

$$\sigma_t = (1 - d_t)E_0(\varepsilon_t - \tilde{\varepsilon}_t^{pl}),$$

$$\sigma_c = (1 - d_c)E_0(\varepsilon_c - \tilde{\varepsilon}_c^{pl}).$$

$$\bar{\sigma}_t = \frac{\sigma_t}{(1 - d_t)} = E_0(\varepsilon_t - \tilde{\varepsilon}_t^{pl}),$$

$$\bar{\sigma}_c = \frac{\sigma_c}{(1 - d_c)} = E_0(\varepsilon_c - \tilde{\varepsilon}_c^{pl}).$$

$$\boldsymbol{\sigma} = (1 - d)\mathbf{D}_0^{el} : (\boldsymbol{\varepsilon} - \boldsymbol{\varepsilon}^{pl}) = \mathbf{D}^{el} : (\boldsymbol{\varepsilon} - \boldsymbol{\varepsilon}^{pl}),$$

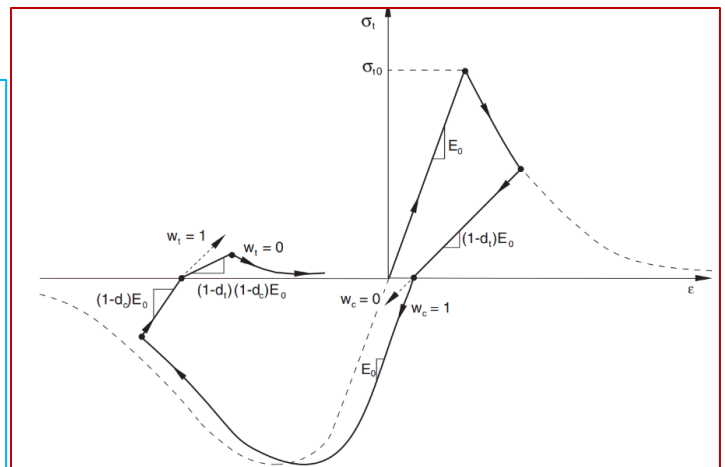
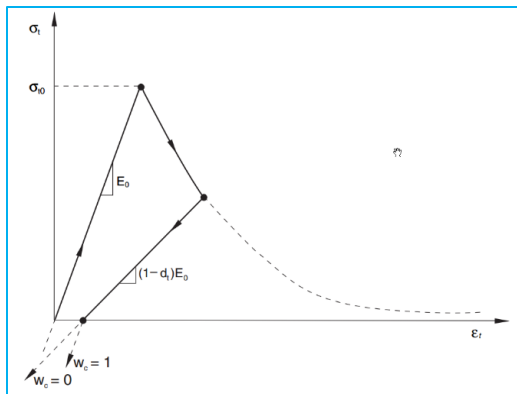
$$\bar{\boldsymbol{\sigma}} \stackrel{\text{def}}{=} \mathbf{D}_0^{el} : (\boldsymbol{\varepsilon} - \boldsymbol{\varepsilon}^{pl})$$

$$\boldsymbol{\sigma} = (1 - d)\bar{\boldsymbol{\sigma}}.$$

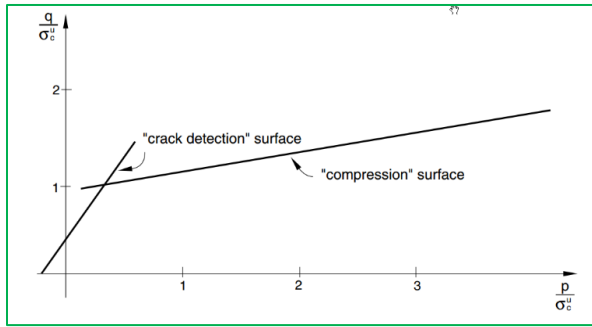
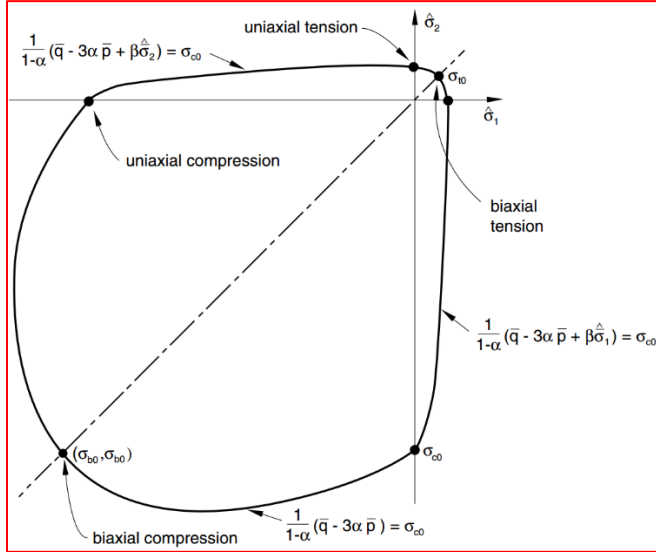
$$(1 - d) = (1 - s_t d_c)(1 - s_c d_t), \quad 0 \leq s_t, s_c \leq 1,$$

$$s_t = 1 - w_t r^*(\bar{\sigma}_{11}); \quad 0 \leq w_t \leq 1,$$

$$s_c = 1 - w_c (1 - r^*(\bar{\sigma}_{11})); \quad 0 \leq w_c \leq 1,$$



$$F(\bar{\boldsymbol{\sigma}}, \tilde{\boldsymbol{\varepsilon}}^{pl}) = \frac{1}{1-\alpha} (\bar{q} - 3\alpha\bar{p} + \beta(\tilde{\boldsymbol{\varepsilon}}^{pl})\langle\hat{\bar{\sigma}}_{\max}\rangle - \gamma\langle-\hat{\bar{\sigma}}_{\max}\rangle) - \bar{\sigma}_c(\tilde{\boldsymbol{\varepsilon}}_c^{pl}) \leq 0,$$



$$\bar{p} = -\frac{1}{3}\bar{\boldsymbol{\sigma}} : \mathbf{I}$$

$$\bar{q} = \sqrt{\frac{3}{2}\bar{\mathbf{S}} : \bar{\mathbf{S}}}$$

$$\bar{\mathbf{S}} = \bar{p}\mathbf{I} + \bar{\boldsymbol{\sigma}}$$

$$\beta(\tilde{\boldsymbol{\varepsilon}}^{pl}) = \frac{\bar{\sigma}_c(\tilde{\boldsymbol{\varepsilon}}_c^{pl})}{\bar{\sigma}_t(\tilde{\boldsymbol{\varepsilon}}_t^{pl})}(1-\alpha) - (1+\alpha),$$

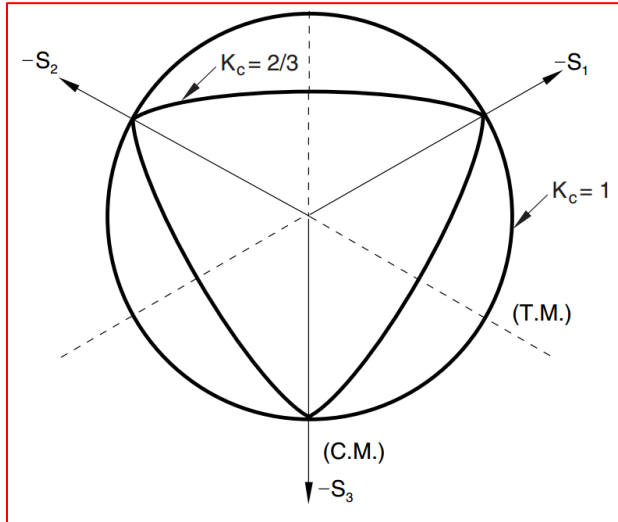
$$\alpha = \frac{\sigma_{b0} - \sigma_{c0}}{2\sigma_{b0} - \sigma_{c0}}$$

$$\left(\frac{2}{3}\gamma + 1\right) \bar{q} - (\gamma + 3\alpha)\bar{p} = (1-\alpha)\bar{\sigma}_c, \quad (\text{TM})$$

$$\left(\frac{1}{3}\gamma + 1\right) \bar{q} - (\gamma + 3\alpha)\bar{p} = (1-\alpha)\bar{\sigma}_c. \quad (\text{CM})$$

$$K_c = \frac{\gamma + 3}{2\gamma + 3}$$

$$\gamma = \frac{3(1 - K_c)}{2K_c - 1}$$



$$F(\bar{\boldsymbol{\sigma}}, \tilde{\boldsymbol{\epsilon}}^{pl}) = \frac{1}{1 - \alpha} (\bar{q} - 3\alpha\bar{p} + \beta(\tilde{\boldsymbol{\epsilon}}^{pl})\langle \hat{\bar{\sigma}}_{\max} \rangle - \gamma\langle -\hat{\bar{\sigma}}_{\max} \rangle) - \bar{\sigma}_c(\tilde{\epsilon}_c^{pl}) \leq 0,$$

If $\hat{\bar{\sigma}}_{\max} > 0$, the yield conditions along the tensile and compressive meridians reduce to

$$\left(\frac{2}{3}\beta + 1\right) \bar{q} - (\beta + 3\alpha)\bar{p} = (1 - \alpha)\bar{\sigma}_c, \quad (\text{TM})$$

$$\left(\frac{1}{3}\beta + 1\right) \bar{q} - (\beta + 3\alpha)\bar{p} = (1 - \alpha)\bar{\sigma}_c. \quad (\text{CM})$$

$$K_t = \frac{\beta + 3}{2\beta + 3}$$

$$\dot{\boldsymbol{\epsilon}}^{pl} = \dot{\lambda} \frac{\partial G(\bar{\boldsymbol{\sigma}})}{\partial \bar{\boldsymbol{\sigma}}}$$

$$G = \sqrt{(\epsilon\sigma_{t0} \tan \psi)^2 + \bar{q}^2} - \bar{p} \tan \psi$$

$$\tilde{\boldsymbol{\varepsilon}}^{pl} = \begin{bmatrix} \tilde{\varepsilon}_t^{pl} \\ \tilde{\varepsilon}_c^{pl} \end{bmatrix}; \quad \dot{\tilde{\boldsymbol{\varepsilon}}}^{pl} = \mathbf{h}(\bar{\boldsymbol{\sigma}}, \tilde{\boldsymbol{\varepsilon}}^{pl}) \cdot \dot{\boldsymbol{\varepsilon}}^{pl},$$

$$\begin{aligned} \bar{\boldsymbol{\sigma}} &= \mathbf{D}_0^{el} : (\boldsymbol{\varepsilon} - \boldsymbol{\varepsilon}^{pl}) \in \{\bar{\boldsymbol{\sigma}} | F(\bar{\boldsymbol{\sigma}}, \tilde{\boldsymbol{\varepsilon}}^{pl}) \leq 0\}, \\ \dot{\tilde{\boldsymbol{\varepsilon}}}^{pl} &= \mathbf{h}(\bar{\boldsymbol{\sigma}}, \tilde{\boldsymbol{\varepsilon}}^{pl}) \cdot \dot{\boldsymbol{\varepsilon}}^{pl}, \\ \dot{\boldsymbol{\varepsilon}}^{pl} &= \dot{\lambda} \frac{\partial G(\bar{\boldsymbol{\sigma}})}{\partial \bar{\boldsymbol{\sigma}}}, \end{aligned}$$

$$\begin{aligned} \dot{\tilde{\varepsilon}}_t^{pl} &= r^* \dot{\varepsilon}_{11}^{pl}, \\ \dot{\tilde{\varepsilon}}_c^{pl} &= -(1 - r^*) \dot{\varepsilon}_{11}^{pl}, \end{aligned}$$

$$\begin{aligned} \dot{\tilde{\varepsilon}}_t^{pl} &\stackrel{\text{def}}{=} r(\hat{\boldsymbol{\sigma}}) \hat{\varepsilon}_{\max}^{pl}, \\ \dot{\tilde{\varepsilon}}_c^{pl} &\stackrel{\text{def}}{=} -(1 - r(\hat{\boldsymbol{\sigma}})) \hat{\varepsilon}_{\min}^{pl}, \end{aligned}$$

$\hat{\varepsilon}_{\max}^{pl}$ and $\hat{\varepsilon}_{\min}^{pl}$ are, respectively, the maximum and minimum eigenvalues of the plastic strain rate

$$r(\hat{\boldsymbol{\sigma}}) \stackrel{\text{def}}{=} \frac{\sum_{i=1}^3 \langle \hat{\sigma}_i \rangle}{\sum_{i=1}^3 |\hat{\sigma}_i|}; \quad 0 \leq r(\hat{\boldsymbol{\sigma}}) \leq 1$$

$$\dot{\tilde{\boldsymbol{\varepsilon}}}^{pl} = \begin{bmatrix} \dot{\tilde{\varepsilon}}_t^{pl} \\ \dot{\tilde{\varepsilon}}_c^{pl} \end{bmatrix} = \hat{\mathbf{h}}(\hat{\boldsymbol{\sigma}}, \tilde{\boldsymbol{\varepsilon}}^{pl}) \cdot \hat{\boldsymbol{\varepsilon}}^{pl}$$

$$\hat{\mathbf{h}}(\hat{\boldsymbol{\sigma}}, \tilde{\boldsymbol{\varepsilon}}^{pl}) = \begin{bmatrix} r(\hat{\boldsymbol{\sigma}}) & 0 & 0 \\ 0 & 0 & -(1 - r(\hat{\boldsymbol{\sigma}})) \end{bmatrix}$$

$$\hat{\boldsymbol{\varepsilon}}^{pl} = \begin{bmatrix} \hat{\varepsilon}_1^{pl} \\ \hat{\varepsilon}_2^{pl} \\ \hat{\varepsilon}_3^{pl} \end{bmatrix}$$

$$\text{Kuhn-Tucker conditions: } \dot{\lambda} F = 0; \quad \dot{\lambda} \geq 0; \quad F \leq 0. \quad F(\bar{\boldsymbol{\sigma}}, \tilde{\boldsymbol{\varepsilon}}^{pl}) \leq 0.$$

$$\begin{aligned} \sigma_t &= \sigma_t(\tilde{\varepsilon}_t^{pl}, \dot{\tilde{\varepsilon}}_t^{pl}, \theta, f_i), \\ \sigma_c &= \sigma_c(\tilde{\varepsilon}_c^{pl}, \dot{\tilde{\varepsilon}}_c^{pl}, \theta, f_i), \end{aligned}$$

$$\tilde{\varepsilon}_t^{pl} = \int_0^t \dot{\tilde{\varepsilon}}_t^{pl} dt \quad \text{and} \quad \tilde{\varepsilon}_c^{pl} = \int_0^t \dot{\tilde{\varepsilon}}_c^{pl} dt$$

$$\begin{aligned} \dot{\tilde{\varepsilon}}_t^{pl} &= \dot{\varepsilon}_{11}^{pl}, \quad \text{in uniaxial tension and} \\ \dot{\tilde{\varepsilon}}_c^{pl} &= -\dot{\varepsilon}_{11}^{pl}, \quad \text{in uniaxial compression} \end{aligned}$$

$$\begin{aligned}d_t &= d_t(\hat{\varepsilon}_t^{pl}, \theta, f_i), \quad (0 \leq d_t \leq 1), \\d_c &= d_c(\hat{\varepsilon}_c^{pl}, \theta, f_i), \quad (0 \leq d_c \leq 1).\end{aligned}$$

$$\dot{\boldsymbol{\varepsilon}}_v^{pl} = \frac{1}{\mu}(\boldsymbol{\varepsilon}^{pl} - \boldsymbol{\varepsilon}_v^{pl})$$

$$\dot{d}_v = \frac{1}{\mu}(d - d_v)$$

$$\boldsymbol{\sigma} = (1 - d_v)\mathbf{D}_0^{el} : (\boldsymbol{\varepsilon} - \boldsymbol{\varepsilon}_v^{pl})$$

$$\begin{aligned}\boldsymbol{\varepsilon} &= \boldsymbol{\varepsilon}^e + \boldsymbol{\varepsilon}^p, & \boldsymbol{\sigma} &= (1 - D)\bar{\boldsymbol{\sigma}}, & \bar{\boldsymbol{\sigma}} &= \mathbf{C}_0 \boldsymbol{\varepsilon}^e, \\ \dot{\boldsymbol{\varepsilon}}^p &= \dot{\lambda} \mathbf{m}(\bar{\boldsymbol{\sigma}}, \kappa), & \dot{\kappa} &= \dot{\lambda} \mathbf{h}(\bar{\boldsymbol{\sigma}}, \kappa)\end{aligned}$$

$$\dot{\lambda} \geq 0, \quad F(\bar{\boldsymbol{\sigma}}, \kappa) \leq 0 \quad \text{and} \quad \dot{\lambda} F(\bar{\boldsymbol{\sigma}}, \kappa) = 0$$

$\{\boldsymbol{\varepsilon}_n, \boldsymbol{\varepsilon}_n^p, \kappa_n\}$ is assumed to be known at time t_n .

the effective stress $\bar{\boldsymbol{\sigma}}_n$ and the damage variable D_n

$$\bar{\boldsymbol{\sigma}}_n = \mathbf{C}_0 (\boldsymbol{\varepsilon}_n - \boldsymbol{\varepsilon}_n^p) \quad \text{and} \quad D_n = D(\kappa_n)$$

$$\kappa = \{\kappa_t; \kappa_c\}$$

$$\boldsymbol{\varepsilon}_{n+1} = \boldsymbol{\varepsilon}_n + \Delta \boldsymbol{\varepsilon}$$

$$\bar{\boldsymbol{\sigma}}_{n+1} = \bar{\boldsymbol{\sigma}}_{n+1}^{trial} - \Delta \lambda \mathbf{C}_0 \mathbf{m} \quad \text{with} \quad \bar{\boldsymbol{\sigma}}_{n+1}^{trial} = \mathbf{C}_0 (\boldsymbol{\varepsilon}_{n+1} - \boldsymbol{\varepsilon}_n^p)$$

$$F(\bar{\boldsymbol{\sigma}}_{n+1}^{trial}, \kappa_n) \leq 0, \quad \text{then this is an elastic state}$$

$$\bar{\boldsymbol{\sigma}}_{n+1} = \bar{\boldsymbol{\sigma}}_{n+1}^{trial} \quad \text{and} \quad \kappa_{n+1} = \kappa_n$$

$$\kappa_{n+1} = \kappa_n + \Delta \lambda \mathbf{h}$$

$$F(\bar{\boldsymbol{\sigma}}_{n+1}, \kappa_{n+1}) = 0$$

$$\mathbf{R}_{\hat{\boldsymbol{\sigma}}} = \hat{\boldsymbol{\sigma}}_{n+1} + \Delta \lambda \hat{\mathbf{C}}_0 \mathbf{m} - \hat{\boldsymbol{\sigma}}_{n+1}^{trial}$$

$$\mathbf{R}_{\kappa} = \kappa_{n+1} - \Delta \lambda \mathbf{h} - \kappa_n$$

$$\mathbf{R}_{\Delta \lambda} = F(\hat{\boldsymbol{\sigma}}_{n+1}, \kappa_{n+1})$$

$$\hat{\mathbf{C}}_0 = \begin{bmatrix} \lambda_L + 2G & \lambda_L & \lambda_L \\ \lambda_L & \lambda_L + 2G & \lambda_L \\ \lambda_L & \lambda_L & \lambda_L + 2G \end{bmatrix}$$

$$\mathbf{x} = \begin{bmatrix} \hat{\boldsymbol{\sigma}}_{n+1} & \boldsymbol{\kappa}_{n+1} & \Delta\lambda \end{bmatrix}^T$$

$$\mathbf{x}^{(k+1)} = \mathbf{x}^{(k)} + \Delta\mathbf{x} \quad \text{with } \Delta\mathbf{x} = -\mathbf{J}^{-1}\mathbf{R}(\mathbf{x}^{(k)})$$

\mathbf{J} is the Jacobian

$$\mathbf{J} = \begin{bmatrix} \mathbf{I}_{n\hat{\boldsymbol{\sigma}}} + \Delta\lambda\hat{\mathbf{C}}_0\frac{\partial\mathbf{m}}{\partial\hat{\boldsymbol{\sigma}}}; & \Delta\lambda\hat{\mathbf{C}}_0\frac{\partial\mathbf{m}}{\partial\boldsymbol{\kappa}}; & \hat{\mathbf{C}}_0\mathbf{m} \\ -\Delta\lambda\frac{\partial\mathbf{h}}{\partial\hat{\boldsymbol{\sigma}}} & \mathbf{I}_{n\boldsymbol{\kappa}} - \Delta\lambda\frac{\partial\mathbf{h}}{\partial\boldsymbol{\kappa}} & -\mathbf{h} \\ \left\{\partial F/\partial\hat{\boldsymbol{\sigma}}\right\}^T & \left\{\partial F/\partial\boldsymbol{\kappa}\right\}^T & 0 \end{bmatrix}$$

$$\mathbf{x}^{(0)} = \begin{bmatrix} \hat{\boldsymbol{\sigma}}_{n+1}^{(0)} \\ \boldsymbol{\kappa}_{n+1}^{(0)} \\ \Delta\lambda^{(0)} \end{bmatrix} = \begin{bmatrix} \hat{\boldsymbol{\sigma}}_{n+1}^{trial} \\ \boldsymbol{\kappa}_n \\ 0 \end{bmatrix}$$

$$\|\mathbf{R}(\mathbf{x}^{(k+1)})\| \leq \text{TOL}$$

Sub-stepping strategy

Damage corrector step

$$D_{n+1} = D(\kappa_{n+1})$$

$$\sigma_{n+1} = (1 - D_{n+1}) \bar{\sigma}_{n+1}.$$

$$\frac{d\sigma_{n+1}}{d\epsilon_{n+1}} = -\bar{\sigma}_{n+1} \frac{dD_{n+1}}{d\kappa_{n+1}} \frac{d\kappa_{n+1}}{d\epsilon_{n+1}} + (1 - D_{n+1}) \frac{d\bar{\sigma}_{n+1}}{d\epsilon_{n+1}}.$$

$$\mathbf{J} \begin{pmatrix} d\hat{\sigma}_{n+1} \\ d\kappa_{n+1} \\ d\Delta\lambda \end{pmatrix} = \begin{pmatrix} \hat{\mathbf{C}}_0 d\hat{\epsilon}_{n+1} \\ \mathbf{0}_{n\kappa} \\ 0 \end{pmatrix}$$

$$\begin{pmatrix} d\hat{\sigma}_{n+1} \\ d\kappa_{n+1} \\ d\Delta\lambda \end{pmatrix} = \begin{bmatrix} \hat{\Xi}_{\hat{\sigma}} & \bullet & \bullet \\ \hat{\Xi}_{\kappa} & \bullet & \bullet \\ \bullet & \bullet & \bullet \end{bmatrix} \begin{pmatrix} \hat{\mathbf{C}}_0 d\hat{\epsilon}_{n+1} \\ \mathbf{0}_{n\kappa,1} \\ 0 \end{pmatrix}$$

$$\frac{d\hat{\sigma}_{n+1}}{d\hat{\epsilon}_{n+1}} = \hat{\Xi}_{\hat{\sigma}} \hat{\mathbf{C}}_0$$

$$\frac{d\kappa_{n+1}}{d\hat{\epsilon}_{n+1}} = \hat{\Xi}_{\kappa} \hat{\mathbf{C}}_0$$

$$\frac{d\hat{\sigma}_{n+1}}{d\hat{\epsilon}_{n+1}} = \left[(1 - D_{n+1}) \hat{\Xi}_{\hat{\sigma}} - \hat{\sigma}_{n+1} \frac{dD_{n+1}}{d\kappa_{n+1}} \hat{\Xi}_{\kappa} \right] \hat{\mathbf{C}}_0$$

$$\begin{aligned} \frac{d\sigma_{n+1}}{d\epsilon_{n+1}} &= \sum_{A=1}^3 \sum_{B=1}^3 \frac{d\hat{\sigma}_A}{d\hat{\epsilon}_B} \mathbf{m}_A^T \mathbf{m}_B + \frac{(1 - D_{n+1})}{2} \\ &\quad \times \sum_{A=1}^3 \sum_{B \neq A} \left[\left(\frac{\hat{\sigma}_B - \hat{\sigma}_A}{\hat{\epsilon}_B - \hat{\epsilon}_A} \right) (\mathbf{m}_{AB}^T \mathbf{m}_{AB} + \mathbf{m}_{AB}^T \mathbf{m}_{BA}) \right] \end{aligned}$$

$$\mathbf{m}_A = \mathbf{v}_A^T \mathbf{v}_A, \quad \mathbf{m}_{AB} = \mathbf{v}_A^T \mathbf{v}_B, \quad A \neq B.$$

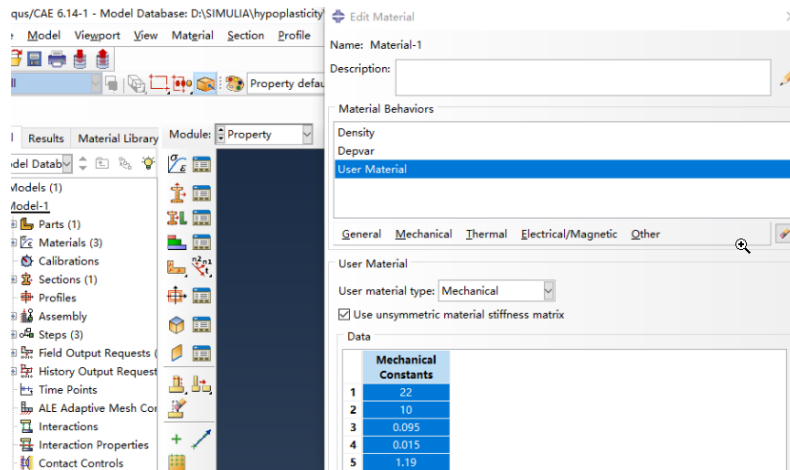
$$\left(\hat{\sigma}_B - \hat{\sigma}_A \right) / \left(\hat{\epsilon}_B - \hat{\epsilon}_A \right) \text{ by } \partial \left(\hat{\sigma}_B - \hat{\sigma}_A \right) / \partial \hat{\epsilon}_B$$


```

c    see Lee, J., and G. L. Fenves, "Plastic-Damage Model
c    for Cyclic Loading of Concrete Structures," Journal of
c    Engineering Mechanics, vol. 124, no. 8, pp. 892-900, 1998.
SUBROUTINE UMAT(sig,statev,DDSDDE,SSE,SPD,SCD,
1  RPL,DDSDDT,DRPLDE,DRPLDT,
2  stran,dstran,TIME,DTIME,TEMP,DTEMP,PREDEF,DPRED,CMNAME,
3  NDI,NSHR,NTENS,NSTATV,PROPS,NPROPS,COORDS,DROT,PNEWDT,
4  CELENT,DFGRD0,DFGRD1,NOEL,NPT,LAYER,KSPT,JSTEP,KINC)

INCLUDE 'ABA_PARAM.INC'
CHARACTER*80 CMNAME
DIMENSION sig(NTENS),statev(NSTATV),
1  DDSDDE(NTENS,NTENS),
2  DDSDDT(NTENS),DRPLDE(NTENS),
3  stran(NTENS),dstran(NTENS),TIME(2),PREDEF(1),DPRED(1),
4  PROPS(NPROPS),COORDS(3),DROT(3,3),DFGRD0(3,3),DFGRD1(3,3),
5  JSTEP(4),cc(ntens,ntens),ps(3),an(3,3),dd1(3,6),dd2(3,6),
$  sig_pr(3),sde_pr(3),dj2_ds2(3,3),cin(3,3),uni(3),dx(6),
$  x(6),ress(6),pjac(6,6),dm(3),dm_ds(3,3),dh(2),dh_ds(2,3),
$  drr_ds(3),pjac2(6,6),dx6(6),dx66(6),dx5(5),px55(5,5),
$  px33(3,3),px23(2,3),sig_tr(6),sig_pr1(3),e_tr(3),e_tr1(3),
$  df_ds(3),df_dk(2),ress1(6),dx55(5),yx33(3,3),dir63(6,3)
PARAMETER(zr=0.0D0,on=1.0D0,tw=2.0D0,thr=3.0D0,fr=4.0D0,
%tol=1.0d-6,tol2=10.0d0)

```



```

pi=atan(on)*fr;
Em=PROPS(1);emu=PROPS(2);fco=props(3);fto=props(4);
fb_fc=props(5);ecc=props(6);omega=props(7);pkc=props(8)
rec_c=props(11);rec_t=props(12);omega=omega*pi/180.0;

```

$$F(\bar{\sigma}, \tilde{\varepsilon}^{pl}) = \frac{1}{1-\alpha} (\bar{q} - 3\alpha\bar{p} + \beta(\tilde{\varepsilon}^{pl})\langle \hat{\sigma}_{\max} \rangle - \gamma\langle -\hat{\sigma}_{\max} \rangle) - \tilde{\sigma}_c(\tilde{\varepsilon}_c^{pl}) \leq 0,$$

$$\alpha = \frac{\sigma_{b0} - \sigma_{c0}}{2\sigma_{b0} - \sigma_{c0}}, \quad \gamma = \frac{3(1-K_c)}{2K_c - 1}$$

```

tan_o=tan(omega);alpha=(fb_fc-on)/(fb_fc*tw-on);
gamma=thr*(on-pkc)/(tw*pkc-on);

```

```

p1=Em/(on+emu)/(on-tw*emu);cc=zr;

```

```

tan_o=tan(omega);alpha=(fb_fc-on)/(fb_fc*tw-on);
gamma=thr*(on-pkc)/(tw*pkc-on);
ept=statev(1);epc=statev(2);dd=statev(3);
p1=Em/(on+emu)/(on-tw*emu);cc=zr;

```

□ Hooke's law in terms of the stress and strain vectors:

$$\begin{aligned} \{\boldsymbol{\varepsilon}\} &\stackrel{\text{def}}{=} \begin{Bmatrix} \varepsilon_x \\ \varepsilon_y \\ \varepsilon_z \\ \gamma_{xy} \\ \gamma_{xz} \\ \gamma_{yz} \end{Bmatrix} \in \mathbb{R}^6 \\ \{\boldsymbol{\sigma}\} &\stackrel{\text{def}}{=} \begin{Bmatrix} \sigma_x \\ \sigma_y \\ \sigma_z \\ \tau_{xy} \\ \tau_{xz} \\ \tau_{yz} \end{Bmatrix} \in \mathbb{R}^6 \end{aligned}$$

$$\begin{cases} \boldsymbol{\sigma} = \mathbb{C} : \boldsymbol{\varepsilon} \\ \mathbb{C} = \lambda \mathbf{1} \otimes \mathbf{1} + 2\mu \mathbb{I} \end{cases} \Rightarrow \begin{cases} \{\boldsymbol{\sigma}\} = \mathbf{D} \cdot \{\boldsymbol{\varepsilon}\} \\ \sigma_i = D_{ij} \varepsilon_j \quad i \in \{1, \dots, 6\} \end{cases}$$

Where \mathbf{D} is the matrix of elastic constants:

$$\mathbf{D} = \frac{E(1-\nu)}{(1+\nu)(1-2\nu)} \begin{bmatrix} 1 & \frac{\nu}{1-\nu} & \frac{\nu}{1-\nu} & 0 & 0 & 0 \\ \frac{\nu}{1-\nu} & 1 & \frac{\nu}{1-\nu} & 0 & 0 & 0 \\ \frac{\nu}{1-\nu} & \frac{\nu}{1-\nu} & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & \frac{1-2\nu}{2(1-\nu)} & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{1-2\nu}{2(1-\nu)} & 0 \\ 0 & 0 & 0 & 0 & 0 & \frac{1-2\nu}{2(1-\nu)} \end{bmatrix}$$

$\{\varepsilon_n, \varepsilon_n^p, \kappa_n\}$ is assumed to be known at time t_n , $\boldsymbol{\varepsilon}_{n+1} = \boldsymbol{\varepsilon}_n + \Delta \boldsymbol{\varepsilon}$

$\bar{\boldsymbol{\sigma}}_n = \mathbf{C}_0 (\boldsymbol{\varepsilon}_n - \boldsymbol{\varepsilon}_n^p)$ and $D_n = D(\kappa_n)$ $\bar{\boldsymbol{\sigma}}_{n+1} = \bar{\boldsymbol{\sigma}}_{n+1}^{trial} - \Delta \lambda \mathbf{C}_0 \mathbf{m}$ with $\bar{\boldsymbol{\sigma}}_{n+1}^{trial} = \mathbf{C}_0 (\boldsymbol{\varepsilon}_{n+1} - \boldsymbol{\varepsilon}_n^p)$

```

cc(1:3,1:3)=p1*emu;
cc(1,1)=(on-emu)*p1;cc(2,2)=(on-emu)*p1;
cc(3,3)=(on-emu)*p1;Gm=Em/(on+emu)/tw;
cc(4,4)=Gm;cc(5,5)=Gm;cc(6,6)=Gm;ddsdde=cc*(on-dd);
sig_tr=sig/(on-dd)+matmul(cc,dstran);

```

```

ept=statev(1);epc=statev(2);dd=statev(3);

```



```

sig_tr=zs;sig_tr(1)=-12.5;ept=zs;epc=zs!0.002-fco/Em+0.0001!!!!
write(*,*) 'epc1',epc
call sprind(sig_tr,ps,an,1,ndi,nshr)
call korder(ps,an,dd1,dd2,ndi)

```

```

43      pi1=ps(1)+ps(2)+ps(3);sig_pr=ps;sde_pr=sig_pr-pi1/thr
44      pj2=(sde_pr(1)**2+sde_pr(2)**2+sde_pr(3)**2)/tw
45      call kaxialy(fc_eff,ft_eff,fc,ft,hc,ht,hc_eff,ht_eff,
46      $ ddt_dept,ddc_depc,epc,ept,dc,dt,fto,fco,Em,tol,tol2)
47      beta=fc_eff/ft_eff*(on-alpha)-(on+alpha)
48      ff=(alpha*pi1+sqrt(thr*pj2)+beta*(sig_pr(1)+abs(sig_pr(1))))
49      %/tw-gamma*(abs(sig_pr(1))-sig_pr(1))/tw/(on-alpha)-fc_eff

```

$$F(\bar{\sigma}, \tilde{\varepsilon}^{pl}) = \frac{1}{1-\alpha} \left(\bar{q} - 3\alpha\bar{p} + \beta(\tilde{\varepsilon}^{pl}) \langle \hat{\sigma}_{\max} \rangle - \gamma \langle -\hat{\sigma}_{\max} \rangle \right) - \bar{\sigma}_c(\tilde{\varepsilon}_c^{pl}) \leq 0,$$

```

if ((ff/Em)<(tol*tw)) then

```

```

    sig=(on-dd)*sig_tr

```

```

else

```

```

    dj2_ds2=-on;dj2_ds2(1,1)=tw;dj2_ds2(2,2)=tw;

```

```

    dj2_ds2(3,3)=tw;dj2_ds2=dj2_ds2/thr;

```

```

    cin=-emu/Em;cin(1,1)=on/Em;cin(2,2)=on/Em;

```

```

    cin(3,3)=on/Em;dx=zs;x=zs;x(1:3)=sig_pr;

```

```

    x(4)=ept;x(5)=epc;sig_pr1=sig_pr;ept1=ept;epc1=epc

```

```

    e_tr=matmul(cin,sig_pr);e_tr1=e_tr;ress=zs;

```

```

    ress(6)=ff;res_n=abs(ress(6)/Em/tol2);res_n1=on;

```

```

    iter=0;uni=zs;uni(1)=on;

```

$$\begin{matrix} \text{the matrix} \\ \text{constants:} \end{matrix} \quad D = \frac{E(1-\nu)}{(1+\nu)(1-2\nu)} \begin{bmatrix} 1 & \frac{\nu}{1-\nu} & \frac{\nu}{1-\nu} & 0 & 0 & 0 \\ \frac{\nu}{1-\nu} & 1 & \frac{\nu}{1-\nu} & 0 & 0 & 0 \\ \frac{\nu}{1-\nu} & \frac{\nu}{1-\nu} & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & \frac{1-2\nu}{2(1-\nu)} & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{1-2\nu}{2(1-\nu)} & 0 \\ 0 & 0 & 0 & 0 & 0 & \frac{1-2\nu}{2(1-\nu)} \end{bmatrix}$$

$$\mathbf{x}^{(0)} = \begin{bmatrix} \hat{\sigma}_{n+1}^{(0)} \\ \kappa_{n+1}^{(0)} \\ \Delta \lambda^{(0)} \end{bmatrix} = \begin{bmatrix} \hat{\sigma}_{n+1}^{trial} \\ \kappa_n \\ 0 \end{bmatrix}$$

$$\mathbf{x}^{(k+1)} = \mathbf{x}^{(k)} + \Delta \mathbf{x} \quad \text{with } \Delta \mathbf{x} = -\mathbf{J}^{-1} \mathbf{R}(\mathbf{x}^{(k)})$$

$$\begin{aligned} \dot{\varepsilon}_t^{pl} &\stackrel{\text{def}}{=} r(\hat{\sigma}) \hat{\varepsilon}_{\max}^{pl}, \\ \dot{\varepsilon}_c^{pl} &\stackrel{\text{def}}{=} -(1 - r(\hat{\sigma})) \hat{\varepsilon}_{\min}^{pl}, \end{aligned}$$

$$\mathbf{J} = \begin{bmatrix} \mathbf{I}_{n\hat{\sigma}} + \Delta\lambda\hat{\mathbf{C}}_0\frac{\partial\mathbf{m}}{\partial\hat{\sigma}}; & \Delta\lambda\hat{\mathbf{C}}_0\frac{\partial\mathbf{m}}{\partial\kappa}; & \hat{\mathbf{C}}_0\mathbf{m} \\ -\Delta\lambda\frac{\partial\mathbf{h}}{\partial\hat{\sigma}} & \mathbf{I}_{n\kappa} - \Delta\lambda\frac{\partial\mathbf{h}}{\partial\kappa} & -\mathbf{h} \\ \left\{\partial F/\partial\hat{\sigma}\right\}^T & \left\{\partial F/\partial\kappa\right\}^T & 0 \end{bmatrix}$$

```
do while(res_n1>=tol/tol2/tw)
    par=tol/tol2
```

```
    iter=iter+1;pjac=zr;
    sqrt1=sqrt((ecc*fto*tan_o)**2+thr*pj2)
    dm=tan_o/thr+thr/tw*sde_pr/sqrt1
    do iii=1,3
        dm_ds(:,iii)=thr/tw*dj2_ds2(:,iii)/sqrt1
        %-thr*thr/fr*sde_pr*sde_pr(iii)/sqrt1**3
    end do
    pi1_n=abs(sig_pr(1))+abs(sig_pr(2))+
    %abs(sig_pr(3))
    rr=(pi1+pi1_n)/pi1_n/tw
    dh(1)=rr*dm(1);dh(2)=(rr-on)*dm(3)
    par=tw*pi1_n**2;
    do iii=1,3
        if (sig_pr(iii)<zr) then
            drr_ds(iii)=(pi1_n+pi1)/par
        else
            drr_ds(iii)=(pi1_n-pi1)/par
        end if
    end do
    dh_ds(1,:)=drr_ds*dm(1)+rr*dm_ds(1,:)
    dh_ds(2,:)=drr_ds*dm(3)+(rr-on)*dm_ds(3,%)
```

$$\dot{\tilde{\epsilon}}^{pl} = \dot{\lambda} \frac{\partial G(\bar{\sigma})}{\partial \bar{\sigma}}$$

$$G = \sqrt{(\epsilon\sigma_{t0} \tan \psi)^2 + \bar{q}^2} - \bar{p} \tan \psi$$

$$r(\hat{\sigma}) \stackrel{\text{def}}{=} \frac{\sum_{i=1}^3 \langle \hat{\sigma}_i \rangle}{\sum_{i=1}^3 |\hat{\sigma}_i|}; \quad 0 \leq r(\hat{\sigma}) \leq 1$$

$$\dot{\tilde{\epsilon}}^{pl} = \begin{bmatrix} \dot{\tilde{\epsilon}}_t^{pl} \\ \dot{\tilde{\epsilon}}^{pl} \\ \dot{\tilde{\epsilon}}_c^{pl} \end{bmatrix} = \hat{\mathbf{h}}(\hat{\sigma}, \tilde{\epsilon}^{pl}) \cdot \hat{\epsilon}^{pl}$$

$$\hat{\mathbf{h}}(\hat{\sigma}, \tilde{\epsilon}^{pl}) = \begin{bmatrix} r(\hat{\sigma}) & 0 & 0 \\ 0 & 0 & -(1-r(\hat{\sigma})) \end{bmatrix}$$

$$\mathbf{J} = \begin{bmatrix} \mathbf{I}_{n\hat{\sigma}} + \Delta\lambda \hat{\mathbf{C}}_0 \frac{\partial \mathbf{m}}{\partial \hat{\sigma}}; & \Delta\lambda \hat{\mathbf{C}}_0 \frac{\partial \mathbf{m}}{\partial \kappa}; & \hat{\mathbf{C}}_0 \mathbf{m} \\ -\Delta\lambda \frac{\partial \mathbf{h}}{\partial \hat{\sigma}} & \mathbf{I}_{n\kappa} - \Delta\lambda \frac{\partial \mathbf{h}}{\partial \kappa} & -\mathbf{h} \\ \left\{ \partial F / \partial \hat{\sigma} \right\}^T & \left\{ \partial F / \partial \kappa \right\}^T & 0 \end{bmatrix}$$

$$F(\bar{\sigma}, \tilde{\varepsilon}^{pl}) = \frac{1}{1-\alpha} (\bar{q} - 3\alpha\bar{p} + \beta(\tilde{\varepsilon}^{pl})\langle \hat{\sigma}_{\max} \rangle - \gamma\langle -\hat{\sigma}_{\max} \rangle) - \tilde{\sigma}_c(\tilde{\varepsilon}_c^{pl}) \leq 0,$$

```

pjac(1:3,1:3)=cin+x(6)*dm_ds;pjac(1:3,6)=dm
pjac(4:5,1:3)=-x(6)*dh_ds;pjac(4:5,6)=-dh;
pjac(4,4)=on;pjac(5,5)=on;
if (sig_pr(1)>zr) then
df_ds=(alpha+thr/tw*sde_pr/sqrt(thr*pj2)
%+beta*uni)/(on-alpha)
df_dk(1)=-ht_eff*fc_eff/ft_eff**2*sig_pr(1)
df_dk(2)=hc_eff/ft_eff*sig_pr(1)-hc_eff
else
df_ds=(alpha+thr/tw*sde_pr/sqrt(thr*pj2)
%+gamma*uni)/(on-alpha)
df_dk(1)=zr;df_dk(2)=-hc_eff
end if
pjac(6,1:3)=df_ds;pjac(6,4:5)=df_dk

pjac2=pjac;ress1=ress;
call gauss_2(pjac2,-on*ress1,dx,6)
pjac2=pjac

```

```

x=x+dx;sig_pr=x(1:3);
ress(1:3)=matmul(cin,x(1:3))-e_tr1+x(6)*dm
if(x(4)<ept1+tol/tol2**5) x(4)=ept1
if(x(5)<epc1+tol/tol2**5) x(5)=epc1
ress(4)=x(4)-ept1-x(6)*dh(1);ept=x(4)
ress(5)=x(5)-epc1-x(6)*dh(2);epc=x(5)

```

$$\mathbf{x}^{(k+1)} = \mathbf{x}^{(k)} + \Delta \mathbf{x} \quad \text{with } \Delta \mathbf{x} = -\mathbf{J}^{-1} \mathbf{R}(\mathbf{x}^{(k)})$$

$$\begin{aligned} \mathbf{R}_{\hat{\sigma}} &= \hat{\sigma}_{n+1} + \Delta\lambda \hat{\mathbf{C}}_0 \mathbf{m} - \hat{\sigma}_{n+1}^{trial} \\ \mathbf{R}_{\kappa} &= \kappa_{n+1} - \Delta\lambda \mathbf{h} - \kappa_n \\ \mathbf{R}_{\Delta\lambda} &= F\left(\hat{\sigma}_{n+1}, \kappa_{n+1}\right) \end{aligned}$$

$$F(\bar{\sigma}, \tilde{\epsilon}^{pl}) = \frac{1}{1-\alpha} (\bar{q} - 3\alpha\bar{p} + \beta(\tilde{\epsilon}^{pl})\langle\hat{\sigma}_{\max}\rangle - \gamma\langle-\hat{\sigma}_{\max}\rangle) - \bar{\sigma}_c(\tilde{\epsilon}_c^{pl}) \leq 0,$$

```

    pi1=sig_pr(1)+sig_pr(2)+sig_pr(3)
    sde_pr=sig_pr-pi1/thr
    pj2=(sde_pr(1)**2+sde_pr(2)**2
%+sde_pr(3)**2)/tw
    call kaxialy(fc_eff,ft_eff,fc,ft,hc,ht,hc_eff,
$ ht_eff,ddt_dept,ddc_depc,epc,ept,dc,dt,fto,fco,Em,tol,tol2)
    beta=fc_eff/ft_eff*(on-alpha)-(on+alpha);
    ff=(alpha*pi1+sqrt(thr*pj2)+beta*(sig_pr(1)
%+abs(sig_pr(1)))/tw-gamma*(abs(sig_pr(1))-sig_pr(1))/tw)
    $/(on-alpha)-fc_eff
    res(6)=ff;res_n=sqrt(res(1)**2+res(2)**2+
$ress(3)**2+res(4)**2+res(5)**2+(res(6)/Em/tol2)**2)
    res_n1=sqrt(res(1)**2+res(2)**2+res(3)**2)+on

    if (iter==200) then
        write(*,*) 'trials alot'
        !exit
        call xit
    end if
end do

```

$$\|\mathbf{R}(\mathbf{x}^{(k+1)})\| \leq \text{TOL}$$

$$\mathbf{J} \begin{pmatrix} d\hat{\sigma}_{n+1} \\ d\kappa_{n+1} \\ d\Delta\lambda \end{pmatrix} = \begin{pmatrix} \hat{\mathbf{C}}_0 d\hat{\epsilon}_{n+1} \\ \mathbf{0}_{n\kappa} \\ 0 \end{pmatrix}$$

$$\begin{pmatrix} d\hat{\sigma}_{n+1} \\ d\kappa_{n+1} \\ d\Delta\lambda \end{pmatrix} = \begin{bmatrix} \hat{\Xi}_{\hat{\sigma}} & \bullet & \bullet \\ \hat{\Xi}_{\kappa} & \bullet & \bullet \\ \bullet & \bullet & \bullet \end{bmatrix} \begin{pmatrix} \hat{\mathbf{C}}_0 d\hat{\epsilon}_{n+1} \\ \mathbf{0}_{n\kappa,1} \\ 0 \end{pmatrix}$$

$$\mathbf{J} = \begin{bmatrix} \mathbf{I}_{n\hat{\sigma}} + \Delta\lambda \hat{\mathbf{C}}_0 \frac{\partial \mathbf{m}}{\partial \hat{\sigma}}; & \Delta\lambda \hat{\mathbf{C}}_0 \frac{\partial \mathbf{m}}{\partial \kappa}; & \hat{\mathbf{C}}_0 \mathbf{m} \\ -\Delta\lambda \frac{\partial \mathbf{h}}{\partial \hat{\sigma}} & \mathbf{I}_{n\kappa} - \Delta\lambda \frac{\partial \mathbf{h}}{\partial \kappa} & -\mathbf{h} \\ \left\{ \partial F / \partial \hat{\sigma} \right\}^T & \left\{ \partial F / \partial \kappa \right\}^T & 0 \end{bmatrix}$$

piac2=piac;

call kinverse(pjac2(1:5,1:5),px55,5)

pjac2=pjac;

call kinverse(pjac2,pjac2,6)

write(*,*) 'px55',px55

dx5=matmul(px55,pjac(1:5,6))

dx55=matmul(transpose(px55),pjac(6,1:5))

par=dx5(1)*pjac(6,1)+dx5(2)*pjac(6,2)+

\$dx5(3)*pjac(6,3)+dx5(4)*pjac(6,4)+dx5(5)*pjac(6,5)

do ii=1,3

px33(ii,:)=px55(ii,1:3)-dx5(ii)*dx55(1:3)/par

end do

do ii=1,2

px23(ii,:)=px55(ii+3,1:3)-dx5(ii+3)*dx55(1:3)/par

end do

dd=on-(on-dc)*(on-dt)

ddc=ddc_depc*(on-dt);ddt=ddt_dept*(on-dc)

do i=1,3

do j=1,3

yx33(i,j)=sig_pr(i)*(px23(1,j)*ddt+px23(2,j)*ddc)

end do

end do

sig_tr=matmul(transpose(dd2),sig_pr)

sig=(on-dd)*sig_tr;

px33=(on-dd)*px33-yx33

$$\begin{aligned} D_{n+1} &= D(\kappa_{n+1}) \\ \sigma_{n+1} &= (1 - D_{n+1}) \bar{\sigma}_{n+1}. \end{aligned}$$

$$\frac{d\sigma_{n+1}}{d\epsilon_{n+1}} = -\bar{\sigma}_{n+1} \frac{dD_{n+1}}{d\kappa_{n+1}} \frac{d\kappa_{n+1}}{d\epsilon_{n+1}} + (1 - D_{n+1}) \frac{d\bar{\sigma}_{n+1}}{d\epsilon_{n+1}}.$$

$$\frac{d\hat{\sigma}_{n+1}}{d\hat{\epsilon}_{n+1}} = \left[(1 - D_{n+1}) \Xi_{\hat{\sigma}} - \hat{\sigma}_{n+1} \frac{dD_{n+1}}{d\kappa_{n+1}} \Xi_{\kappa} \right] \hat{\mathbf{C}}_0$$

$$\frac{d\hat{\sigma}_{n+1}}{d\hat{\epsilon}_{n+1}} = \hat{\Xi}_{\hat{\sigma}} \hat{\mathbf{C}}_0$$

$$\frac{d\kappa_{n+1}}{d\hat{\epsilon}_{n+1}} = \hat{\Xi}_{\kappa} \hat{\mathbf{C}}_0$$

$$(1 - d) = (1 - s_t d_c)(1 - s_c d_t), \quad 0 \leq s_t, s_c \leq 1,$$

$$s_t = 1 - w_t r^*(\bar{\sigma}_{11}); \quad 0 \leq w_t \leq 1,$$

$$s_c = 1 - w_c (1 - r^*(\bar{\sigma}_{11})); \quad 0 \leq w_c \leq 1,$$


```

call kinverse(px33,px33,3)
e_tr=matmul(px33,sig_pr)
!!!!!!!!!!!!!!!!!!!!!!
do i=1,2
  do j=i+1,3
    iii=iii+1
    dir63(1,iii)=2.0*an(i,1)*an(j,1)
    dir63(2,iii)=2.0*an(i,2)*an(j,2)
    dir63(3,iii)=2.0*an(i,3)*an(j,3)
    dir63(4,iii)=an(i,1)*an(j,2)+an(i,2)*an(j,1)
    dir63(5,iii)=an(i,1)*an(j,3)+an(i,3)*an(j,1)
    dir63(6,iii)=an(i,3)*an(j,2)+an(i,2)*an(j,3)
    if (abs(e_tr(i)-e_tr(j))<tol) then
      rati=cc(i,i)-cc(i,j)
    else
      rati=(sig_pr(i)-sig_pr(j))/(e_tr(i)-e_tr(j))
    end if
    do ii=1,6
      do jj=1,6
        ddsdde(ii,jj)=ddsdde(ii,jj)
        $+0.5*(on-dd)*rati*dir63(ii,iii)*dir63(jj,iii)
      end do
    end do
  end do
end do
end if
write(*,*) 'ddsdde',ddsdde
statev(1)=ept;statev(2)=epc;statev(3)=dd;
call xit
return

```

$$\mathbf{m}_A = \mathbf{v}_A^l \mathbf{v}_A, \quad \mathbf{m}_{AB} = \mathbf{v}_A^l \mathbf{v}_B, \quad A \neq B.$$

$$\frac{d\sigma_{n+1}}{d\mathbf{e}_{n+1}} = \sum_{A=1}^3 \sum_{B=1}^3 \frac{d\hat{\sigma}_A}{d\hat{\mathbf{e}}_B} \mathbf{m}_A^T \mathbf{m}_B + \frac{(1-D_{n+1})}{2} \times \sum_{A=1}^3 \sum_{B \neq A} \left[\left(\frac{\hat{\sigma}_B - \hat{\sigma}_A}{\hat{\mathbf{e}}_B - \hat{\mathbf{e}}_A} \right) (\mathbf{m}_{AB}^T \mathbf{m}_{AB} + \mathbf{m}_{AB}^T \mathbf{m}_{BA}) \right] \left(\hat{\sigma}_B - \hat{\sigma}_A \right) / \left(\hat{\mathbf{e}}_B - \hat{\mathbf{e}}_A \right) \text{ by } \partial \left(\hat{\sigma}_B - \hat{\sigma}_A \right) / \partial \hat{\mathbf{e}}_B$$


```

subroutine korder(ps,an,dd1,dd2,ndi)
  real*8 ps(3),an(3,3),dd1(3,6),dd2(3,6),temp11(3),temp1
  integer ndi
  do ii=1,ndi
    if (ps(ii)>ps(1)) then
      temp1=ps(1);ps(1)=ps(ii);ps(ii)=temp1
      temp11=an(1,:);an(1,:)=an(ii,:);
      an(ii,:)=temp11
    end if
    if (ps(ii)<ps(ndi)) then
      temp1=ps(ndi);ps(ndi)=ps(ii);ps(ii)=temp1
      temp11=an(ndi,:);an(ndi,:)=an(ii,:);
      an(ii,:)=temp11
    end if
  end do
  do ii=1,ndi
    dd1(ii,1)=an(ii,1)*an(ii,1);
    dd1(ii,2)=an(ii,2)*an(ii,2);
    dd1(ii,3)=an(ii,3)*an(ii,3);
    dd1(ii,4)=2.*an(ii,1)*an(ii,2);
    dd1(ii,5)=2.*an(ii,1)*an(ii,3);
    dd1(ii,6)=2.*an(ii,2)*an(ii,3);
  end do
  dd2=dd1;dd2(:,4:6)=0.5*dd1(:,4:6)
  !ds_pr=dd1*ds      ds=transpose(dd2)*ds_pr
return
end

```



```

subroutine kaxialy(fc_eff,ft_eff,fc,ft,hc,ht,hc_eff,ht_eff,
$ ddt_dept,ddc_depc,epc,ept,dc,dt,fto,fco,Em,tol,tol2)
  real*8 fc_eff,ft_eff,fc,ft,hc,ht,hc_eff,ht_eff,
$ ddt_dept,ddc_depc,epc,ept,dc,dt,fto,fco,Em,faci,tol,tol2
  pbb=0.002-fco/Em;pcc=0.01;faci=100.0
  if (abs(epc)<tol/tol2**5) then
    fc_eff=0.4*fco;fc=fc_eff
    hc_eff=Em*faci;hc=Em*faci;
    ddc_depc=0.0;dc=0.0;
  elseif (epc<pbb) then
    paa=epc/pbb;fc_eff=0.4+(0.6-0.01)*paa**3+
$(0.01-0.6)*3.0*paa**2+(0.6*3.0-0.01*2.0)*paa;
    fc_eff=fc_eff*fco;fc=fc_eff;
    hc_eff=(0.6-0.01)*3.*paa**2+(0.01-0.6)*6.0*paa
$(0.6*3.0-0.01*2.0);hc_eff=hc_eff*fco/pbb;hc=hc_eff;
    ddc_depc=0.0;dc=0.0
  elseif (epc>=pbb.and.epc<pbb*5.0) then
    paa=epc/pbb;fc_eff=(1.0+0.01*(paa-1.0))*fco;
    fc=(1.0-0.95/4.0*(paa-1))*fco;
    hc_eff=0.01*fco/pbb;hc=-0.95/4.0*fco/pbb;
    ddc_depc=-hc/fc_eff;
    dc=1.0-fc/fc_eff;
    !write(*,*) 'hc',hc,dc,ddc_depc,pbb,paa,fc

  else
    paa=epc/pbb;fc_eff=(1.0+0.01*(paa-1.0))*fco;
    fc=0.05*fco;
    hc_eff=0.01*fco/pbb;hc=0.0;
    ddc_depc=0.0;dc=1.0-fc/fc_eff;
  end if
  if (abs(ept)<tol/tol2**5) then
    ft_eff=fto;ft=ft_eff;
    ht_eff=Em*faci;ht=Em*faci;
    ddt_dept=0.0;dt=0.0;
  elseif (ept<pcc*0.9) then
    ft_eff=fto+0.01*fco/pbb*ept;
    ft=fto*(pcc-ept)/pcc;
    ht_eff=0.01*fco/pbb;ht=-1.0*fto/pcc;
    ddt_dept=-ht/fto;dt=1.0-ft/ft_eff;
  else
    ft_eff=fto+0.01*fco/pbb*ept;
    ft=fto*0.1;
    ht_eff=0.01*fco/pbb;ht=0.0;
    ddt_dept=0.0;dt=1.0-ft/ft_eff;
  end if

```



```

subroutine kinverse(a,c,n)
!=====
! kinverse matrix
! Method: Based on Doolittle LU factorization for  $Ax=b$ 
! Alex G. December 2009
! -----
! input ...
! a(n,n) - array of coefficients for matrix A
! n      - dimension
! output ...
! c(n,n) - kinverse matrix of A
! comments ...
! the original matrix a(n,n) will be destroyed
! during the calculation

```

```

subroutine gauss_2(a,b,x,n)
!=====
! Solutions to a system of linear equations  $A*x=b$ 
! Method: Gauss elimination (with scaling and pivoting)
! Alex G. (November 2009)
! -----

```