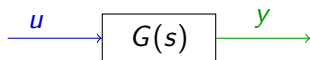


Frequency response

Kjartan Halvorsen

September 29, 2022

Response of LTI systems to sinusoids



Let $u(t) = \sin \omega_1 t$. Then, after transients have died out,

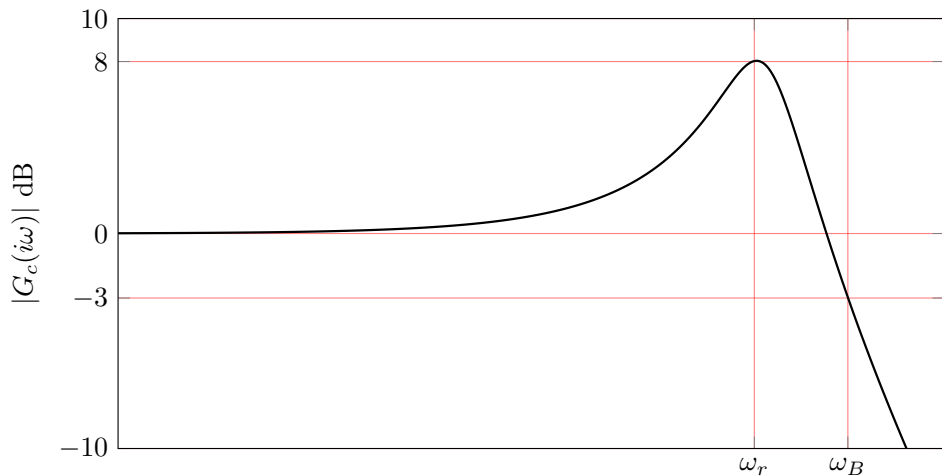
$$y(t) = |G(\omega_1)| \sin(\omega_1 t + \arg G(i\omega_1)).$$

The Bode diagram

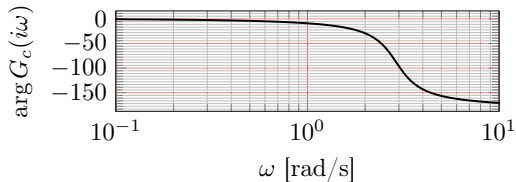
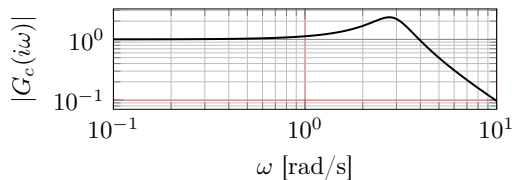
$$y(t) = \underbrace{|G(i\omega_1)|}_{\text{amplification}} \sin(\omega_1 t + \underbrace{\arg G(i\omega_1)}_{\text{phase shift}})$$

The Bode diagram shows the **magnitude** and **phase** of the transfer function evaluated on the positive imaginary axis. It thus contains all information about the steady-state response of the system to input signals of different frequency.

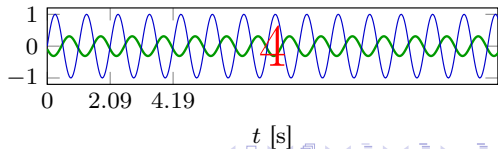
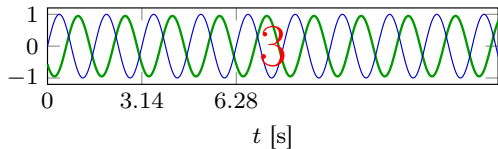
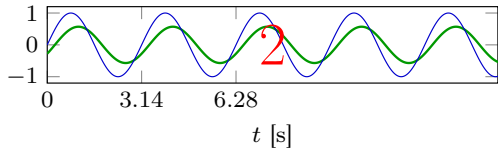
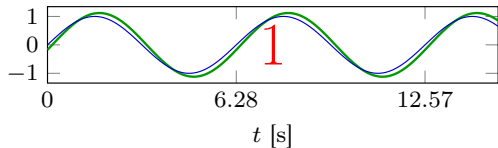
Specifications on the frequency properties of the closed-loop system



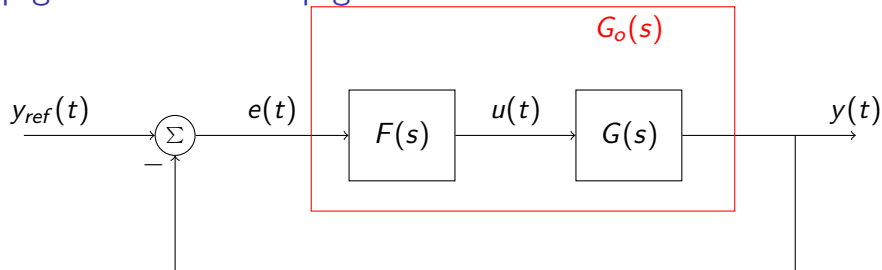
Exercise: Reading the Bode diagram



which of the below responses **is not** compatible with the Bode diagram?

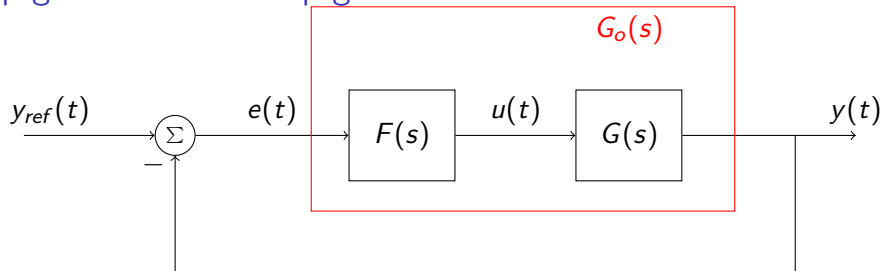


From loop gain to closed-loop gain



$$G_c(i\omega) = \frac{G(i\omega)F(i\omega)}{1 + G(i\omega)F(i\omega)} = \frac{G_o(i\omega)}{1 + G_o(i\omega)}$$

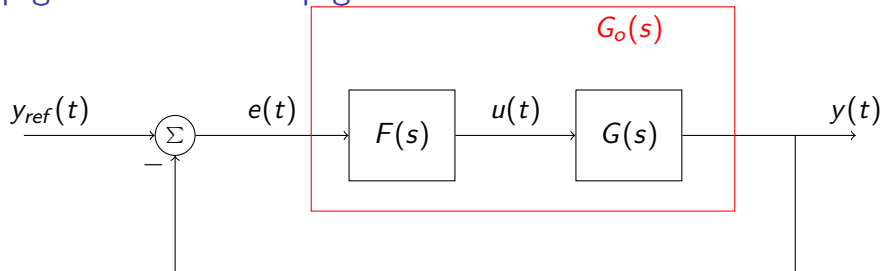
From loop gain to closed-loop gain



$$G_c(i\omega) = \frac{G(i\omega)F(i\omega)}{1 + G(i\omega)F(i\omega)} = \frac{G_o(i\omega)}{1 + G_o(i\omega)}$$

$$|G_c(i\omega)| = \frac{|G_o(i\omega)|}{|1 + G_o(i\omega)|} = \frac{|G_o(i\omega)|}{|G_o(i\omega) - (-1)|}$$

From loop gain to closed-loop gain



$$G_c(i\omega) = \frac{G(i\omega)F(i\omega)}{1 + G(i\omega)F(i\omega)} = \frac{G_o(i\omega)}{1 + G_o(i\omega)}$$

$$|G_c(i\omega)| = \frac{|G_o(i\omega)|}{|1 + G_o(i\omega)|} = \frac{|G_o(i\omega)|}{|G_o(i\omega) - (-1)|}$$

Keep the loop gain $G_o(i\omega)$ away from -1!

If $G_o(i\omega_1) = -1$

$$G_o(i\omega_1) = -1, \quad |G_o(i\omega_1)| = 1, \quad \arg G_o(i\omega_1) = -\pi$$

$$u(t) = \sin(\omega_1 t)$$



If $G_o(i\omega_1) = -1$

$$G_o(i\omega_1) = -1, \quad |G_o(i\omega_1)| = 1, \quad \arg G_o(i\omega_1) = -\pi$$

$$u(t) = \sin(\omega_1 t)$$



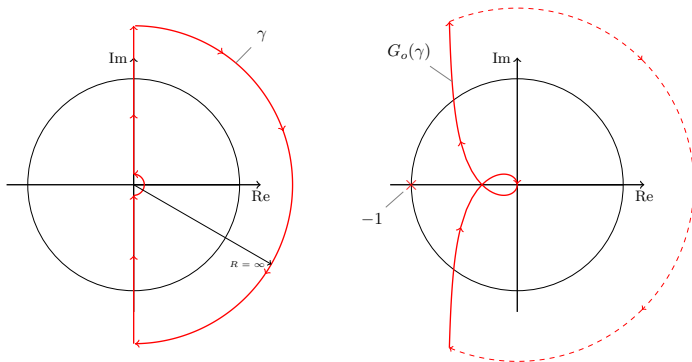
Closed-loop transfer function: $G_c(s) = \frac{G_o(s)}{1+G_o(s)}$ We want

$$1 + G_o(i\omega) \neq 0, \quad \forall \omega$$

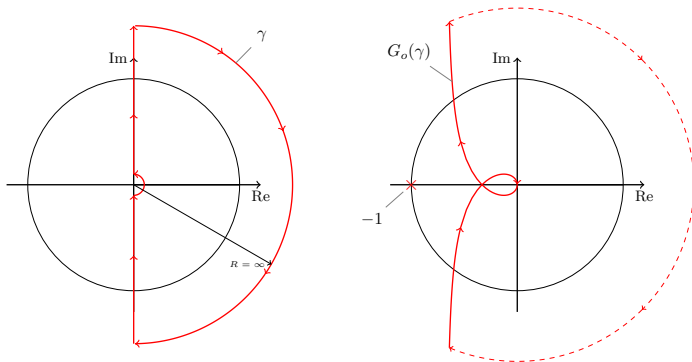
If not, then the closed-loop system will have poles on the imaginary axis (in the s-domain).

The simplified Nyquist criterion in the s-plane

The simplified Nyquist criterion in the s-plane

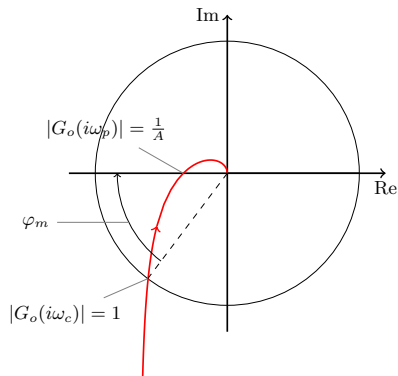


The simplified Nyquist criterion in the s-plane



If the open-loop system (the loop gain) is not unstable, i.e. $G_o(s)$ has no poles in the right-half plane, then the closed-loop system will be stable if the Nyquist curve **do not encircle the point** $s = -1$. The point $s = -1$ should stay on the left side of the Nyquist curve when we go along the curve from low to high frequencies.

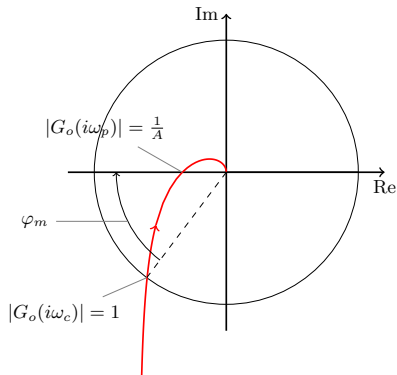
Stability margins



- ▶ Cross-over frequency: The frequency ω_c for which $|G_o(i\omega)| = 1$.
- ▶ Phase margin: The angle φ_m to the negative real axis for the point where the Nyquist curve intersects the unit circle.

$$\varphi_m = \arg G_o(i\omega_c) - (-180^\circ) = \arg G_o(i\omega_c) + 180^\circ$$

Stability margins



- ▶ phase-cross-over frequency: The frequency ω_p for which $\arg G_o(i\omega) = -180^\circ$.
- ▶ Gain margin: The gain $K = A$ that would make the Nyquist curve of $KG_o(i\omega h)$ go through the point $-1 + i0$. This means that

$$|G_o(i\omega_p h)| = \frac{1}{A}.$$

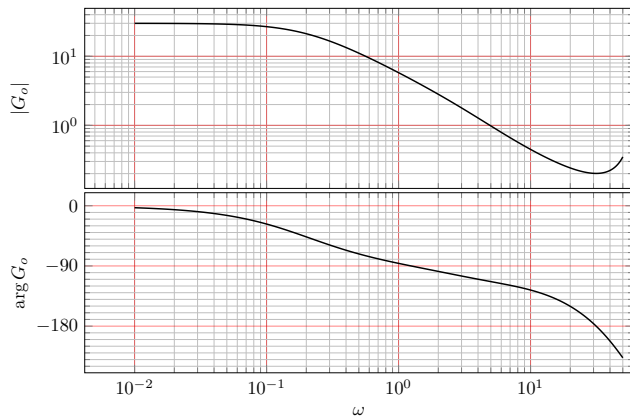
How to achieve the frequency-domain specifications

$$G_c(i\omega) = \frac{G_o(i\omega)}{1 + G_o(i\omega)}$$

Activity

1. If $G_o(i\omega_1) = -0.5$ what is $|G_c(i\omega_1)|$?
2. If $G_o(i\omega_1) = -i$ what is $|G_c(i\omega_1)|$?

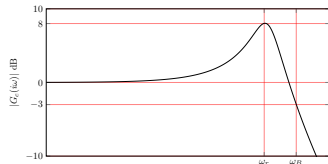
Stability margins exercise



Activity Determine the cross-over frequency ω_c , the phase cross-over frequency ω_p , the phase margin and the amplitude margin.

How to achieve the frequency-domain specifications

$$G_c(i\omega) = \frac{G_o(i\omega)}{1 + G_o(i\omega)}$$



Which of the Bode plots to the right shows the correct loop gain $G_o(i\omega)$?

