

A study on the energy transfer of a square prism under fluid-elastic galloping

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Abstract

Extracting useful energy from flow induced vibrations has become a developing area of research in recent years. In this paper, we analyse power transfer of an elastically mounted body under the influence of fluid-elastic galloping. The system and the power transfer is analysed by numerically integrating the quasi-steady state model equations. The power transfer is analysed for both high ($Re = 22300$) and low ($Re = 200$) Reynolds numbers cases.

A combined mass-damping coefficient, Π_2 , that can be derived from the equation of motion, is shown to be the parameter that governs power output. The system is a balance between the power delivered to the system due to fluid-dynamic forcing and power removed through mechanical damping which are governed by the fluid-dynamic forcing characteristics (i.e. the lift force as a function of incident angle) and mechanical damping coefficient respectively. Comparing the DNS results with the QSS data uncovered that a good agreement of the data could be obtained even at low Reynolds numbers when the inertia of the system (mass ratio) is substantially high.

Keywords:

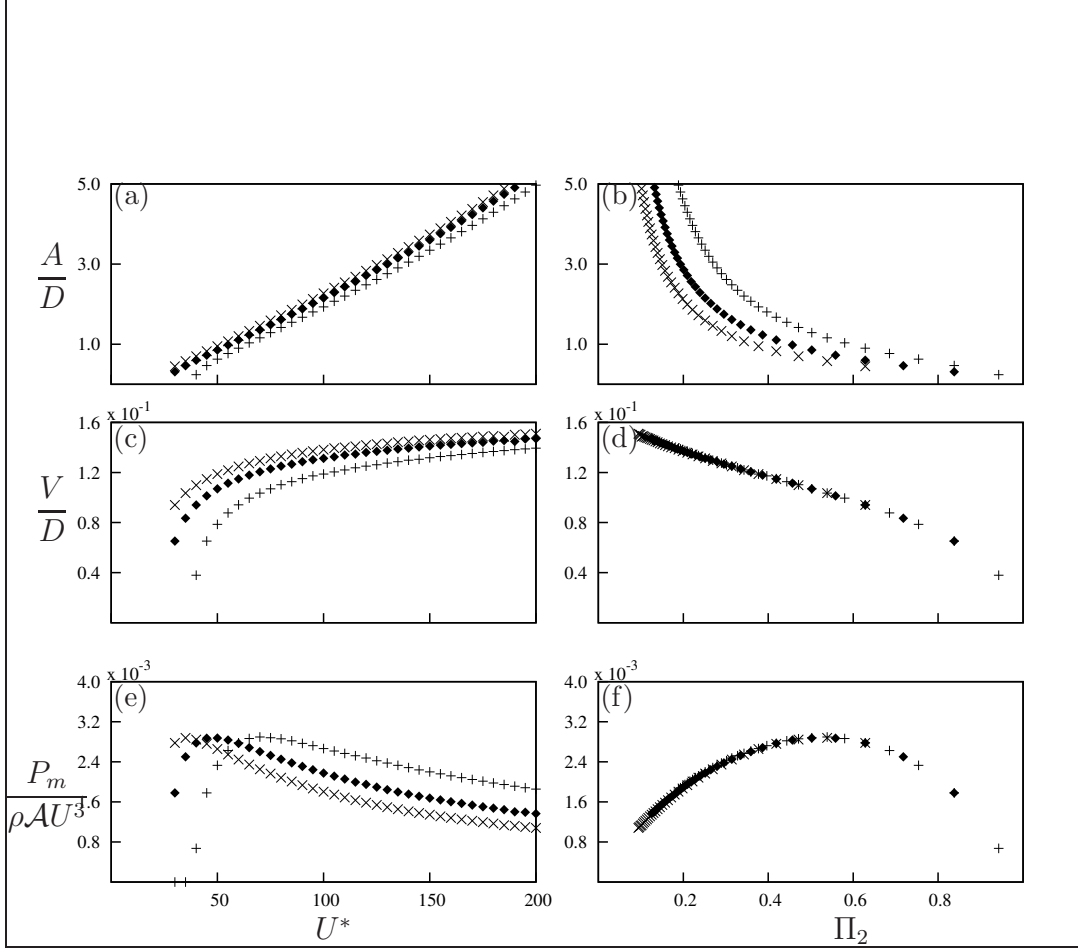


Figure 1: Displacement amplitude, velocity amplitude and mean power data as functions of two different independent variables. Data presented in (a), (c) and (e) using the classical VIV parameter U^* , obtained at $Re = 200$ and $m^* = 20$ at three different damping ratios: $\zeta = 0.075$ (\times), $\zeta = 0.1$ (\blacklozenge) and $\zeta = 0.15$ ($+$). (b) (d) and (f) are the same data presented using the combined mass-damping parameter (Π_2) as the independent variable.

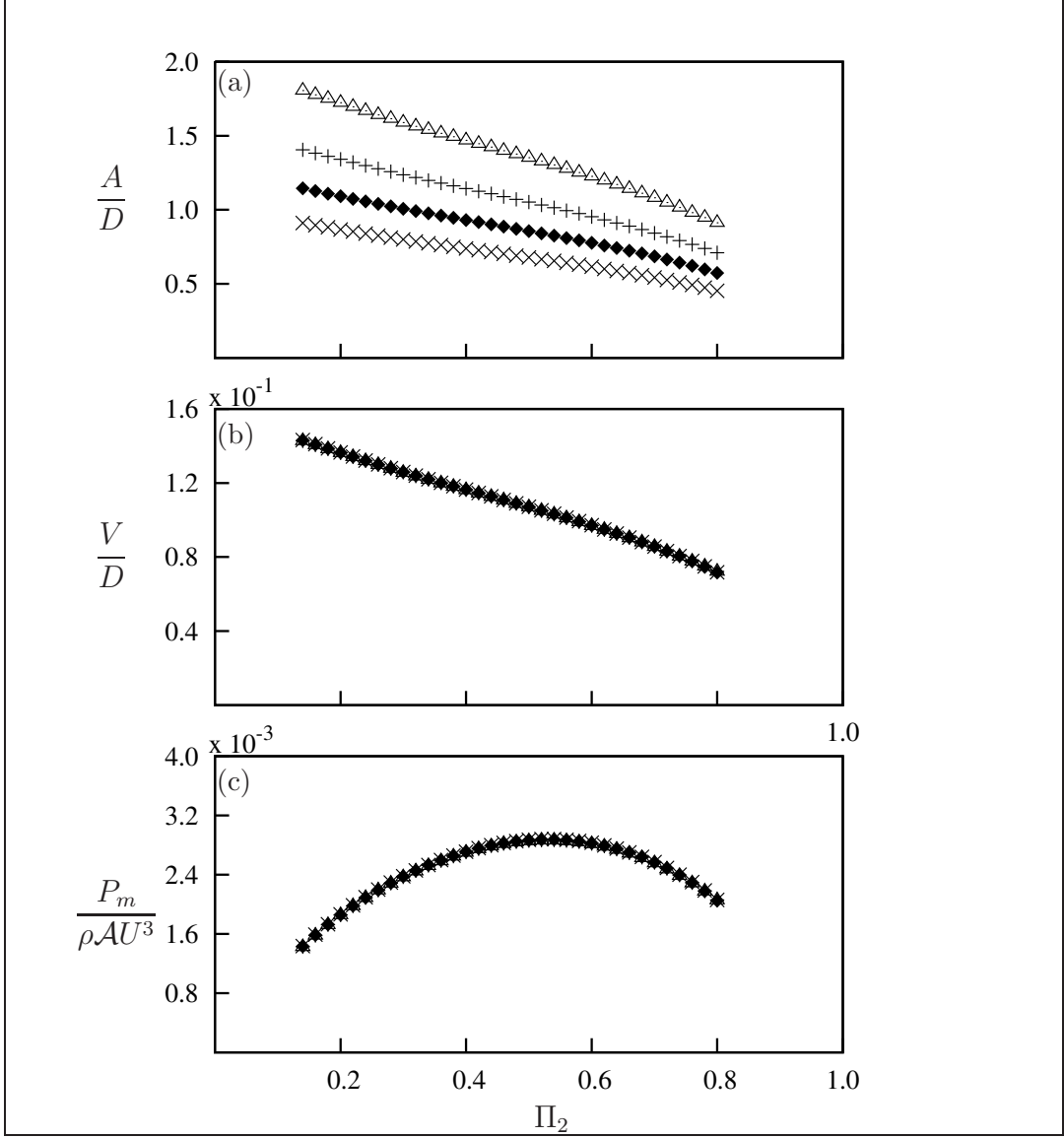


Figure 2: QSS data at high Π_1 levels. (a) displacement amplitude, (b) velocity amplitude and (c) mean power as a function of Π_2 . Data presented at four different combined mass-stiffness levels. $\Pi_1 = 10$ ($m^* = 20$, $U^* \approx 40$) (\times), $\Pi_1 = 100$ ($m^* = 80$, $U^* \approx 50$) (+), $\Pi_1 = 500$ ($m^* = 220$, $U^* \approx 60$) (\blacklozenge) and $\Pi_1 = 1000$ ($m^* = 400$, $U^* \approx 40$) (\triangle).

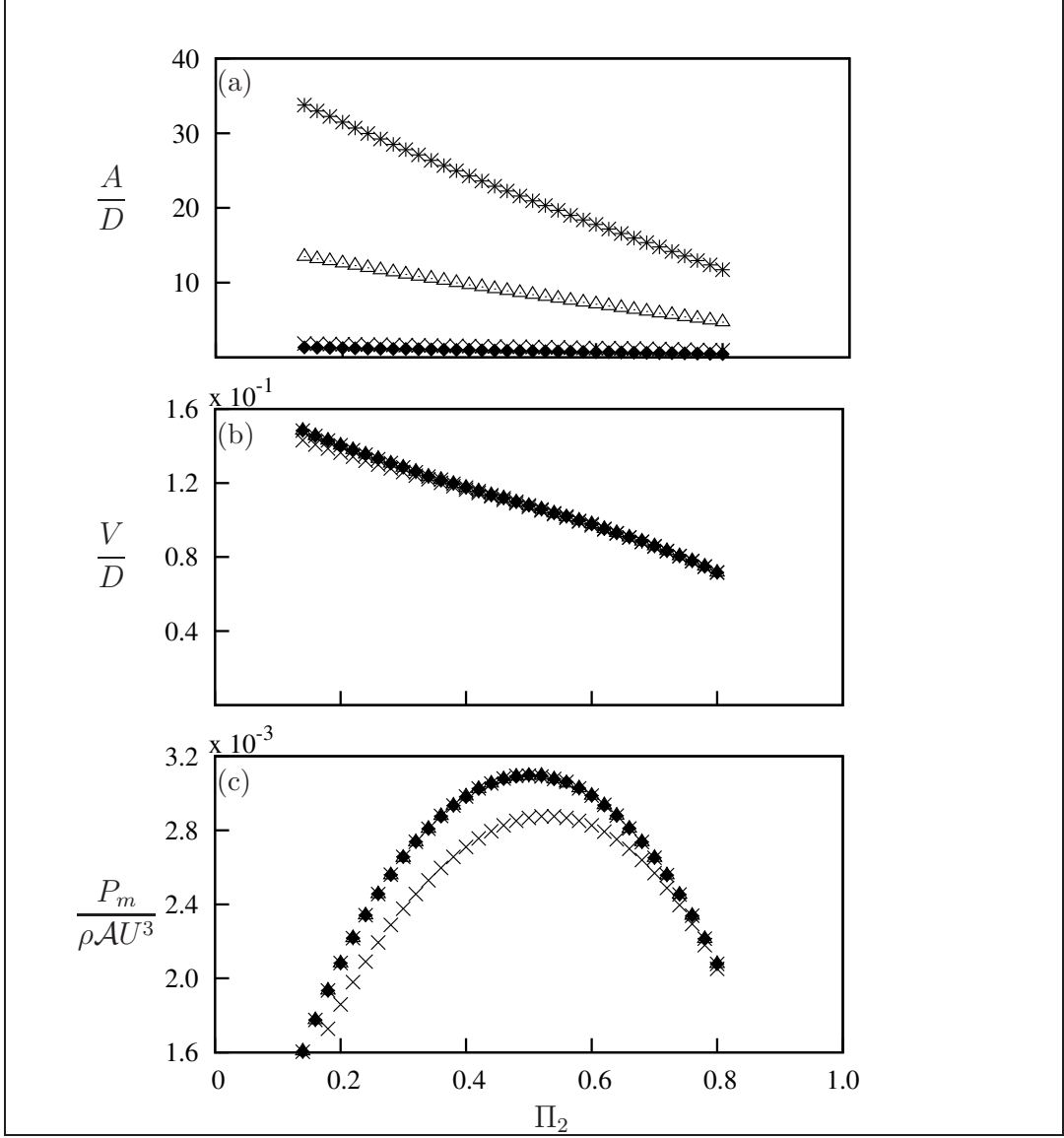


Figure 3: Comparison of QSS data at high and low Π_1 . (a) displacement amplitude, (b) velocity amplitude and (c) mean power as a function of Π_2 . Data presented at $\Pi_1 = 100 \text{ } m^* = 130(+)$, $\Pi_1 = 0.1 \text{ } m^* = 2 (\blacklozenge)$, $\Pi_1 = 0.1 \text{ } m^* = 20 (\triangle)$ and $\Pi_1 = 0.1 \text{ } m^* = 50 (*)$.

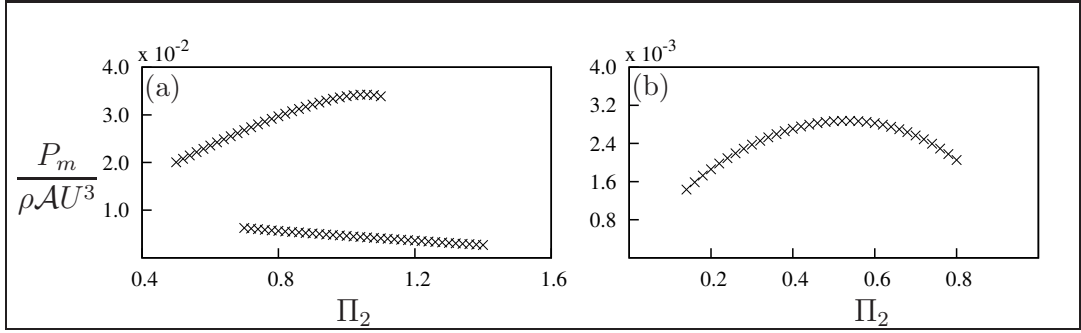


Figure 4: Mean power as a function of Π_2 . Data presented at (a) $Re = 22300$, $\Pi_2 = 20000$ and (b) $Re = 200$, $\Pi_2 = 100$. Hysteresis could be observed at high Re

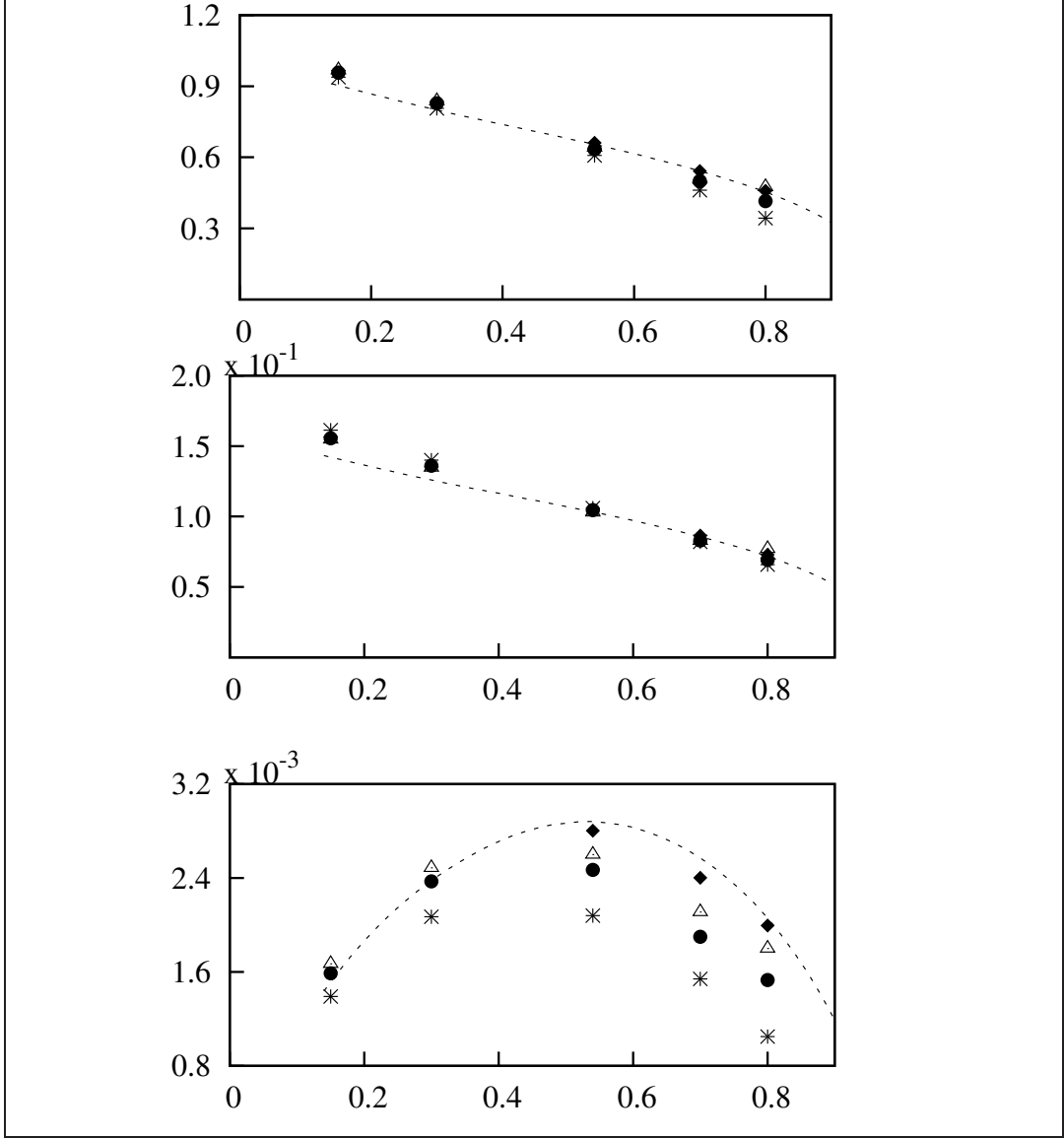


Figure 5: Comparison of data generated using the quasi-static theory and full DNS simulations . (a) Displacement amplitude, (b) velocity amplitude and (c) mean power as functions of Π_2 . Data were obtained at $\text{Re} = 200$ at three different combined values $\Pi_1 = 10$ ($m^* \approx 20$) (*), $\Pi_1 = 60$ ($m^* \approx 50$) (●), $\Pi_1 = 250$ ($m^* \approx 100$) (△), $\Pi_1 = 1000$ ($m^* \approx 250$) and $\Pi_1 = 6200$ ($m^* \approx 500$).

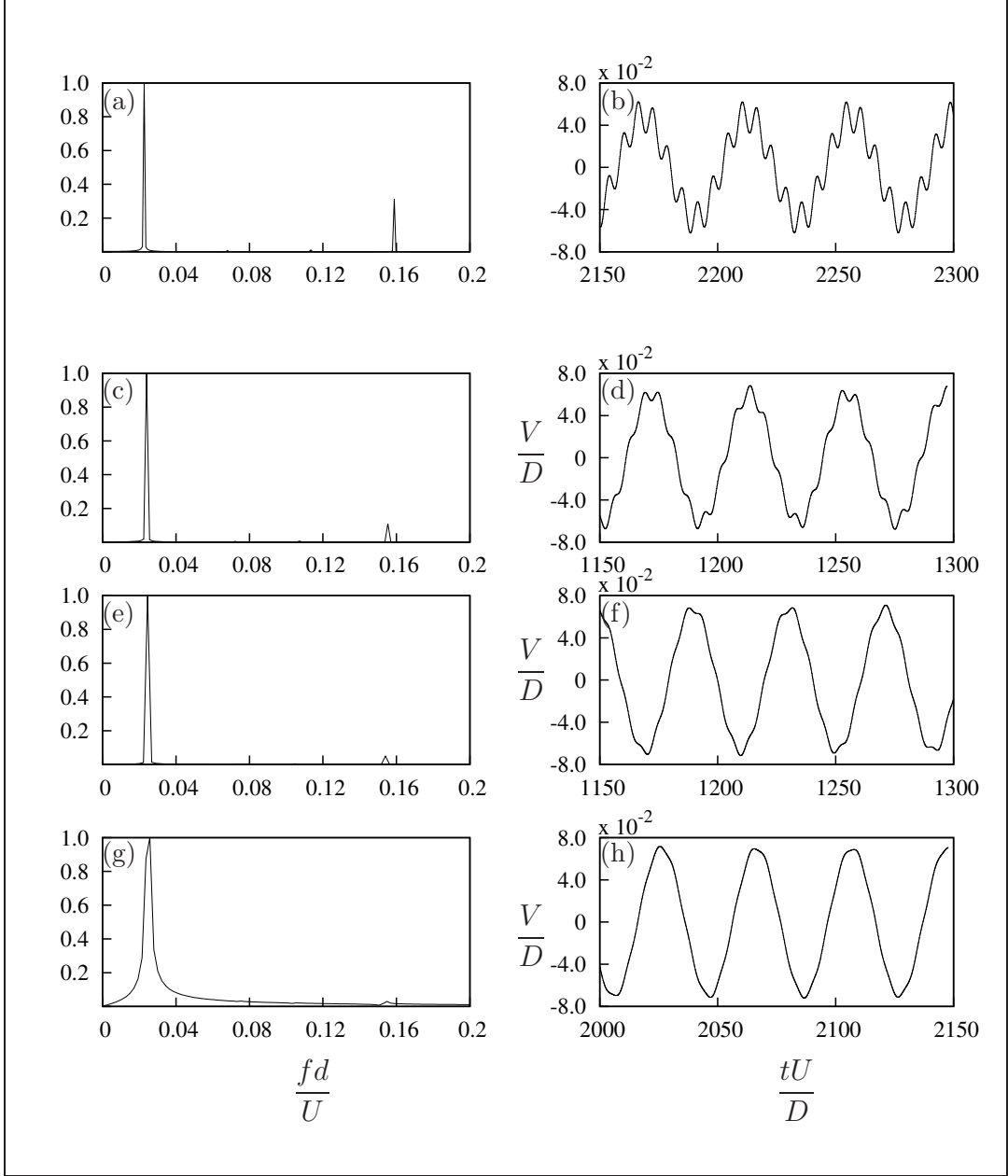


Figure 6: Velocity signal (right) and the corresponding power spectrum (left) of the DNS data at 3 different Π_1 and $\Pi_2 = 0.8$. =(a) and (b) $\Pi_1 = 10$, (c) and (d) $\Pi_1 = 60$, (e) and (f) $\Pi_1 = 250$, (g) and (h) $\Pi_1 = 1000$. U^* is kept at 40 therefore the mass ratio increases as Π_1 increases. It is evident that the influence of vortex shedding reduces as the inertia of the system increases.

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