ESO204A, Fluid Mechanics and rate Processes

Momentum conservation: integral formulation

Very useful for calculation of forces

Chapter 3 of F M White Chapter 4 of Fox McDonald (uploaded)

Reynolds Transport Theorem:

$$\frac{dB_{\text{sys}}}{dt} = \frac{\partial}{\partial t} \int_{\text{CV}} \rho \beta dV + \int_{\text{CS}} \rho \beta \left(\vec{u} . \vec{n} \right) dS$$

For Momentum conservation: $B_{\text{sys}} = m\vec{u} \Rightarrow \beta = \vec{u}$

$$\frac{d(m\vec{u})}{dt} = \frac{\partial}{\partial t} \int_{CV} \rho \vec{u} dV + \int_{CS} \rho \vec{u} (\vec{u}.\vec{n}) dS$$

Momentum conservation principle: $\frac{d(m\vec{u})}{dt} = \vec{F}$

Momentum conservation
$$\vec{F} = \frac{\partial}{\partial t} \int_{CV} \rho \vec{u} dV + \int_{CS} \rho \vec{u} (\vec{u}.\vec{n}) dS$$
 (integral formulation)

$$\vec{F} = \vec{F}_S + \vec{F}_B$$

 $\vec{F}_{\scriptscriptstyle S}$: Surface force, all forces acting at the control surface

 \vec{F}_{B} : Body forces (gravity, electromagnetic)

Surface forces usually come from pressure, shear and interaction with solid objects/surfaces

$$\vec{F}_{S} + \vec{F}_{B} = \frac{\partial}{\partial t} \int_{CV} \rho \vec{u} dV + \int_{CS} \rho \vec{u} (\vec{u}.\vec{n}) dS$$

Incompressible flow:
$$\vec{F}_{\rm S} + \vec{F}_{\rm B} = \rho \frac{\partial}{\partial t} \int_{\rm CV} \vec{u} dV + \rho \int_{\rm CS} \vec{u} \left(\vec{u} . \vec{n} \right) dS$$

In a non-deformable CV

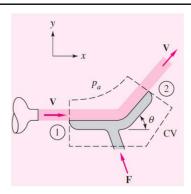
Steady flow:
$$\vec{F}_{\rm S} + \vec{F}_{\rm B} = \int_{\rm CS} \rho \vec{u} (\vec{u}.\vec{n}) dS$$

Steady, incompressible flow: $\vec{F}_{S} + \vec{F}_{B} = \rho \int_{CS} \vec{u} (\vec{u}.\vec{n}) dS$

Water jet (area A) hits a fixed vane, flow direction changes

Find the force F necessary to hold the vane fixed

Assumption: 1. steady, incompressible flow, 2. flow is in horizontal plane, 3. uniform flow at inlet/exit, 4. $p = p_a$



$$\int_{CS} (\vec{u}.\vec{n}) dS = 0$$

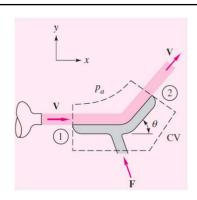
Analysis:
$$\int_{CS} (\vec{u}.\vec{n}) dS = 0 \qquad \vec{F}_{S} = \rho \int_{CS} \vec{u} (\vec{u}.\vec{n}) dS$$

$$\int_{CS} (\vec{u}.\vec{n}) dS = 0$$

$$u_1 = u_2 = V \text{ (since } A = \text{constant)}$$

$$\vec{F}_{S} = \rho \int_{CS} \vec{u} (\vec{u}.\vec{n}) dS = \rho \sum_{CS} \vec{u} (\vec{u}.\vec{A})$$

$$\left(\vec{u}.\vec{A}\right)_1 = -VA = -\left(\vec{u}.\vec{A}\right)_2$$



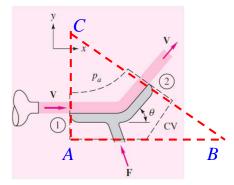
In *x* direction:

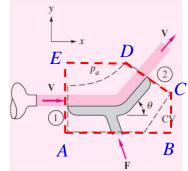
$$F_x + F_{px} (pressure forces) = \rho V (\vec{u}.\vec{A})_1 + \rho V \cos \theta (\vec{u}.\vec{A})_2$$
$$= -\rho V^2 A + \rho V^2 A \cos \theta$$

$$F_{x} = -\rho V^{2} A + \rho V^{2} A \cos \theta$$

Since gage pressure $F_{px} = 0$ is zero everywhere

$$rac{1}{px} = 0$$
 is zero every





$$F_{px} = p \times AC - p \times BC \cos \theta$$
$$= 0$$

$$F_{px} = p \times AE - p \times BC$$
$$-p \times CD \cos \theta = 0$$

В

Pressure force always at the CS toward the CV (compressive)

In *y* direction:

$$F_{y} + F_{py} = \rho V \sin \theta (\vec{u}.\vec{A})_{2}$$
$$= \rho V^{2} A \sin \theta$$

$$F_{py} = p \times AB - p \times BC \sin \theta$$
$$= 0$$

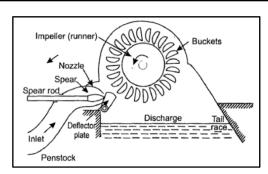
$$F_{y} = \rho V^{2} A \sin \theta$$

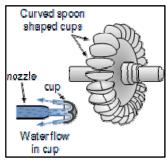
$$F_{x} = -\rho V^{2} A + \rho V^{2} A \cos \theta$$

$$F = \sqrt{F_x^2 + F_y^2} = \rho V^2 A \sqrt{\sin^2 \theta + (\cos \theta - 1)^2} = 2\rho V^2 A \sin \frac{\theta}{2}$$

Also find the direction of the above force

- Pressure force always at the CS toward the CV (compressive)
- Thumb rules for choice of CV: surface normal (at CS) should be along or opposite to the flow direction or coordinate axes
- Uniform pressure distribution over a closed CS leads to zero pressure force (proof is left as an exercise)
- Wise choice of 'reference pressure' simplifies the force calculation





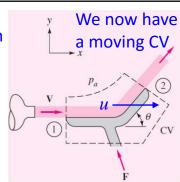
Application: Hydraulic turbine such as Pelton Wheel



Vane moving in *x*-direction with velocity *u* (constant)

Nozzle exit velocity V

Observer (and the axes) will move with the CV



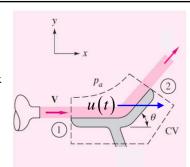
$$(\vec{u}.\vec{A})_1 = -(\vec{u}.\vec{A})_2 = -(V-u)A = -V_1A$$

In x direction: $F_x == \rho V_1^2 A(\cos \theta - 1)$

In y direction: $F_y = \rho V_1^2 A \sin \theta$

Starting of a turbine

If we remove the force $F_{\rm x}$ the vane will accelerate



We are in a non-inertial frame now

$$(\vec{u}.\vec{A})_1 = -(\vec{u}.\vec{A})_2 = -(V-u)A = -V_1(t)A$$

$$-m\frac{du}{dt} = \rho(V-u)^2 A(\cos\theta - 1); u(t=0) = 0$$

$$\frac{u}{V} = \frac{Vbt}{1 + Vbt}; b = \frac{(1 - \cos\theta)\rho A}{m}$$

What happens during shutdown?