

1 Theory

1.1 Question 1

Based on the assumption that there is no noise or error in the control system, predict the next pose p_{t+1} as a nonlinear function of the current pose p_t and the control inputs d_t and α_t . (5 points)

Answer: Here, we are given that there is no noise or error in the control system. Therefore, we can predict the next pose with our prediction of the previous pose without a control input with the effect of the control input. This is equivalent to just finding the mean at the next timestep with identity covariance

$$\begin{aligned}\mu_{t+1} &= g(u_{t+1}, \mu_t) \\ \mu_{t+1} &= g([d_t \ \alpha_t]^T, [x_t \ y_t \ \theta_t]^T) \\ \mu_{t+1} &= \begin{bmatrix} x_t + d_t \cos(\theta_t) \\ y_t + d_t \sin(\theta_t) \\ \theta_t + \alpha_t \end{bmatrix} \\ p_{t+1} &= \mathcal{N}(\mu_{t+1}, I)\end{aligned}$$

1.2 Question 2

However, in reality there are some errors when the robot moves due to the mechanism and the terrain. Assume the errors follow Gaussian distributions: $e_x \sim N(0, \sigma_x^2)$ in x-direction, $e_y \sim N(0, \sigma_y^2)$ in y-direction, and $e_\alpha \sim N(0, \sigma_\alpha^2)$ in rotation respectively (all in robot's coordinates). For details, please see Fig. 1. Now if the uncertainty of the robot's pose at time t can be represented as a 3-dimensional Gaussian distribution $N(0, \Sigma_t)$, what is the predicted uncertainty of the robot at time $t+1$? Please express it as a Gaussian distribution with zero mean. (5 points)

Answer: In this problem, we are still in the prediction step but now have to consider the process error in correctly predicting the pose. Below G_t is the jacobian of our non-linear process function g and R_t is the process noise. If we know the function g , we can calculate this by hand as well.

$$\begin{aligned}R_{t+1} &= \begin{bmatrix} \sigma_x^2 & 0 & 0 \\ 0 & \sigma_y^2 & 0 \\ 0 & 0 & \sigma_\alpha^2 \end{bmatrix} \\ G_{t+1} &= \begin{bmatrix} \frac{\partial g_x}{\partial x} & \frac{\partial g_x}{\partial y} & \frac{\partial g_x}{\partial \theta} \\ \frac{\partial g_y}{\partial x} & \frac{\partial g_y}{\partial y} & \frac{\partial g_y}{\partial \theta} \\ \frac{\partial g_\theta}{\partial x} & \frac{\partial g_\theta}{\partial y} & \frac{\partial g_\theta}{\partial \theta} \end{bmatrix} \\ G_{t+1} &= \begin{bmatrix} 1 & 0 & -d_t \sin(\theta_t) \\ 0 & 1 & d_t \cos(\theta_t) \\ 0 & 0 & 1 \end{bmatrix} \\ \Sigma_{t+1} &= G_{t+1} \Sigma_t G_{t+1}^T + R_{t+1}\end{aligned}$$

$$\mathcal{N}(\vec{0}, \Sigma_{t+1})$$

1.3 Question 3

Consider a landmark l being observed by the robot at time t with a laser sensor which gives a measurement of the bearing angle β (in the interval $(-\pi, \pi]$) and the range r , with noise $n_\beta \sim \mathcal{N}(0, \sigma_\beta^2)$ and $n_r \sim \mathcal{N}(0, \sigma_r^2)$ respectively. Write down the estimated position (l_x, l_y) of landmark l in global coordinates as a function of p_t , β , r , and the noise terms. (5 points)

Answer: You can calculate the landmark position as follows:

We clarify the decomposition of the robot's pose below:

$$p_x, p_y, p_\theta = p_t$$

We then calculate the landmark component estimates using our inputs:

$$l_x = p_x + \mathcal{N}(r, \sigma_r^2) * \cos(p_\theta + \mathcal{N}(\beta, \sigma_\beta^2))$$

$$l_y = p_y + \mathcal{N}(r, \sigma_r^2) * \sin(p_\theta + \mathcal{N}(\beta, \sigma_\beta^2))$$

That is, you can displace by the pose to get the robot location components for x and y . From there, We can sample from the range with mean r and variance σ_r^2 in order to obtain a range estimate. Then we can take the orientation of the robot and adjust the angle by the bearing β to get the angle in the world frame. We must sample the bearing angle, however, from a normal distribution with mean β and with variance σ_β^2 in order to estimate the uncertainty of the measurement

1.4 Question 4

Answer: For this, we can formulate backwards in order to calculate r and β

We can first calculate the distance from the robot to the landmark then impart the range noise to get the estimate

$$r = \sqrt{(l_y - p_y)^2 + (l_x - p_x)^2} + n_r$$

We can use the *arctan2* function to calculate to angle in the world frame to the landmark. From here, we can subtract the robot's orientation angle in order to retrieve the value for the bearing β . Lastly, we can impart the noise in order to get a validate estimate then validate that our angle is in the valid range of $[-\pi, \pi)$

$$\beta = \text{wrap2pi}(\text{arctan2}(l_y - p_y, l_x - p_x) - p_\theta + n_\beta)$$

1.5 Question 5

Answer: Reminder that this matrix should be $(2, 3)$ which will transform poses to measurements. This is the jacobian so it should be the first derivative of measurements w.r.t. components of the pose

$$H_p = \begin{bmatrix} \frac{\partial \beta}{\partial p_x} & \frac{\partial \beta}{\partial p_y} & \frac{\partial \beta}{\partial p_\theta} \\ \frac{\partial r}{\partial p_x} & \frac{\partial r}{\partial p_y} & \frac{\partial r}{\partial p_\theta} \end{bmatrix}$$

$\frac{r}{p_x}$ Derivative

$$\frac{\partial r}{\partial p_x} = \frac{1}{2}((l_y - p_y)^2 + (l_x - p_x)^2)^{-\frac{1}{2}} * -2(l_x - p_x)$$

$$\frac{\partial r}{\partial p_x} = -\frac{l_x - p_x}{((l_y - p_y)^2 + (l_x - p_x)^2)^{\frac{1}{2}}}$$

$\frac{r}{p_y}$ Derivative

$$\frac{\partial r}{\partial p_y} = -\frac{l_y - p_y}{((l_y - p_y)^2 + (l_x - p_x)^2)^{\frac{1}{2}}}$$

$\frac{r}{p_\theta}$ Derivative

$$\frac{\partial r}{\partial p_\theta} = 0$$

$\frac{\beta}{p_x}$ Derivative

$$\frac{\partial \beta}{\partial p_x} = \frac{1}{1 + \left(\frac{l_y - p_y}{l_x - p_x}\right)^2} * \frac{(l_y - p_y)}{(l_x - p_x)^2}$$

$$\frac{\partial \beta}{\partial p_x} = \frac{(l_x - p_x)^2}{(l_x - p_x)^2 + (l_y - p_y)^2} * \frac{(l_y - p_y)}{(l_x - p_x)^2}$$

$$\frac{\partial \beta}{\partial p_x} = \frac{(l_y - p_y)}{(l_x - p_x)^2 + (l_y - p_y)^2}$$

$\frac{\beta}{p_y}$ Derivative

$$\frac{\partial \beta}{\partial p_y} = \frac{1}{1 + \left(\frac{l_y - p_y}{l_x - p_x}\right)^2} * -\frac{l_x - p_x}{(l_x - p_x)^2}$$

$$\frac{\partial \beta}{\partial p_y} = \frac{(l_x - p_x)^2}{(l_x - p_x)^2 + (l_y - p_y)^2} * -\frac{l_x - p_x}{(l_x - p_x)^2}$$

$$\frac{\partial \beta}{\partial p_y} = \frac{-(l_x - p_x)}{(l_x - p_x)^2 + (l_y - p_y)^2}$$

$\frac{\beta}{p_\theta}$ Derivative

$$\frac{\partial \beta}{\partial p_\theta} = -1$$

Putting it all together Let's create some intermediate variables for simplicity:

$$\delta_x = l_x - p_x$$

$$\delta_y = l_y - p_y$$

$$\delta = (l_x - p_x)^2 + (l_y - p_y)^2$$

$$H_p = \begin{bmatrix} \frac{\delta_y}{\delta} & \frac{-\delta_x}{\delta} & -1 \\ \frac{\delta_x}{\delta} & \frac{\delta_y}{\delta} & 0 \\ \frac{1}{\delta^{\frac{1}{2}}} & \frac{1}{\delta^{\frac{1}{2}}} & 0 \end{bmatrix}$$

1.6 Question 6

$$H_t = \begin{bmatrix} \frac{\partial r}{\partial l_x} & \frac{\partial r}{\partial l_y} \\ \frac{\partial \beta}{\partial l_x} & \frac{\partial \beta}{\partial l_y} \end{bmatrix}$$

$$\frac{\partial r}{\partial l_x} = \frac{1}{2} \delta^{-\frac{1}{2}} * -2\delta_x = \frac{-\delta_x}{\delta^{\frac{1}{2}}}$$

$$\frac{\partial r}{\partial l_y} = \frac{1}{2} \delta^{-\frac{1}{2}} * -2\delta_y = \frac{-\delta_y}{\delta^{\frac{1}{2}}}$$

$$\frac{\partial \beta}{\partial l_x} = \frac{\delta_x^2}{\delta_y^2} * \frac{-\delta_y}{\delta_x^2} = \frac{-1}{\delta_y}$$

$$\frac{\partial \beta}{\partial l_y} = \frac{1}{\delta_x}$$

$$H_t = \begin{bmatrix} \frac{-\delta_x}{\delta^{\frac{1}{2}}} & \frac{-\delta_y}{\delta^{\frac{1}{2}}} \\ \frac{-1}{\delta_y} & \frac{1}{\delta_x} \end{bmatrix}$$

2 Implementation and Evaluation

Question 1

6 landmarks present

Question 2

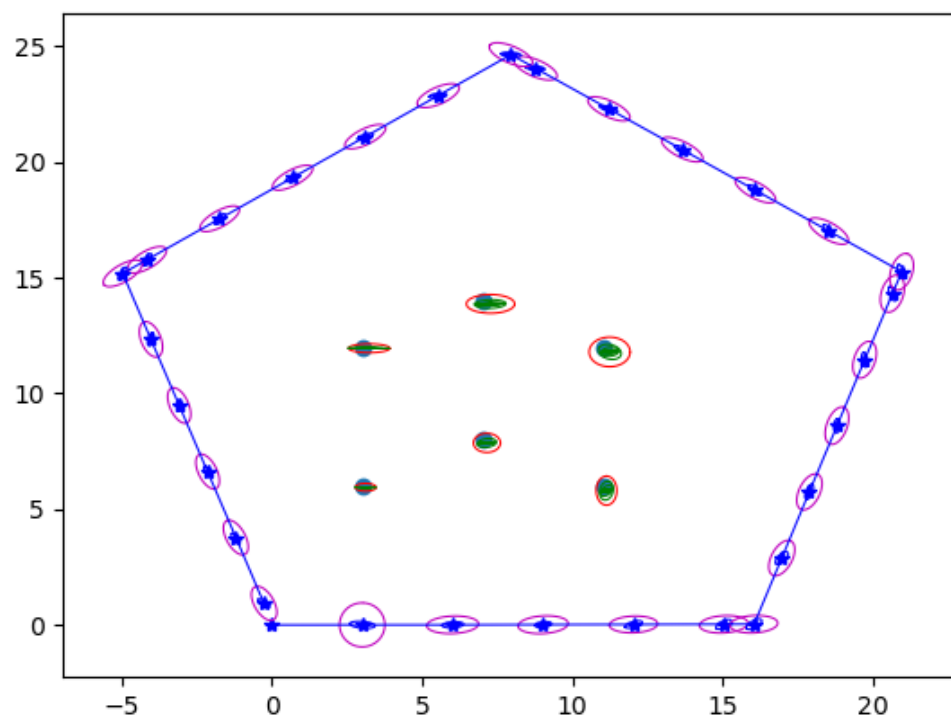


Figure 1: EKF SLAM Result