

Projection Method for Incompressible Flow

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Abstract

1. Introduction

In physics, few equations span as wide a range of applications as the Navier-Stokes equations of fluid dynamics. They govern the motion of viscous fluids in a continuum framework, and as such have applications in *e.g.* climate modelling^[1,2], aerodynamics^[3–5], medicinal research^[6,7] and petroleum engineering^[8–11], to name a few. Named after Claude Navier and George Stokes for their major contributions^[12,13] to its formulation in the first half of the nineteenth century, the equations have constituted a major field of research in their own right since their formulation, and continue to do so today. Apart from their numerous applications, the equations are fundamentally interesting from a mathematical point of view. In fact, (dis-)proving the existence and uniqueness of their solutions is one of the seven Millenium prize problems^[14] for which a prize of one million US dollars is associated.

The generalized Navier-Stokes equations are based on the conservation of mass through the continuity equation,

$$\partial_t \rho + \nabla \cdot (\rho \mathbf{u}) = 0, \quad (1)$$

in addition to conservation of momentum as given by the Cauchy momentum equation

$$\rho (\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u}) = -\nabla p + \nabla \cdot \boldsymbol{\tau} + \mathbf{f}. \quad (2)$$

Here, we have introduced the primitive variables density ρ , velocity \mathbf{u} and pressure p , in addition to the deviatoric stress tensor $\boldsymbol{\tau}$. The vector \mathbf{f} accounts for external body sources such as gravity acting on the fluid, and shall henceforth be disregarded. The Navier-Stokes equations are an extension of Eqns. (1) and (2) derived under the assumptions that the strain tensor $\boldsymbol{\tau}$ is a linear function of

the strain tensor $\dot{\boldsymbol{\gamma}} = \nabla \mathbf{u} + (\nabla \mathbf{u})^T$, that $\nabla \cdot \boldsymbol{\tau} = 0$ for fluids at rest, and that the fluid is isotropic. Given these assumptions, Eq. (2) can be rewritten

$$\rho (\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u}) = -\nabla p + \nabla \cdot (\mu \dot{\boldsymbol{\gamma}}) + \nabla (\lambda \nabla \cdot \mathbf{u}) \quad (3)$$

where μ and λ are the first and second coefficients of viscosity, respectively.

When the fluid density ρ is constant, the flow is said to be incompressible. The second coefficient of viscosity, λ , is related to bulk viscosity and disappears for incompressible flow. Subsequently, we shall refer to μ as the viscosity of the fluid in the following.

- Show how they simplify under the assumption of incompressibility. Nondimensionalize the equations.
- Define stream function and vorticity.
- Talk about viscosity, and the two different representations we consider (Newtonian fluid with $\mu = \text{const}$, Non-Newtonian fluid exemplified by Bingham plastic).
- Introduce the lid-driven cavity test problem, explain what has been done in the literature.

2. Numerical methods

2.1. Newtonian fluid

- (Fractional step) projection methods
- Spatial discretization: the finite volume method
- Remember staggered grid!
- Boundary conditions

- Choice of time step for stability
- Solving the systems of equations with Eigen
- Checking if steady-state has been reached
- Transforming results to vorticity streamline formulation

2.2. Bingham plastic fluid

- Transient solution possible, cite appropriate paper and explain difficulty in discretizing the viscous term
- Reynolds number zero leads to removal of time-dependency because of alternative nondimensionalization of pressure
- Treatment of singularity in effective viscosity: regularization
- Finite volume method w/o need for staggered grid, discretization of viscous term
- Solution of steady-state system: SIMPLE and its extensions

3. Results

3.1. Transient behaviour

- Impulsively started
- What happens as a function of time?
- Results for different Re?

3.2. Steady-state solution

All results for Re=100,400,1000,3200.....

- 1D slices in the geometric center, including Ghia's results
- Stream lines and velocity vector fields
- Vorticity
- (Pressure field)!

3.3. Computational efficiency

- Computational complexity of the linear systems
- Runtime (and no of time steps) as a function of Re and N
- Plots of Δt vs. N for different Re

4. Discussion

- Everything works, results exactly as in literature
- Transient method is slow for high Re, SIMPLE could be better
- Other improvements include Hockney algorithm and multigrid methods
- Discuss stability and computational efficiency of

5. Conclusions

References

- [1] J. Marshall, A. Adcroft, C. Hill, L. Perelman, C. Heisey, A finite-volume, incompressible Navier-Stokes model for studies of the ocean on parallel computers, *Journal of Geophysical Research: Oceans* 102 (C3) (1997) 5753–5766.
- [2] F. X. Giraldo, M. Restelli, A study of spectral element and discontinuous Galerkin methods for the Navier-Stokes equations in nonhydrostatic mesoscale atmospheric modeling: Equation sets and test cases, *Journal of Computational Physics* 227 (8) (2008) 3849–3877.
- [3] M. M. Rai, Navier-Stokes simulations of rotor/stator interaction using patched and overlaid grids, *Journal of Propulsion and Power* 3 (5) (1987) 387–396.
- [4] J. L. Thomas, W. K. Anderson, S. T. Krist, Navier-Stokes computations of vortical flows over low-aspect-ratio wings, *AIAA journal* 28 (2) (1990) 205–212.
- [5] A. Jameson, L. Martinelli, N. Pierce, Optimum aerodynamic design using the Navier-Stokes equations, *Theoretical and Computational Fluid Dynamics* 10 (1-4) (1998) 213–237.
- [6] C. S. Peskin, Numerical analysis of blood flow in the heart, *Journal of Computational Physics* 25 (3) (1977) 220–252.
- [7] M. Mihaescu, S. Murugappan, M. Kalra, S. Khosla, E. Gutmark, Large eddy simulation and Reynolds-averaged Navier-Stokes modeling of flow in a realistic pharyngeal airway model: An investigation of obstructive sleep apnea, *Journal of Biomechanics* 41 (10) (2008) 2279–2288.
- [8] J. Deiber, W. Schowalter, Flow through tubes with sinusoidal axial variations in diameter, *AIChE Journal* 25 (4) (1979) 638–645.
- [9] G. Vinay, A. Wachs, J.-F. Agassant, Numerical simulation of weakly compressible Bingham flows: the restart of pipeline flows of waxy crude oils, *Journal of non-newtonian fluid mechanics* 136 (2) (2006) 93–105.
- [10] M. B. Cardenas, D. T. Slottke, R. A. Ketcham, J. M. Sharp, Navier-Stokes flow and transport simulations using real fractures shows heavy tailing due to eddies, *Geophysical Research Letters* 34 (14).
- [11] F. Boyer, C. Lapuerta, S. Minjeaud, B. Piar, M. Quintard, Cahn–Hilliard/Navier–Stokes model for the simulation of three-phase flows, *Transport in Porous Media* 82 (3) (2010) 463–483.

- [12] C. L. M. H. Navier, Memoire sur les lois du mouvement des fluides, Mémoires de l'Académie Royale des Sciences de l'Institut de France 6 (1822) 389–440.
- [13] G. G. Stokes, On the theories of the internal friction of fluids in motion and of the equilibrium and motion of elastic solids, Transactions of the Cambridge Philosophical Society 8 (1845) 287–319.
- [14] C. L. Fefferman, Existence and smoothness of the Navier-Stokes equation, The Millennium Prize Problems (2006) 57–67.