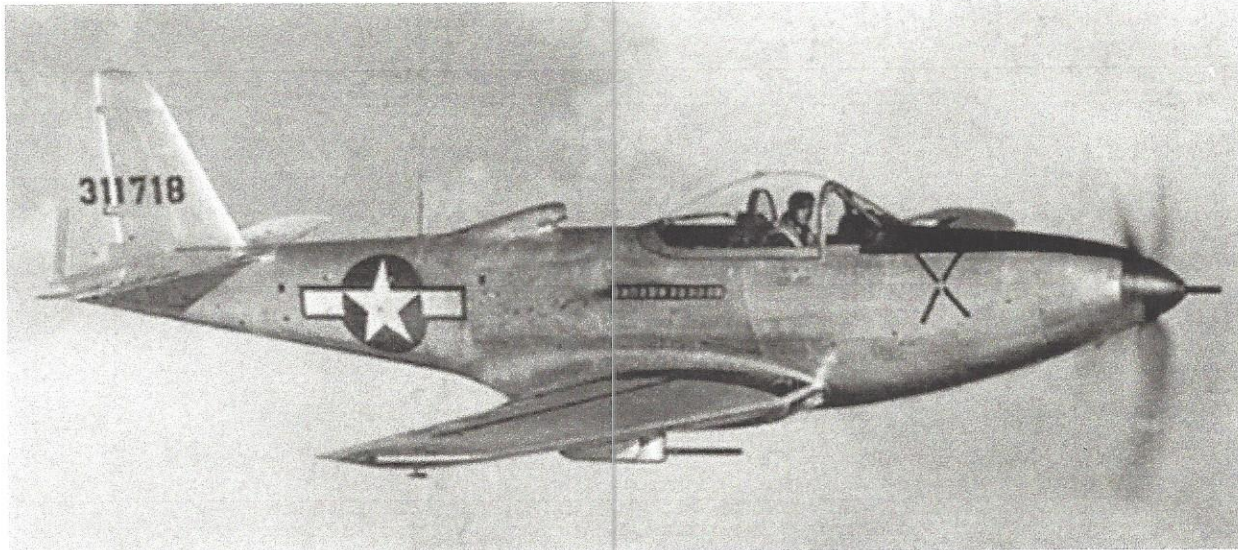


# Drag Prediction Project

## Aircraft #1 – Bell P-63 D-1 Kingcobra



*Only one P-63D was built with a bubble canopy. It was the fastest version of the P-63.*

Despite being heavier, the P-63D was the fastest version of the P-63 reaching 437 mph at 30,000 feet. The wing was lengthened by 10 inches and it was powered by an Allison V-1710-109 engine producing 1,425 hp. A major change was the removal of the automobile-type doors and the installation of a bubble canopy. The performance of the P-63D put it on par with the P-51 Mustang and P-47 Thunderbolt, but it was destroyed during diving tests.

Wing span:	Length:	Height:	Empty:	Max T/O:	Maximum Speed:	Service Ceiling:	Normal Range:	Max. Range:	Powerplant		
39 ft 2 in (11.94 m)	32 ft 8 in (9.96 m)	11 ft 2 in (3.40 m)	7,076 lb (3,210 kg)	11,100 lb (5,035 kg)	437 mph (703 km/h) at 30,000 ft (9,144 m)	39,000 ft (11,887 m)	950 miles (1,529 km)	2,000 miles (3,219 km)	<a href="#">One Allison V-1710-109</a>	1,425 hp (1,062 kW)	V-12, liquid cooled engine.

Using the data above and the drawings provided, estimate the  $C_{D0}$  of the aircraft for the following configurations: (scale drawings according to published lengths)

- Clean
- with just gear down for takeoff, and
- with gear and flaps (at  $30^\circ$ ) for landing

Assume the cruise altitude is 25,000 feet and the cruise velocity is 370 mph. Neglect all guns, gun pods and antennas. Include the cooling drag of the radiators.

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<b>P-63 D</b>			GW =	11,000	ESHP =	1,425	Allison V-1710-109A		
Item	Planform	(A <sub>wet net</sub> /		Interference					
	Area (ft <sup>2</sup> )	A <sub>wet gross</sub> )	C <sub>D</sub>	factor (%)	δf <sub>e</sub>	Δf <sub>e</sub>	Misc	Δf <sub>e</sub>	(see component calcs)
<b>Lifting Surfaces</b>									
Wing	250.8	0.929	0.008		1.864	2.237	Main Gear	6.237	
Wing/Fuse fair int				10	0.186		Nose Gear	3.802	
3D & roughness				5	0.093		Flaps @ 30°	3.010	
cntrl surf.gaps etc.				5	0.093				
Horz Tail	52.5	0.967	0.010		0.508		<b>SUMMARY</b>		(ft <sup>2</sup> )
Vert Tail int				10	0.051	0.610	Components		4.652
3D & roughness				5	0.025		Protuberances	10	0.465
cntrl surf.gaps etc.				5	0.025		Trim		0.30
Vert Tail	35.13	1.000	0.010		0.351		Momentum		0.23
Horz Tail int				5	0.018	0.422	<b>Airplane cruise mode</b>		5.645
Fuse int				5	0.018		<b>Airplane cruise mode</b>	5.65	(ft <sup>2</sup> )
3D & roughness				5	0.018		<b>Airplane T/O mode</b>	15.68	(ft <sup>2</sup> )
cntrl surf.gaps etc.				5	0.018		<b>Airplane LNDG mode</b>	18.69	(ft <sup>2</sup> )
<b>Bodies of Rev</b>	A <sub>w</sub> /A <sub>r</sub>	C <sub>d</sub> /C <sub>f</sub>		Interference					
	(ft <sup>2</sup> )	(N/D)	δf <sub>e</sub>	factor (%)	δf <sub>e</sub>				
<b>Fuselage</b>									
skin friction	270.26	0.002287	0.618		0.681	Δf <sub>e</sub>	C <sub>do</sub> =	0.0225	
frontal	9.52	0.078153	0.744			0.852			
Wing/fuse fairing int				10	0.068		C <sub>do</sub> =	0.0625	
Vert tail int				5	0.034				
3D & roughness				5	0.034		C <sub>do</sub> =	0.0745	
doors.gaps etc.				5	0.034				
<b>Canopy</b>	(ft <sup>2</sup> )	(N/D)	δf <sub>e</sub>	factor (%)	δf <sub>e</sub>				
skin friction	26.32	0.005805	0.153		0.156	Δf <sub>e</sub>			
frontal	4.06	0.039211	0.159			0.326			
canopy/fuse				10	0.068				
Vert tail int				5	0.034				
3D & roughness				5	0.034				
doors.gaps etc.				5	0.034				
<b>Carb Inlet</b>	(ft <sup>2</sup> )	(N/D)	δf <sub>e</sub>	factor (%)	δf <sub>e</sub>				
skin friction	4.19	0.007109	0.030		0.070	Δf <sub>e</sub>			
frontal	2.48	0.044550	0.111			0.206			
carb/fuse				10	0.068				
3D & roughness				5	0.034				
doors.gaps etc.				5	0.034				
<b>Component sub total</b>						4.652			



$$V_{\text{design or (ktas)}} = 370 \quad h_{\text{alt}} (\text{ft}) = 25,000 \quad \rho = 0.001065293 \quad \nu = 0.0003047$$

**Lifting Surfaces**

	Ref L (in)	Ref L (ft)	log Re	$C_{FB}$
Wing	85.8	7.15	7.1661	0.0028274
Horz Tail	46.8	3.90	6.9028	0.0031140
Vert Tail	62.4	5.20	7.0277	0.0029732

**Bodies of Rev**

	Ref L (in)	Ref L (ft)	log Re	$C_{FB}$	Maximum Perimeter (ft)	$A_{\text{wet gross}}$ (ft <sup>2</sup> )	$A_{\text{wet net}}$ (ft <sup>2</sup> )	$A_{\text{front}}$ (ft <sup>2</sup> )	$Dia_{\text{hyd}}$ (ft)	$l/d$	$d/l$	$C_{D \text{ WET}}$	$C_{Df}$
Fuselage	476.0	39.67	7.9104	0.0021911	10.94	312.45	270.26	9.52	3.48	11.39	0.08779	0.002287	0.078153
Carb Inlet	44.5	3.71	6.8816	0.0031389	5.58	7.46	4.19	2.48	1.78	2.09	0.47873	0.007109	0.04455
Canopy	86.9	7.24	7.1716	0.0028218	10.10	26.32	26.32	8.12	3.21	2.25	0.44412	0.005805	0.039211

$$V_{\text{design gear speed (ktas)}} = 120 \quad h_{\text{alt}} (\text{ft}) = 3000 \quad \rho = 0.002175257 \quad \nu = 0.000171$$

**MISC**

	Ref L (ft)	log Re	$C_{FB}$	$A_{\text{wet}}$	q	Drag	$\delta f_e$
main gear doors	0.974	6.3007	0.0039408	4.501	44.679	0.793	0.018
nose gear doors	6.496	7.1246	0.0028700	7.234	44.679	0.928	0.021
wing fairing	4.919	7.0038	0.0029995	1.585	44.679	0.212	0.005

	$A_{\text{frontal}}$	$C_{DF}$	$\delta f_e$
main gear oleos, etc.	8.407	0.50	4.204
main gear wheels	4.031	0.50	2.016
nose gear oleos, etc.	5.237	0.50	2.619
nose gear wheels	2.326	0.50	1.163
	20.002		

**flaps @ 30°**

flap/chord ratio	0.109
$\delta \alpha_o / \Delta \delta$	0.25
$\Delta C_D$	0.05
$b_f/b$	0.24
$\delta f_e$	3.010

Atmosphere

alt <sub>press</sub> =	25,000	(ft)	$\delta T(\Delta^{\circ}C)$		or $T_{amb} (^{\circ}F)$		or assume STD Day	
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(Input either  $\delta$  or amb temp value, but not both for non std day. Input "0" in both for a std day calc.)

Atm data		STD		SLS			
$h_{press}$ =	25000	(ft)	25000	(ft)			
$T_{amb}$ =	-34.528	( $^{\circ}C$ )	-30.150	( $^{\circ}F$ )			
$\delta$	0.3711	(N/D)	0.3711	(N/D)	$P_o$	2116.22	(lb/ft <sup>2</sup> )
$\theta$	0.8281	(N/D)	0.8281	(N/D)	$T_o$	518.688	(deg R)
$\sigma'$	0.4482	(N/D)	0.4481	(N/D)	$\rho_o$	0.002377	(slugs/ft <sup>3</sup> )
					$\mu_o$	3.7846E-07	(slug/ft-sec)
					$\nu_o$	1.5922E-04	(ft <sup>2</sup> /sec)

## Dimensional data from drawings.

TOP/FRONT VIEW				(scale factor=	
Wing				5.3872 mm/ft)	
T <sub>W</sub>		mm	ft		
	C <sub>R</sub>	48	8.910	area=	114.447
	C <sub>T</sub>	25	4.641	cx=	3.548
	L	91	16.892	cy=	7.559
E <sub>W1</sub>	c =		0.087		
	a	13	2.413	area=	5.277
	b	15	2.784	cx=	5.517
E <sub>W2</sub>				cy=	6.366
	a	14	2.599	area=	5.683
	b	15	2.784	cx=	5.942
Λ <sub>LE</sub>	5 degrees			cy=	6.366
HT					
T <sub>HT</sub>					
	C <sub>R</sub>	28	5.197	area=	23.215
	C <sub>T</sub>	10.5	1.949	cx=	2.059
	L	35	6.497	cy=	2.756
E <sub>HT1</sub>	c =		0.259		
	a	7.5	1.392	area=	1.522
	b	7.5	1.392	cx=	3.183
E <sub>HT2</sub>				cy=	3.183
	a	7.5	1.392	area=	1.522
	b	7.5	1.392	cx=	3.183
Λ <sub>LE</sub>	15 degrees			cy=	3.183
HT/F					
int "c"	c	26.5	4.919	area=	2.741
	t	3.8	0.705		
CARB INLET					
	w	6	1.114		

<b>MG</b>			
	mm	ft	
oleo-1	d	7 1.299	area= 2.412
	l	10 1.856	
oleo-2	d	7 1.299	area= 2.412
	l	10 1.856	
fork-1	w	5 0.928	area= 0.689
	l	4 0.742	
fork-2	w	2 0.371	area= 1.447
	l	21 3.898	
scissors	w	2 0.371	area= 1.447
	l	21 3.898	
wheel	w	9 1.671	area= 4.031
	d	13 2.413	
<b>NG</b>			
oleo	d	3 0.557	area= 2.067
	l	20 3.712	
fork-1	w	2.5 0.464	area= 1.723
	l	20 3.712	
scissors	w	2 0.371	area= 1.447
	l	21 3.898	
wheel	w	7.5 1.392	area= 2.326
	d	9 1.671	

<b>COOLING</b>			
	mm	ft	
<b>INLETS</b>			
Preston	w	7 1.299	area= 2.412
	h	10 1.856	total = 4.824
oil	w	10 1.856	area= 1.723
	h	10 1.856	total = 3.446
<b>W fairing/w int</b>			
	c	46 8.539	area= 1.585
	w	2 0.371	
<b>W/F int</b>			
	c	46 8.539	area= 12.679
	w	16 2.970	
<b>F/HT int</b>			
	c1	8 1.485	area= 3.721
	c2	4 0.742	
	l	18 3.341	

SIDE VIEW	(scale factor=	
	5.3878 mm/ft)	

VT	mm	ft
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T <sub>VT1</sub>			
C <sub>R</sub>	11	2.042	area= 11.368
C <sub>T</sub>	9	1.670	cx= 0.931
L	33	6.125	cy= 2.960

Λ <sub>LE</sub>	35	degrees	
T <sub>VT2</sub>			
C <sub>R</sub>	32	5.939	area= 18.887
C <sub>T</sub>	11	2.042	cx= 2.154
L	25.5	4.733	cy= 0.807

Λ <sub>LE</sub>	0	degrees	
E <sub>VT1</sub>			
a	9	1.670	area= 2.679
b	11	2.042	cx= 3.820
			cy= 4.669
E <sub>VT2</sub>			
a	9	1.670	area= 2.192
b	9	1.670	cx= 3.820
			cy= 3.820

CARB INLET			
L	20	3.712	
h	6	1.114	

CANOPY			
L	39	7.239	
h	10	1.856	
w	14	2.598	

W fairing int			
c	26.5	4.919	area= 2.741
t	3.8	0.705	

HT/F int	mm	ft	
c	26.5	4.919	area= 2.741
t	3.8	0.705	

VT/F int	mm	ft	
c	32	5.939	area= 2.177
t	2.5	0.464	

CARB INLET/F int			
L	20	3.712	area= 3.266
w	6	1.114	

CANOPY/F int	mm	ft	
L	39	7.239	area= 14.859
w	14	2.598	

W fairing/F int	mm	ft	
c	26.5	4.919	area= 2.741
t	3.8	0.705	

MG	mm	ft	
strut door	w	4.5	0.835
	l	6	1.114

MG	mm	ft	
wheel door	w	32	5.939
	l	2.5	0.464

NG	mm	ft	
wheel door	w1	4	0.742
	w2	2	0.371
	l	35	6.496

#### FUSELAGE MAX PERIMETER

E <sub>F1</sub>			
a	8	1.485	area= 2.597
b	12	2.227	
E <sub>F2</sub>			
a	8	1.485	area= 2.165
b	10	1.856	
total area = 9.524			
D <sub>HYD</sub> = 3.482			
P <sub>MAX</sub> = 10.940			

#### CANOPY MAX PERIMETER

E <sub>C1</sub>			
a	7.5	1.392	area= 2.029
b	10	1.856	
total frontal area = 4.058			
extended BofR frontal area = 8.117			
D <sub>HYD</sub> = 3.215			
P <sub>MAX</sub> = 10.100			

#### CARB INLET MAX PERIMETER

E <sub>CI1</sub>			
a	6	1.114	area= 1.240
b	6	1.114	
total frontal area = 2.480			
extended BofR frontal area = 2.480			
D <sub>HYD</sub> = 1.777			
P <sub>MAX</sub> = 5.583			

## REFERENCE AREAS & CENTROIDS

### Lifting Surfaces

#### Wing

g			mm	(ft)	Gross Wetted Area=	541.757	
Area=	250.8135	(ft <sup>2</sup> )	mgc=	38.5	7.147	Intersection areas =	38.463
Cy =	7.455	(ft)			85.758	Net Wetted Area =	503.295
Cx =	3.739	(ft)				A <sub>N</sub> /A <sub>G</sub> =	0.929

#### HT

				Gross Wetted Area=		113.441		
Area=	52.519	(ft <sup>2</sup> )		mm	(ft)	Intersection areas =	3.721	
Cy =	2.806	(ft)	15.115	mgc=	21	3.898	Net Wetted Area =	109.720
Cx =	2.189	(ft)				46.777	A <sub>N</sub> /A <sub>G</sub> =	0.967

#### VT

				Gross Wetted Area=		75.871		
Area=	35.126	(ft <sup>2</sup> )		mm	(ft)	Intersection areas =	0.000	
Cy =	1.986	(ft)	10.703	mgc=	28	5.197	Net Wetted Area =	75.871
Cx =	1.989	(ft)				62.364	A <sub>N</sub> /A <sub>G</sub> =	1.000

### Bodies of Revolution

#### Fuselage

length =	39.667	(ft)	Gross Wetted Area=	312.446
max P =	10.940	(ft)	Intersection areas =	42.183
	476.004		Net Wetted Area =	270.262
			$A_N/A_G$ =	0.865

#### CARB INLET

length =	3.712	(ft)	Gross Wetted Area=	7.461
max P =	5.583	(ft)	Intersection areas =	3.266
	44.545		Net Wetted Area =	4.195
			$A_N/A_G$ =	0.562

#### Canopy

length =	7.239	(ft)	Gross Wetted Area=	26.318
max P =	10.100	(ft)	Intersection areas =	0.000
	86.864		Net Wetted Area =	26.318
			$A_N/A_G$ =	1.000



MAX cross sectional area

A | B | C | D | E | F

G | H | J | K

$T_{HT}$   $CR=32$   
 $CF=11$   
 $L=25.5$

$E_{HT}$   $a=8$   
 $b=11$

$E_{LT}$   $a=8$   
 $b=9$

all measurements in mm  
Scale factor side view  
(based on fuselage length)  
5.38776 → 1 mm

$L_{canopy}$

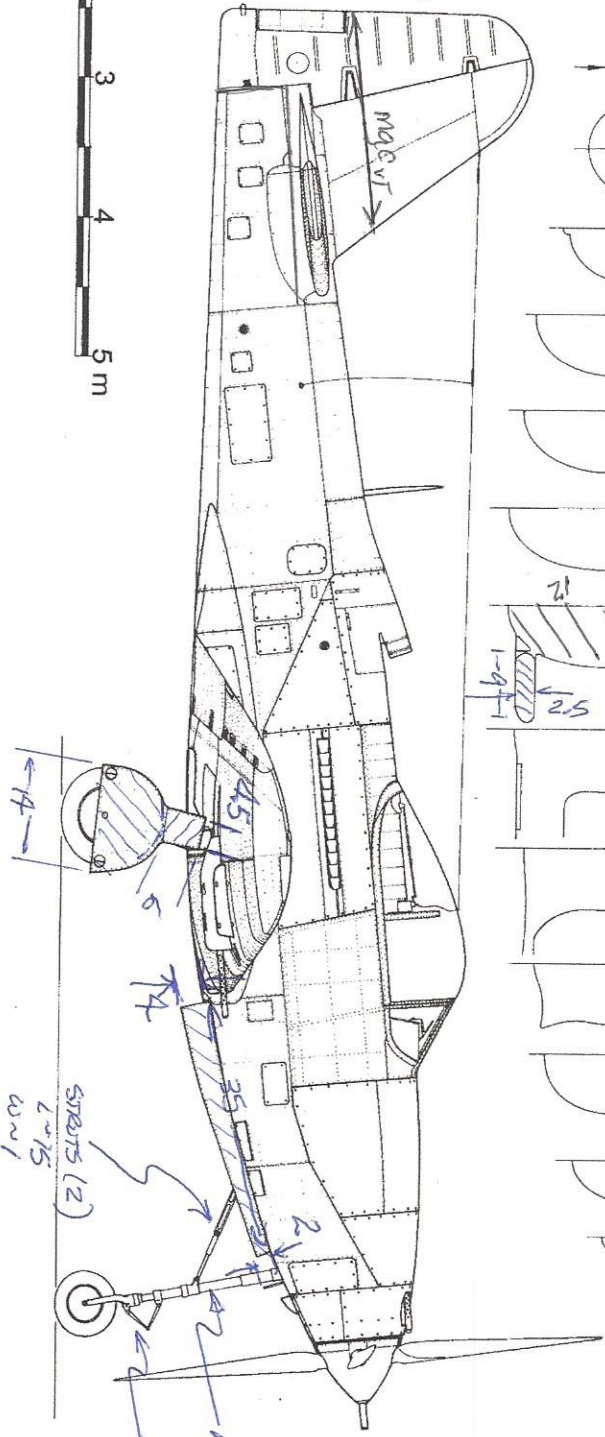
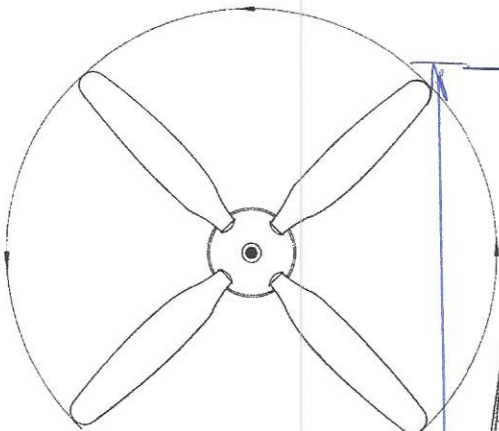
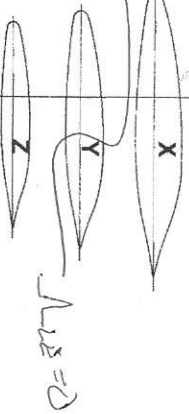
$L_{cabin}$

$L_{fuselage}$

$L_{faring}=65, t=11$

P-63 D-1

$L_{HT}$   $CR=11$   
 $CF=19$   
 $L=23$



AVG SPURT DIA 1.5  
SCISSOR  $\approx 2.0$  wide  
 $L=7$

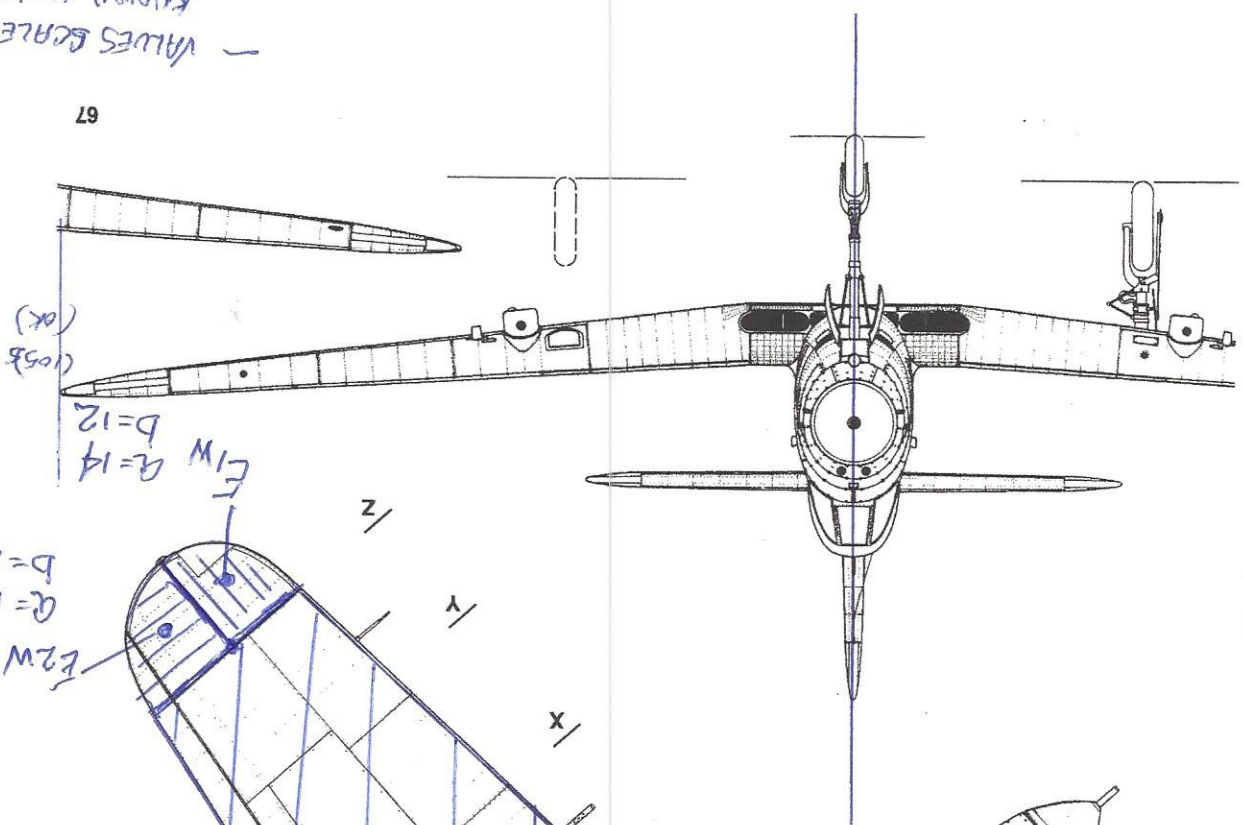
SPURTS (2)

$L=15$   
 $W=1$



— VALUES SCALING USING  
KNOWN WING SPAN.

67



$E_{1W} \quad a=14$   
 $b=12$   
 $a=14$   
 $b=13.5$   
 $E_{2W}$

$L=91$   
 $C_T=25$   
 $C_R=50$   
 $I_W$

P-63 D-1



$E_{1HT} \quad a=7.5$   
 $b=7.5$

$C_T=28$   
 $C_T=10.5$   
 $L=30$

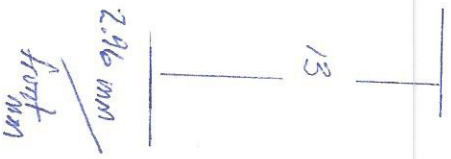
$E_{2HT} \quad b=7.5$   
 $a=7.5$

0 1 2 3m

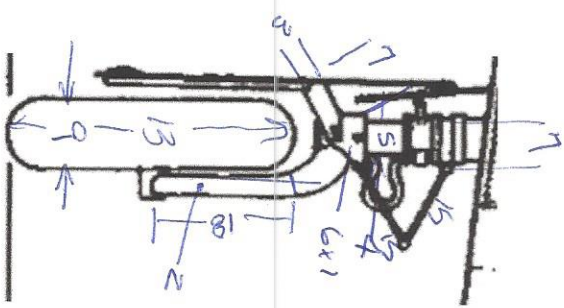
$\angle LE=15^\circ$

$\angle LE=50^\circ$

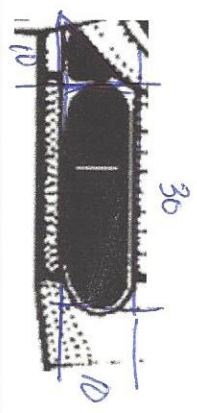
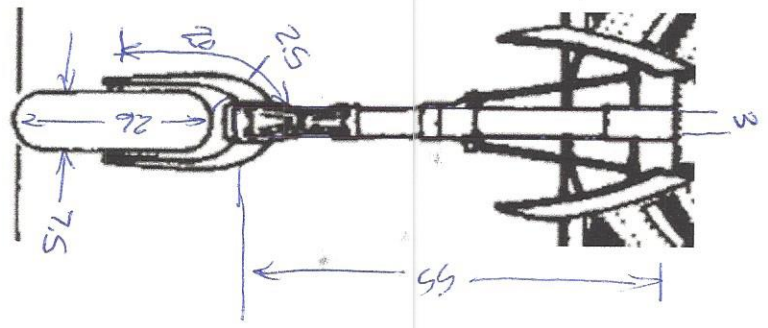
— All measurements are in  
mm  
Scale factor for top front  
5.3872 mm/lp



main landing gear

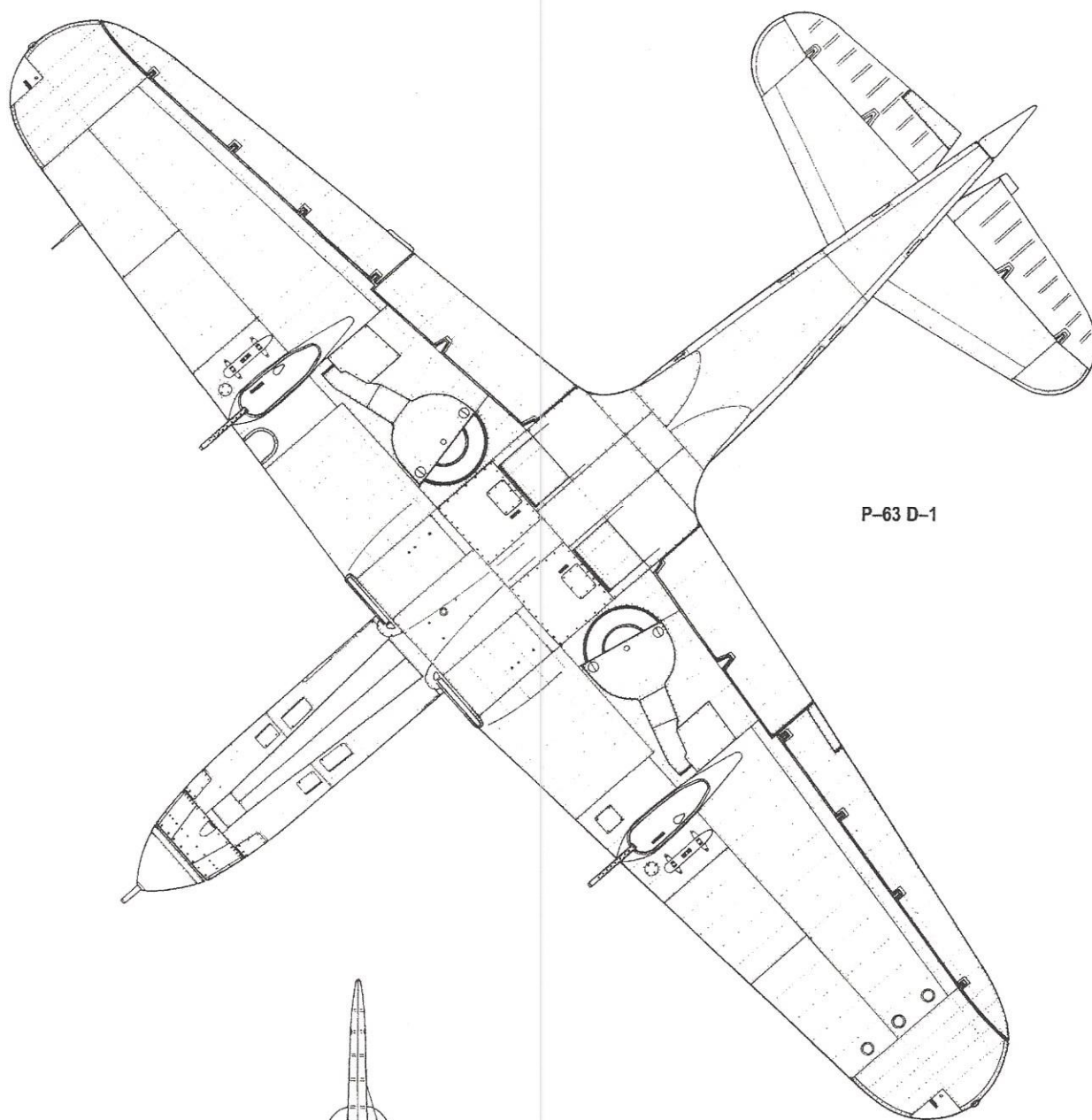


nose landing gear

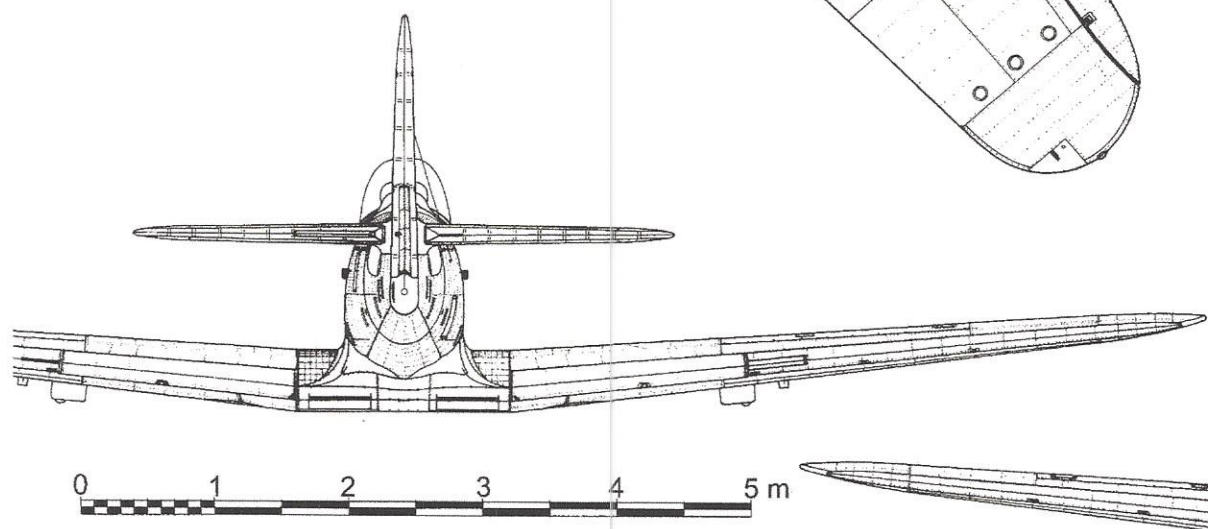


Preston & oil cooler inlet

scaled up by  $\approx 3x$   
to measure

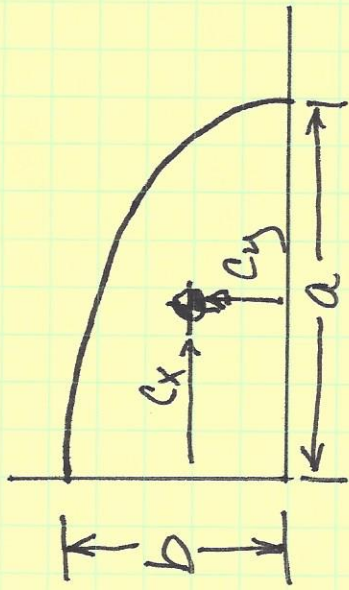


P-63 D-1



*not used*





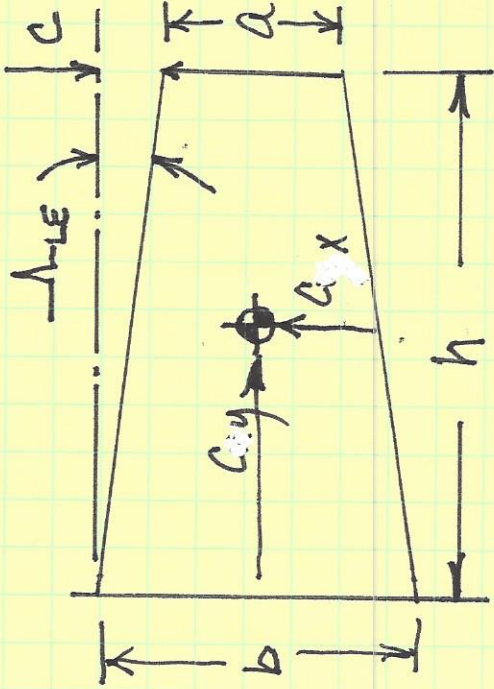
AREA

$$\text{area} = \frac{\pi ab}{4}$$

CENTROID

$$\bar{X} = \frac{4a}{3\pi}$$

$$\bar{Y} = \frac{4b}{3\pi}$$



AREA

$$\text{area} = \frac{h(a+b)}{2}$$

$$\bar{C}_x = \frac{2ac + a^2 + cb + ab + b^2}{3(a+b)}$$

$$\bar{C}_y = \frac{h(2a+b)}{3(a+b)}$$

$$c = h \sin \angle_{LE}$$

check: if  $b=a$  [rectangle]  $= 1 \Rightarrow \angle_{LE} = 0^\circ$  let  $h=2$

then  $c = h \sin \angle_{LE} = h(0) = 0$

$$\bar{C}_x = \frac{(2)(0) + (1)^2 + (0)(1) + (1)(1) + (1)^2}{3(1+1)} = \frac{3}{3(2)} = \frac{1}{2} \quad \checkmark$$

$$\bar{C}_y = \frac{(2)[(2)(1) + 1]}{3(1+1)} = \frac{6}{6} = 1 \quad \checkmark$$