
```

2. More numerically stable method

```
L = place(A, B, pd)
K = place(A', C', po)'
```

Example - Position control of the DC motor



State-space model with physical states



State variables corresponding to physical signals:

$$x = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} \omega \\ \theta \end{bmatrix}$$

With dynamics

$$\tau \dot{\omega} = -\omega + ku$$
$$\dot{\theta} = \omega$$

State-space model with physical states



State variables corresponding to physical signals:

$$x = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} \omega \\ \theta \end{bmatrix}$$

With dynamics

$$\tau \dot{\omega} = -\omega + \mathbf{k}\mathbf{u}$$
$$\dot{\theta} = \omega$$

Activity Fill the matrix A and vectors B and C.

$$\dot{x} = \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \underbrace{\begin{bmatrix} \\ \\ A \end{bmatrix}} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \underbrace{\begin{bmatrix} \\ \\ \\ B \end{bmatrix}} u$$

$$y = \theta = \underbrace{\left[\begin{array}{c} x_1 \\ x_2 \end{array}\right]} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

State-space model with physical states



State variables corresponding to physical signals:

$$x = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} \omega \\ \theta \end{bmatrix}$$

With dynamics

$$\tau \dot{\omega} = -\omega + ku$$
$$\dot{\theta} = \omega$$

Activity Fill the matrix A and vectors B and C.

$$\dot{x} = \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \underbrace{\begin{bmatrix} -\frac{1}{\tau} & 0 \\ 1 & 0 \end{bmatrix}}_{A} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \underbrace{\begin{bmatrix} \frac{k}{\tau} \\ 0 \end{bmatrix}}_{B} u$$

$$y = \theta = \underbrace{\begin{bmatrix} 0 & 1 \end{bmatrix}}_{C} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

State-space model on controllable canonical form

The system with transfer function

$$G(s) = \frac{b_1 s^{n-1} + \dots + b_{n-1} s + b_n}{s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n}$$

can be represented on state-space form as

$$\dot{x} = \begin{bmatrix} -a_1 & -a_2 & \cdots & -a_{n-1} & -a_n \\ 1 & 0 & \cdots & 0 & 0 \\ 0 & 1 & \cdots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \cdots & 1 & 0 \end{bmatrix} x + \begin{bmatrix} 1 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix} u$$

$$y = \begin{bmatrix} b_1 & b_2 & \cdots & b_n \end{bmatrix} x$$

$$\underbrace{ \begin{array}{c} u(t) \\ \hline \\ \tau s+1 \end{array} } \underbrace{ \begin{array}{c} \omega(t) \\ \hline \\ \hline \\ \end{array} } \underbrace{ \begin{array}{c} \frac{1}{s} \\ \hline \end{array} } \underbrace{ \begin{array}{c} \theta(t) \\ \hline \\ \end{array} }$$

$$G(s) = \frac{rac{k}{ au}}{s(s+rac{1}{ au})}$$

State-space model on controllable canonical form

The system with transfer function

$$G(s) = \frac{b_1 s^{n-1} + \dots + b_{n-1} s + b_n}{s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n}$$

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$$y = \begin{bmatrix} b_1 & b_2 & \cdots & b_n \end{bmatrix} x$$

Activity Determine the state-space model of the DC motor on controllable canonical form

$$\underbrace{ \begin{array}{c} u(t) \\ \hline \\ \tau s+1 \end{array} } \underbrace{ \begin{array}{c} \omega(t) \\ \hline \\ \hline \\ \end{array} } \underbrace{ \begin{array}{c} \frac{1}{s} \\ \hline \end{array} } \underbrace{ \begin{array}{c} \theta(t) \\ \hline \end{array} }$$

$$G(s) = \frac{\frac{k}{\tau}}{s(s + \frac{1}{\tau})}$$

State-space model on observable canonical form

The system with transfer function

$$G(s) = \frac{b_1 s^{n-1} + \dots + b_{n-1} s + b_n}{s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n}$$

can be represented on state-space form as

$$\dot{x} = \begin{bmatrix} -a_1 & 1 & 0 & \cdots & 0 \\ -a_2 & 0 & 1 & \cdots & 0 \\ -a_3 & 0 & 0 & \cdots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ -a_n & 0 & 0 & \cdots & 0 \end{bmatrix} x + \begin{bmatrix} b_1 \\ b_2 \\ b_3 \\ \vdots \\ b_n \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 & \cdots & 0 \end{bmatrix} x$$

$$\begin{array}{c|c} u(t) & \hline \\ \frac{k}{\tau s+1} & \omega(t) & \hline \\ \frac{1}{s} & \end{array}$$

$$G(s) = \frac{rac{k}{ au}}{s(s+rac{1}{ au})}$$

State-space model on observable canonical form

The system with transfer function

$$G(s) = \frac{b_1 s^{n-1} + \dots + b_{n-1} s + b_n}{s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n}$$

can be represented on state-space form as

$$\dot{x} = \begin{bmatrix} -a_1 & 1 & 0 & \cdots & 0 \\ -a_2 & 0 & 1 & \cdots & 0 \\ -a_3 & 0 & 0 & \cdots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ -a_n & 0 & 0 & \cdots & 0 \end{bmatrix} x + \begin{bmatrix} b_1 \\ b_2 \\ b_3 \\ \vdots \\ b_n \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 & \cdots & 0 \end{bmatrix} x$$

Activity Determine the state-space model of the DC motor on observable canonical form

$$G(s) = \frac{\frac{k}{\tau}}{s(s + \frac{1}{\tau})}$$

$$\dot{x} = \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \underbrace{\begin{bmatrix} -\frac{1}{\tau} & 0 \\ 1 & 0 \end{bmatrix}}_{A} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \underbrace{\begin{bmatrix} \frac{K}{\tau} \\ 0 \end{bmatrix}}_{B} u$$

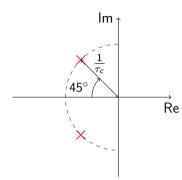
Feedback $u = -Lx + l_0r$ gives closed-loop system

$$\dot{x} = (A - BL)x + l_0Br$$

$$= \begin{bmatrix} -\frac{1}{\tau} - l_1\frac{k}{\tau} & -l_2\frac{k}{\tau} \\ 1 & 0 \end{bmatrix} x + l_0Br$$

with characteristic polynomial

$$s^2 + (\frac{1}{\tau} + \frac{1}{1}\frac{k}{\tau})s + \frac{1}{2}\frac{k}{\tau}$$



Desired closed-loop characteristic polynomial

$$(s-p_1)(s-p_2) = s^2 + rac{\sqrt{2}}{ au_c} s + rac{1}{ au_c^2}$$

Characteristic polynomial obtained with state feedback

$$s^2 + (\frac{1}{\tau} + \frac{1}{1}\frac{k}{\tau})s + \frac{1}{2}\frac{k}{\tau}$$

Desired characteristic polynomial

$$s^2 + \frac{\sqrt{2}}{\tau_c}s + \frac{1}{\tau_c^2}$$

Characteristic polynomial obtained with state feedback

$$s^2 + (\frac{1}{\tau} + \frac{1}{\tau})s + \frac{k}{\tau}$$

Desired characteristic polynomial

$$s^2 + \frac{\sqrt{2}}{\tau_c}s + \frac{1}{\tau_c^2}$$

Activity Determine the feedback gains!

Characteristic polynomial obtained with state feedback

$$s^2 + (\frac{1}{\tau} + \frac{1}{\tau})s + \frac{k}{\tau}$$

Desired characteristic polynomial

$$s^2 + \frac{\sqrt{2}}{\tau_c}s + \frac{1}{\tau_c^2}$$

Activity Determine the feedback gains!

Solution

Characteristic polynomial obtained with state feedback

$$s^2 + (\frac{1}{\tau} + \frac{1}{\tau})s + \frac{k}{\tau}$$

Desired characteristic polynomial

$$s^2 + \frac{\sqrt{2}}{\tau_c}s + \frac{1}{\tau_c^2}$$

Activity Determine the feedback gains!

Solution

$$I_1 = \frac{\tau}{k} \left(\frac{\sqrt{2}}{\tau_c} - \frac{1}{\tau} \right) = \frac{\sqrt{2}\tau - \tau_c}{k\tau_c}$$

$$I_2 = \frac{\tau}{k\tau_c^2}$$

The observer is given by

$$\dot{\hat{x}} = \underbrace{A\hat{x} + Bu}_{\text{simulation}} + \underbrace{\frac{K(y - C\hat{x})}{\text{correction}}}$$

$$= (A - KC)\hat{x} + Bu + Ky$$

$$= \begin{bmatrix} -\frac{1}{\tau} & -k_1 \\ 1 & -k_2 \end{bmatrix} \hat{x} + Bu + Ky$$

with poles given by the eigenvalues of the matrix $A_o = A - \frac{K}{K}C$, which has characteristic polynomial

$$\det \begin{pmatrix} \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} -\frac{1}{\tau} & -k_1 \\ 1 & -k_2 \end{bmatrix} \end{pmatrix}$$
$$= s^2 + (\frac{1}{\tau} + k_2)s + (k_1 + \frac{k_2}{\tau})$$

The observer is given by

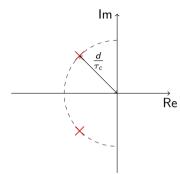
$$\dot{\hat{x}} = \underbrace{A\hat{x} + Bu}_{\text{simulation}} + \underbrace{K(y - C\hat{x})}_{\text{correction}}$$

$$= (A - KC)\hat{x} + Bu + Ky$$

$$= \begin{bmatrix} -\frac{1}{\tau} & -k_1 \\ 1 & -k_2 \end{bmatrix} \hat{x} + Bu + Ky$$

with poles given by the eigenvalues of the matrix $A_o = A - KC$, which has characteristic polynomial

$$\det \begin{pmatrix} \begin{bmatrix} s & 0 \\ 0 & s \end{bmatrix} - \begin{bmatrix} -\frac{1}{\tau} & -k_1 \\ 1 & -k_2 \end{bmatrix} \end{pmatrix}$$
$$= s^2 + (\frac{1}{\tau} + k_2)s + (k_1 + \frac{k_2}{\tau})$$



Choose *d* between 2 and 10 and obtain desired closed-loop characteristic polynomial

$$(s - p_{o,1})(s - p_{o,2}) = s^2 + \frac{d\sqrt{2}}{\tau_c}s + \frac{d^2}{\tau_c^2}$$

Characteristic polynomial of the observer

$$s^2 + (\frac{1}{\tau} + k_2)s + (k_1 + \frac{k_2}{\tau})$$

Desired characteristic polynomial

$$s^2 + \frac{\sqrt{2}d}{\tau_c}s + \frac{d^2}{\tau_c^2}$$

Characteristic polynomial of the observer

$$s^2 + (\frac{1}{\tau} + k_2)s + (k_1 + \frac{k_2}{\tau})$$

Desired characteristic polynomial

$$s^2 + \frac{\sqrt{2}d}{\tau_c}s + \frac{d^2}{\tau_c^2}$$

Activity Determine the observer gains!

Characteristic polynomial of the observer

$$s^2 + (\frac{1}{\tau} + k_2)s + (k_1 + \frac{k_2}{\tau})$$

Desired characteristic polynomial

$$s^2 + \frac{\sqrt{2}d}{\tau_c}s + \frac{d^2}{\tau_c^2}$$

Activity Determine the observer gains!

Solution

Characteristic polynomial of the observer

$$s^2 + (\frac{1}{\tau} + k_2)s + (k_1 + \frac{k_2}{\tau})$$

Desired characteristic polynomial

$$s^2 + \frac{\sqrt{2}d}{\tau_c}s + \frac{d^2}{\tau_c^2}$$

Activity Determine the observer gains!

Solution

$$k_1 = \frac{d^2}{\tau_c^2} - \frac{\sqrt{2}d}{\tau_c\tau} + \frac{1}{\tau^2}$$
$$k_2 = \frac{\sqrt{2}d}{\tau_c} - \frac{1}{\tau}$$