ESO204A, Fluid Mechanics and rate Processes

Conduction Heat Transfer

Chapter 2 of Cengel

General Eq. of heat conduction $\frac{\partial T}{\partial t} = \alpha \nabla^2 T + \frac{\dot{e}_{\rm gen}}{\rho c}$

$$\frac{\partial T}{\partial t} = \alpha \nabla^2 T + \frac{\dot{e}_{\text{gen}}}{\rho c}$$

Unsteady, no generation $\frac{\partial T}{\partial t} = \alpha \nabla^2 T$

$$\frac{\partial T}{\partial t} = \alpha \nabla^2 T$$

Steady: $\nabla^2 T + \frac{\dot{e}_{\text{gen}}}{k} = 0$

Steady, no generation: $\nabla^2 T = 0$

 k, α : thermal conductivity and diffusivity (both being material properties) respectively



Fourier: 1768-1830

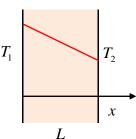
Conduction occurs in all media (solid, liquid gas) through diffusion and lattice vibration

Steady, 1-D Heat Transfer in a Slab $\frac{d^2T}{dx^2} = 0 \Rightarrow T = c_1x + c_2$

$$T(x=0) = T_1 \implies c_2 = T_1$$

$$T(x=L) = T_2 \implies c_1 L + c_2 = T_2$$

$$T = T_1 + (T_2 - T_1)\frac{x}{L}$$
 linear temperature variation



Heat flux
$$q''_x = -k \frac{dT}{dx} = -k \frac{d}{dx} \left[T_1 + (T_2 - T_1) \frac{x}{L} \right] = \frac{k(T_1 - T_2)}{L}$$

Heat transfer rate
$$\dot{Q} = q_x'' \times \text{Area} = \frac{kA(T_1 - T_2)}{L}$$

Other Heat Transfer Mechanisms

Convection

Heat transfer due to fluid flow





Radiation

Heat transfer due to electromagnetic radiation

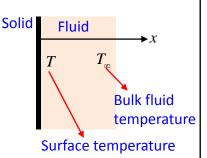
Example: solar radiation on earth

Convective heat transfer at a solid fluid interface

Newton's law of cooling

$$q_x'' = h(T - T_{\infty})$$
 $\dot{Q} = hA(T - T_{\infty})$

h: convective heat transfer coefficient



Unlike thermal conductivity, convective heat transfer coefficient is NOT a material property; it is a function of thermophysical properties and flow variables (velocity, shear)

Radiative Heat Transfer

Every object emits, absorbs, transmits, reflects radiation (at various amounts) all the time; part of radiation manifests as heat

Maximum emission: Blackbody emission,

Stefan-Boltzmann law $Q = A \sigma T^4$

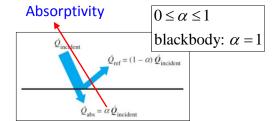
Emissivity

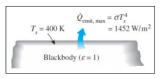
Non-blackbody $\dot{Q} = A\varepsilon\sigma T^4$ emission

 $0 < \varepsilon \le 1$

Stefan-Boltzmann constant

 $5.67 \times 10^{-8} \, Wm^{-2} K^{-4}$





Radiative Heat Transfer

Kirchhoff's law
$$\varepsilon = \alpha$$

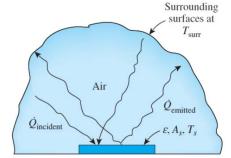
$$\dot{Q}_{\rm rad} = A_{\rm s} \varepsilon \sigma T_{\rm s}^4 - A_{\rm s} \alpha \sigma T_{\rm surr}^4$$

$$\dot{Q}_{\rm rad} = A_s \varepsilon \sigma \left(T_{\rm s}^4 - T_{\rm surr}^4 \right)$$

$$q_{
m rad}^{\prime\prime} = arepsilon \sigma ig(T_{
m s}^4 - T_{
m surr}^4 ig)$$

Following form is sometimes useful

$$\dot{Q}_{\rm rad} = h_{\rm rad} A_s \left(T_{\rm s} - T_{\rm surr} \right)$$



At high temperature, radiation dominates over other modes

where
$$h_{\text{rad}} = \frac{\varepsilon \sigma \left(T_{\text{s}}^4 - T_{\text{surr}}^4\right)}{T_{\text{s}} - T_{\text{surr}}} = \varepsilon \sigma \left(T_{\text{s}} + T_{\text{surr}}\right) \left(T_{\text{s}}^2 + T_{\text{surr}}^2\right)$$

In many practical heat transfer applications, all three modes occur simultaneously

Steady, 1-D Heat Transfer in a Slab $T = c_1 x + c_2$

$$T(x=0) = T_1 \implies c_2 = T_1$$

$$x = L: -k\frac{dT}{dx} + h(T_{\infty} - T) = 0$$

$$\Rightarrow -kc_1 + h(T_{\infty} - c_1L - c_2) = 0$$

$$\Rightarrow c_1 = \frac{h(T_{\infty} - T_1)}{k + hL}$$

$$\Rightarrow C_1 = \frac{1}{k + hL} \times \frac{1}{k + hL$$

$$T(x=0) = T_1 \implies c_2 = T_1$$
Net heat flux is zero at $x = L$

$$x = L : -k\frac{dT}{dx} + h(T_{\infty} - T) = 0$$

$$\implies -kc_1 + h(T_{\infty} - c_1 L - c_2) = 0$$

$$T_1 = \frac{d^2T}{dx^2} = 0$$

$$T_2 = ?$$

$$h, T_{\infty}$$

$$\Rightarrow c_1 = \frac{h(T_{\infty} - T_1)}{k + hL}$$

$$T = T_1 + \frac{h(T_{\infty} - T_1)}{k + hL}x$$

$$\dot{Q} = q_x'' \times \text{Area} = \frac{kAh(T_1 - T_\infty)}{k + hL}$$

Steady, 1-D Heat Transfer in a Slab: Electrical Analogy
$$T_1-T_2=\Delta T$$
 $\dot{Q}=\frac{kA\left(T_1-T_2\right)}{L}$

$$\Delta T = \dot{Q} \left(\frac{L}{kA} \right) \equiv \Delta V = IR \qquad R_{\rm cond} = \frac{L}{kA} \qquad I_{\rm cond} = \frac{L}{kA} \qquad I_{\rm cond} = \frac{L}{R} \qquad I_$$

Similarly
$$\dot{Q}_{\rm conv} = hA\Delta T$$
 $\dot{Q}_{\rm rad} = h_{\rm rad}A\Delta T$

We can now have series and parallel combination as in electrical circuit

Steady, 1-D Heat Transfer in a Slab $T = T_1 + \frac{h(T_{\infty} - T_1)}{k + hL}x$ $T_2 = T_1 + \frac{hL(T_{\infty} - T_1)}{k + hL} \quad \dot{Q} = \frac{kAh(T_1 - T_{\infty})}{k + hL}$ Electrical analogy $\dot{Q} = \frac{T_1 - T_{\infty}}{L/(kA) + 1/(hA)}$ $T_1 = T_1 + \frac{h(T_{\infty} - T_1)}{k + hL}x$ $T_1 = T_2 = T_1 + \frac{h(T_{\infty} - T_1)}{k + hL}x$

$$T_2 = T_1 + \frac{hL(T_{\infty} - T_1)}{k + hL} \quad \dot{Q} = \frac{kAh(T_1 - T_{\infty})}{k + hL}$$

$$\frac{d^2T}{dx^2} = 0 \qquad T_2 = ?$$

$$h, T_{\infty}$$

$$L$$

To find T_2

$$\dot{Q} = \frac{T_1 - T_{\infty}}{L/(kA) + 1/(hA)} = \frac{T_1 - T_2}{L/(kA)}$$

$$\frac{T_2 - T_1}{T_{\infty} - T_1} = \frac{L/(kA)}{L/(kA) + 1/(hA)} = \frac{hL}{k + hL}$$

