Design and Implementation of Broadband RF Power Divider over 800 MHz -12 GHz

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Introduction

Objective

Design a Broadband Multi-Section Wilkinson Power Divider for a frequency range of 800 MHz -12 GHz

Design Targets

- Frequency Range: 800 MHz to 12 GHz
- Input Reflection Coefficient: S11 value below -10 dB across the bandwidth, ensuring minimal reflection at the input.
- \bullet Power Split: S12 and S13 values between -3 to -3.5 dB, indicating a balanced power distribution between the two output ports.
- Isolation: S23 and S32 below -10 dB, ensuring minimal cross-coupling and interference

Literature Survey

Wilkinson Power Divider

 Provides equal power split between output ports with good isolation and matching properties

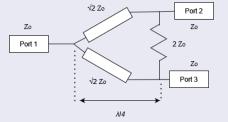


Figure 1: Wilkinson Equal Power Divider

The S parameters for Wilkinson Power Divider is as follows

$$\left[\begin{array}{ccc} S \end{array}\right] = \frac{-j}{\sqrt{2}} \left[\begin{array}{ccc} 0 & 1 & 1\\ 1 & 0 & 0\\ 1 & 0 & 0 \end{array}\right]$$

Literature Survey

Limitations of Wilkinson Power Divider

- Optimized for narrowband performance
- \bullet $\lambda/4$ transmission lines are typically designed for a specific center frequency

Multi-Section Broadband Wilkinson Power Divider

- ullet Cascading multiple $\lambda/4$ sections with different characteristic impedances increases broadbandness
- Smooth impedance transitions ensure expanded bandwidth and effective matching



Figure 2: Multi-Section Power Divider

Proposed Design

Calculation of Frequency Parameters

- Center Frequency $f_c = \frac{0.8+12}{2} \text{ GHz} = 6.4 \text{ GHz}$
- Bandwidth (BW) = (12-0.8) GHz = 11.2 GHz
- Fractional Bandwidth (FBW)= $\frac{BW}{f_c}=\frac{11.2}{6.4}=1.75$

Calculation of Number of Sections

- Number of Sections $N=\frac{f_c}{f_l}=\frac{6.4}{0.8}=8$, where f_c is the center frequency and f_l is the lower frequency of the broadband frequency range.
- Reference: Microwaves101 How many sections do you need?

Proposed Design

Impedance Calculation

- ullet Line impedances calculated using Chebyshev transformer model to ensure smooth impedance transitions and a low S_{11} at the input
- Applied even and odd mode analysis to simplify the mathematical modeling of the Wilkinson power divider

Calculation of Isolation Resistors

- Ensured minimal crosstalk by optimizing resistor values based on the virtual ground effect in odd mode
- Even mode analysis
 - ► Signals at ports 2 and 3 are in phase; Isolation resistors are ignored
- Odd mode analysis
 - ► Signals at ports 2 and 3 are 180° out of phase; Virtual ground forms along the symmetry axis, halving the values of isolation resistors

Proposed Design

Calculated Line Impedance

 Followed Seymour Cohn's 1968 IEEE paper, "A Class of Broadband Three-Port TEM-Mode Hybrids," for naming conventions of line impedances, isolation resistors and ports. (Fig 1)

Z_n	Values
Z1	58.66 ohms
Z2	61.59 ohms
Z3	64.96 ohms
Z4	68.72 ohms
Z5	72.76 ohms
Z6	76.97 ohms
Z7	81.18 ohms
Z8	85.23 ohms

Table	1:	Section	impedances	,
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R_n	Values
R1	339 ohms
R2	389 ohms
R3	613 ohms
R4	478 ohms
R5	362 ohms
R6	257 ohms
R7	162 ohms
R8	403 ohms

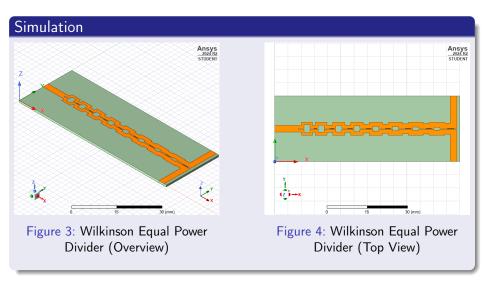
Table 2: Isolation resistor values

Implementation

Simulation

- Software Tool: Ansys HFSS for electromagnetic simulations
- Substrate Selection: Initially FR4 epoxy, but switched to Taconic for better high-frequency performance
- The physical length of each section was derived from the Chebyshev transformer calculation and based on the required impedances and the operating frequency range
- Isolation resistors are modeled using lumped RLC boundaries
- Lumped port excitations were applied to the ports to simulate the signal inputs and outputs
- An open region of air was applied around the entire structure to simulate the real-world operating conditions

Implementation



Results

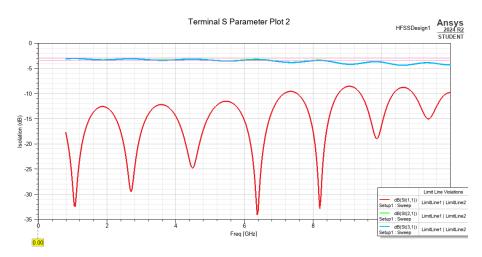


Figure 5: Terminal S Parameter Plot for S11, S21, S3

Results

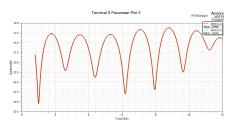


Figure 6: Terminal S Parameter Plot for S_{23} and S_{32}

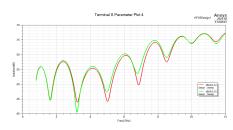


Figure 7: Terminal S Parameter Plot for S_{22} and S_{33}

Results

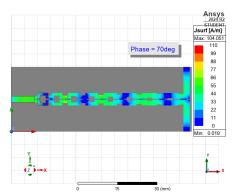


Figure 8: Flow of Surface current density (Top View)

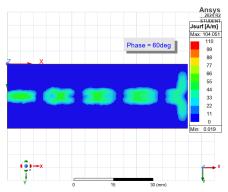


Figure 9: Flow of Surface current density (Bottom View)

Future Work

- Some small error in length or disturbance in power flow can cause this irregularity
- Refinement of transmission line lengths using parameter sweep
- Extending the design to cover higher frequency ranges
- Electromagnetic coupling considerations
- Experimental validation of the design by fabricating and testing the power divider

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