

NE506 HW5: Part II

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Abstract

What follows is a compilation of the responses to questions posed in Part III of homework #5 for NE506. All answers are already contained in the `readme.txt` files of the appropriate part's subdirectory, but they have been copied here for convenience.

Note that the input file in this directory does **not** contain the changes outlined in part 2.

Situation

Consider the simple aqueous reactor model in the file `hw5.2.i`. Assume a reactor power of 250 kW.

Part 1

Question

Determine the U-235 enrichment that will make this system critical. Give an answer to the nearest 0.1%.

Response

Via guess and check, the appropriate material was determined to be:

```
M1 1001 2 8016 1 92235 0.00649 92238 0.09351
```

This level of enrichment yields $k_{\text{eff}} = 0.99942$.

Part 2

Question

Show that this is subcritical with the central control rod fully inserted.

Code

Some changes were made to the geometry in order to model a fully inserted control rod. The lines

```

6 3 -4 -6 106
16 0 -6 -106
...
imp:n 1 10r 0

```

Were changed to:

```

6 3 -4 -6
...
imp:n 1 9r 0

```

Response

With these geometry changes, MCNP5 yields a new value: $k_{\text{eff}} = 0.96823$.

Part 3

Question

Create a Cartesian mesh tally with a 3 cm mesh over the entire system. Provide the following plots:

- across the core at axial heights of 30 cm, 55 cm, 75 cm
- on the y-z plane

Code

A mesh tally FMESH card was created for this problem.

```

c 3 cm mesh
FMESH4:n GEOM=xyz ORIGIN=-51 -51 -1
      IMESH=51 IINTS=34
      JMESH=51 JINTS=34
      KMESH=101 KINTS=34

```

Results

The following plots (Fig 1) were obtained from the mesh tally:

Part 4

Question

Approximate the dose to a worker by calculating the dose at a point 1 m off the ground and 5 m outside the reactor.

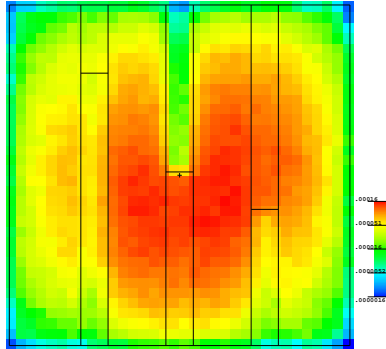
```

04/18/13 12:09:38
Simple aqueous reactor model

probid = 04/18/13 12:00:32
basis: 32
( 0.000000, 1.000000, 0.000000)
( 0.000000, 0.000000, 1.000000)
origin:
( 0.00, 0.00, 50.00)
extent = ( 51.00, 51.00)

Mesh Tally 4
nps 750287
runtime = runtime 2
dump

```



(a) The y-z plane.

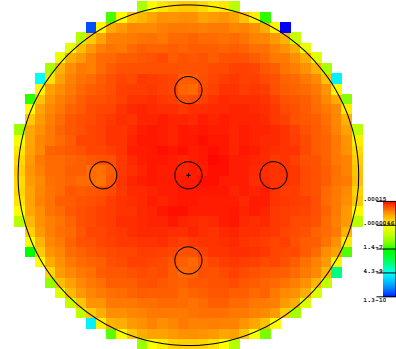
```

04/18/13 12:07:31
Simple aqueous reactor model

probid = 04/18/13 12:00:32
basis: 32
( 1.000000, 0.000000, 0.000000)
( 0.000000, 1.000000, 0.000000)
origin:
( 0.00, 0.00, 30.00)
extent = ( 51.00, 51.00)

Mesh Tally 4
nps 750287
runtime = runtime 2
dump

```



(b) Across the core at an axial height of 30cm.

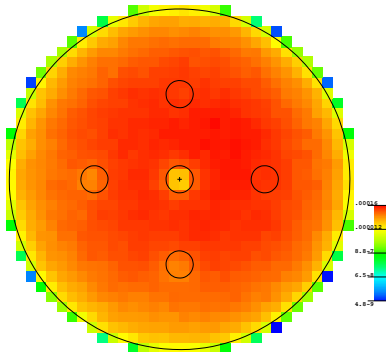
```

04/18/13 12:09:29
Simple aqueous reactor model

probid = 04/18/13 12:00:32
basis: 32
( 1.000000, 0.000000, 0.000000)
( 0.000000, 1.000000, 0.000000)
origin:
( 0.00, 0.00, 55.00)
extent = ( 51.00, 51.00)

Mesh Tally 4
nps 750287
runtime = runtime 2
dump

```



(c) Across the core at an axial height of 55cm.

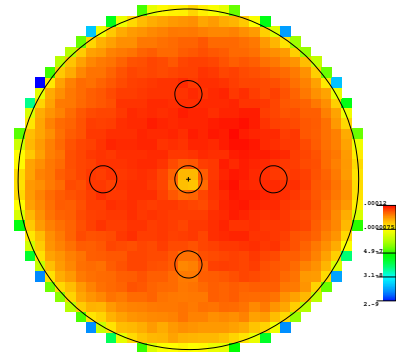
```

04/18/13 12:10:59
Simple aqueous reactor model

probid = 04/18/13 12:00:32
basis: 32
( 1.000000, 0.000000, 0.000000)
( 0.000000, 1.000000, 0.000000)
origin:
( 0.00, 0.00, 75.00)
extent = ( 51.00, 51.00)

Mesh Tally 4
nps 750287
runtime = runtime 2
dump

```



(d) Across the core at an axial height of 75cm.

Figure 1: Plots of mesh tally results from various slices of the core.

Code

First, a fission “F7” tally was carried out to determine the source strength.

```

c Fission tally for source strength
F7:n (1 2 12 3 13 4 14 5 15 6 16)
SD7 1
FM7 1.6e-19

```

Then, using the results from the fission tally, the dose could be calculated.

```

c Detector tally
F5:n 0 550 100 0.1
c Neutron dose multipliers
DE5 2.5e-8 1e-7 5ILOG 1e-1 5e-1 1 2 5 10 20
DF5 3.85e-6 4.17e-6 4.55e-6 4.35e-6 4.17e-6 3.7e-6 3.57e-6
      2.08e-5 7.14e-5 1.18e-4 1.43e-4 1.47e-4 1.47e-4 1.54e-4
FM5 2.116473785E+16

```

Additionally, to ensure that the detector was not placed in a region of zero importance, some additional geometry was defined¹.

C Cell cards

```

1  1 -1  -1 2 3 4 5 6
2  2 -1  -2 -102
12 0      -2 102
3  2 -1  -3 -103
13 0      -3 103
4  2 -1  -4 -104
14 0      -4 104
5  2 -1  -5 -105
15 0      -5 105
6  3 -4  -6 106
16 0      -6 -106
101 0  1 -9
100 0  0  9

```

C Surf cards

```

9 RPP -50 50 -50 560 0 110
1 RCC  0   0 0 0 0 100 50
2 RCC 25   0 0 0 0 100  4
3 RCC  0  25 0 0 0 100  4
4 RCC -25   0 0 0 0 100  4
5 RCC  0 -25 0 0 0 100  4
6 RCC  0   0 0 0 0 100  4
102 pz 20
103 pz 40
104 pz 60
105 pz 80
106 pz 51
...
imp:n 1 11r 0

```

Response

First, MCNP5 was used to determine the fission energy tally for the geometry. The tally yielded $1.18121 \times 10^{-17} \frac{\text{MW}}{\frac{n_{\text{src}}}{\text{s}}}$. To find the source strength, we take the reactor power, 250 kW, and divide by this value:

$$\frac{0.25 \text{ MW}}{1.18121 \times 10^{-17} \frac{\text{MW}}{\frac{n_{\text{src}}}{\text{s}}}} = 2.116473785 \times 10^{16} \frac{n_{\text{src}}}{\text{s}} \quad (1)$$

Now we can use this source strength as a multiplier to the detector tally in order to approximate the neutron dose at that point. We run MCNP5 again to find that the dose associated with uncollided neutron flux is $4.36349 \times 10^4 \frac{\text{rem}}{\text{hr}}$.

¹Note that cell 101 and surface 9 have been added to the default geometry and cell 101 has been given a nonzero neutron importance.