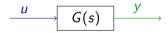
Frequency response

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Response of LTI systems to sinusoids



Let $u(t) = \sin \omega_1 t$. Then, after transients have died out,

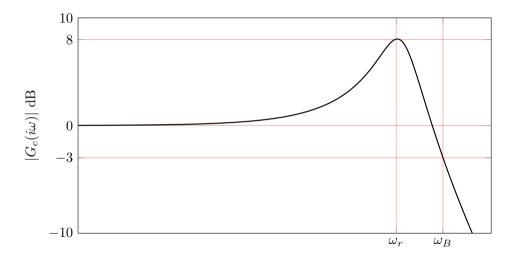
$$y(t) = |G(\omega_1)| \sin (\omega_1 t + \arg G(i\omega_1)).$$

The Bode diagram

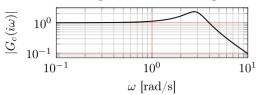
$$y(t) = \underbrace{|G(i\omega_1)|}_{\text{amplification}} \sin\left(\omega_1 t + \underbrace{\arg G(i\omega_1)}_{\text{phase shift}}\right)$$

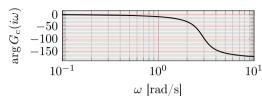
The Bode diagram shows the magnitude and phase of the transfer function evaluated on the positive imaginary axis. It thus contains all information about the steady-state response of the system to input signals of different frequency.

Specifications on the frequency properties of the closed-loop system

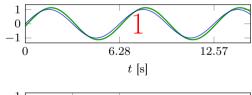


Exercise: Reading the Bode diagram





which of the below responses is not compatible with the Bode diagram?

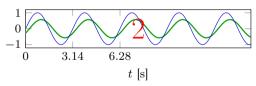


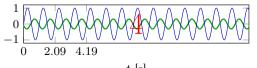
6.28

t [s]

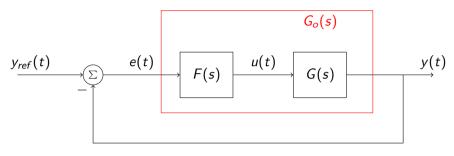
3.14





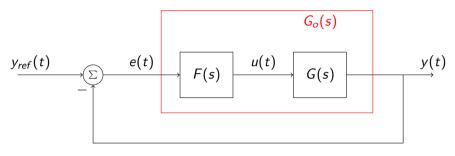


From loop gain to closed-loop gain



$$G_c(i\omega) = rac{G(i\omega)F(i\omega)}{1+G(i\omega)F(i\omega)} = rac{G_o(i\omega)}{1+G_o(i\omega)}$$
 $|G_c(i\omega)| = rac{|G_o(i\omega)|}{|1+G_o(i\omega)|} = rac{|G_o(i\omega)|}{|G_o(i\omega)-(-1)|}$

From loop gain to closed-loop gain



$$G_c(i\omega) = \frac{G(i\omega)F(i\omega)}{1 + G(i\omega)F(i\omega)} = \frac{G_o(i\omega)}{1 + G_o(i\omega)}$$
$$|G_c(i\omega)| = \frac{|G_o(i\omega)|}{|1 + G_o(i\omega)|} = \frac{|G_o(i\omega)|}{|G_o(i\omega) - (-1)|}$$

Keep the loop gain $G_o(i\omega)$ away from -1!



If the phase shift is π

$$G_o(i\omega_1) = -1$$
, $|G_o(i\omega_1)| = 1$, $\arg G_o(i\omega_1) = -\pi$

$$u(t) = \frac{\sin(\omega_1 t)}{G_o(s)}$$

$$y(t) = \sin(\omega_1 t - \pi) = -\sin(\omega_1 t)$$

If the phase shift is π

$$G_o(i\omega_1) = -1$$
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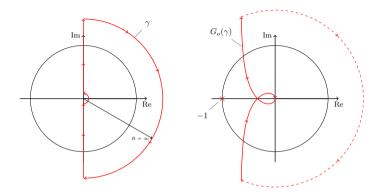
$$y(t) = \sin(\omega_1 t - \pi) = -\sin(\omega_1 t)$$

Closed-loop transfer function: $G_c(s) = \frac{G_o(s)}{1 + G_o(s)}$ We want

$$1 + G_o(i\omega) \neq 0, \quad \forall \omega$$

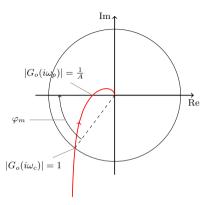
If not, then the closed-loop system will have poles on the imaginary axis (in the s-domain).

The simplified Nyquist criterion in the s-plane



If the open-loop system (the loop gain) is not unstable, i.e. $G_o(s)$ has no poles in the right-half plane, then the closed-loop system will be stable if the Nyquist curve **do not** encircle the point s=-1. The point s=-1 should stay on the left side of the Nyquist curve when we go along the curve from low to high frequencies.

Stability margins

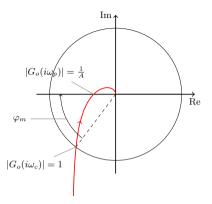


- ► Cross-over frequency: The frequency ω_c for which $|G_o(i\omega)| = 1$.
- Phase margin: The angle φ_m to the negative real axis for the point where the Nyquist curve intersects the unit circle.

$$\varphi_m = \arg G_o(i\omega_c) - (-180^\circ) = \arg G_o(i\omega_c) + 180^\circ$$



Stability margins



- **•** phase-cross-over frequency: The frequency ω_p for which arg $G_o(i\omega) = -180^\circ$.
- ▶ Gain margin: The gain K = A that would make the Nyquist curve of $KG_o(i\omega h)$ go through the point -1 + i0. This means that

$$|G_o(i\omega_p h)| = \frac{1}{A}.$$

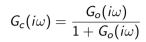


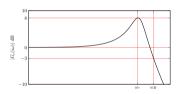
How to achieve the frequency-domain specifications

$$G_c(i\omega) = rac{G_o(i\omega)}{1 + G_o(i\omega)}$$

Activity If $Go(i\omega) = -0.5$ what is $|G_c(i\omega)|$? If $Go(i\omega) = -i$ what is $|G_c(i\omega)|$?

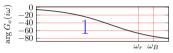
How to achieve the frequency-domain specifications





Which of the Bode plots to the right shows the correct loop gain $G_o(i\omega)$?











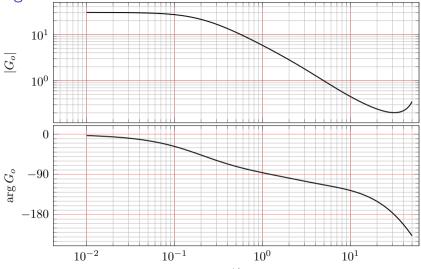






How to achieve the frequency-domain specifications

Stability margins excercise



Activity Determine the cross-over frequency ω_c , the phase cross-over frequency $\omega_{\bar{p}}$, the