CE394M: Critical State and Cam-Clay

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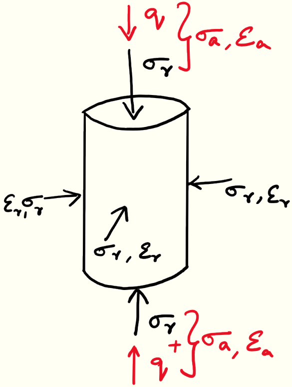
Overview

Roscoe et al., (1958), Schofield & Worth (1968), Wood (1990):

- Provides a conceptual framework in which to interpret stress-strain-strength-volumetric strain response of soil.
- Started as a qualitative, rather than a mathematical model
- A unified framework of known or observed soil responses: drained / undrained / etc

Critical state variables

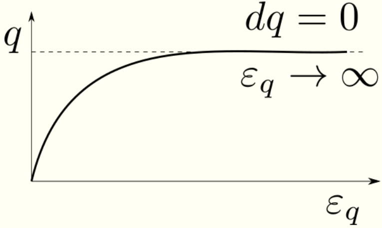
- Mean stress: $p' = \frac{\sigma'_a + 2\sigma'_r}{3} = p - u$.
- Deviatoric stress: $q = \sigma'_a - \sigma'_r = \sigma_a - \sigma_r$
- Specific volume: $v = \frac{V_T}{V_s} = \frac{V_s + V_v}{V_s} = 1 + e$.

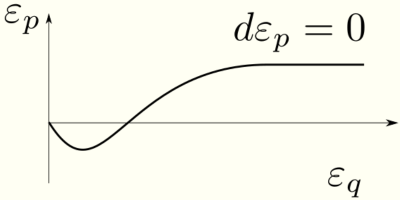


Critical State Hypothesis: I

Roscoe, Schofield & Worth (1958): **At shear-failure, soil exists at a unique state**

- $d\varepsilon_s >> 0$ unlimited shear strain potential.
- $dp' = dq = d\varepsilon_v = 0$ no change in p', q, ε_v.
- Critical state stress ratio: $\eta = q/p' = const = M$ at failure $q = Mp'$.





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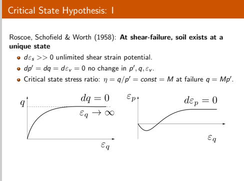
CE394M: Cam-Clay
└─Critical State Soil Mechanics
└─Critical State Hypothesis: I

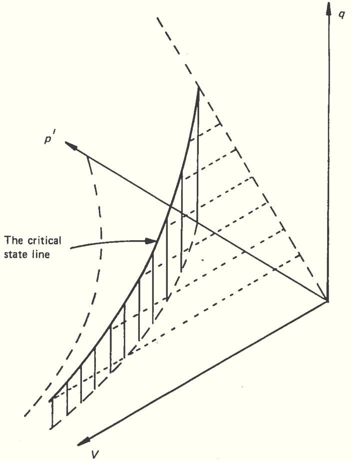


Soil is sheared to a point where stresses are stationary ($dq = dp' = 0$) with no futher change in volume ($d\varepsilon_v = 0$), unlimited shear strains ($d\varepsilon_s >> 0$) and q/p' has a fixed value: **critical state**.

M can be related to phi': $M = \frac{6 \sin \phi'}{3 - \sin \phi'}$.

Critical State Hypothesis: II

Critical state is a function of q, p', v.



The CSL (p', v, q) space is given by the intersection of two planes: $q = Mp'$ and a cruved vertical plane $v = \Gamma - \lambda \ln p'$

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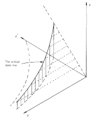

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Critical state curve connecting critical state points:

- Crticial state line
- Defined in 3D but we'll look at projections into $q - p'$ and $v - p'$ space

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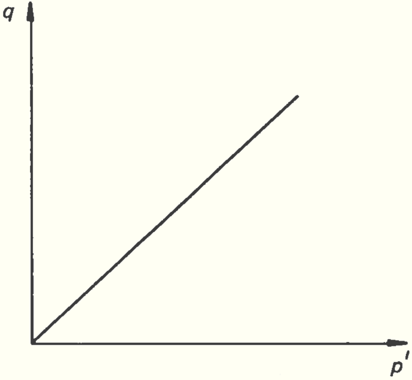
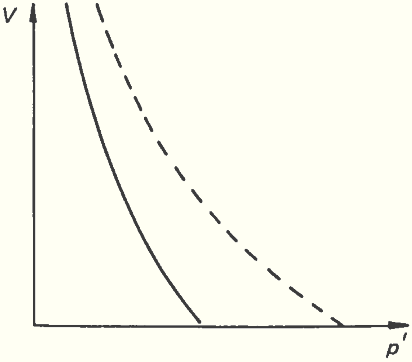
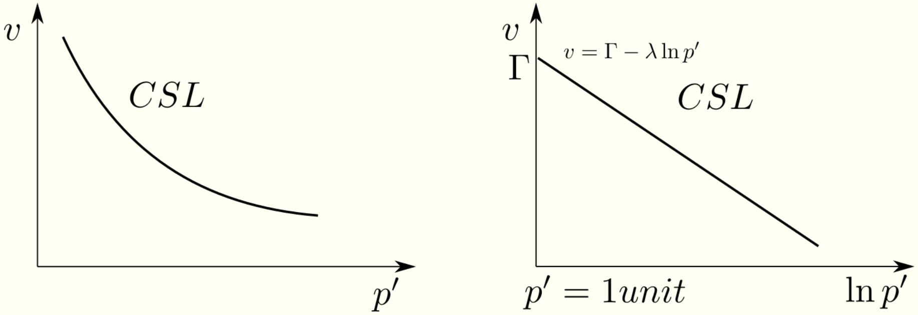




The CSL in (a) (p', q) plot and (b) (p', v) plot (isotropic normal compression line is shown in dashed)

Critical state is a function of q, p', v.



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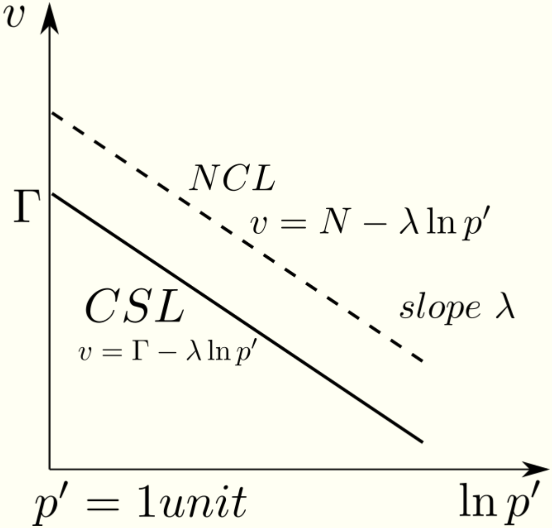
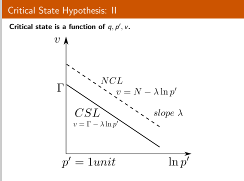
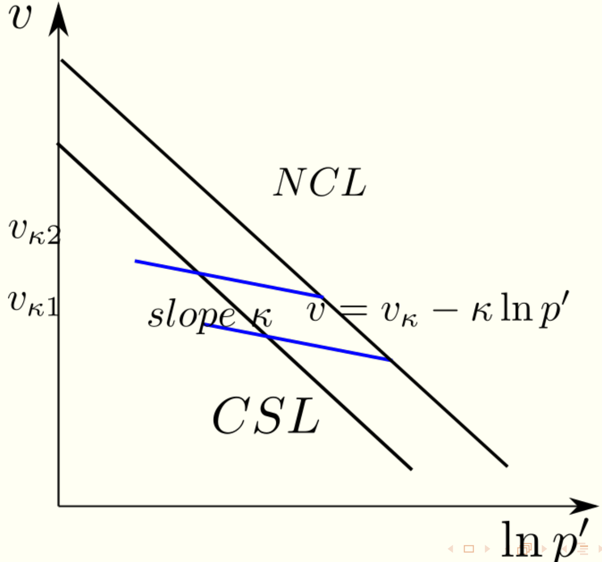
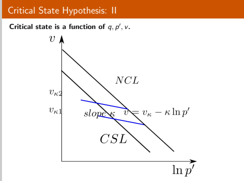




Isotropic virgin compression line (VCL) $\eta = 0$. NCL is parallel to CSL. VCL is $\eta = 0$, while CSL $\eta = M$. Oedometer falls between VCL and CSL at a constant η: $0 < \eta < M$.

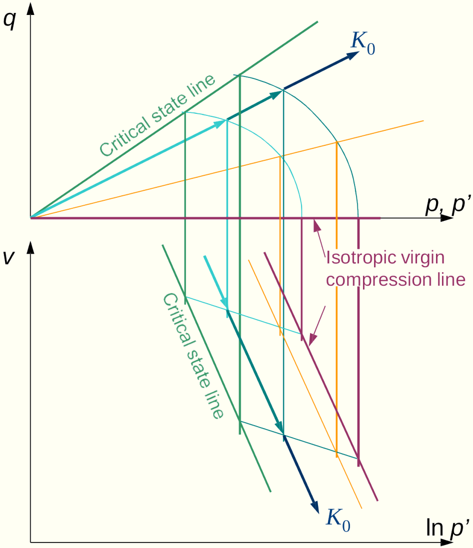
Critical state is a function of q, p', v.



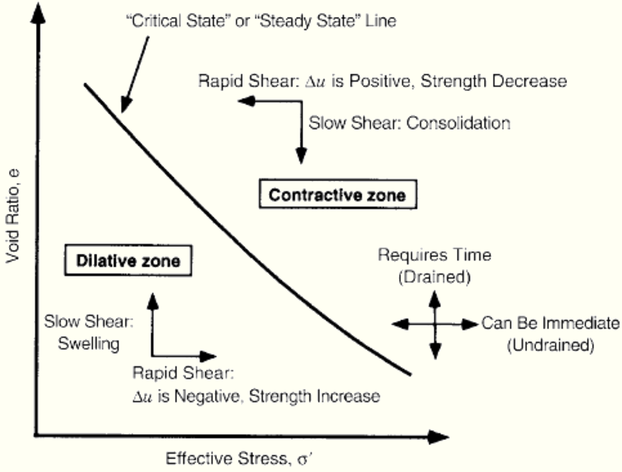


v_κ depends on which κ line you are on. $\kappa \neq c_r$ and $\lambda \neq C_c$

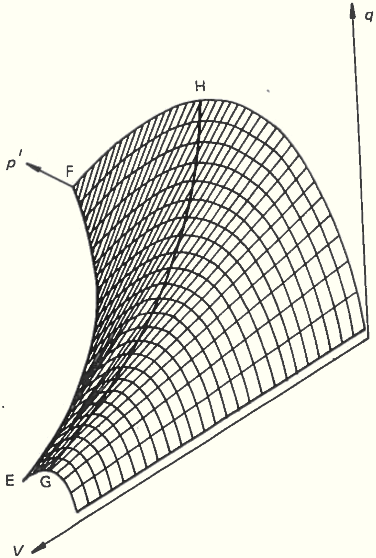
Stress paths $\sigma'_3/\sigma'_1 = K_c = const$



Clay behavior



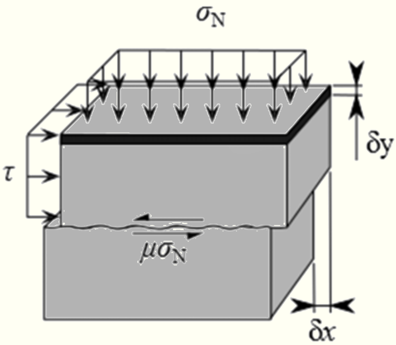
Critical state boundary surface



Summary of critical state behavior

- Can only traverse NCL in one direction
- Can traverse RCL (κ-line) in both directions
- To move from one κ-line to another must move along NCL. Hence, plastic volumetric strains must occur.
- Critical state line is **NOT** a yield surface. It's where it's going but a lot of plastic straining is needed to get there. (if $CSL = F = 0$) then with associative flow rule $d\varepsilon_v^p \neq 0$ at critical state. Real F is horizontal at critical state.

Stress - dilatancy theory (Taylor, 1948)



Work in friction and dilation:

$$\tau dx - \sigma'_n dy = \mu \sigma'_n dx$$

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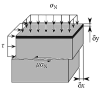


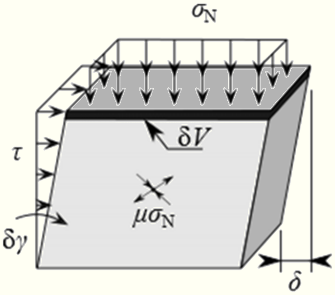
Work in friction and dilation:

$$\tau dx - \sigma_n' dy = \mu \sigma_n' dx$$

Taylor (1948) proposed a stress-dilatancy theory based on the work balance equation: The external work corresponds to the product of the measured displacements and forces (assuming that the elastic deformation is negligible). The internal work corresponds to the frictional force.

Formulation of elasto-plastic Cam-Clay (OCC): Yield function

Derived from work consideration:



External work: $\delta w^p_{ext} = p' d\varepsilon^p_v + q d\varepsilon^p_s$ Assume that the internal work is dissipated by internal friction only: $\delta w^p_{int} = M p' d\varepsilon^p_s$

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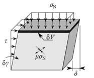

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$$\delta w^p_{ext} = p' d\varepsilon^p_v + q d\varepsilon^p_s = Mp' d\varepsilon^p_s = \delta w^p_{int}$$

This dissipation function can be regarded simply as generalisation of Taylor's equation. It should be noted that both Taylor's equation and Cam-Clay dissipation function equation assume that when there is some combination of volumechange (dy or $\partial\varepsilon_v$) and of shear distortion (dx or $\partial\varepsilon_s$) it is the shear strain that determines the dissipation rate. The dilation or volume change is a geometrical consequence of interlocking, and does not appear explicitly in the dissipation function.

Cam-Clay (OCC): Stress dilatancy relation

$$p' d\varepsilon_v^p + q d\varepsilon_s^p = M p' d\varepsilon_s^p$$

Rearranging the terms (divide by $p' d\varepsilon_s^p$):

$$\frac{d\varepsilon_v^p}{d\varepsilon_s^p} = M - \frac{q}{p'} = M - \eta$$

Where $\eta = q/p'$ is defined as the stress-ratio. This equation is known as the dilatancy expression and expresses the ratio in plastic volumetric and deviatoric components.

$$q/p < M : \quad \frac{d\varepsilon^p \varepsilon_v}{d\varepsilon_q^p} > 0 \rightarrow \quad d\varepsilon^p \varepsilon_v > 0 \quad \text{Contractive response}$$

$$q/p > M : \quad \frac{d\varepsilon^p \varepsilon_v}{d\varepsilon_q^p} > 0 \rightarrow \quad d\varepsilon^p \varepsilon_v < 0 \quad \text{Dilative response}$$

$$q/p = M : \quad d\varepsilon^p \varepsilon_v = 0 \quad \text{No volume change}$$

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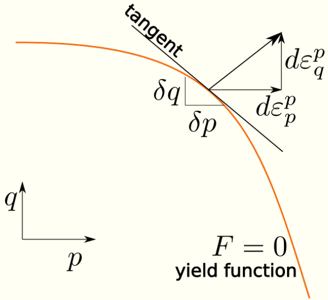
The critical state is defined by an absence of volume change or, in other words, a nil dilatancy conditions. Therefore, at critical state, the stress-dilatancy rule yields to the critical state condition $\eta = M$.

Cam-Clay (OCC): flow-rule

The original idea was very simple. The yield locus must be such that each associated flow rule $(\delta\varepsilon_v, \delta\varepsilon_s)$ would be orthogonal to the tangent to the yield locus.

$$\frac{\delta\varepsilon_v}{\delta\varepsilon_s} = -\frac{\delta\varepsilon_s}{\delta\varepsilon_v'}$$



From stress dilation condition:

$$\frac{dq}{dp'} = -(M - \eta) = -M + \eta$$

Integrating we obtain:

$$q = Mp' \ln\left(\frac{p_c'}{p'}\right)$$

Where p_c' is the value of p' at $q = 0$.

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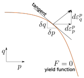

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$$q = Mp' \ln\left(\frac{p'_c}{p'}\right)$$

Where p'_c is the value of p' at $q = 0$.

Original Cam-Clay integration

$$\eta = q/p \quad \rightarrow d\eta = \frac{\partial\eta}{\partial q}dq + \frac{\partial\eta}{\partial p'}dp'$$

Which gives:

$$d\eta = \frac{dq}{p} - \frac{q}{p^2}dp \rightarrow \quad dq = pd\eta + \eta dp$$

We know from flow rule and orthogonality: $dq = dp(-M + \eta)$
Equating the above 2 equations:

$$dp = pd\eta + \eta dp = dp(-M + \eta)$$

$$pd\eta = -Mdp \rightarrow \quad deta = -M\frac{dp}{p}$$

Integrating this expression we obtain:

$$\eta = -M \ln p + C \tag{1}$$

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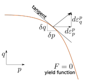

From stress dilation condition:

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Integrating we obtain:

$$q = Mp' \ln\left(\frac{p_c'}{p'}\right)$$

Where p_c' is the value of p' at $q = 0$.

Original Cam-Clay integration

$$\eta = -M \ln p + C \tag{2}$$

To find the constants, for $\eta = 0$, we get $p = p_c$:

$$0 = -M \ln p_c + C \quad C = M \ln p_c$$

Which gives:

$$\eta = M \ln p_c - M \ln p$$
$$q/p = M \ln(p_c/p)$$

Yield function:

$$F = q - Mp' \ln(p_c'/p') = 0$$

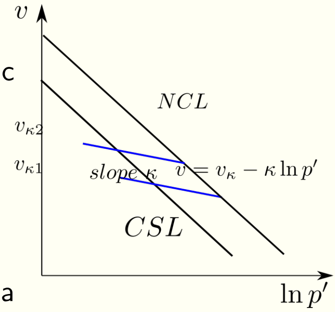
Cam-Clay (OCC): Elastic properties

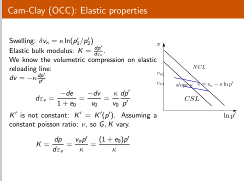
Swelling: $\delta v_\kappa = \kappa \ln(p'_1/p'_2)$
Elastic bulk modulus: $K = \frac{dp'}{d\varepsilon_v}$.
We know the volumetric compression on elastic reloading line:
$dv = -\kappa \frac{dp'}{p'}$

$$d\varepsilon_v = \frac{-de}{1+e_0} = \frac{-dv}{v_0} = \frac{\kappa}{v_0}\frac{dp'}{p'}$$

K' is not constant: $K' = K'(p')$. Assuming a constant poisson ratio: ν, so G, K vary.

$$K = \frac{dp}{d\varepsilon_v} = \frac{v_o p'}{\kappa} = \frac{(1+e_0)p'}{\kappa}$$





Observation:

- Stiffness K increases with p': correct.
- Stiffness increases with void ratio (not right)!

Note: The original derivation assumed that there were no recoverable (elastic) shear strains so $G = \infty$. We can find the stress-strain relationships for a single element in this case, but for a finite element forumulation we need to have a finite G^e. So there are two options:

- Define $G = f(e, p')$.
- Use a constant "elastic" Poisson ratio. Ratio between the shear and bulk modulus is constant. $2G/K = const$.

The first alternative has the shortcoming that depending on the choice of G we may have unreasonable values of the "elastic" Poisson's ratio. I prefer the second choice.

Cam-Clay (OCC): Hardening law

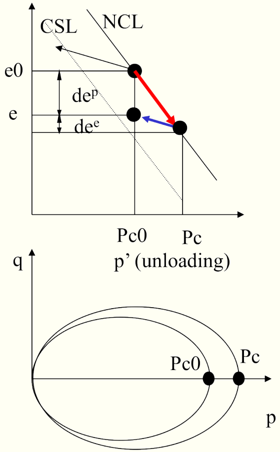
We need to define how the yield surface hardens as plastic work is being performed. Only "*memory*" parameter in our yield surface is the size: p'_c. From the isotropic NCL:

$$d\varepsilon_v = \frac{-dv}{v} = \frac{-de}{1+e} = \frac{+\lambda}{v}\frac{dp'_c}{p'_c}$$

But the increment in elastic volumetric strain is:

$$d\varepsilon_v^e = \left(\frac{-dv}{v}\right)^{elastic} = +\frac{\kappa}{v}\left(\frac{dp'_c}{p'_c}\right)$$

$$d\varepsilon_{vol} = -\frac{de}{(1+e)}$$
$$= \frac{\kappa}{(1+e)}\frac{dp'}{p'} + \frac{\lambda-\kappa}{(1+e)}\frac{dp'_c}{p'_c}$$
$$= elastic + plastic$$
$$= d\varepsilon^e_{vol} + d\varepsilon^p_{vol}$$



Therefore the increment of p_c can be related to the increment of plastic volumetric strain:

$$d\varepsilon^p_v = d\varepsilon_v - d\varepsilon^e_v = (\lambda-\kappa)\left(\frac{dp'_c}{p'_c}\right)$$
$$dp'_c = \left(\frac{v \cdot p'_c}{(\lambda-\kappa)}\right) \cdot d\varepsilon^p_v$$

Cam-Clay (OCC): Hardening law

We have seen that the hardening law:

$$H = -\left(\frac{\partial F}{\partial Wp}\right)\left(\frac{\partial Wp}{\partial \varepsilon^p}\right)^T \cdot \frac{\partial G}{\partial \sigma}$$

W_p is the vector of memory parameters. In our case, the CC model has only one parameter: p'_c and it's variation is only a function of the plastic volumetric strain. So:

$$H = -\left(\frac{\partial F}{\partial p'_c}\right)\left(\frac{\partial p'_c}{\partial \varepsilon^p}\right)^T \cdot \frac{\partial G}{\partial \sigma}$$

Cam-Clay (OCC): Hardening law

We know:

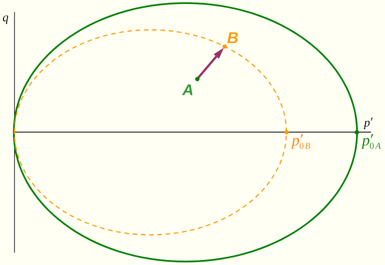
$$\frac{\partial F}{\partial p'_c} = -Mp'/p'_c$$

$$\frac{\partial p'_c}{\partial \varepsilon^p} = \frac{v}{(\lambda - \kappa)} p'_c$$

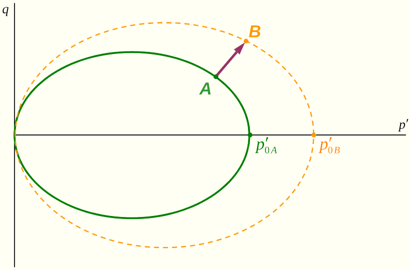
$$\frac{\partial G}{\partial \sigma} = P_p = Q_p = M - \eta$$

$$\boxed{H = -\left(\frac{\partial F}{\partial p'_c}\right)\left(\frac{\partial p'_c}{\partial \varepsilon^p}\right)^T \cdot \frac{\partial G}{\partial \sigma} = M\frac{(M - \eta)}{(\lambda - \kappa)} \cdot (1 + e) \cdot p'}$$

Deformations under an applied stress path

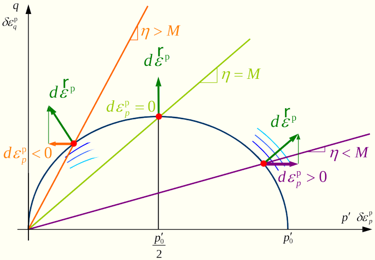


$P'_{0B} > P'_{0A}$ Elastic



$P'_{0B} < P'_{0A}$ Elasto-plastic

Hardening law



$$d\varepsilon_p^p = \frac{\lambda - \kappa}{v p'_0} dp'_0$$

- $\eta < M \rightarrow d\varepsilon_p^p > 0 \quad dp' > 0$
  Yield surface "*expands*"
- $\eta > M \rightarrow d\varepsilon_p^p < 0 \quad dp' < 0$
  Yield surface "*contracts*"
- $\eta = M \rightarrow d\varepsilon_p^p = 0 \quad dp' = 0$
  Yield surface "*constant*"

Stress-strain relation in (p', q) and $(\varepsilon_v, \varepsilon_s)$ drained TX

1. Give strain and/or stress increments
2. Check if the current stress state is inside the yield surface or outside the yield surface $q/p' = M \ln(p_c/p')$
   1. If Elastic (stress inside yield surface):
   $$\begin{bmatrix} d\varepsilon_v \\ d\varepsilon_s \end{bmatrix} = \begin{bmatrix} 1/K & 0 \\ 0 & 1/3G \end{bmatrix} \begin{bmatrix} dp' \\ dq \end{bmatrix}$$
   2. If Elastic-plastic (stress on the yield surface)
   $$\begin{bmatrix} d\varepsilon_v \\ d\varepsilon_s \end{bmatrix} = D^{ep} \begin{bmatrix} dp' \\ dq \end{bmatrix}$$

$$D^{ep} = \left[\begin{bmatrix} 1/K & 0 \\ 0 & 1/3G \end{bmatrix} + \frac{1}{Mp'} \frac{(\lambda - \kappa)}{(1 + e_0)} \begin{bmatrix} M - (q/p') & 1 \\ 1 & 1/(M - (q/p')) \end{bmatrix} \right]$$

3. Compute the unknown stress or strain increments and update the stress and strains
4. If plastic deformation, update p_c to satisfy Cam-Clay yield surface
5. Go back to step 1

Stress-strain relation in (p', q) and $(\varepsilon_v, \varepsilon_s)$ undrained TX

$d\varepsilon_v = d\varepsilon_a + 2d\varepsilon_r = 0$ (constant volume)
$d\varepsilon_s = (2/3)(d\varepsilon_a - d\varepsilon_r) = (2/3)(d\varepsilon_a - (-0.5d\varepsilon_a)) = d\varepsilon_a$

1. Give axial strain increment $d\varepsilon_a$ or dq
2. Check if the current stress state is inside the yield surface or outside the yield surface $q/p' = M \ln(p_c/p')$
   - If Elastic (stress inside yield surface):

$$\begin{bmatrix} d\varepsilon_v \\ d\varepsilon_s \end{bmatrix} = \begin{bmatrix} 1/K & 0 \\ 0 & 1/3G \end{bmatrix} \begin{bmatrix} dp' \\ dq \end{bmatrix}$$

     $d\varepsilon_v =$ from the first equation gives $dp' = 0$. This means that the effective stress path is fixed to go in the vertical direction in $p' - q$ space irrespective of any total stress path.
     The second equation gives $d\varepsilon_s$ for a given dq or dq for a $d\varepsilon_s$.

Stress-strain relation in (p', q) and $(\varepsilon_v, \varepsilon_s)$ undrained TX

4. - If Elastic-plastic (stress on the yield surface)

$$\begin{bmatrix} d\varepsilon_v \\ d\varepsilon_s \end{bmatrix} = D^{ep} \begin{bmatrix} dp' \\ dq \end{bmatrix}$$

$$D^{ep} = \left[\begin{bmatrix} 1/K & 0 \\ 0 & 1/3G \end{bmatrix} + \frac{1}{Mp'} \frac{(\lambda - \kappa)}{(1 + e_0)} \begin{bmatrix} M - (q/p') & 1 \\ 1 & 1/(M - (q/p')) \end{bmatrix} \right]$$

$d\varepsilon_v = 0$ and $d\varepsilon_s = d\varepsilon_a$ give dp' and dq
or
$d\varepsilon_v = 0$ and dq gives $d\varepsilon_s (= d\varepsilon_a)$ and dp'.

5. Update the stress and strain. The difference between the total mean pressure p and the effective mean pressure will give the pore pressure.
6. If plastic deformation, update p_c to satisfy Cam-Clay yield surface.
7. Go back to step 1

Limitations of original Cam-Clay

1. For an isotropically normally consolidated (saturated clay) specimen in TXC: Overpredicts the excess pore-pressure at failure.
2. Yield surface / plastic potential function produces too much shearing at low stress-ratios. At low stress ratio you would expect mostly plastic volumetric strains rather than deviatoric stress.
3. Yield surface is discontinous at the hydrostatic axis.
4. Overpredicts K_0 for a normally consolidated clay under 1D loading. For low $\phi_c s$ we get K_0 larger than 1 (unrealistic).
5. Other modes of shearing?
6. Anisotropy?

2019-04-29

CE394M: Cam-Clay
└Cam-Clay
└Limitations of original Cam-Clay

Limitations of original Cam-Clay

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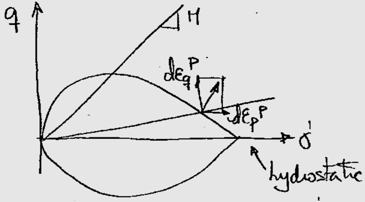
- Other modes of shearing?
- Anisotropy?



What can we change?

1. Yield function (yes)
2. Elastic constants (not really)   controlled by the compression model.
3. Flow rule (for associated models it is tied to the yield function).
4. Hardening laws (constrained already by the compression model)

MCC: Yield function

Derived from work considerations (Burland 1965, Roscoe and Burland 1968):

$$dW_{int}^p = p\sqrt{(d\varepsilon_v^p)^2 + (Md\varepsilon_s^p)^2}$$

This is the new equation describing the energy dissipated by the soil. Following similar arguments to CC:

$$dW_{ext}^p = pd\varepsilon_v^p + qd\varepsilon_s^p = p\sqrt{(d\varepsilon_v^p)^2 + (Md\varepsilon_s^p)^2} = dW_{int}^p$$

Squaring and re-arranging the terms:

$$\frac{d\varepsilon_v^p}{d\varepsilon_s^p} = \frac{M^2 - \eta^2}{2\eta} = -\frac{dq}{dp'}$$

Assuming an associative flow rule gives an elliptic yield surface:

$$\boxed{F(q,p) = q^2 - M^2 p^2 \left(\frac{p'_c}{p'} - 1\right) = 0}$$

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This is referred to as the dilatancy expression. In contrast to the original Cam-Clay, this equation predicts only plastic volumetric strain at $\eta = 0$ (isotropic state).

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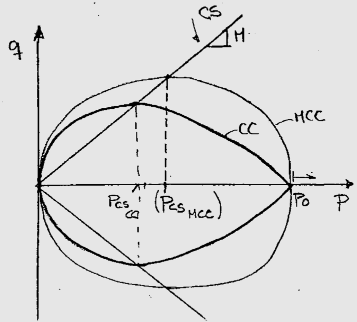
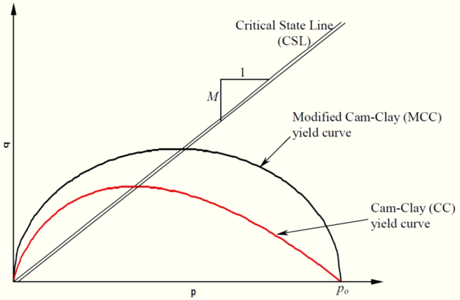


For the MCC we can find the value of p_{cs} the stress corresponding to the critical stress at CS: $q_{cs} = Mp'_{cs}$ and should be on the yield surface:

$$(Mp'_{cs})^2 = M^2(p'_{cs})^2\left(\frac{p'_c}{p'_{cs}} - 1\right) \qquad \frac{p'_c}{p'_{cs}} = 2 \rightarrow \quad p'_{cs} = p'_c/2$$

OCC v MCC

	Original Cam-clay model (Schofield and Wroth, 1968)	Modified Cam-clay model (Roscoe and Burland, 1968)
Dissipative work	$p' d\varepsilon_v^p + q d\varepsilon_s^p = M p' d\varepsilon_s^p$	$p' d\varepsilon_v^p + q d\varepsilon_s^p = p'\sqrt{(d\varepsilon_v^p)^2 + (M d\varepsilon_s^p)^2}$
Associated flow rule	$(d\varepsilon_s^p / d\varepsilon_v^p)(dq/dp') = -1$	$(d\varepsilon_s^p / d\varepsilon_v^p)(dq/dp') = -1$
Yielding of Cam-clay	$q = Mp' \ln (p_c/p')$	$q^2 + M^2 p'^2 = M^2 p' p_c$
N and Γ	$N = \Gamma + \lambda - \kappa$	$N = \Gamma + (\lambda - \kappa) \ln 2$



MCC: Stress-strain relationship

$$\begin{bmatrix} d\sigma_{11} \\ d\sigma_{22} \\ d\sigma_{33} \\ d\tau_{12} \\ d\tau_{23} \\ d\tau_{31} \end{bmatrix} = \left[D(6\times 6) \right] \begin{bmatrix} d\varepsilon_{11} \\ d\varepsilon_{22} \\ d\varepsilon_{33} \\ d\gamma_{12} \\ d\gamma_{23} \\ d\gamma_{31} \end{bmatrix}$$

$$d\sigma' = \left[\boxed{D_e} - \frac{\boxed{D_e}(\partial F / \partial \sigma')(\partial F / \partial \sigma')^T \boxed{D_e}}{-(\partial F / \partial p_c)(dp_c / d\varepsilon_v^p)(\partial F / \partial p') + (\partial F / \partial \sigma')^T \boxed{D_e}(\partial F / \partial \sigma')} \right] d\varepsilon$$

Elastic Stiffness

$$D_e = \begin{bmatrix} K+4/3G & K-2/3G & K-2/3G & 0 & 0 & 0 \\ K-2/3G & K+4/3G & K-2/3G & 0 & 0 & 0 \\ K-2/3G & K-2/3G & K+4/3G & 0 & 0 & 0 \\ 0 & 0 & 0 & G & 0 & 0 \\ 0 & 0 & 0 & 0 & G & 0 \\ 0 & 0 & 0 & 0 & 0 & G \end{bmatrix} \qquad K = \frac{vp'}{\kappa}, G = \frac{3K(1-2\nu)}{2(1+\nu)}$$

$$d\sigma' = \left[D_e - \frac{D_e \boxed{(\partial F / \partial \sigma')} \boxed{(\partial F / \partial \sigma')^T} D_e}{-(\partial F / \partial p_c)(dp_c / d\varepsilon_v^p)(\partial F / \partial p') + \boxed{(\partial F / \partial \sigma')^T} D_e \boxed{(\partial F / \partial \sigma')}} \right] d\varepsilon$$

(A) Calculation of $\partial F / \partial \sigma'$

$$F = \frac{q^2}{M^2} - p' p_c + p^2 = 0$$

$$\frac{\partial F}{\partial \sigma'} = \frac{\partial F}{\partial p'} \frac{\partial p'}{\partial \sigma'} + \frac{\partial F}{\partial q} \frac{\partial q}{\partial \sigma'}$$

$$\partial F / \partial p' = 2p - p_c$$

$$\partial F / \partial q = 2q / M^2$$

$$\partial p' / \partial \sigma' = \begin{Bmatrix} 1/3 \\ 1/3 \\ 1/3 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$

$$\partial q / \partial \sigma' = (3/2q) \begin{Bmatrix} \sigma_{xx} - p \\ \sigma_{yy} - p \\ \sigma_{zz} - p \\ 2\sigma_{xy} \\ 2\sigma_{yz} \\ 2\sigma_{zx} \end{Bmatrix}$$

$$\frac{\partial F}{\partial \sigma'} = \begin{Bmatrix} (2p - p_c)/3 + 3(\sigma_{xx} - p)/M^2 \\ (2p - p_c)/3 + 3(\sigma_{yy} - p)/M^2 \\ (2p - p_c)/3 + 3(\sigma_{zz} - p)/M^2 \\ 6\sigma_{xy}/M^2 \\ 6\sigma_{yz}/M^2 \\ 6\sigma_{zx}/M^2 \end{Bmatrix}$$

MCC: II

$$d\sigma' = \left[D_e - \frac{D_e(\partial F / \partial \sigma')(\partial F / \partial \sigma')^T D_e}{\boxed{-(\partial F / \partial p_c)(dp_c / d\varepsilon_v^p)(\partial F / \partial p')} + (\partial F / \partial \sigma')^T D_e (\partial F / \partial \sigma')} \right] d\varepsilon$$

(B) Calculation of $(\partial F / \partial p_c)(dp_c / d\varepsilon_v^p)(\partial F / \partial p)$

$$\frac{\partial F}{\partial p_c} = -p \qquad \frac{dp_c}{d\varepsilon_v^P} = \frac{vp_c}{(\lambda - \kappa)} \qquad \frac{\partial F}{\partial p} = 2p - p_c$$

$$(\partial F / \partial p_c)(dp_c / d\varepsilon_v^p)(\partial F / \partial p) = -p \frac{vp_c}{(\lambda - \kappa)}(2p - p_c)$$

(C) Assemble [6x6] matrix

$$d\sigma' = \left[D_e - \frac{D_e(\partial F / \partial \sigma')(\partial F / \partial \sigma')^T D_e}{-(\partial F / \partial p_c)(dp_c / d\varepsilon_v^p)(\partial F / \partial p') + (\partial F / \partial \sigma')^T D_e (\partial F / \partial \sigma')} \right] d\varepsilon$$

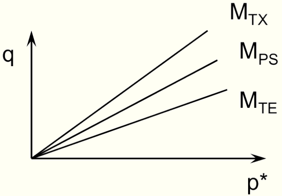
$$[6\text{x}1] = \left[[6\text{x}6] - \frac{[6\text{x}6][6\text{x}1][1\text{x}6][6\text{x}6]}{-[1\text{x}1][1\text{x}1][1\text{x}1] + [1\text{x}6][6\text{x}6][6\text{x}1]} \right] [6\text{x}1]$$

Test required

1. Slow drained or undrained test with pore pressure measurement at different preconsolidation pressure. Test must be taken to very large strains to reach to the critical state.
2. Isotropic consolidateion test or incrementental loading consolidation test.

Slope of failure line: M If ϕ_{cs} is assumed to be constant, then M is not constant.

- In TXC: $M_{TXC} = \frac{6 \sin \phi_{cs}}{3 - \sin \phi_{cs}}$
- In TXE: $M_{TXE} = \frac{6 \sin \phi_{cs}}{3 + \sin \phi_{cs}}$
- In PS: $M_{PS} = 2 \sin \phi_{cs}$ (assuming $\sigma_2 \approx \frac{\sigma_1 + \sigma_3}{2}$)



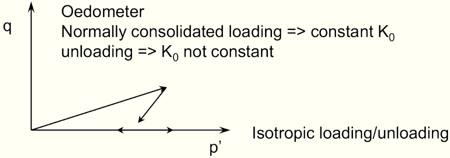
Cam-Clay material properties determination: II

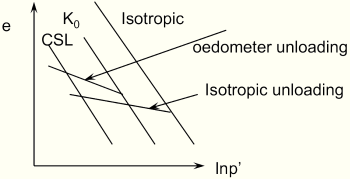
λ and κ: Compression index and swelling index

1. Use isotropic consolidation. Plot in $v - \ln p'$ plane. Measure λ & κ.
2. From odeometer test, plot void ratio e vs $\log \sigma'_v$:

$$\lambda = 0.4343 C_c$$
$$\kappa = 0.4343(1.4 C_{r/s}) = 0.63 C_{r/s} = (0.2\ 0.33)\lambda$$

1. swelling and recompression lines are highly nonlinear in $e - \ln p'$ space.
2. κ is usually not less than 0.1λ or greater than 0.5λ.
3. $\kappa$is about 0.03 to 0.06 for many medium plasticity clays.
4. modify κ to try to fit data. λ is usually easier to accurately calculate.

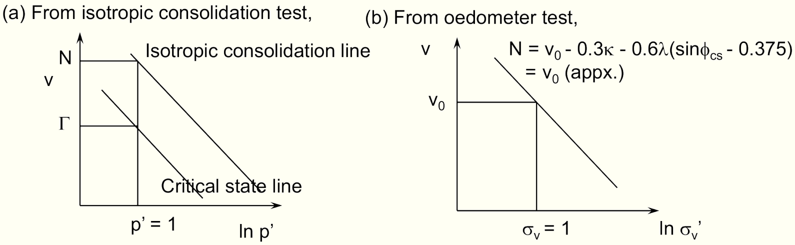




Cam-Clay material properties determination: III

Γ or N

1. Critical state line: $v = \Gamma - \lambda \ln p'$
2. Isotropic normally consolidated line: $v = N - \lambda \ln p'$
3. Original Cam-Clay: $N = \Gamma + (\lambda - \kappa)$
4. Modified Cam-Clay: $N = \Gamma + (\lambda - \kappa) \ln 2$



Cam-Clay material properties determination: IV

Elastic properties: G **or** ν

1. Elastic bulk modulus $K_e = dp'/d\varepsilon_v = vp^prime/\kappa$
2. Choosing Poisson's ratio ν constant gives G_e which varies as K_e.
3. Typically $\nu = 0.2 - 0.4$.

Preconsolidation pressure p_c

1. Estimate OCR
2. $\sigma_{v,max} = OCR\sigma_{v,current}$
3. $\sigma_{h,max} = K_{0,nc}\sigma_{v,max}$
4. $q_{max} = \sigma_{v,max} - \sigma_{h,max}, p_{max} = (1/3)(\sigma_{v,max} + 2\sigma_{h,max})$
5. Define p_c:
    - Cam-Clay: $q_{max} = Mp_{max}\ln(p_c/p_{max})$
    - MCC: $q^2_{max} = M^2 p_{max}(p_c - p_max)$

Cam-Clay material properties determination: V

Cam-clay parameters : Correlation For clayey soils, attempts have been made to obtain the cam-clay parameters from index tests, especially plasticity index. It should be remembered that most of the soils tested for correlation were remoulded and direct application to natural clays requires caution. The users should be fully aware that limitations exist and these correlations should be regarded as a first approximation.

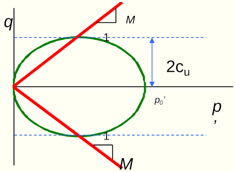
- Atkinson (1993) $\lambda = PIG_s/460 \quad \Gamma = 1.25 + \lambda \ln 10,000$
- Nakase, Kamei and Kusakabe (1988)- study based on Japanese clays: $\lambda = 0.02 + 0.0045PI \qquad \kappa = 0.00084(PI - 4.6) \qquad N = 1.52 + 0.19PI$
- Nakase et al. (1988) and Frydman (1990) observed that M was independent of PI. Atkinson (1993) finds that M tends to increase with decreasing PI.

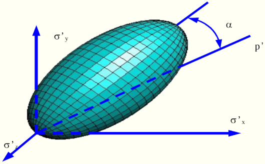
Drawbacks of MCC: Computational problems

- In undrained triaxial test on a heavily overconsolidated soil, after the stress point reaches the yield surface (above M line), due to the negative direction of volumetric plastic strain vector, the yield surface contracts.
- This phenomenon is referred to as **strain softening**.
- Even though the constitutive model is perfectly able to model this aspect of mechanical behaviour, strain softening may lead to problems in a finite element analysis: e.g. mesh dependency and problems with convergence.
- That can be overcome with good coding & algorithms, but many leading codes still struggle and diverge or give erroneous results!

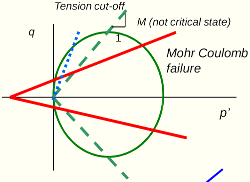
Drawbacks of MCC: Strength prediction in undrained conditions

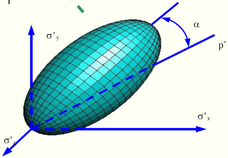
- MCC model assumes Drucker-Prager failure condition, which overestimates undrained strength in triaxial extension.
- Better predictions if Mohr Coulomb failure or Lode angle dependency is introduced
- Real soils are anisotropic and both the shape and size of the yield surface would need to change (see e.g., Wheeler et al. 2003, Can Geotech J for S-Clay1 model)





- Given MCC assumes an associated flow rule, the model predicts unrealistically high K_0 values in normally consolidated range
- This has been fixed e.g. in the Soft Soil model by de-coupling the volumetric yield surface (cap) from the failure line
- Consequently, in the Soft Soil model, M as become a "*shape*" coefficient and no longer corresponds to the critical state line
- Alternatively, the anisotropic S-CLAY1 model also gives good K0 prediction
- Non-associated flow rule is also an option which will help with that issue





Advantages and Limitations of Cam-Clay models

Advantages:

- Unified framework of elastic - plastic behaviour, deals with volumetric & shearing strains, drained & undrained, prefailure and failure,
- Uses a small number of parameters $(M, \lambda, \kappa, \Gamma, \nu)$
- fairly well established,
- Qualitative prediction of soil behaviour - replicates many behaviour not possible to replicate in e.g. Mohr-Coulomb model.

Limitations:

1. Largely elastic for heavily OC clays (and dense sands).
2. Soils do not always reach the critical state or necessarily stay there, such as by breakdown in fabric strain softening.
3. No anisotropy.
4. Stress reversals within elastic domain are purely elastic after initial yielding.
5. No creep.
6. Model predicts conservative K_0 value.