

EE445M/EE360L.6

Embedded and Real-Time Systems/ Real-Time Operating Systems

Lecture 6: Analog Input, Analog Filters, Analog-to-Digital Conversion

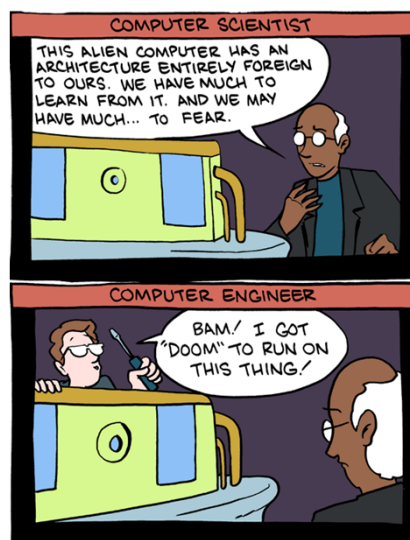
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EE445M vs. CS372

THE DIFFERENCE:

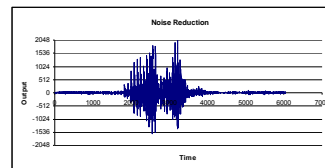
<http://www.smbc-comics.com/index.php?db=comics&id=2158#comic>

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Class Agenda

- Recap: RTOS Kernel
 - Multi-tasking, context switch, scheduling
 - Synchronization, communication, semaphores
- Outlook: Applications of RTOS
 - Lab 4: Digital scope & spectrum analyzer
 - Analog input and filters
 - Digital filter, FFT
 - Display amplitude vs. time/frequency on LCD



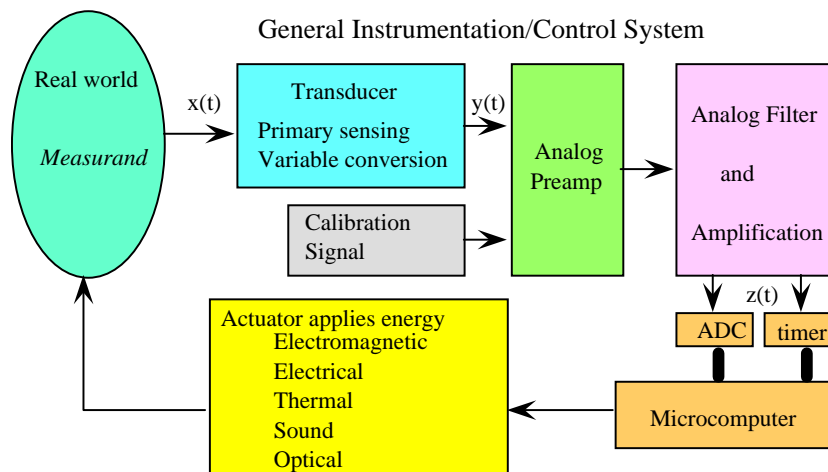
Reference book, Chapter 5

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Instrumentation & Control



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Data Acquisition System (DAS)

- Quantitative (thermometer in EE445L)
 - Range (r_x)
 - Resolution (Δx)
 - Precision (n_x in alternatives)
 - Frequencies of interest (f_{\min} to f_{\max})
- Qualitative (sound recording in EE445M)
 - “sounds good”
 - “looks pretty”
 - “feels right”

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Data Acquisition System (DAS)

- Other qualitative DAS
 - Detection of events (baby apnea monitor)
 - true positive (TP): stop breathing & monitor alarm
 - false positive (FP): breathing OK, but monitor alarm
 - false negative (FN): stop breathing & no alarm
 - Prevalence = $(TP + FN) / (TP + TN + FP + FN)$
 - Sensitivity = $TP / (TP + FN)$
 - Specificity = $TN / (TN + FP)$
 - PPV = $TP / (TP + FP)$
 - NPV = $TN / (TN + FN)$

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Analog Signal Processing

- Analog circuit design with single supply
 - MAX494CPD/TLC2274ACN rail to rail op amp
- Instrumentation amps (EE445L)
 - INA122
- Noise measurements and reduction
- Analog sensors
 - Electret microphones (sound)
 - IR distance sensor
- Analog filters



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Convert to Single Supply

- $V_{cc} = 3.3V$, start with design using $+V_s$ $-V_s$
- Assume ADC range is 0 to V_{max} (0 to 3V)
- Add an analog reference, $V_{ref} = \frac{1}{2} V_{max}$
- **Map**

– $-V_s$ (-12)	to	digital ground
– Analog ground	to	V_{ref} reference
– $+V_s$ (+12)	to	V_{cc} supply

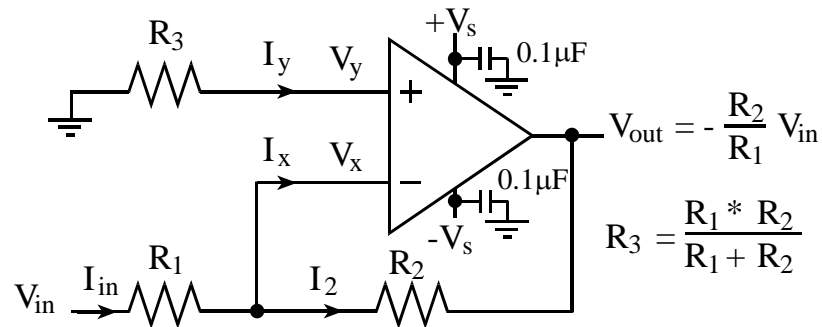
Reference EE345L book, Chapter 5

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Inverting Amp



Use a rail-to-rail op-amp and map

-Vs	to	digital ground
Analog ground	to	Vref reference
+Vs	to	Vcc supply

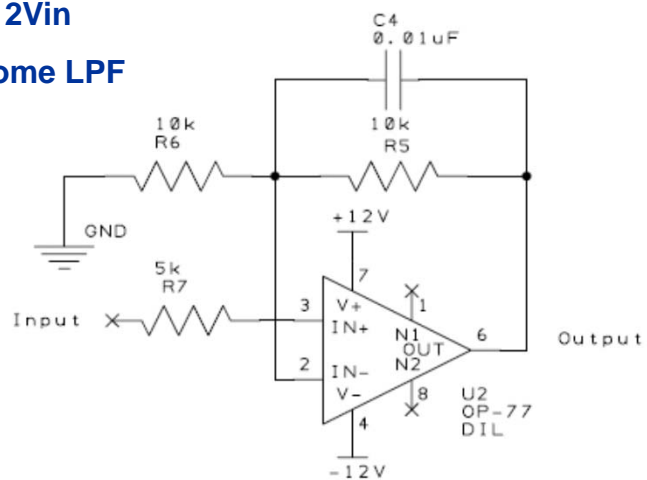
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Original Design

Vout = 2Vin
with some LPF



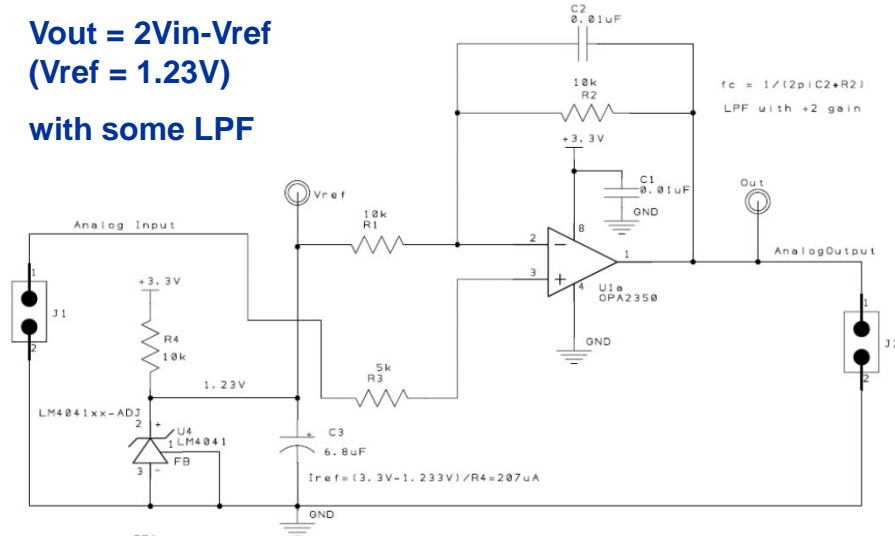
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New Design

$V_{out} = 2V_{in} - V_{ref}$
($V_{ref} = 1.23V$)
with some LPF



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Instrumentation Amp

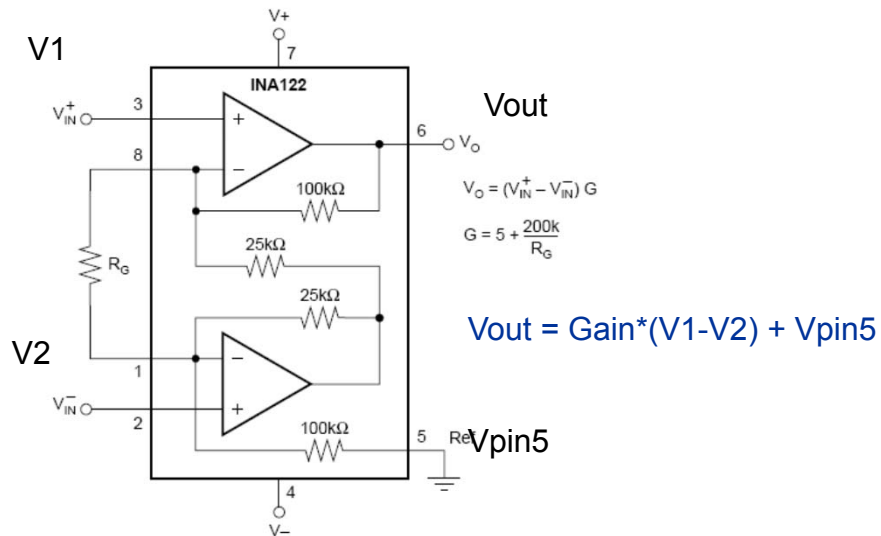
- Necessary conditions (must be true)
 - Differential input (as in any op-amp)
- Motivation (at least one must be true)
 - Large gain
 - Large input impedance
 - Large common mode rejection ratio (CMMR)
 - Low noise
 - Small package

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Burr-Brown INA122

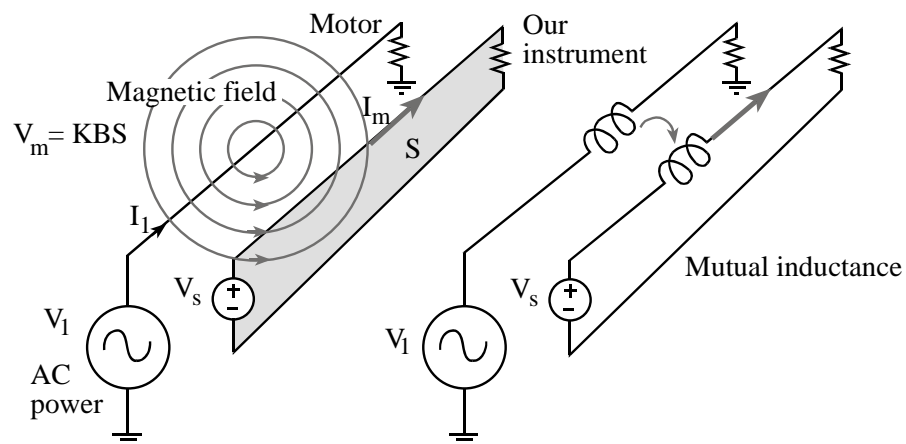


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Magnetic Field Noise

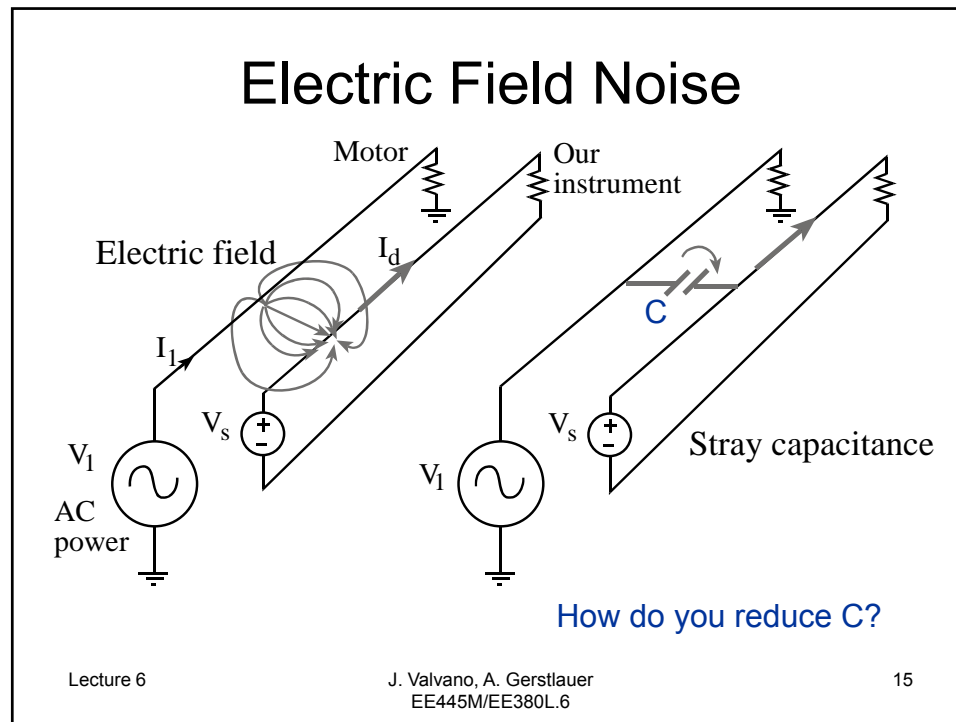


How do you reduce S?

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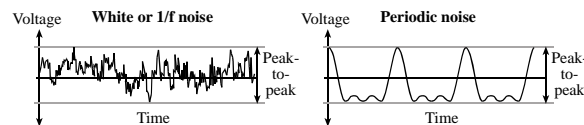
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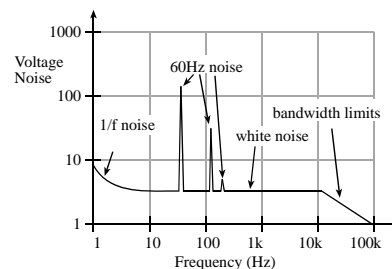
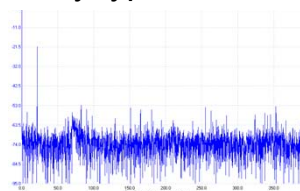


Noise Measurement

- Digital volt meter (AC mode)
 - Most accurate quantitative noise measure
- Oscilloscope (line trigger)
 - Shape



- Spectrum Analyzer
 - Classify type



Noise Reduction (1)

1. Reducing noise from the source

- Shielding
 - Enclose noisy sources in a grounded metal box
- Filter noisy signals
- Limit the rise/fall times of noisy signals.
- Limiting the di/dt in the coil.



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Noise Reduction (2)

2. Limiting the coupling between the noise source and instrument

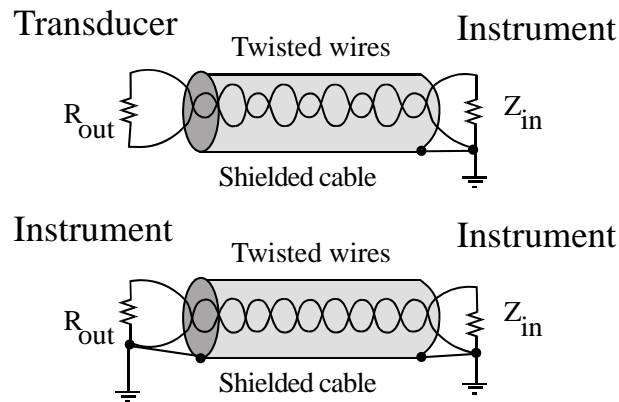
- Maximize the distance from source to instrument
- Cables with noisy signals should be twisted together
- Cables should also be shielded.
- For high frequency signals, use coaxial
- Reduce the length of a cable
- Place the delicate electronics in a grounded case
- Optical or transformer isolation circuits

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Limiting the Coupling



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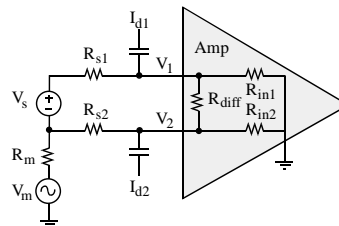
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Noise Reduction (3)

3. Reduce the noise at the receiver

- Bandwidth should be as small as possible.
- Add frequency-reject digital filters
- Use power supply decoupling capacitors on each
- Twisted wires then I_{d1} should equal I_{d2}
 - $V_1 - V_2 = R_{s1} I_{d1} - R_{s2} I_{d2}$

Henry Ott, *Noise Reduction Techniques in Electronic Systems*, Wiley, 1988.
Ralph Morrison, *Grounding and Shielding Techniques*, Wiley, 1998.

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Electret Condenser Microphone

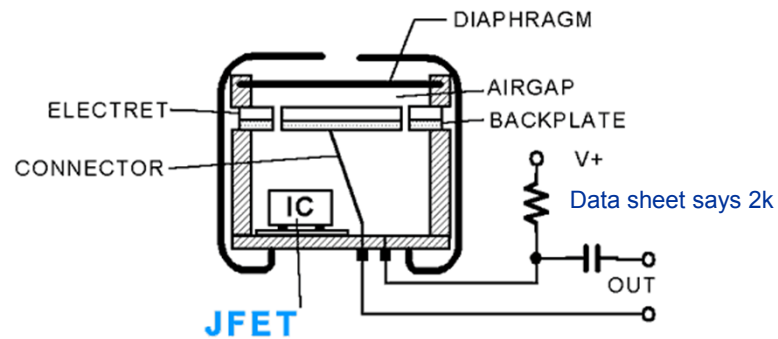


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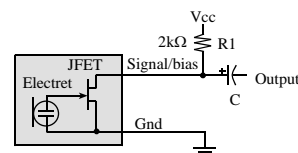
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Cross-Section of Typical ECM



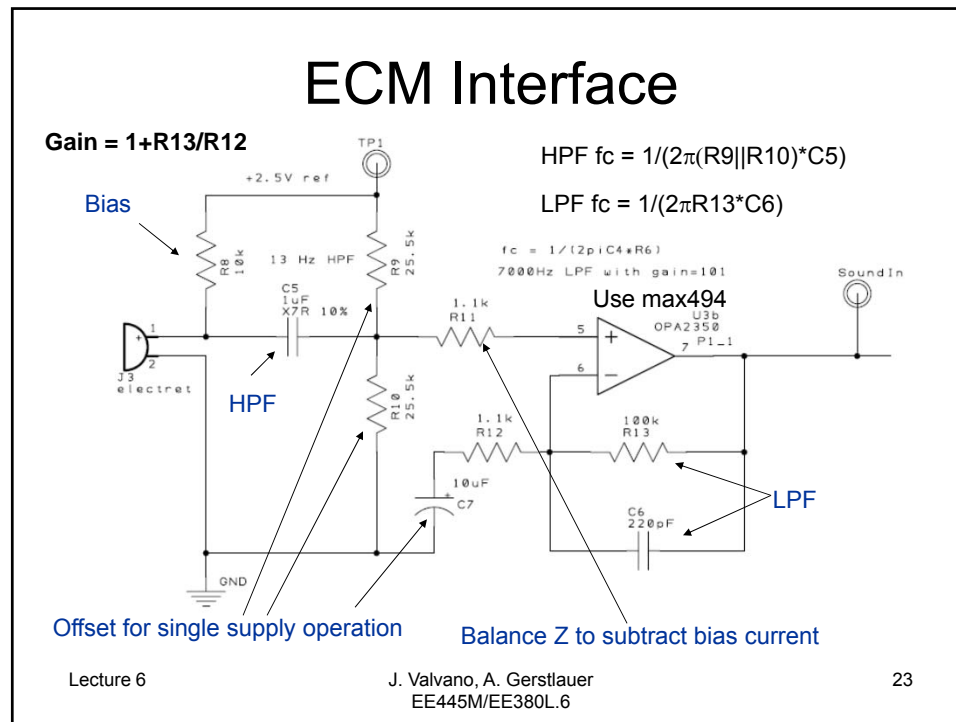
- JFET Buffer
- Phantom Biasing



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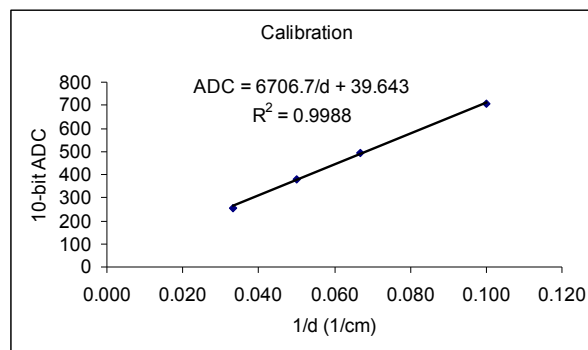
Sharp GP2Y0A21YK

- Infrared distance sensor
 - You will need 5V to power IR sensor
 - Needs analog LPF
 - Reduces noise
 - Analog input protection
 - Needs digital median filter
 - Needs 10 mF or larger +5V to Gnd cap for each sensor



IR Sensor Calibration

d (cm)	1/d	ADC
10	0.100	703
15	0.067	484
20	0.050	380
30	0.033	260



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Sharp GP2Y0A21YK

- Accuracy => Calibration
- Resolution => Noise

$$\begin{aligned} \text{ADC} &= 6707/d + 40 \\ d &= 6707/(\text{ADC} - 40) \\ d \text{ (0.01cm)} &= 6706700/(\text{ADC} - 40) \end{aligned}$$



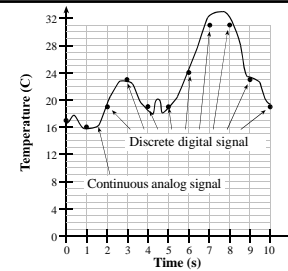
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Sampling

- Time & value quantizing
 - Precision $n_z = 2^n$
- Nyquist theory
 - If sampled at f_s , digital samples only contain frequency components from 0 to $\frac{1}{2}f_s$
 - If analog signal contains frequency components larger than $\frac{1}{2}f_s$, **aliasing** error
- System design
 - Choice of sampling rate: $f_s > 2 f_{\max}$
 - Low pass analog filter to remove frequency components above $0.5f_s$
 - A digital filter can not be used to remove aliasing



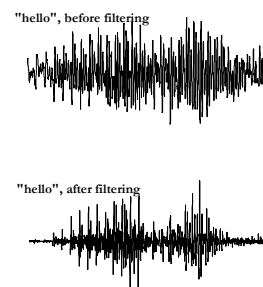
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Filter Types

- Analog
 - Low pass filter (LPF)
 - High pass filter (HPF)
 - Band pass filter (BPF)
- Digital
 - Extremely flexible
 - But only available after sampling



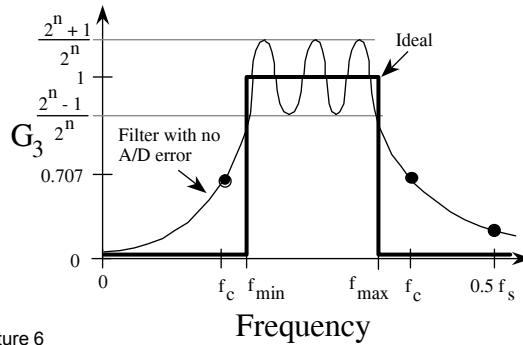
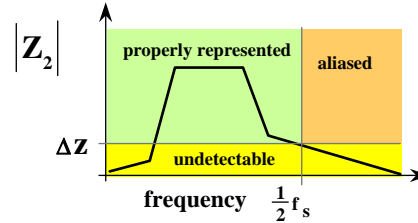
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Analog Filters

- Prevent aliasing
 - No signal $> 0.5f_s$
- Band-pass filter

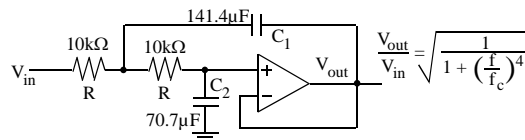


Gain $G_3 = |H_3(s)|$
 Pass $f_{min} \leq f \leq f_{max}$
 Min. error seen by ADC

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Butterworth Filters



- 2-pole Butterworth filter
 1. Select the cutoff frequency, f_c
 2. Divide the two capacitors by $2\pi f_c$
 - $C_{1A} = 141.4\mu F / 2\pi f_c$
 - $C_{2A} = 70.7\mu F / 2\pi f_c$
 3. Locate two standard value capacitors (with 2/1 ratio) in the same order of magnitude as the desired values
 - $C_{1B} = C_{1A}/x$
 - $C_{2B} = C_{2A}/x$
 4. Adjust the resistors to maintain the cutoff frequency
 - $R = 10k\Omega \cdot x$

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lpf.xls
 TI FilterPro

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