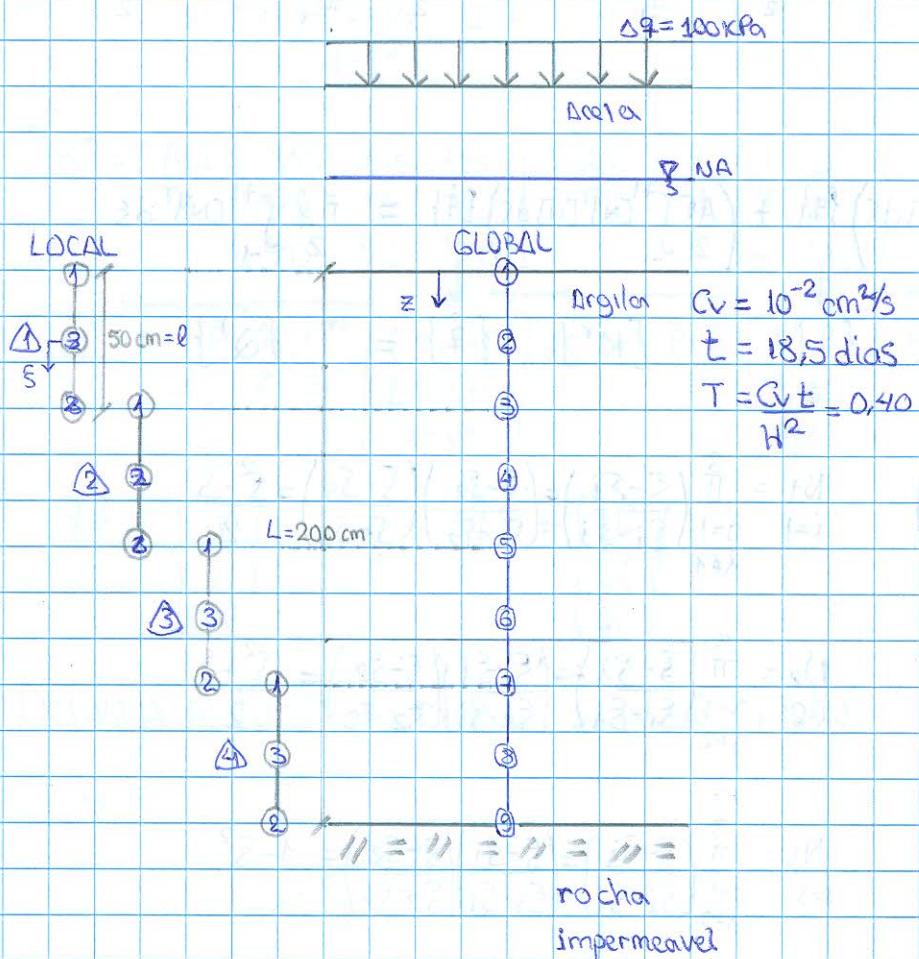


Lista de Exercícios N° 03

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Materia: Métodos Numéricos em Engenharia Civil



Formulação Variacional:

$$S_L = \int_V \left[\frac{1}{2} C_v \left(\frac{\partial u_e}{\partial z} \right)^2 + \frac{\partial u_e \cdot u_e}{\partial t} \right] dv - \int_{z_1}^{z_2} \bar{P} u_e dz$$

Onde $\bar{P} = \bar{P}(z)$ é excesso de pressão neutra prescrita por unidade de comprimento

$$u_e = [N]\{q\}$$

$$\frac{\partial u_e}{\partial z} = \frac{d}{dz} [N]\{q\} = [B]\{q\}$$

$$\frac{\partial U_e}{\partial t} = \frac{\partial}{\partial t} [N]\{q\} = [N]\{\dot{q}\}$$

$$dV = Adz = A \frac{Q}{2} \delta S$$

Substituindo no funcional:

$$S_L = \frac{A}{2} \int_{-1}^{+1} \{q\}^T [B]^T [R] [B] \{q\} \frac{Q}{2} dS + A \int_{-1}^{+1} \{q\}^T [N]^T [N] \{\dot{q}\} \frac{Q}{2} dS - \int_{-1}^{+1} \{q\}^T [N]^T \bar{P} \frac{Q}{2} dS$$

$$\delta S_L = 0$$

$$\underbrace{\left(\frac{AQ}{2} \int_{-1}^{+1} [B]^T [R] [B] dS \right) \{q\}}_{[K']} + \underbrace{\left(\frac{AQ}{2} \int_{-1}^{+1} [N]^T [N] dS \right) \{\dot{q}\}}_{[K^*]} = \underbrace{\frac{PQ}{2} \int_{-1}^{+1} [N]^T dS}_{[Q']}$$

$$N_i = \prod_{\substack{j=1 \\ j \neq i}}^n \left(\frac{s - s_j}{s_i - s_j} \right)$$

$$N_1 = \prod_{j=1}^3 \left(\frac{s - s_j}{s_i - s_j} \right) = \left(\frac{s - s_2}{s_1 - s_2} \right) \left(\frac{s - s_3}{s_1 - s_3} \right) = \frac{s^2 - s}{2}$$

$$N_2 = \prod_{\substack{j=1 \\ j \neq 2}}^3 \left(\frac{s - s_j}{s_2 - s_j} \right) = \left(\frac{s - s_1}{s_2 - s_1} \right) \left(\frac{s - s_3}{s_2 - s_3} \right) = \frac{s^2 + s}{2}$$

$$N_3 = \prod_{\substack{j=1 \\ j \neq 3}}^2 \left(\frac{s - s_j}{s_3 - s_j} \right) = \left(\frac{s - s_1}{s_3 - s_1} \right) \left(\frac{s - s_2}{s_3 - s_2} \right) = 1 - s^2$$

$$N = [N_1 \ N_2 \ N_3] = \left[\frac{s^2 - s}{2}, \frac{s^2 + s}{2}, 1 - s^2 \right]$$

$$B = \frac{\partial N}{\partial S} \cdot \frac{ds}{dz} = \frac{\partial}{\partial s} \left[\frac{s^2 - s}{2}, \frac{s^2 + s}{2}, 1 - s^2 \right] \cdot \frac{2}{2} = \frac{1}{2} [2s-1, 2s+1, -4s]$$

$$K' = \frac{AL}{2} \int_{-1}^{+1} \frac{1}{2} \begin{bmatrix} 2S-1 \\ 2S+1 \\ -4S \end{bmatrix} Cv \frac{1}{2} \begin{bmatrix} 2S-1, 2S+1, -4S \end{bmatrix} dS = \frac{ACv}{6L} \begin{bmatrix} 14 & 2 & -16 \\ 2 & 14 & -16 \\ -16 & -16 & 32 \end{bmatrix}$$

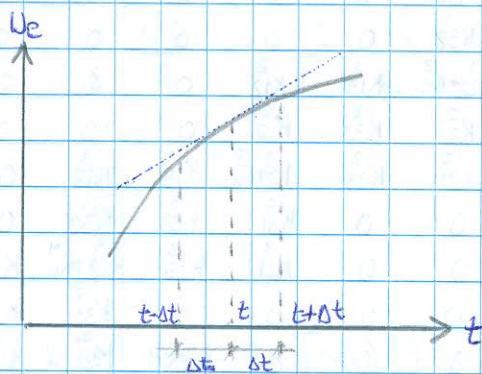
$$K^* = \frac{AL}{2} \int_{-1}^{+1} \begin{bmatrix} (\xi^2 S)/2 \\ (\xi^2 + S)/2 \\ 1 - \xi^2 \end{bmatrix} \begin{bmatrix} \xi^2 - S \\ \xi^2 + S \\ 1 - \xi^2 \end{bmatrix} d\xi = \frac{AL}{2} \int_{-1}^{+1} \begin{bmatrix} \frac{1}{4} \xi^2 (\xi-1)^2 & \frac{1}{4} \xi^2 (\xi^2-1) & \frac{1}{2} \xi (\xi-1)(1-\xi^2) \\ \frac{1}{4} \xi^2 (\xi+1)^2 & \frac{1}{2} \xi (\xi+1)(1-\xi^2) & \\ & (1-\xi^2)^2 & \end{bmatrix} d\xi$$

$$K^* = \frac{AL}{2} \begin{bmatrix} 4/15 & -1/15 & 2/15 \\ -1/15 & 4/15 & 2/15 \\ 2/15 & 2/15 & 16/15 \end{bmatrix} = AL \begin{bmatrix} 4 & -1 & 2 \\ -1 & 4 & 2 \\ 2 & 2 & 16 \end{bmatrix}$$

$$Q' = \bar{P} \frac{L}{2} \int_{-1}^{+1} \begin{bmatrix} \frac{1}{2} S(S-1) \\ \frac{1}{2} S(S+1) \\ 1 - S^2 \end{bmatrix} dS = \bar{P} \frac{L}{2} \begin{bmatrix} 1/3 \\ 4/3 \\ 4/3 \end{bmatrix} = \bar{P} L \begin{bmatrix} 1 \\ 1 \\ 4 \end{bmatrix}$$

$$\{\dot{q}\} = \begin{Bmatrix} \dot{U}_e^1 \\ \dot{U}_e^2 \\ \dot{U}_e^3 \\ \dot{D}_e \end{Bmatrix} \quad \{\ddot{q}\} = \begin{Bmatrix} \ddot{U}_e^1 \\ \ddot{U}_e^2 \\ \ddot{U}_e^3 \\ \ddot{D}_e \end{Bmatrix}$$

Derivada no tempo do excesso de pressão neutra:



Diferença finita central: $\ddot{U}_e = \lim_{\Delta t \rightarrow 0} \frac{U_e(t+\Delta t) - U_e(t-\Delta t)}{2\Delta t}$

No tempo t ,

$$[K']\{\dot{q}\}_t + [K^*]\{\ddot{q}\}_t = \{\ddot{Q}\}_t$$

$$[K']\{\dot{q}(t)\} + [K^*]\{\ddot{q}(t)\} = \{\ddot{Q}(t)\}$$

Pode ser re-escrita, considerando-se

$$\{q(t)\} = (1-\theta)\{q\}_{t-\Delta t} + \theta\{q\}_t$$

$$\{q(t)\} = \frac{\{q\}_t - \{q\}_{t-\Delta t}}{\Delta t}$$

$$\{Q(t)\} = (1-\theta)\{Q\}_{t-\Delta t} + \theta\{Q\}_t$$

$$[K]\left[(1-\theta)\{q\}_{t-\Delta t} + \theta\{q\}_t\right] + [K^*]\left[\frac{\{q\}_t - \{q\}_{t-\Delta t}}{\Delta t}\right] = (1-\theta)\{Q\}_{t-\Delta t} + \theta\{Q\}_t$$

$$(\Delta t [K] + [K^*])\{q\}_t = ([K^*] - (1-\theta)\Delta t [K])\{q\}_{t-\Delta t} + \Delta t (1-\theta)\{Q\}_{t-\Delta t} + \theta\{Q\}_t$$

$\theta = 1/2$ (Método Implícito, Crank-Nicolson)

$$\left(\frac{[K^*] + \Delta t [K]}{2}\right)\{q\}_t = \left(\frac{[K^*] - \Delta t [K]}{2}\right)\{q\}_{t-\Delta t} + \frac{\Delta t}{2} (1\{Q\}_{t-\Delta t} + 1\{Q\}_t)$$

Global	LOCAL											
	1	2	3	4								
1	1				K_{11}^1	K_{13}^1	K_{12}^1	0	0	0	0	0
2	3				K_{31}^1	K_{33}^1	K_{32}^1	0	0	0	0	0
3	2	1			K_{21}^1	K_{23}^1	$K_{22}^1 + K_{11}^2$	K_{13}^2	K_{12}^2	0	0	0
4	3				0	0	K_{31}^2	K_{33}^2	K_{32}^2	0	0	0
5	2	1			0	0	K_{21}^2	K_{23}^2	$K_{22}^2 + K_{11}^3$	K_{13}^3	K_{12}^3	0
6		3			0	0	0	0	K_{31}^3	K_{33}^3	K_{32}^3	0
7		2	1		0	0	0	0	K_{21}^3	K_{23}^3	$K_{22}^3 + K_{11}^4$	K_{13}^4
8			3		0	0	0	0	0	K_{31}^4	K_{33}^4	K_{32}^4
9			2		0	0	0	0	0	K_{21}^4	K_{23}^4	K_{22}^4

Para $t = 18,5$ dias = 1598400 seg, 10 intervalos de t entero $\Delta t = 159840$ seg

$$\Delta T = 10^{-2} \text{ cm}^2/\text{seg} \times 159840 \text{ seg} = 0,63936$$

$$(50 \text{ cm})^2$$

$$K^* = \begin{vmatrix} 4 & 2 & -1 \\ 2 & 16 & 2 \\ -1 & 2 & 8 \end{vmatrix} \begin{vmatrix} 2 & 16 & 2 \\ -1 & 2 & 8 \end{vmatrix} \begin{vmatrix} 2 & 16 & 2 \\ -1 & 2 & 8 \end{vmatrix} \begin{vmatrix} 2 & 16 & 2 \\ -1 & 2 & 4 \end{vmatrix}$$

$$\underline{A}\underline{l} = [M] \underline{A}\underline{l}, \quad A = 1\text{cm}^2$$

$$K' = \begin{vmatrix} 14 & -16 & 2 \\ -16 & 32 & -16 \\ 2 & -16 & 28 \end{vmatrix} \begin{vmatrix} 2 & -16 & 28 \\ -16 & 32 & -16 \end{vmatrix} \begin{vmatrix} 2 & -16 & 28 \\ -16 & 32 & -16 \end{vmatrix} \begin{vmatrix} 2 & -16 & 14 \end{vmatrix}$$

$$\underline{A}\underline{C}_x = [N] \underline{A}\underline{C}_v, \quad A = 1\text{cm}^2$$

$$Q' = \begin{vmatrix} 1 \\ 4 \\ 2 \\ 4 \\ 2 \\ 4 \\ 1 \end{vmatrix} \begin{vmatrix} \bar{P}\bar{l} \\ 0 \end{vmatrix} = \begin{vmatrix} \bar{P}\bar{l} \\ 6 \end{vmatrix}$$

$$\left(\frac{2}{30} [M] + \frac{\Delta t}{2} C_v [N] \right) \{q\}_t = \left(\frac{2}{30} [M] - \frac{\Delta t}{2} C_v [N] \right) \{q\}_{t-\Delta t} + \frac{\Delta t}{2} \left(\bar{P}l [0] + \bar{P}l [0] \right)$$

$$x(12/2) \left(\frac{2}{5} [M] + \Delta T [N] \right) \{q\}_t = \left(\frac{2}{5} [M] - \Delta T [N] \right) \{q\}_{t-\Delta t} + 3 \Delta t \bar{P} \left([0] + [0] \right)$$

$$\bar{P} = 0, \quad t_1 = t_0 + \Delta t = 159840 \text{ sec} \Leftrightarrow 185 \text{ days}$$

$$[X] = \frac{2}{S} [M] + \Delta T [N] = \begin{bmatrix} 10,55 & -9,43 & 0,88 \\ -9,43 & 26,86 & -9,43 \\ 0,88 & -9,43 & 21,10 \end{bmatrix}$$

$$\begin{bmatrix} -9,43 & 26,86 & -9,43 \\ 0,88 & -9,43 & 21,10 \\ -9,43 & 26,86 & -9,43 \end{bmatrix}$$

$$\begin{bmatrix} 0,88 & -9,43 & 21,10 \\ -9,43 & 26,86 & -9,43 \\ 0,88 & -9,43 & 21,10 \end{bmatrix}$$

$$\begin{bmatrix} -9,43 & 26,86 & -9,43 \\ 0,88 & -9,43 & 21,10 \\ -9,43 & 26,86 & -9,43 \end{bmatrix}$$

$$\begin{bmatrix} 0,88 & -9,43 & 21,10 \\ -9,43 & 26,86 & -9,43 \\ 0,88 & -9,43 & 21,10 \end{bmatrix}$$

$$[Y] = \frac{2}{S} [M] - \Delta T [N] = \begin{bmatrix} -7,35 & 11,03 & -1,68 \\ 11,03 & -14,06 & 11,03 \\ -1,68 & 11,03 & -14,70 \end{bmatrix}$$

$$\begin{bmatrix} 11,03 & -14,06 & 11,03 \\ -1,68 & 11,03 & -14,70 \\ 11,03 & -14,06 & 11,03 \end{bmatrix}$$

$$\begin{bmatrix} -1,68 & 11,03 & -14,70 \\ 11,03 & -14,06 & 11,03 \\ -1,68 & 11,03 & -14,70 \end{bmatrix}$$

$$\begin{bmatrix} 11,03 & -14,06 & 11,03 \\ -1,68 & 11,03 & -14,70 \\ 11,03 & -14,06 & 11,03 \end{bmatrix}$$

$$\begin{bmatrix} 11,03 & -14,70 & 11,03 \\ 11,03 & -14,06 & 11,03 \\ -1,68 & 11,03 & -14,70 \end{bmatrix}$$

$$[X] \{q\}_t = [Y] \{q\}_{t-\Delta t}$$

$$t_1 = 1,85 \text{ dias}$$

$$t_1 - \Delta t = 1,85 - 1,85 = 0 \text{ dias}$$

$$[X] \{q\}_{1,85} = [Y] \{q\}_0$$

$$\begin{array}{c|c} [X] & [Y] \\ \hline U_e^1 & U_e^1 \\ U_e^2 & U_e^2 \\ U_e^3 & U_e^3 \\ U_e^4 & U_e^4 \\ U_e^5 & U_e^5 \\ U_e^6 & U_e^6 \\ U_e^7 & U_e^7 \\ U_e^8 & U_e^8 \\ U_e^9 & U_e^9 \end{array} = \begin{array}{c|c} [Y] & [Y] \\ \hline 100 & 200 \\ 100 & 200 \\ 100 & 400 \\ 100 & 800 \\ 100 & 400 \\ 100 & 800 \\ 100 & 400 \\ 100 & 800 \\ 100 & 200 \end{array} = \begin{array}{c|c} [Y] & [Y] \\ \hline 200 & 400 \\ 200 & 400 \\ 400 & 800 \\ 800 & 1600 \\ 400 & 800 \\ 400 & 800 \\ 400 & 800 \\ 800 & 1600 \\ 200 & 400 \end{array}$$

U_e^1	0
U_e^2	58,822
U_e^3	82,710
U_e^4	92,879
U_e^5	97,008
U_e^6	98,763
U_e^7	99,468
U_e^8	99,750
U_e^9	99,821

$$t_2 = 3,7 \text{ días}$$

$$t_2 - \Delta t = 1,85 \text{ días}$$

$$[x] [U_e]_{3,7} = [y] [U_e]_{1,85} = \begin{bmatrix} 509,854 \\ 85,254 \\ 294,452 \\ 676,411 \\ 381,735 \\ 778,523 \\ 386,746 \\ 795,673 \\ 198,493 \end{bmatrix} \Rightarrow [U_e]_{3,7} = \begin{bmatrix} 0 \\ 21,916 \\ 53,385 \\ 74,414 \\ 86,842 \\ 93,425 \\ 96,707 \\ 98,194 \\ 98,609 \end{bmatrix}$$

$$t_3 = 5,55 \text{ días}$$

$$t_3 - \Delta t = 3,7 \text{ días}$$

$$[x] [U_e]_{5,55} = [y] [U_e]_{3,7} = \begin{bmatrix} 152,047 \\ 280,698 \\ 131,866 \\ 500,443 \\ 322,532 \\ 710,990 \\ 380,407 \\ 773,728 \\ 195,836 \end{bmatrix} \Rightarrow [U_e]_{5,55} = \begin{bmatrix} 0 \\ 24,638 \\ 40,412 \\ 58,674 \\ 73,643 \\ 84,128 \\ 90,585 \\ 93,958 \\ 94,990 \end{bmatrix}$$

$$t_4 = 7,4 \text{ días}$$

$$t_4 - \Delta t = 5,55 \text{ días}$$

$$[x] [U_e]_{7,4} = [y] [U_e]_{5,55} = \begin{bmatrix} 203,865 \\ 99,334 \\ 201,155 \\ 433,070 \\ 272,479 \\ 328,595 \\ 349,386 \\ 725,843 \\ 185,937 \end{bmatrix} \Rightarrow [U_e]_{7,4} = \begin{bmatrix} 0 \\ 16,926 \\ 37,678 \\ 52,093 \\ 64,778 \\ 75,191 \\ 82,735 \\ 87,201 \\ 88,672 \end{bmatrix}$$

$$t_5 = 9,25 \text{ días}$$

$$t_5 - \Delta t = 7,4 \text{ días}$$

$$[x] [U_e]_{9,25} = [y] [U_e]_{7,4} = \begin{bmatrix} 123,395 \\ 177,609 \\ 98,586 \\ 397,662 \\ 249,412 \\ 569,883 \\ 317,183 \\ 664,573 \\ 171,093 \end{bmatrix} \Rightarrow [U_e]_{9,25} = \begin{bmatrix} 0 \\ 17,346 \\ 30,572 \\ 46,061 \\ 58,457 \\ 68,168 \\ 75,275 \\ 79,656 \\ 81,138 \end{bmatrix}$$

$$t_6 = 11,1 \text{ días}$$

$$t_6 - \Delta t = 9,25 \text{ días}$$

$$[x] [U_e]_{11,1} = [y] [U_e]_{9,25} = \begin{bmatrix} 139,965 \\ 93,324 \\ 151,763 \\ 334,372 \\ 222,805 \\ 516,622 \\ 289,937 \\ 605,272 \\ 155,779 \end{bmatrix} \Rightarrow [U_e]_{11,1} = \begin{bmatrix} 0 \\ 13,889 \\ 29,664 \\ 41,290 \\ 52,487 \\ 61,676 \\ 68,402 \\ 72,472 \\ 73,839 \end{bmatrix}$$

$$t_7 = 12,95$$

$$t_7 - \Delta t = 11,1$$

$$[x] [Ue]_{12,95} = [y] [We]_{11,1} = \begin{bmatrix} 103,360 \\ 131,915 \\ 84,385 \\ 328,588 \\ 199,405 \\ 466,249 \\ 261,915 \\ 549,962 \\ 141,734 \end{bmatrix} \Rightarrow [We]_{12,95} = \begin{bmatrix} 0 \\ 13,655 \\ 24,906 \\ 37,562 \\ 47,558 \\ 55,812 \\ 61,972 \\ 65,975 \\ 67,057 \end{bmatrix}$$

$$t_8 = 14,8$$

$$t_8 - \Delta t = 12,95$$

$$[x] [Ue]_{14,8} = [y] [We]_{12,95} = \begin{bmatrix} 108,773 \\ 82,724 \\ 118,908 \\ 271,156 \\ 184,858 \\ 423,399 \\ 237,563 \\ 498,393 \\ 128,516 \end{bmatrix} \Rightarrow [We]_{14,8} = \begin{bmatrix} 0 \\ 11,515 \\ 24,025 \\ 33,653 \\ 43,077 \\ 50,616 \\ 56,197 \\ 59,628 \\ 60,791 \end{bmatrix}$$

$$t_9 = 16,65$$

$$t_9 - \Delta t = 14,8$$

$$[x] [Ue]_{16,65} = [y] [We]_{14,8} = \begin{bmatrix} 86,648 \\ 103,095 \\ 72,666 \\ 266,974 \\ 161,482 \\ 383,331 \\ 215,397 \\ 452,008 \\ 116,472 \end{bmatrix} \Rightarrow [We]_{16,65} = \begin{bmatrix} 0 \\ 11,044 \\ 20,525 \\ 30,808 \\ 38,916 \\ 45,810 \\ 50,917 \\ 54,050 \\ 58,105 \end{bmatrix}$$

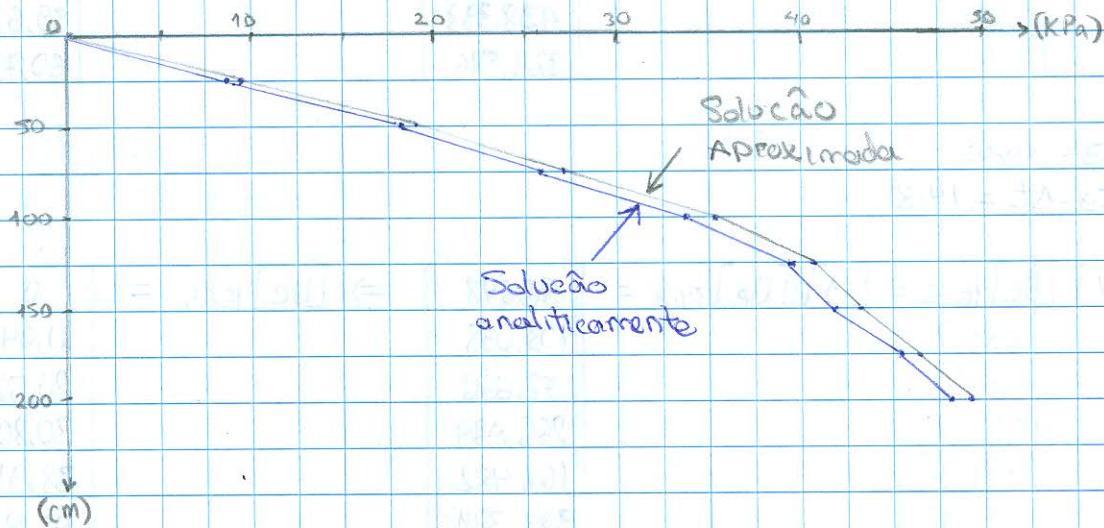
$$t_{10} = 18,5$$

$$t_{10} - \Delta t = 16,65$$

$$[X] [U_e]_{18,5} = [y] [U_e]_{16,65} = \begin{bmatrix} 87,333 \\ 71,112 \\ 94,531 \\ 222,474 \\ 153,009 \\ 346,769 \\ 195,021 \\ 409,480 \\ 805,609 \end{bmatrix} \Rightarrow [U_e]_{18,5} = \begin{bmatrix} 0 \\ 9,526 \\ 19,592 \\ 27,591 \\ 35,405 \\ 41,537 \\ 46,184 \\ 48,974 \\ 29,937 \end{bmatrix}$$

Comparando resultados com os valores da tabela abaixo no tempo $t = 18,5$ dias

Z (cm)	0	25	50	75	100	125	150	175	200
U_e (analisamente)	0	9,27	18,18	26,40	33,59	39,50	43,88	46,58	47,50
U_e (aproximada)	0	9,52	19,59	27,59	35,40	41,53	46,13	48,97	49,93



Comparando resultados com a solução gráfica $T = 0,40$

$$H = 200$$

$Z = 0$	$Z = 0$
25	0,125
50	0,25
75	0,375
100	0,5
125	0,625
150	0,75
175	0,875
200	1

$$W_0 = 100 \text{ kPa}$$

$U_e = 0$	$U_z = 1$
9,526	0,904
19,592	0,904
27,591	0,724
35,405	0,625
41,587	0,584
46,134	0,538
48,974	0,510
49,937	0,500

$$T = 0,4$$

$Z = 0$	$U_z = 1$
0,2	0,86
0,35	0,76
0,48	0,7
0,6	0,62
0,7	0,58
0,85	0,54
1	0,53

