## Fluid Mechanics and Rate Processes: Tutorial 8

**P1.** In Fig.P1 the pipe entrance is sharp-edged. If the flow rate is 0.004 m<sup>3</sup>/s, what power, in W, is extracted by the turbine?

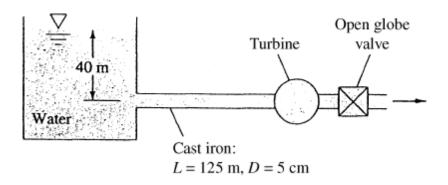


Fig.P1

**Solution:** For water at 20°C, take  $\rho = 998 \text{ kg/m}^3$  and  $\mu = 0.001 \text{ kg/m} \cdot \text{s}$ . For cast

iron,  $\varepsilon \approx 0.26$  mm, hence  $\varepsilon/d = 0.26/50 \approx 0.0052$ . The minor loss coefficients are Entrance:  $K \approx 0.5$ ; 5-cm( $\approx 2''$ ) open globe valve:  $K \approx 6.9$ 

The flow rate is known, hence we can compute V, Re, and f:

$$V = \frac{Q}{A} = \frac{0.004}{(\pi/4)(0.05)^2} = 2.04 \ \frac{m}{s}, \quad Re = \frac{998(2.04)(0.05)}{0.001} \approx 102000, \quad f \approx 0.0316$$

The turbine head equals the elevation difference minus losses and exit velocity head:

$$\begin{aligned} h_t &= \Delta z - h_f - \sum h_m - \frac{V^2}{2g} = 40 - \frac{(2.04)^2}{2(9.81)} \bigg[ (0.0316) \bigg( \frac{125}{0.05} \bigg) + 0.5 + 6.9 + 1 \bigg] \approx 21.5 \text{ m} \\ &\text{Power} = \rho g Q h_t = (998)(9.81)(0.004)(21.5) \approx \textbf{840 W} \quad \textit{Ans.} \end{aligned}$$

**P2**. The parallel galvanized-iron pipe system of Fig.P2 delivers gasoline at 20°C with a total flow rate of 0.036 m<sup>3</sup>/s. Let the pump be running and delivering 45 kW to the flow in pipe 2. Determine (a) the flow rate in each pipe, and (b) the overall pressure drop.

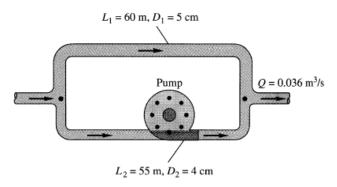


Fig.P2

**Solution:** For gasoline at 20°C, take  $\rho = 680 \text{ kg/m}^3$  and  $\mu = 2.92\text{E}-4 \text{ kg/m} \cdot \text{s}$ . For galvanized iron, take  $\varepsilon = 0.15 \text{ mm}$ , hence  $\varepsilon/d_1 = 0.0030 \text{ and } \varepsilon/d_2 = 0.00375$ . The volume-flow relation is the same as in Prob. 6.113, but the head loss in pipe 2 is reduced by the pump head delivered:

$$h_{f1} = f_1 \frac{L_1}{d_1} \frac{V_1^2}{2g} = h_{f2} - h_{pump} = f_2 \frac{L_2}{d_2} \frac{V_2^2}{2g} - \frac{45000 \text{ W}}{\rho g Q_2}$$

$$Q_1 + Q_2 = (\pi/4) d_1^2 V_1 + (\pi/4) d_2^2 V_2 = Q_{total} = 0.036 \text{ m}^3/\text{s}$$

If we introduce the given data, we obtain two simultaneous algebraic equations:

$$\begin{split} f_1 \frac{60}{0.05} \frac{V_1^2}{2(9.81)} &= f_2 \frac{55}{0.04} \frac{V_2^2}{2(9.81)} - \frac{45000}{680(9.81)(\pi/4)(0.04)^2 V_2}, \\ \text{or:} \quad 61.16 \ f_1 V_1^2 &= 70.08 \ f_2 V_2^2 - 5368/V_2 \quad \text{with V in m/s} \\ \text{plus} \quad (\pi/4)(0.05)^2 V_1 + (\pi/4)(0.04)^2 V_2 &= 0.036 \ \text{m}^3/\text{s} \end{split}$$

The right hand side of the 1st equation should not be negative, hence  $V_2 > 15$  m/s. One solution scheme is to guess  $V_2 \ge 15$  and then calculate  $V_1$  from each equation. We also guess  $f_1 \approx 0.026$  and  $f_2 \approx 0.028$  from the solution to Prob. 6.113—but remember, the fluid is *gasoline* now:

If 
$$V_2 \approx 15 \frac{m}{s}$$
, head loss gives  $V_1 \approx 7.19 \frac{m}{s}$ , volume flow gives  $V_1 \approx 8.73 \frac{m}{s}$   
If  $V_2 \approx 16 \frac{m}{s}$ , head loss gives  $V_1 \approx 10.18 \frac{m}{s}$ , volume flow gives  $V_1 \approx 8.09 \frac{m}{s}$ 

Clearly the correct V<sub>2</sub> is somewhere between 15 and 16 m/s. The iteration converges to:

$$V_2 = 15.39 \text{ m/s}, \text{ Re}_2 = 1.43\text{E}6, \quad f_2 \approx 0.0280, \quad Q_2 = A_2 V_2 = \textbf{0.0193 m}^3/\text{s} \quad \textit{Ans.} \text{ (a)}$$
  
 $V_1 = 8.48 \text{ m/s}, \text{ Re}_1 = 9.94\text{E}5, \quad f_1 \approx 0.0263, \quad Q_1 = A_1 V_1 = \textbf{0.0167 m}^3/\text{s} \quad \textit{Ans.} \text{ (a)}$ 

The pressure drop is the same in either leg:

$$\Delta p = f_1 \frac{L_1}{d_1} \frac{\rho V_1^2}{2} = f_2 \frac{L_2}{d_2} \frac{\rho V_2^2}{2} - \frac{45000}{Q_2} \approx 774,000 \text{ Pa} \quad \textit{Ans. (b)}$$

**P3.** In Fig.P3 all pipes are 8-cm-diameter cast iron. Determine the flow rate from reservoir (1) if valve C is (a) closed; and (b) open, with  $K_{\text{valve}} = 0.5$ .

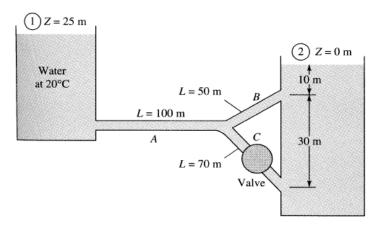


Fig.P3

**Solution:** For water at 20°C, take  $\rho = 998$  kg/m<sup>3</sup> and  $\mu = 0.001$  kg/m·s. For cast iron,  $\varepsilon \approx 0.26$  mm, hence  $\varepsilon/d = 0.26/80 \approx 0.00325$  for all three pipes. Note  $p_1 = p_2$ ,  $V_1 = V_2 \approx 0$ . These are long pipes, but we might wish to account for minor losses anyway:

sharp entrance at A:  $K_1 \approx 0.5$ ; line junction from A to B:  $K_2 \approx 0.9$  (Table 6.5)

branch junction from A to C:  $K_3 \approx 1.3$ ; two submerged exits:  $K_B = K_C \approx 1.0$ 

If valve C is closed, we have a straight *series* path through A and B, with the same flow rate Q, velocity V, and friction factor f in each. The energy equation yields

$$z_1 - z_2 = h_{fA} + \sum h_{mA} + h_{fB} + \sum h_{mB},$$
or:  $25 \text{ m} = \frac{\text{V}^2}{2(9.81)} \left[ f \frac{100}{0.08} + 0.5 + 0.9 + f \frac{50}{0.08} + 1.0 \right], \text{ where } f = \text{fcn} \left( \text{Re}, \frac{\varepsilon}{d} \right)$ 

Guess  $f \approx f_{\text{fully rough}} \approx 0.027$ , then  $V \approx 3.04$  m/s,  $Re \approx 998(3.04)(0.08)/(0.001) \approx 243000$ ,  $\varepsilon/d = 0.00325$ , then  $f \approx 0.0273$  (converged). Then the velocity through A and B is V = 3.03 m/s, and  $Q = (\pi/4)(0.08)^2(3.03) \approx 0.0152$  m<sup>3</sup>/s. Ans. (a).

If valve C is open, we have parallel flow through B and C, with  $Q_A = Q_B + Q_C$  and, with d constant,  $V_A = V_B + V_C$ . The total head loss is the same for paths A-B and A-C:

$$\begin{split} z_1 - & \ z_2 = h_{fA} + \sum h_{mA-B} + h_{fB} + \sum h_{mB} = h_{fA} + \sum h_{mA-C} + h_{fC} + \sum h_{mC}, \\ \text{or:} \quad & 25 = \frac{V_A^2}{2(9.81)} \Bigg[ f_A \frac{100}{0.08} + 0.5 + 0.9 \Bigg] + \frac{V_B^2}{2(9.81)} \Bigg[ f_B \frac{50}{0.08} + 1.0 \Bigg] \\ & = \frac{V_A^2}{2(9.81)} \Bigg[ f_A \frac{100}{0.08} + 0.5 + 1.3 \Bigg] + \frac{V_C^2}{2(9.81)} \Bigg[ f_C \frac{70}{0.08} + 1.0 \Bigg] \end{split}$$

plus the additional relation  $V_A = V_B + V_C$ . Guess  $f \approx f_{fully\ rough} \approx 0.027$  for all three pipes and begin. The initial numbers work out to

$$\begin{split} 2g(25) &= 490.5 = V_A^2(1250f_A + 1.4) + V_B^2(625f_B + 1) = V_A^2(1250f_A + 1.8) + V_C^2(875f_C + 1) \\ &\text{If } f \approx 0.027, \text{ solve (laboriously)} \quad V_A \approx 3.48 \text{ m/s}, \ V_B \approx 1.91 \text{ m/s}, \ V_C \approx 1.57 \text{ m/s}. \\ &\text{Compute } \text{Re}_A = 278000, \quad f_A \approx 0.0272, \quad \text{Re}_B = 153000, \quad f_B = 0.0276, \\ &\text{Re}_C = 125000, \quad f_C = 0.0278 \end{split}$$

Repeat once for convergence:  $V_A \approx 3.46$  m/s,  $V_B \approx 1.90$  m/s,  $V_C \approx 1.56$  m/s. The flow rate from reservoir (1) is  $\mathbf{Q_A} = (\pi/4)(0.08)^2(3.46) \approx \mathbf{0.0174} \, \mathbf{m}^3/\mathbf{s}$ . (14% more) Ans. (b)