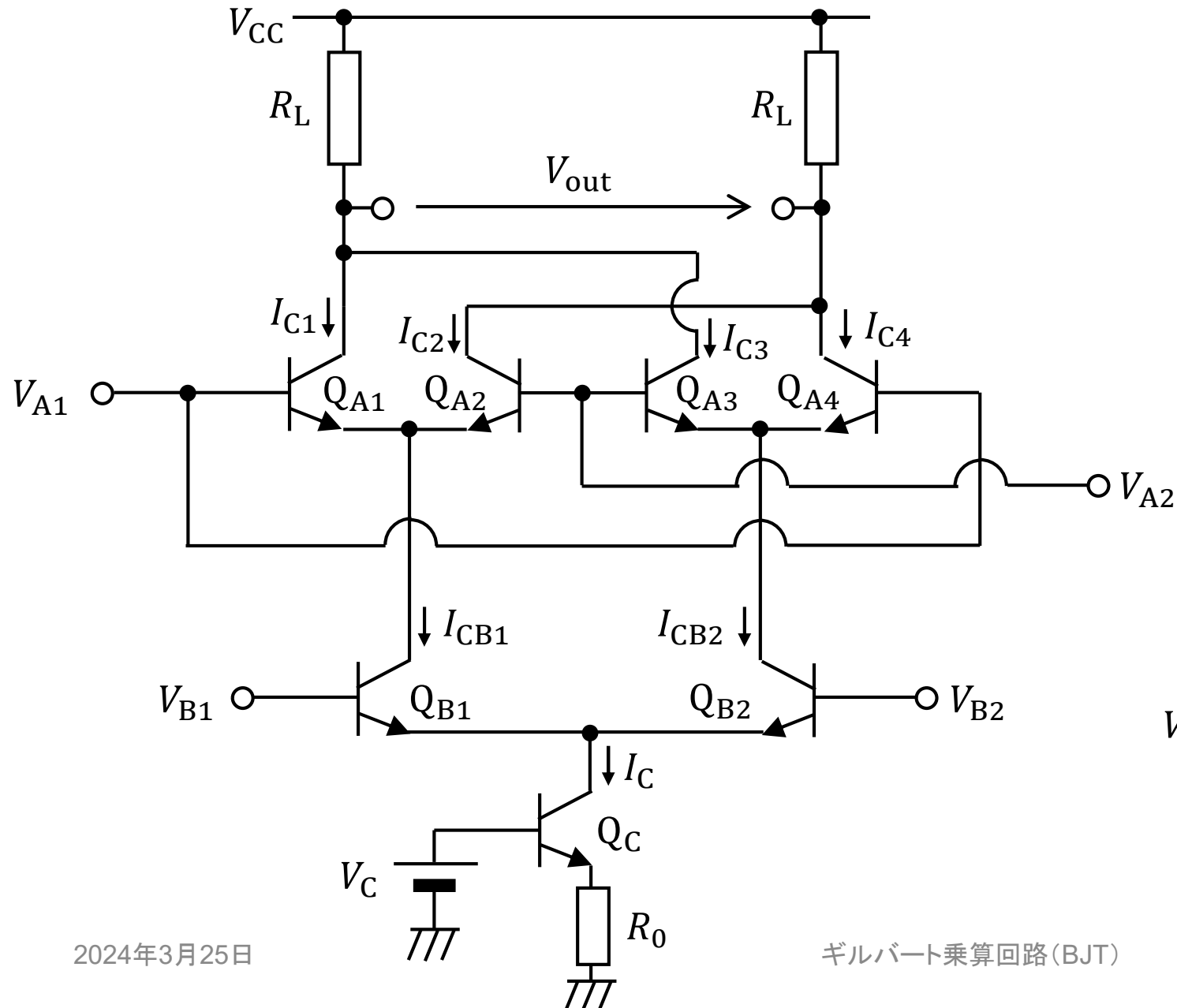


ギルバート乗算回路 (BJT)

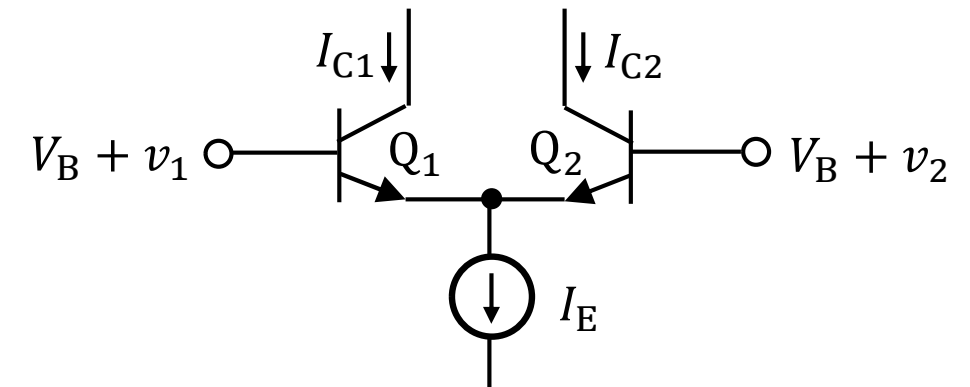
2024年3月25日 (月)

和田

ギルバート乗算回路



基本は差動対

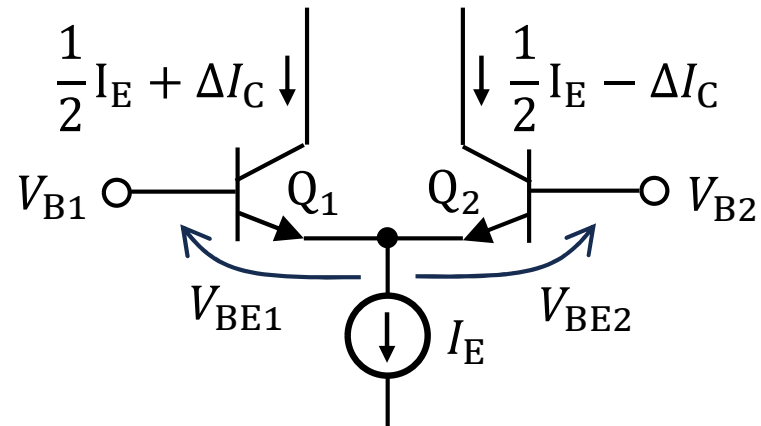


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$$V_{out} = R_L I_C \tanh\left(\frac{V_{A1} - V_{A2}}{2V_T}\right) \tanh\left(\frac{V_{B1} - V_{B2}}{2V_T}\right)$$

$$\simeq R_L I_C \left(\frac{V_{A1} - V_{A2}}{2V_T}\right) \left(\frac{V_{B1} - V_{B2}}{2V_T}\right)$$

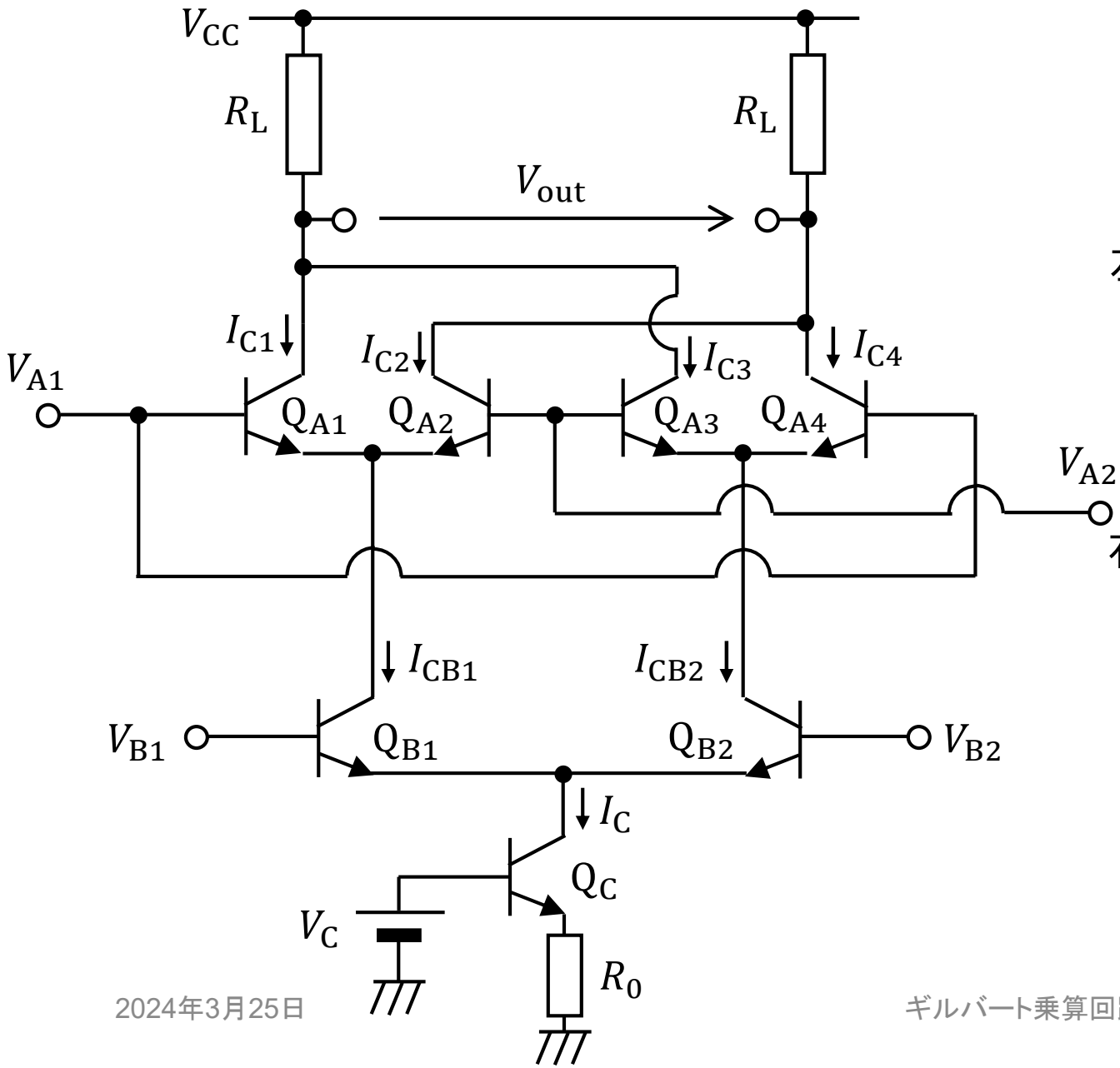
差動対



$$\frac{\frac{1}{2}I_E + \Delta I_C}{\frac{1}{2}I_E - \Delta I_C} = \frac{I_S \exp\left(\frac{V_{BE1}}{V_T}\right)}{I_S \exp\left(\frac{V_{BE2}}{V_T}\right)} = \exp\left(\frac{V_{BE1} - V_{BE2}}{V_T}\right) = \exp\left(\frac{V_{B1} - V_{B2}}{V_T}\right)$$

$$\Delta I_C = \frac{I_E}{2} \tanh\left(\frac{V_{B1} - V_{B2}}{2V_T}\right)$$

直流特性



下

$$I_{CB1} = \frac{I_C}{2} + \Delta I_{CB}, \quad I_{CB2} = \frac{I_C}{2} - \Delta I_{CB}$$

$$\Delta I_{CB} = \frac{I_C}{2} \tanh \left(\frac{V_{B1} - V_{B2}}{2V_T} \right)$$

左上

$$\frac{I_{C1}}{I_{C2}} = \frac{\frac{1}{2} \left(\frac{I_C}{2} + \Delta I_{CB} \right) + \Delta I_{A1}}{\frac{1}{2} \left(\frac{I_C}{2} + \Delta I_{CB} \right) - \Delta I_{A1}} = \exp \left(\frac{V_{A1} - V_{A2}}{V_T} \right)$$

$$\Delta I_{A1} = \frac{1}{2} \left(\frac{I_C}{2} + \Delta I_{CB} \right) \tanh \left(\frac{V_{A1} - V_{A2}}{2V_T} \right)$$

右上

$$\frac{I_{C4}}{I_{C3}} = \frac{\frac{1}{2} \left(\frac{I_C}{2} - \Delta I_{CB} \right) + \Delta I_{A2}}{\frac{1}{2} \left(\frac{I_C}{2} - \Delta I_{CB} \right) - \Delta I_{A2}} = \exp \left(\frac{V_{A1} - V_{A2}}{V_T} \right)$$

$$\Delta I_{A2} = \frac{1}{2} \left(\frac{I_C}{2} - \Delta I_{CB} \right) \tanh \left(\frac{V_{A1} - V_{A2}}{2V_T} \right)$$

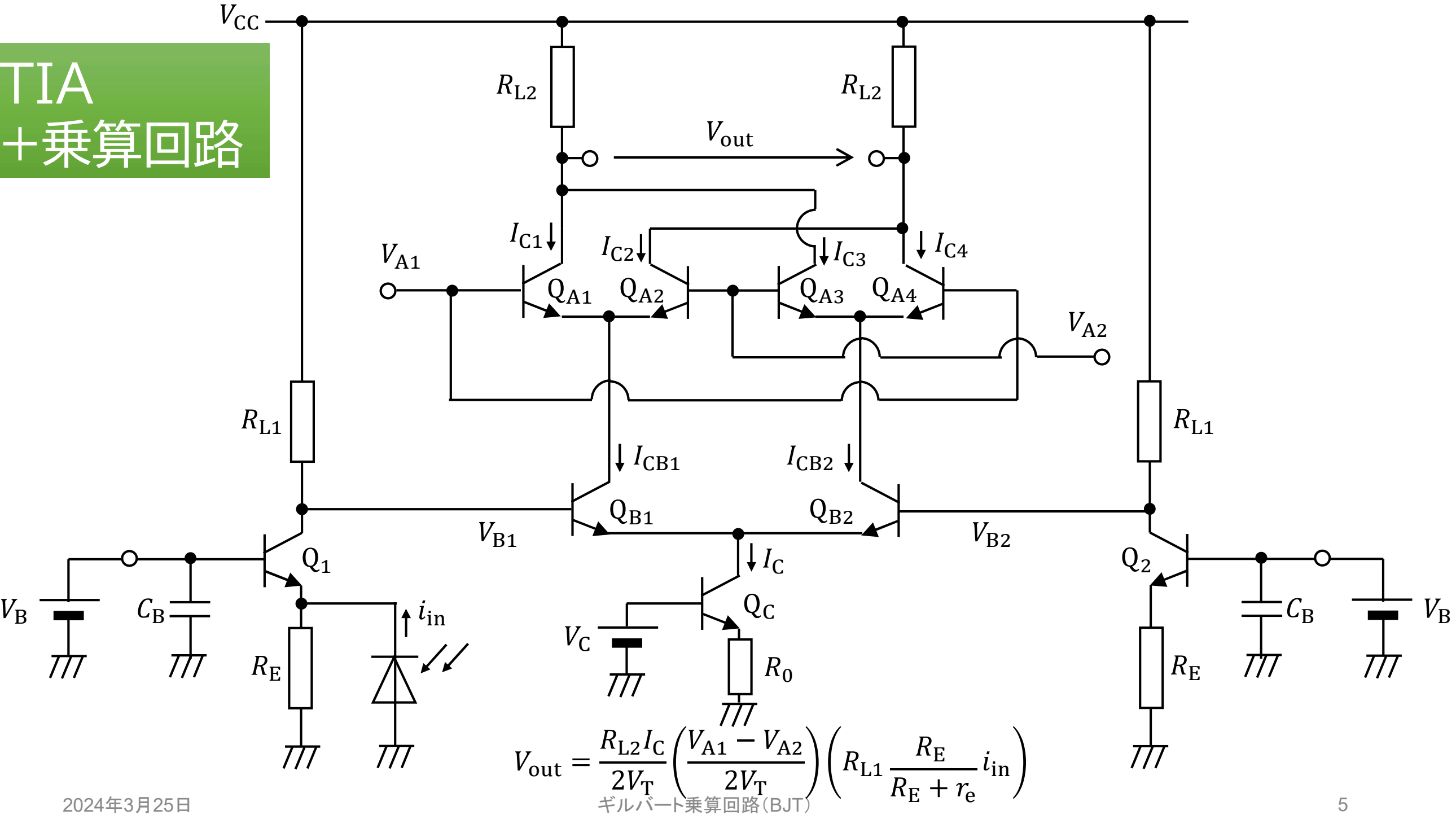
$$(I_{C1} + I_{C3}) - (I_{C2} + I_{C4}) = (I_{C1} - I_{C2}) + (I_{C3} - I_{C4})$$

$$= 2(\Delta I_{A1} - \Delta I_{A2})$$

$$= 2\Delta I_{CB} \tanh \left(\frac{V_{A1} - V_{A2}}{2V_T} \right)$$

$$V_{out} = R_L(I_{C1} + I_{C3}) - R_L(I_{C2} + I_{C4})$$

TIA +乗算回路



数値例

$$r_e \left(= \frac{1}{g_m} \right) = R_E, \quad R_{L1} = 1.4 \text{ k}\Omega, \quad V_T = 26 \text{ mV},$$

$$V_{A1} - V_{A2} = 2V_T, \quad R_0 = 100 \text{ }\Omega, \quad I_C = 1 \text{ mA} \text{ (} V_C \text{ を調整)}, \quad R_{L2} = 400 \text{ }\Omega$$

$$\begin{aligned} V_{\text{out}} &= R_{L2} I_C \tanh \left(\frac{V_{A1} - V_{A2}}{2V_T} \right) \tanh \left(\frac{R_{L1} \frac{R_E}{R_E + r_e} i_{\text{in}}}{2V_T} \right) \\ &= 0.4 \times \tanh 1 \times \tanh \left(\frac{0.7 \text{ k}\Omega}{52 \text{ mV}} i_{\text{in}} \right) \end{aligned}$$

$$V_{\text{out}} [\text{mV}] \simeq 1000 \times 0.4 \times \frac{2.7 - 0.37}{2.7 + 0.37} \times \frac{0.7 i_{\text{in}} [\mu\text{A}]}{52} \doteq 4 i_{\text{in}} [\mu\text{A}]$$

$$\frac{V_{\text{out}}}{i_{\text{in}}} \doteq 4 \text{ k}\Omega$$

この設計では出力 V_{out} をさらに 10～40 dB程度増幅する(SF+DA 等) 必要がある。