

Energy balance

$$\frac{P_1}{\rho g} + \frac{1}{2g} \alpha_1 v_1^2 + z_1 = \frac{P_2}{\rho g} + \frac{1}{2g} \alpha_2 v_2^2 + z_2 + h_f - h_p - h_t$$

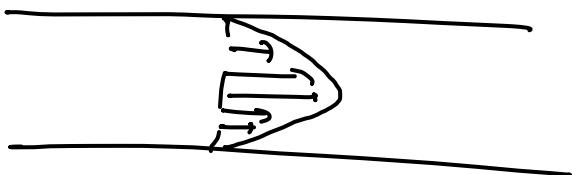
How to find $h_f \leftarrow$ Head loss or frictional loss

Empirical method

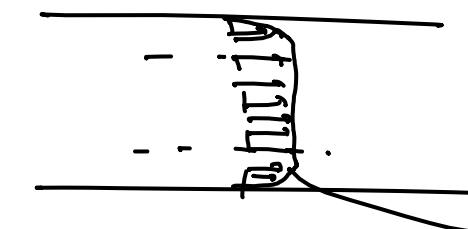
$$h_f = f \frac{L}{d} \frac{v^2}{2g} \text{ for a circular pipe}$$

$$f = \frac{64}{Re} \quad \begin{array}{l} \text{for laminar flow (by darcy +)} \\ \text{for circular pipe} \end{array}$$

Turbulent flow \rightarrow Navier-Stokes' is not valid for turbulent flow \Rightarrow So we can not get the velocity profile \Rightarrow we use empirical method to find Velocity profile for turbulent flow



Laminar velocity profile

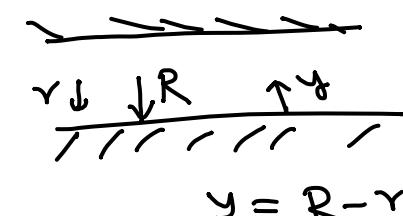


Turbulent velocity profile

$$U = \text{time-averaged velocity} = \frac{\int u dt}{\int dt}$$


Sharp change in velocity near the surface \Rightarrow can be captured by Logarithmic velocity Profile

$$\frac{U}{U^*} = \frac{1}{k} \ln \frac{y U^*}{\nu} + B$$



$$u^* = \sqrt{\frac{\tau_{\text{w}}}{\rho}} = \text{dimension of velocity} \Leftarrow \underline{\text{frictional velocity}}$$

B, k = constant that has to be determined for a geometry

find f

$$\frac{u}{u^*} = \frac{1}{k} \ln \frac{y u^*}{\delta} + B$$

$$\frac{v}{R} = \frac{1}{k} \ln \frac{y u^*}{\delta} + B$$

$$\frac{u(r)}{u^*} = \frac{1}{k} \ln \frac{(R-r) u^*}{\delta} + B$$

$$V = \text{cross-section averaged velocity} = v = \frac{\int u(r) 2\pi r dr}{\pi R^2}$$

$$v = \frac{1}{2} u^* \left(\frac{2}{k} \ln \frac{R u^*}{\delta} + 2B - \frac{3}{k} \right)$$

$$\text{for } V \text{ circular pipe} \quad k = 0.41, \quad B = 5.0$$

Smooth pipe ($f \neq 0$)

$$\frac{V}{u^*} \approx 2.44 \ln \left(\frac{R u^*}{\delta} \right) + 1.34$$

$$\left(\frac{V}{u^*} \right) = \sqrt{\frac{\rho V^2}{\tau_{\text{w}}} \Leftrightarrow f = \frac{\tau_{\text{w}}}{\frac{1}{f} \rho V^2} \Rightarrow \frac{V}{u^*} = \left(\frac{8}{f} \right)^{y_2}}$$

$$\left(\frac{R u^*}{\delta} \right) = \frac{1}{2} \left(\frac{d u^*}{\delta} \right) = \frac{1}{2} \text{Re}_d \left(\frac{u^*}{\delta} \right) = \frac{1}{2} \text{Re}_d \left(\frac{1}{8} \right)^{y_2}$$

$$\Rightarrow \frac{1}{f^{y_2}} \approx 1.97 \log \left(\text{Re}_d f^{y_2} \right) - 1.02 \quad (\text{Smooth pipe, turbulent flow})$$

(implicit in f)

has been modified by Prandtl

Explicit eqn for f $\quad 400 < \text{Re}_d < 500$

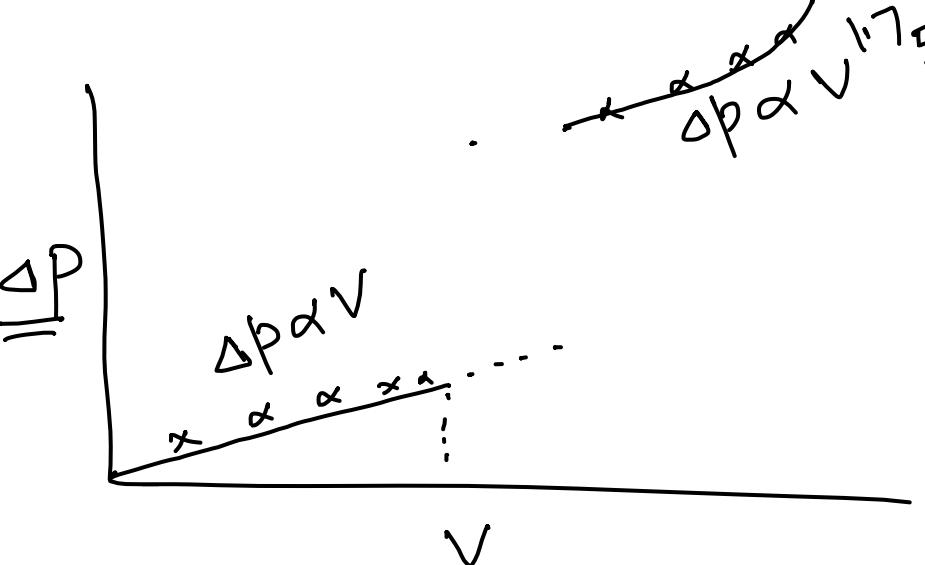
$f = \frac{0.316}{\text{Re}_d^{y_2}} \quad (\text{Blasius})$

$f = - \frac{\Delta P}{\rho V^2} \quad (\text{Smooth})$

$f = f(\text{Re}_d, \frac{\epsilon}{d}, \text{shape})$

$$\frac{1}{f^{y_2}} = 2.0 \log \text{Re}_d f^{y_2} - 0.8 \quad (\text{Prandtl})$$

Hagen's experiment



$$f = \frac{64}{Re}$$

$$\ln f = \ln 64 - \ln(Re)$$

for laminar flow

$$h_f = \frac{\Delta P}{\rho g} = f \frac{L}{d} \frac{V^2}{2g} = \frac{64 \mu}{\rho V d} \frac{L}{d} \frac{V^2}{2g} \propto V$$

for turbulent

$$h_f = \frac{\Delta P}{\rho g} = \frac{0.312 \mu^{1/4}}{(\rho V d)^{1/4}} \frac{L}{d} \frac{V^2}{2g} \propto V^{1.75}$$

($\frac{\varepsilon}{d}$) The moody chart by experiment (vary $\varepsilon \rightarrow \Delta P$)

[At constant Re]

$$\frac{1}{f^{1/2}} = -2.0 \log \left(\frac{\varepsilon/d}{3.7} \right)$$

[for smooth pipe]

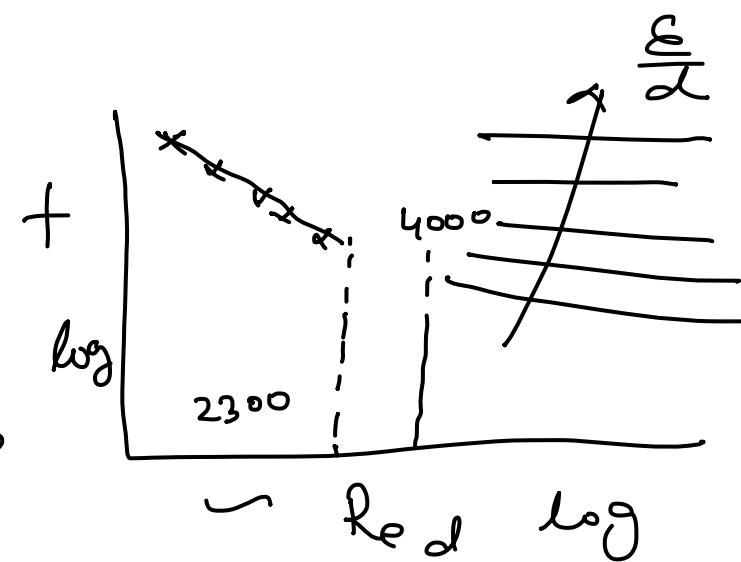
$$\frac{1}{f^{1/2}} = -2.0 \log Re + C - 0.8$$

Colebrook \rightarrow

$$\frac{1}{f^{1/2}} = -2.0 \log \left[\frac{\varepsilon/d}{3.7} + \frac{2.51}{Re f^{1/2}} \right]$$

implicit in f

[Rough pipe) matches



Explicit Correlation by Haaland

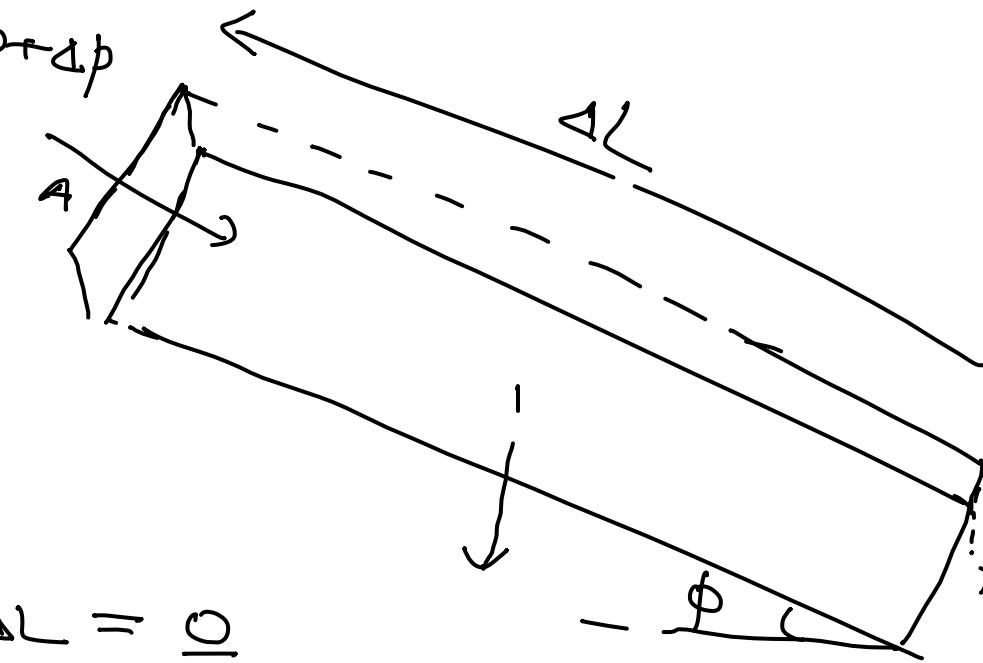
$$\frac{1}{f^{1/2}} = -1.8 \log \left[\frac{6.9}{Re} + \left[\frac{(\varepsilon/d)}{3.7} \right]^{1.11} \right] \quad \leftarrow \text{Also matches with 1-b moody chart}$$

$$f = \frac{64}{Re} \quad \rightarrow h_f \rightarrow \Delta p \quad (\text{so far we have discussed about circular pipe})$$

Flow in a non-circular Duct
to define
How h_f → How to find +

momentum balance

$$(\Delta p) A + \rho g A \Delta L \sin \phi - \tau_w f \Delta L = 0$$



f = Perimeter

$$h_f = \frac{\Delta p}{\rho g} + \Delta Z = \frac{\tau_w}{\rho g} \frac{\Delta L}{(A/f)}$$

R_h = hydraulic radius =
 $f = \tau_w / (\rho v^2)$

$$h_f = \frac{1}{8} \frac{\rho v^2}{\rho g} \frac{\Delta L}{A/f} = f \frac{\Delta L}{4R_h} \frac{V^2}{2g} = f \frac{\Delta L}{D_h} \frac{V^2}{2g}$$



$$R_h = \frac{\pi (R_2^2 - R_1^2)}{\pi (D_1 + D_2)}$$

Hydraulic diameter = $D_h = 4 R_h$

$f = f\left(\frac{D_h V}{\nu}, \frac{\epsilon}{D_h}\right)$ for any shape

$$f = \begin{cases} \left(\frac{64}{Re} \right)^{-1} & \text{error} \pm 4\% \quad \text{Laminar flow} \\ f_{\text{moody}} \left(Re, D_h, \frac{\epsilon}{D_h} \right) & \pm 15\% \quad \text{Turbulent} \end{cases}$$

→ Although moody chart is for circular pipe, we use it for non circular duct in case of turbulent

for Laminar flow

