

TASS: A Toolkit for Aircraft Sizing and Synthesis

Komahan Boopathy `komahan@gatech.edu`

January 25, 2016

Abstract

A Toolkit for Aircraft Sizing and Synthesis (TASS), capable of performing sizing and synthesis calculations in the context of conceptual design of aircraft is developed in Matlab.⁵ The TASS implements energy-based constraint and weight-fraction approach for the mission sizing analyses, and provides the user with a design point that is a function of *thrust-weight ratio* and *wing-loading*. The performance of the TASS is benchmarked against the known metrics of a transonic jet fighter aircraft F-86 Sabre (Sabrejet).

Contents

1	Introduction and Motivation	4
2	Installation and Working	4
2.1	Installation	4
2.2	Constraint Analysis Layout	5
2.3	Weight Analysis Layout	6
2.4	Mission Summary Layout	7
2.5	Theory and Models	7
3	Fighter Aircraft Design	9
3.1	Aircraft Requirements	9
3.2	Constraint Analysis	10
3.3	Weight Estimation	11
3.4	Mission Summary	15
3.5	Benchmarking the design	15
4	Conclusion	16
A	Flexibility of the Tool	17
A.1	Versatility of the Tool	17
A.2	Challenges and Cons	18

List of Figures

2.1	Figure showing the constraint analysis layout.	5
2.2	Figure showing the weight estimation layout.	6
2.3	Figure showing the mission summary layout.	8
2.4	A top level overview of sizing and synthesis process implemented in TASS. ⁷	8
3.1	Figure showing the inputs for constraint analysis.	12
3.2	Plot showing the constraints for the required design.	13
3.3	Plot showing standard constraints along with load factor $n = 3$	13
3.4	Panel designed for inputting the payload and crew weights.	13
3.5	Input panel facilitating the selection of different models for empirical estimation of empty weights.	14
3.6	Input panel for fuel weight calculations.	14
3.7	A pie-chart showing the weight fractions (top) and the table summarizing the actual weights (bottom).	15
3.8	Breakdown of mission parameters across different mission segments.	16
3.9	Plot of drag polar for two representative velocities at sea-level.	16

List of Tables

1	Parameters in Mattingly Energy Equation	9
2	Requirements of the fighter aircraft and for different stages in the mission profile . .	10
3	Performance requirements of the desired aircraft	11
4	Validation of the F-86L Sabre design produced by the TASS	15

1 Introduction and Motivation

Design of aircraft is subject to tens of thousands of constraints that span across a variety of disciplines such as aerodynamics, structures, controls and performance.^{3,4,9,10} Examples of such constraints, to name a few are: achieving a long cruise range, minimizing the take-off distance, fuel-efficient engines, stealth capabilities for reconnaissance, lift-constrained-drag-minimization, stress and strain requirements, and so on. These constraints are indeed the ones that drive the design and play a pivotal role in shaping the end-design. There has been an increased interest in exploring more at initial stages of design to identify conventional as well as non-conventional configurations – a strategy that helps one to get a better insight of potential configurations that can meet the design requirements and eliminate retrospective changes that may be due at later stages of the design process, that are known to be prohibitively expensive.

Similar motivations have led to development of tools that ably perform conceptual analysis in various platforms.^{8,11} To this end, this work too aims to develop a toolkit in Matlab⁵ known as TASS, that performs an analysis of the early phases of aircraft design *i.e.*, the sizing and synthesis. The scope of current work is limited to the conceptual design phase of aircraft design; more advanced phases in aircraft design (e.g. preliminary, detailed design *etc.*) fall beyond the scope of current work. Nevertheless, modularity is a key consideration in the development of the toolkit, which enables further advancements a function of time.

Energy based constraint analyses encompass an attractive way to start with aircraft design. The main advantage of energy-based approach over conventional approaches is that it employs Lagrangian paradigm of mechanics, as opposed to Newton’s world of vector mechanics. The key idea is that aircraft is treated as a system that converts energy from one form to another as the mission progresses. For example, combustion in the engines convert the chemical energy of the fuel into thermal energy, which in-turn accelerates the gases to rotate the turbines to provide mechanical energy to sustain motion. It is easier to think in terms of scalars such as potential energy (depends on position) and kinetic energy (depends on rate of change of position), compared to resolving forces (e.g. lift, thrust) along different directions (e.g. vertical, horizontal) and invoking force and moment balances. Due to such advantages, the TASS preferably employs energy based constraint analyses. The mathematical and physical models used in various stages of the mission are explained as and when they are introduced in later sections and are not explained here for brevity.

2 Installation and Working

This section is devoted to provide a high-level overview of the of the software. A Graphical User Interface (GUI) is designed to collect all the mission-specific inputs that the user supplies to the software. From an user-standpoint these input parameters are decided based on the complete break-down of mission requirements (e.g. humanitarian, rescue, military missions).

2.1 Installation

The TASS uses native Matlab code for all of its functionality – including initialization, iterative calculations and graphics, therefore a working version of Matlab⁵ is sufficient. The software is tested to work on both UNIX and Windows based workstations. The source code can be obtained

by using `git clone https://github.com/komahanb/tass.git` from a *terminal* or *shell* program or by downloading `tass.zip` file and extracting it in a working folder of convenience.

2.2 Constraint Analysis Layout

The constraint analysis layout is designed to take a large number of input parameters. This, indeed increases the complexity of use but makes the tool more robust in terms of accommodating wide array of inputs and helps the user to analyze more flight conditions. Figure 2.1 shows the layout designed for the constraint analyses.

Execution: The user can run this layout by typing `constraint_analysis` in MATLAB command line or by opening `constraint_analysis.fig` file.

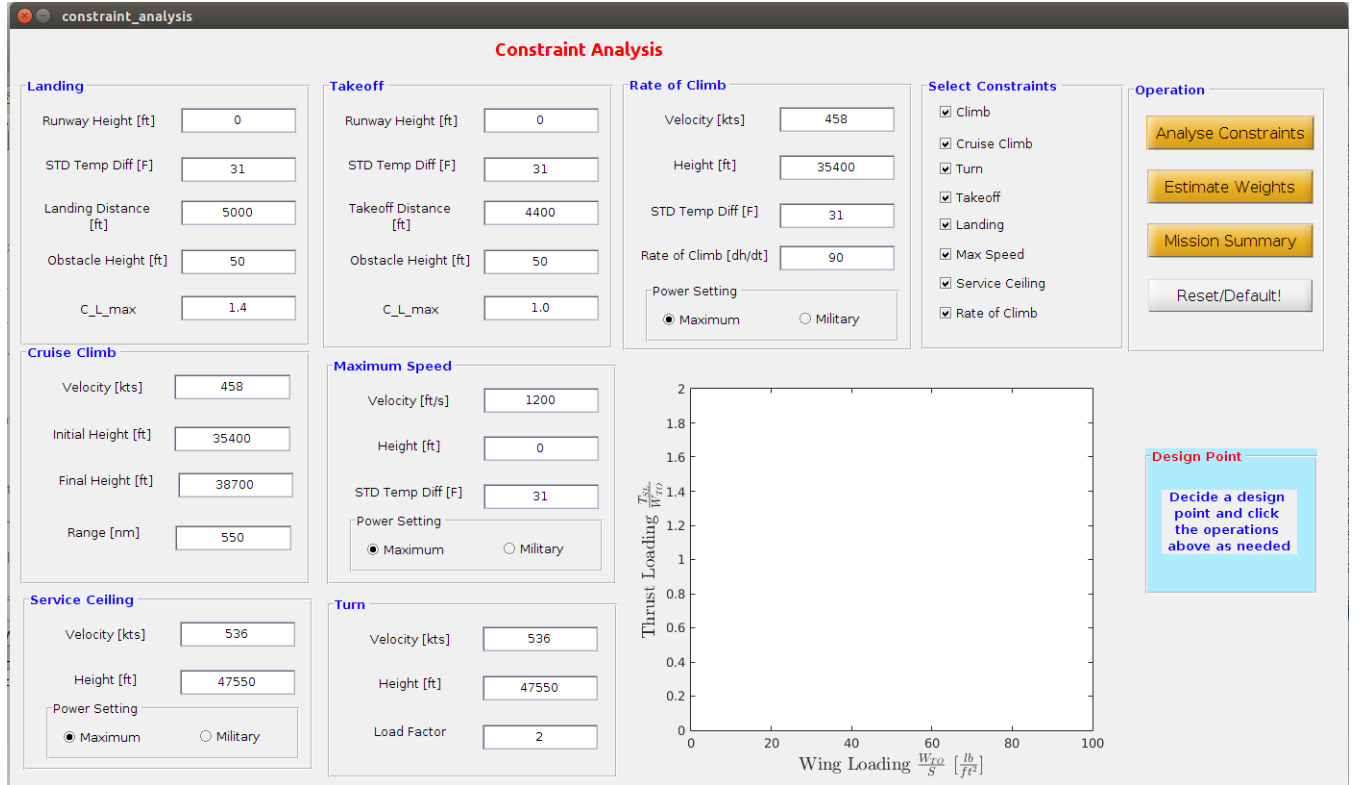


Figure 2.1: Figure showing the constraint analysis layout.

Input: The general inputs are velocity, height, range, thrust setting, rate of climb etc. These general inputs are assembled across different segments of mission and for different performance requirements for analysis. The constraint analyses automatically computes the fuel-burn correction factor (using Mach number, height, temperature), β , and the thrust lapse factor, α (using “internal” mission analyses). This accommodates the effects of the coupling of the *Constraint Analysis* with that of Weight Estimation shown in Figure 2.4.

Output: The TASS provides a constraint analysis plot and enables the user to directly identify a design point in terms of thrust to weight ratio and wing loading. For further analyses, the user can now click appropriate buttons: *Estimate Weights* and *Mission Summary*. Note that the *Mission Summary* needs the results of *Estimate Weights* and therefore should be the last operation to perform.

2.3 Weight Analysis Layout

This layout (see Figure 2.2) provides a mission weight analysis for the sizing of the system indicating the converged estimated gross takeoff weight and weight contributions from the different weight groups such as payload, fuel and crew.

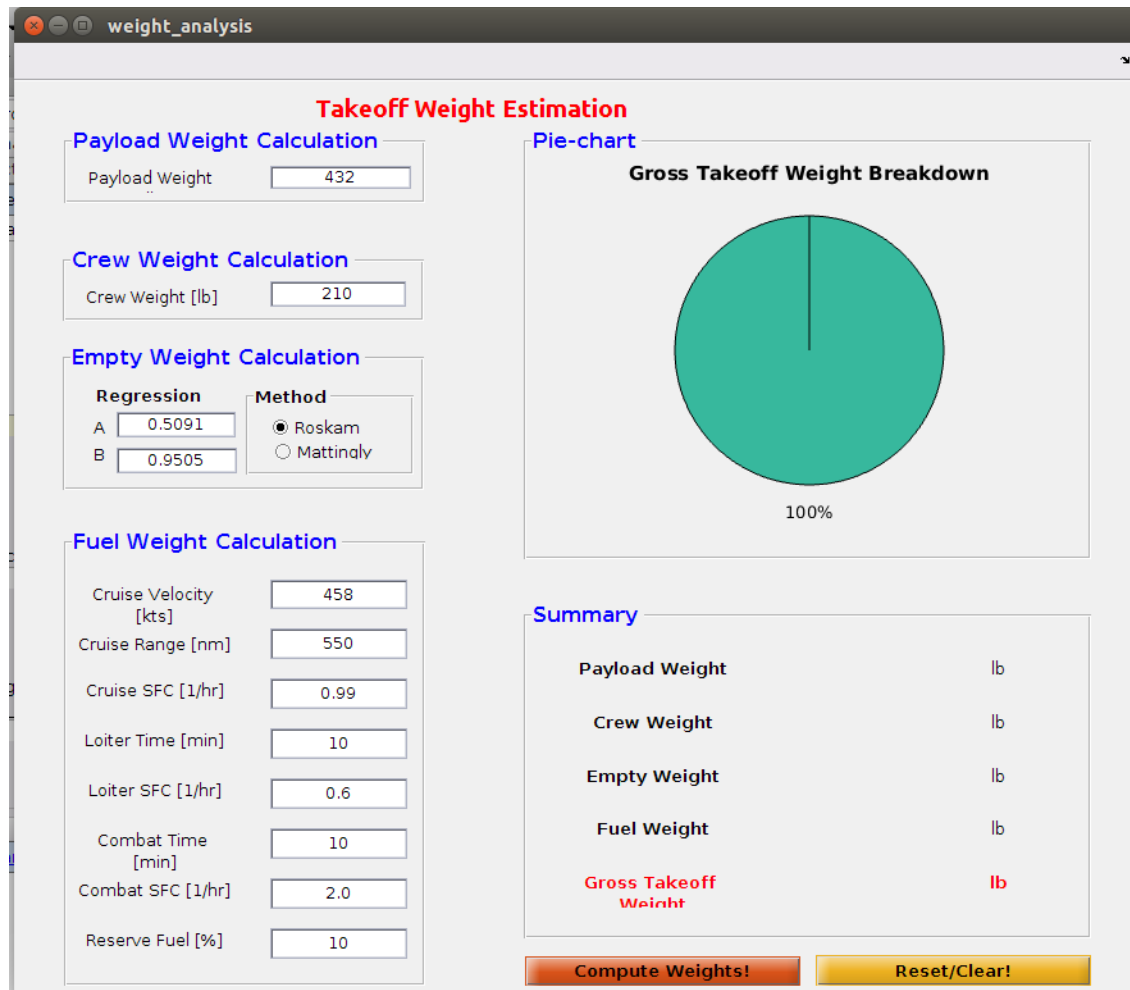


Figure 2.2: Figure showing the weight estimation layout.

Execution: This layout can be executed by typing `weight_analysis` in MATLAB command line or by clicking the `weight_analysis.fig` file. Alternatively, it can be executed by clicking the *Estimate Weights* button in *Constraint Analysis* layout.

Input: The user supplies known information such as crew and payload weights, information about mission such as the velocity, range, loiter time and reserve fuel required. The user can experiment with nominal perturbations of these values for detailed studies.

Output:

- a pie-chart which represents the weight fractions (weights) as percentages of total weight
- a table listing out the converged results of weight estimation.

2.4 Mission Summary Layout

Figure 2.3 shows the layout designed for producing the summary of the mission in terms of different segments identified in Table 2.

Execution: There are two ways to run this layout:

- by typing `mission_summary` in the MATLAB command line or by opening `mission_summary.fig` file
- by clicking **Mission Summary** button from *constraint analysis* layout

Input: The user will supply the design point which is selected from the *constraint analysis* layout and click the **Generate Summary** button.

Output: The layout will then automatically generate the following results:

- drag-polar plots for two representative velocities 100 *ft/s* and 1200 *ft/s*
- table containing the breakdown of performance related quantities such as β , $\frac{W_{n-1}}{W_n}$, the weight of fuel burnt, variation of gross take off weight, wing loading and thrust loading, with respect to different mission-segments
- a text box displaying the wing planform area S

2.5 Theory and Models

A rough outline of the theory, physical and mathematical models used in TASS follows. A rather comprehensive discussion on these topics can be found in the literature.^{3,4,6,9,10} Figure 2.4 provides a generic overview of the elements involved in the sizing and synthesis process. As it can be seen, *constraint analyses* and *weight estimations* are pivotal in producing the design.

Standard Atmosphere Model: The toolkit automatically computes the standard atmosphere conditions based on the U.S. Standard Atmosphere model.^{13,14} The standard atmosphere model provides the temperature, speed of sound (Mach number), pressure and density as a function of height in the calculations.



Figure 2.3: Figure showing the mission summary layout.

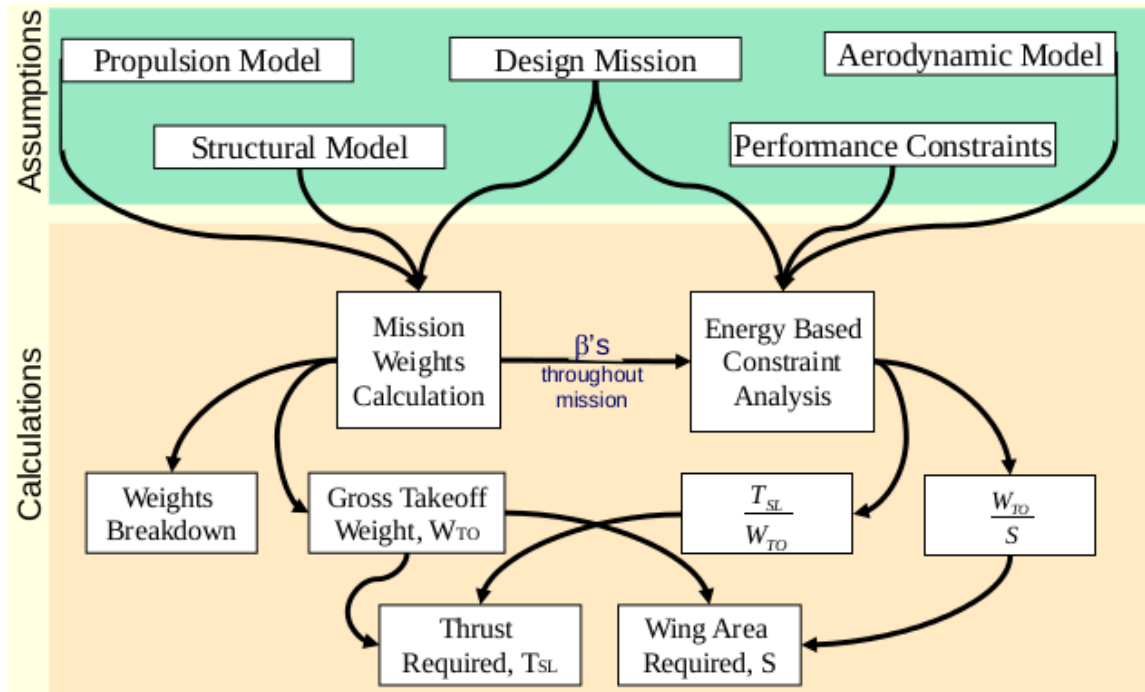


Figure 2.4: A top level overview of sizing and synthesis process implemented in TASS.⁷

Mattingly Energy Equation: The performance constraints and requirements are set as functions of *thrust loading* (thrust-to-weight ratio) and *wing loading*, the two sizing parameters that

contain key information about the top level characteristics of the system.⁶ The Mattingly Master Energy equation is:

$$\frac{T_{SL}}{W_{TO}} = \frac{\beta}{\alpha} \left\{ \frac{qS}{\beta W_{TO}} \left[K_1 \left(\frac{n\beta W_{TO}}{qS} \right)^2 + K_2 \left(\frac{n\beta W_{TO}}{qS} \right) + C_{D_0} + \frac{R}{qS} \right] + \frac{1}{V} \frac{d}{dt} \left(h + \frac{V^2}{2g_0} \right) \right\} \quad (2.1)$$

Table 1 contains a short definition of the parameters in Eq. 2.1.

Table 1: Parameters in Mattingly Energy Equation

Parameter	Description	English Unit
T_{SL}	sea-level thrust	lb
W_{TO}	take-off gross weight	lb
q	dynamic pressure	lb/ft^2
S	wing planform area	ft^2
C_{D_0}	drag at zero lift	no unit
K_1	Parasitic Drag constant	no unit
K_2	Interference drag	no unit
q	load factor	no unit
R	Resistance Drag	lb
V	velocity(speed)	ft/s
h	altitude from sea level	ft
g_0	gravity at sea level	ft/s^2
α	thrust lapse correction	no unit
β	fuel burn correction	no unit

3 Fighter Aircraft Design

This section describes the results of the aircraft designed using TASS in response to the mission and requirements are outlined in RFP.⁷ After the discussion of individual results, the design produced by the TASS will be compared to the design of the actual aircraft.

3.1 Aircraft Requirements

The conceptual design process begins with a defined set of requirements. These requirements lay-out specific constraints and design goals that the end-system must be capable of achieving. These goals and constraints are often presented the form of Request for Proposal (RFP).

Mission Profile: Table 2 breaks-down the performance requirements of the aircraft to be designed using the TASS.

Functional Requirements: The functional requirement of the aircraft is to carryout a military mission, which is:

- to carry a crew member weighing 210 *lbs*
- to carry a payload of 432 *lb*

Table 2: Requirements of the fighter aircraft and for different stages in the mission profile

Segment	Phase	Performance Requirements
0-1	Takeoff	Distance 4400 <i>ft</i> Clear obstacle at 50 <i>ft</i> Maximum power with afterburners Sea level runway at 90 <i>F</i>
1-2	Climb	Altitude 35400 ft Full military power without afterburners Maximum rate of climb 90 <i>ft/s</i>
2-3	Cruise climb	Altitude 38700 ft Distance 550 nautical miles Cruise speed 458 knots Normal power
3-4	Loiter	Altitude 38700 ft 10 minutes loiter normal power
4-5	Climb	Altitude 47550 ft
5-6	Combat	Maximum power with afterburners Duration 5 minutes Speed 536 knots
6-7	Descend	Descend to 37000 ft
7-8	Cruise	Altitude 37000 ft Distance 550 nautical miles Normal power
8-9	Loiter	10 minutes Altitude 35000 ft Maximum endurance conditions
9-10	Descend	Descend and line up for landing
10-11	Landing	Distance 5000 ft Without highlift devices 10% fuel reserve

Performance Requirements: The elements in mission profile are decomposed into performance requirements that are tabulated in Table 3. This table gives rise to the following constraints that take part in the constraint analysis.

3.2 Constraint Analysis

By manipulating Eq. 2.1 various constraints pertaining to the mission can be derived. Detailed derivation and treatment of such constraints can be found in Mattingly *et al.*⁶ TASS implemented seven constraints pertaining to the requirements.

1. Rate of climb constraint
2. Takeoff constraint

Table 3: Performance requirements of the desired aircraft

Item	Performance Requirements
Takeoff distance	4400 <i>ft</i> at sea-level and 90 <i>F</i> temperature
Landing distance	5000 <i>ft</i> at sea-level and 90 <i>F</i> temperature
Maximum air speed	1200 <i>ft/s</i> at sea-level
Maximum rate of climb	90 <i>ft/s</i>
Manueverability at Peak Altitude	47550 ft
Turn	2g sustained turn ¹

3. Landing constraint
4. 2*g* combat turn maneuver constraint
5. service ceiling constraint
6. maximum speed constraint
7. cruise climb constraint

These constraints are derived from the requirements given in the previous sections. The inputs pertaining to these constraints are adopted from the requirements and nominal values given in the literature.⁶

Input: Figure 3.1 shows the default inputs that were used for the constraint analysis. The user can use the layout for other set of inputs too.

Output: Figure 3.2 shows the plot of all the seven constraints. It can be seen that the most critical constraints that drive the design are (a) the 1200 *ft* maximum speed requirement at sea-level and (b) the landing in a 5000 *ft* runway past a 50 *ft* obstacle. This yields the feasible design space as the ones that are between these two constraints. A simple perturbation of load factor as 3 gives the constraint plot shown in Figure 3.3. Similar perturbations can be carried out for detailed analysis but such a scope is not explored in this document.

3.3 Weight Estimation

The takeoff gross weight W_{TO} can be estimated using

$$W_{TO} = W_C + W_P + W_E + W_F \quad (3.1)$$

where W_C is the crew weight, W_P is the payload weight, W_E is the empty weight and W_F is the fuel weight.

Payload and Crew Weights: The design is done to carry a crew member who weighs 210 *lbs* and a payload of 432 *lbs*. Though this is an expendable payload as per the requirement which is dropped-off at some point in the mission, it is assumed that in the event of aborting the mission, the airplane has to carry the payload back to the base, and thus it is treated as a non-expendable payload. User input panels that facilitate the inputs of these weights is shown in Figure 3.4.

The interface consists of several input panels and a graph:

- Landing:** Runway Height [ft] (0), STD Temp Diff [F] (31), Landing Distance [ft] (5000), Obstacle Height [ft] (50), C_L_max (1.4).
- Takeoff:** Runway Height [ft] (0), STD Temp Diff [F] (31), Takeoff Distance [ft] (4400), Obstacle Height [ft] (50), C_L_max (1.0).
- Rate of Climb:** Velocity [kts] (458), Height [ft] (35400), STD Temp Diff [F] (31), Rate of Climb [dh/dt] (90). Power Setting: ☒ Maximum, ☐ Military.
- Cruise Climb:** Velocity [kts] (458), Initial Height [ft] (35400), Final Height [ft] (38700), Range [nm] (550).
- Maximum Speed:** Velocity [ft/s] (1200), Height [ft] (0), STD Temp Diff [F] (31). Power Setting: ☒ Maximum, ☐ Military.
- Service Ceiling:** Velocity [kts] (536), Height [ft] (47550). Power Setting: ☒ Maximum, ☐ Military.
- Turn:** Velocity [kts] (536), Height [ft] (47550), Load Factor (2).
- Graph:** Thrust Loading $\frac{T_{SL}}{W_{TO}}$ vs Wing Loading. The y-axis ranges from 0 to 2.0, and the x-axis ranges from 0 to 40.

Figure 3.1: Figure showing the inputs for constraint analysis.

Empty Weight Estimation: It is rather difficult to estimate the empty and fuel weight compared to the other counterparts. The empty weight is found using empirical correlations of historical data. In the toolkit both, Mattingly⁶ (Eq. 3.52) and Roskam¹² text based models are implemented and the user has the flexibility to choose between the two. The user only needs to input the regression constants A and B in the **weight analysis layout**, under *empty weight panel*. The panel uses the following default values: $A = 0.5091$ and $B = 0.9505$, which pertains to the current design under study and is adopted from Roskam¹² (Eq. 2.16). The input panel is shown in Figure 3.5:

Fuel Weight Estimation: Fuel consumed throughout the mission is modeled by breaking down the mission into various segments as shown in Table 2. The fuel consumed during each segment is modeled based on the values provided in Raymer.¹⁰ For the cruise segments alone, the fuel burn ordinary differential equation is integrated using the values and procedure given in Section (3.4.1) of Mattingly.⁶ The the purpose of reusability for similar missions, important inputs have been externalized in the panel, as shown in Figure 3.6. The default values are the ones that are pertaining to the current mission and are assembled from RPF and sources cited above. The user can use the panel for analyzing similar configurations that follow the same mission with different

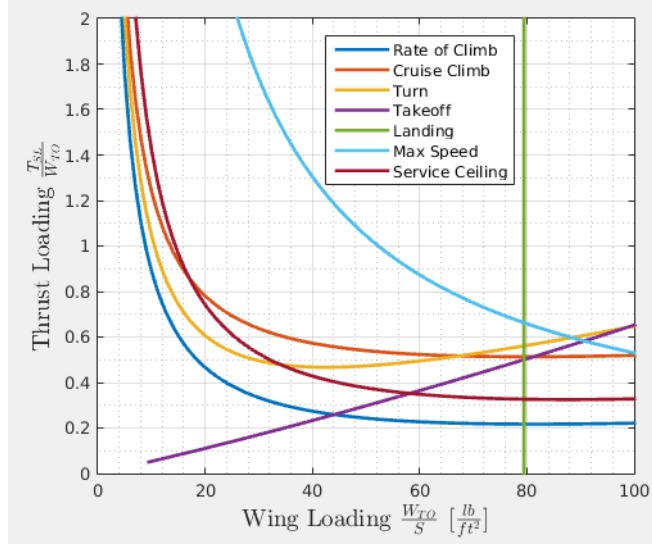


Figure 3.2: Plot showing the constraints for the required design.

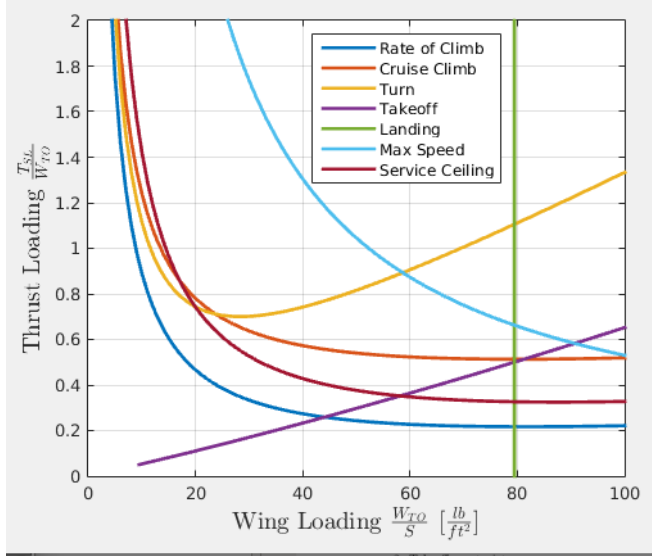


Figure 3.3: Plot showing standard constraints along with load factor $n = 3$.

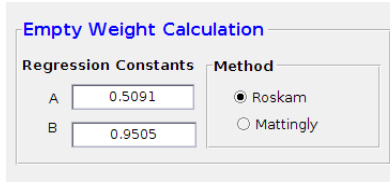
Payload Weight Calculation

Payload Weight [lb]

Crew Weight Calculation

Crew Weight [lb]

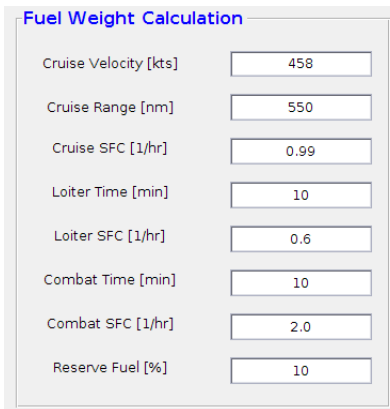
Figure 3.4: Panel designed for inputting the payload and crew weights.



Empty Weight Calculation

Regression Constants		Method
A	<input type="text" value="0.5091"/>	<input checked="" type="radio"/> Roskam
B	<input type="text" value="0.9505"/>	<input type="radio"/> Mattingly

Figure 3.5: Input panel facilitating the selection of different models for empirical estimation of empty weights.



Fuel Weight Calculation

Cruise Velocity [kts]	<input type="text" value="458"/>
Cruise Range [nm]	<input type="text" value="550"/>
Cruise SFC [1/hr]	<input type="text" value="0.99"/>
Loiter Time [min]	<input type="text" value="10"/>
Loiter SFC [1/hr]	<input type="text" value="0.6"/>
Combat Time [min]	<input type="text" value="10"/>
Combat SFC [1/hr]	<input type="text" value="2.0"/>
Reserve Fuel [%]	<input type="text" value="10"/>

Figure 3.6: Input panel for fuel weight calculations.

values.

Weights Breakdown: At the end of the mission analysis segment-by-segment, the toolkit provides the weights breakdown in the form of a pie-chart and table (see Figure 3.7).

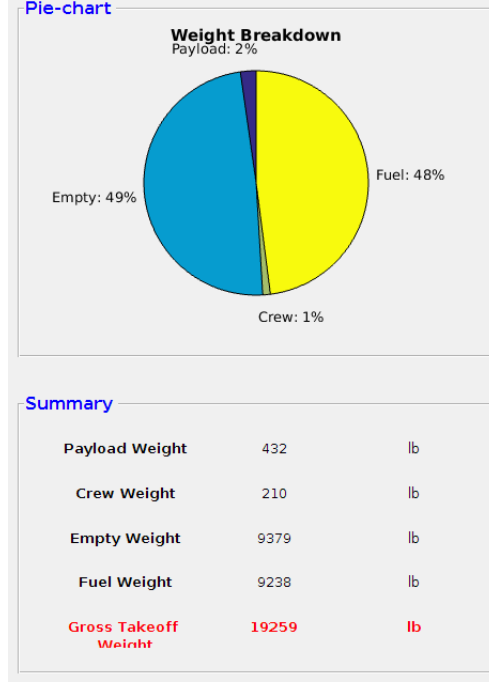


Figure 3.7: A pie-chart showing the weight fractions (top) and the table summarizing the actual weights (bottom).

3.4 Mission Summary

Finally the summary of the mission is obtained by inputting the design point to *Mission Summary* layout. A complete breakdown of important parameters is shown (see Figure 3.8). Also a drag-polar plot is generated by this layout (see Figure 3.9). The reference area is found to be 275 ft^2 .

3.5 Benchmarking the design

Table 4: Validation of the F-86L Sabre design produced by the TASS

Design	Wing Loading [lb/ft^2]	Thrust Loading	Gross Weight [lb]	Planform Area [ft^2]
TASS	70	0.80	19259	275
Actual	68	0.38	19975	290

The comparison of the design obtained using the tool with known configuration of the aircraft follows next. Table 4 presents the performance parameters that are calculated using the tool with that of the existing similar design.^{1,2} For this benchmark F86-Sabre-D, the forerunner of F86-Sabre-L and also the RFP data for the J47-GE-33 engine are used. An overall good agreement can be seen between the values except for the thrust loading, which is due to the maximum-speed constraint shown in the constraint plot. Perturbing this constraint (e.g. altitude of 40000 instead of sea-level, maximum speed of 1000 ft/s instead of 1200 ft/s will provide the user with a design that has a lower thrust loading.

	beta	W _(n-i) /W _n	Fuel Burnt [lb]	Gross Weight [lb]	Wing Loading [lb/ft ²]	Thrust Loading
Idle	1	1	0	19258.9	70	0.8
Takeoff	0.9703	0.9703	274.368	18686.9	67.921	0.824487
Climb	0.955746	0.985	138.57	18406.6	66.9022	0.837043
Cruise Climb	0.806459	0.843801	1442.96	15531.5	56.4521	0.991991
Loiter	0.797548	0.98895	102.076	15359.9	55.8284	1.00307
Climb	0.785585	0.985	138.57	15129.5	54.9909	1.01835
Combat	0.73492	0.935507	595.786	14153.8	51.4444	1.08855
Descend	0.73492	1	0	14153.8	51.4444	1.08855
Cruise	0.598183	0.813943	1718.79	11520.4	41.8728	1.33738
Loiter	0.591574	0.98895	102.076	11393.1	41.4102	1.35233
Descend	0.591574	1	0	11393.1	41.4102	1.35233
Land	0.588616	0.995	46.19	11336.1	41.2031	1.35912

Figure 3.8: Breakdown of mission parameters across different mission segments.

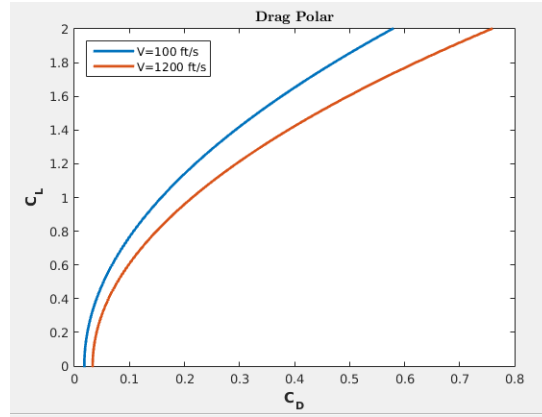


Figure 3.9: Plot of drag polar for two representative velocities at sea-level.

4 Conclusion

This work presented a toolkit that performs sizing and synthesis of the aircraft configurations at the conceptual design level. The toolkit is provided with a graphical user-interface that helps non-expert users to simulate different requirements at the same time. It is validated against a known

configuration of F-86 Sabrejet.

References

- [1] North american f-86 sabre. *http : //www.fighter – planes.com/info/f86sabre.htm*.
- [2] The north american f-86 sabre jet. *http : //www.456fis.org/F – 86sABER.htm*.
- [3] J. P. Fielding. *Introduction to Aircraft Design*. Cambridge University Press, New York, NY, 1st edition, 1999.
- [4] D. Howe. *Aircraft conceptual design synthesis*. Professional Engineering Publishing, London, 1st edition, 2000.
- [5] MATLAB and Statistics Toolbox Release 2015a. *version 8.5.0 (R2015a)*. The MathWorks Inc., Natick, Massachusetts, 2015.
- [6] J. D. Mattingly, W. H. Heiser, and D. T. Pratt. *Aircraft Engine Design*. American Institute of Aeronautics and Astronautics, Reston, VA, 2nd edition, 2002.
- [7] D. Mavris. *Fixed Wing Aircraft Design I*. Lecture Notes, Georgia Institute of Technology, 2015.
- [8] N. E. Antoine and I. M. Kroo. Framework for Aircraft Conceptual Design and Environmental Performance Studies. *AIAA Journal*, 43, No. 10, 2005.
- [9] L. M. Nicolai. *Fundamentals of Aircraft Design*. E. P. Domicone Printing Services, Fairborn, OH, 1st edition, 1975.
- [10] D. P. Raymer. *Aircraft Design: A Conceptual Approach*. American Institute of Aeronautics and Astronautics, Reston, VA, 3rd edition, 1999.
- [11] D. P. Raymer. Modern Use of Spreadsheet Methods for Aircraft Design, Sizing, and Performance Analysis. *AIAA Paper*, 2004-0534, 2004.
- [12] J. Roskam. *Airplane Design: Part I, Preliminary Sizing of Airplanes*. Roskam Aviation and Engineering Corporation, Ottawa, TX, 1985.
- [13] S. Sartorius. STDATMO: Standard atmosphere function. MATLAB Central, 2010.
- [14] 1976 U.S. standard atmosphere. *United States Committee on Extension to the Standard Atmosphere*. U.S. Government Printing Office, Washington, D.C., 1976.

A Flexibility of the Tool

A.1 Versatility of the Tool

1. The Graphical User Interface (GUI) enables easy inputting of mission parameters to perform the analyses

2. The user can input any “physically sound” set of values as inputs to the three layouts that are the core-part of the TASS: (a) constraint analysis (b) mission analysis (c) mission summary
3. The plots and tables are co-located with the inputs to help study the effect of different parameter perturbations with ease
4. Clear/Reset push-buttons are provided in the tool that helps the user to start-off again with default values
5. TASS employs interpolations and extrapolations whenever it encounters data that are rather difficult to supply or unavailable:
 - it models the drag polar plots presented in Mattingly⁶ Section (2.3.1)
 - standard atmosphere model function¹³ used in the code that eliminated the need for treating them as constants at different stages in the mission

A.2 Challenges and Cons

1. Since it is extremely laborious to implement sanity checks on the user-supplied values, it is recommended that the users proactively consider the physical meaning of the values supplied (e.g. range, rate of climb)
2. The current version of TASS can only be used for designing airplanes that follow the “same mission profile” given in the RFP
3. In the *constraint analysis layout*, provision has been made for picking only the constraints that the user determines to choose for analysis. Currently this facility is not-fully implemented due to time constraints!