# POWER SYSTEM

## Term Project Report



## Optimal Network Reconfiguration for Improved Microgrid Resilience

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## Introduction

With the increasing occurrences of extreme weather events, the challenges of power outages and the need for rapid system restoration have gained significant attention. Strengthening the resilience of power delivery at the distribution level has become a key priority, and network topology reconfiguration has emerged as an effective restoration strategy.

Simulations are carried out on a modified IEEE 33-bus distribution system. The results clearly demonstrate that the strategy enhances the system's ability to maintain reliable service to critical loads, even in the event of three or four simultaneous line outages, thereby ensuring a more resilient and robust power supply.

## **Objective**

The purpose is to develop and validate an optimal reconfiguration strategy for the modified IEEE 33-bus distribution system to enhance power distribution resilience and efficiency. By altering the system topology through strategic switch operations, the study aims to restore power supply during contingencies while maintaining a radial network structure.

Key constraint considered in the reconfiguration process include radial topology enforcement.

## <u>Methodology</u>

This study focuses on the optimal reconfiguration of network topology using the IEEE 33-bus distribution system as the test platform.

The proposed methodology aims to enhance system reliability, minimise total load shedding, and ensure efficient power delivery.

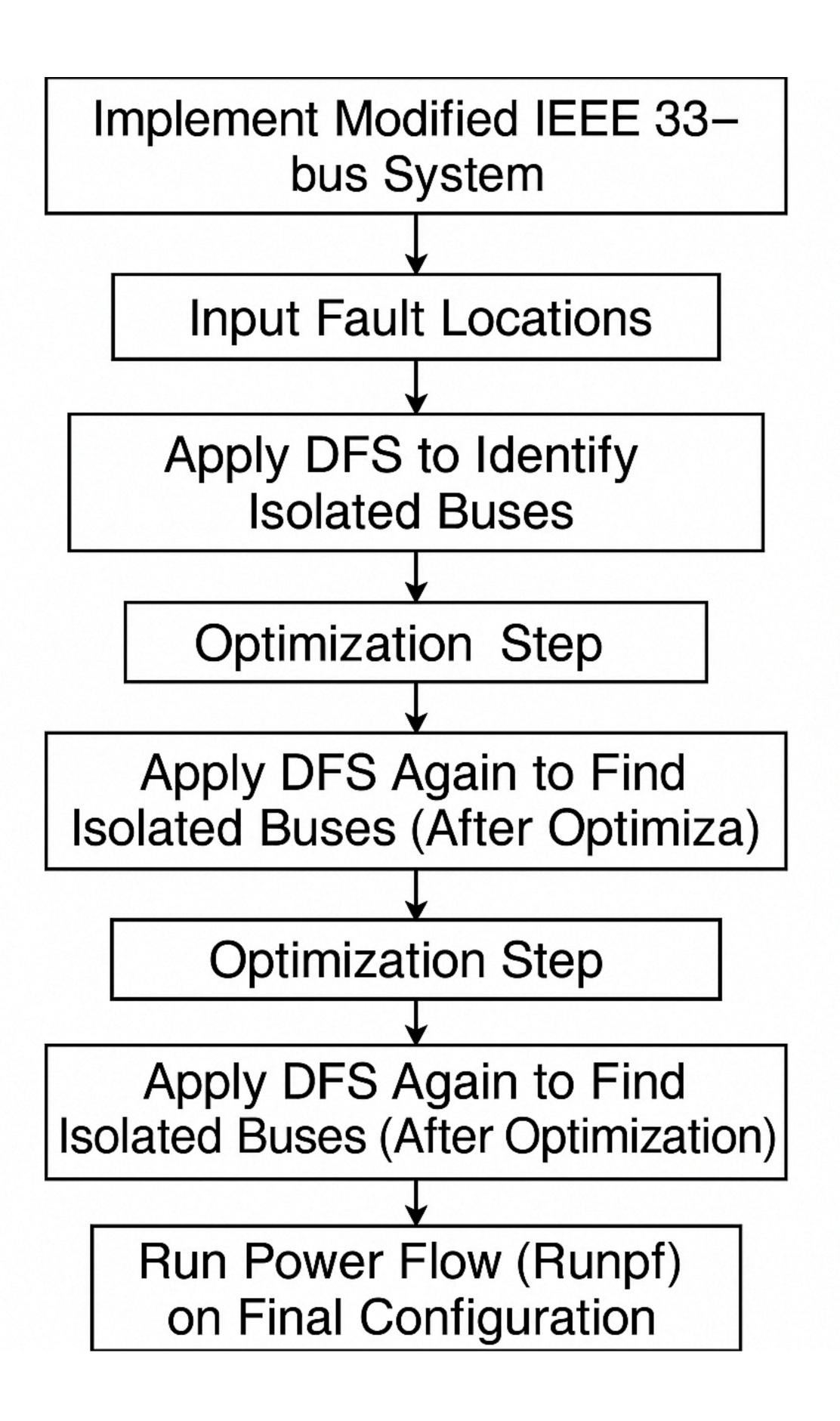
Throughout the reconfiguration process, the radial structure of the distribution network is strictly maintained to preserve operational simplicity and fault isolation capabilities. By strategically altering the network configuration, the approach seeks to reduce system load shedding and increase overall resilience against disturbances.

Used branch and bound technique for optimally switching on/off of tie switches(RCS).

#### **Constraints:**

$$\sum_{ij} z_{ij} = |N| - 1 - |A|, \ \forall ij \in L$$

## Workflow

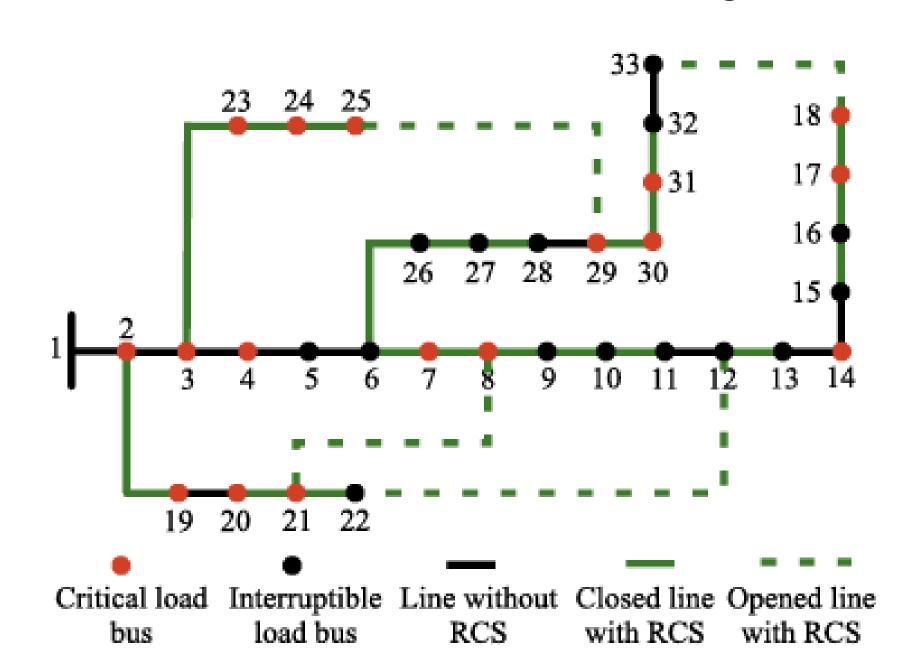


## Pseudo Code

#### Algorithm 1 Reconfiguration of Faults in IEEE-33 Modified Bus System

- 1: Define IEEE 33-bus system with bus, generator, and branch data
- 2: Convert bus loads from kW/kVAR to MW/MVAR
- 3: Convert branch impedances from Ohm to per-unit (p.u.)
- 4: Plot initial system layout with:
- 5: Active branches (black lines)
- 6: Critical buses (red markers)
- 7: Non-critical buses (green markers)
- 8: Ask user for number of faults to simulate, n
- 9: Plot during fault layout
- 10: Using DFS Algorithm calculate isolated buses
- 11: Using isolated buses calculate load\_shed
- 12: **for** i = 1 to n **do**
- 13: Prompt user to enter from\_bus and to\_bus
- 14: Find corresponding branch between from\_bus and to\_bus
- 15: Set branch status to 0 (disconnect branch)
- 16: **end for**
- 17: Replot system layout with updated branch statuses
- 18: Recalculate isolated buses and Update minimum load\_shed
- 19: Running PowerFlow (runpf)

#### The modified IEEE 33-bus distribution system



## Code

```
function mpc = case33bw
%CASE33BW Power flow data for 33 bus distribution system from Baran & Wu
  Please see CASEFORMAT for details on the case file format.
   Data from ...
       M. E. Baran and F. F. Wu, "Network reconfiguration in distribution
       systems for loss reduction and load balancing," in IEEE Transactions
       on Power Delivery, vol. 4, no. 2, pp. 1401-1407, Apr 1989.
       doi: 10.1109/61.25627
    URL: https://doi.org/10.1109/61.25627
%% MATPOWER Case Format : Version 2
mpc.version = '2';
%%----- Power Flow Data -----%%
%% system MVA base
mpc.baseMVA = 10;
%% bus data
   bus i type Pd Qd Gs Bs area Vm Va baseKV zone Vmax
                                                                     Vmin
mpc.bus = [ %% (Pd and Qd are specified in kW & kW here, converted to MW & MW below)
                      0 0 1 1 0 12.66 1 1 1;
       3 0
   1
   2 1 490 0 0 0 1 1 0 12.66 1 1.1 0.9;
     1 495 0 0 0 1 1 0 12.66 1 1.1 0.9;
   4 1 585 0 0 0 1 1 0 12.66 1 1.1 0.9;
   5 1 440 0 0 0 1 1 0 12.66 1 1.1 0.9;
   6 1 460 0
                  0 0 1 1 0 12.66 1 1.1 0.9;
                   0 0 1 1 0 12.66 1 1.1 0.9;
   7 1 395 0
           395
                8
                         0
                             1
                                 1
                                        12.66 1
                                                  1.1 0.9;
   8
       1
                      8
                                    0
   9
       1
           380
                0
                         0
                             1
                                 1
                                        12.66
                                                   1.1 0.9;
                      8
                                    0
                                               1
           380
                                 1
                                        12.66
   10
      1
                0
                      0
                         0
                             1
                                    0
                                               1
                                                   1.1 0.9;
                                 1
   11
      1
                0
                         0
                             1
                                        12.66
                                                   1.1 0.9;
           380
                      8
                                    0
                                               1
                             1
                                 1
   12
      1
           380
                8
                      8
                         0
                                    0
                                        12.66
                                                   1.1 0.9;
                                               1
   13 1
                         Ø
                             1
                                 1
           380
                0
                      0
                                    8
                                        12.66
                                                   1.1 0.9;
                                               1
   14 1
                         0
                             1
                                 1
                                                   1.1 0.9;
           395
                0
                                        12.66
                      0
                                               1
                                    8
                                                   1.1 0.9;
   15
           480
                0
                      0
                             1
                                 1
                                    8
                                        12.66
      1
                         0
                                               1
   16
           480
                         0
                             1
                                 1
                                        12.66
                8
                      0
                                    0
                                                  1.1 0.9;
      1
                                               1
   17 1
           495
                0
                         0
                             1
                                 1
                                    0
                                        12.66
                                                   1.1 0.9;
                      0
                                               1
                                        12.66
                         0
                                 1
                                                   1.1 0.9;
   18 1
           495
                      0
                             1
                8
                                    0
                                               1
      1
                         0
                             1
                                 1
                                                  1.1 0.9;
   19
           495
                0
                      0
                                        12.66 1
                                    0
           495
                                 1
   20
      1
                0
                      0
                         0
                             1
                                        12.66
                                                   1.1 0.9;
                                    0
                                               1
           442.5 0
                                 1
   21
      1
                      0
                         0
                             1
                                    0
                                        12.66
                                                   1.1 0.9;
                                               1
                             1
                                 1
   22
      1
           560
                0
                      0
                         0
                                    0
                                        12.66
                                                   1.1 0.9;
                                               1
          490
   23
                         0
                             1
                                 1
                                        12.66
                                                   1.1 0.9;
      1
                0
                      0
                                    0
                                               1
      1
           885
                         0
                             1
                                 1
   24
                8
                      0
                                    8
                                        12.66
                                                   1.1 0.9;
                                               1
          742.5 0
                         Ø
                             1
                                 1
                                                   1.1 0.9;
   25
      1
                      0
                                        12.66
                                    0
                                               1
   26
           1760
                         0
                             1
                                 1
                                        12.66
                                                   1.1 0.9;
               8
                      0
                                    8
      1
                                               1
   27
           420
                0
                      8
                         0
                             1
                                 1
                                    0
                                        12.66
                                                   1.1 0.9;
      1
                                               1
   28
      1
           460
                0
                      8
                         0
                             1
                                 1
                                        12.66
                                                   1.1 0.9;
                                    0
                                               1
           442.5 0
   29 1
                      0
                         0
                             1
                                 1
                                        12.66
                                                   1.1 0.9;
                                               1
                                    8
                             1
                                 1
   30
      1
           585
                0
                      0
                         0
                                        12.66
                                                   1.1 0.9;
                                    0
                                               1
   31
           595
                         0
                             1
                                 1
      1
                0
                                        12.66
                                                   1.1 0.9;
                      8
                                               1
                                    0
   32
      1
           580
                      8
                         0
                             1
                                 1
                                    8
                                        12.66
                                                   1.1 0.9;
                                               1
   33 1
                      0
                         0
                             1
                                 1
           590
                                    0
                                        12.66
                                                   1.1 0.9;
                                               1
];
```

### **Generator Data**

	genei		r da																		
%	bus	Pg	Qg	Qmax		Qmin	Vg	mBas	se	sta	tus	Pma:	X	Pmi	n	Pc1	Pc2	Qc1ı	nin	Qc1max	Q
mpc	.gen	= [																			
	1	0	0		-10			10	0	0	0	0	0	0	0	0	0	0	0	0;	
	2	0	0		-10			0.4		0	0	0	0	0	0	0	0	0	0	0;	
	3	0	0		-10			0.4		0	0	0	0	0	0	0	0	0	0	0;	
	4	0	0		-10			0.5		0	0	0	0	0	0	0	0	0	0	0;	
	5	0	0		-10			0.4		0	0	0	0	0	0	0	0	0	0	0;	
	6	0	0		-10			0.3		0	0	0	0	0	0	0	0	0	0	0;	
	7	0	0	10	-10	1 100	1	0.3	0	0	0	0	0	0	0	0	0	0	0	0;	
	8	0	0	10	-10	1 100	1	0.2	0	0	0	0	0	0	0	0	0	0	0	0;	
	9	0	0	10	-10	1 100	1	0.2	0	0	0	0	0	0	0	0	0	0	0	0;	
	10	0	0	10	-10	1 100	1	0.2	0	0	0	0	0	0	0	0	0	0	0	0;	
	11	0	0	10	-10	1 100	1	0.2	0	0	0	0	0	0	0	0	0	0	0	0;	
	12	0	0	10	-10	1 100	1	0.3	0	0	0	0	0	0	0	0	0	0	0	0;	
	13	0	0	10	-10	1 100	1	0.3	0	0	0	0	0	0	0	0	0	0	0	0;	
	14	0	0	10	-10	1 100	1	0.3	0	0	0	0	0	0	0	0	0	0	0	0;	
	15	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	16	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	17	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	18	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	19	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	20	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	21	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	22	0	0	10	-10	1 100	1	0.5	0	0	0	0	0	0	0	0	0	0	0	0;	
	23	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	24	0	0	10	-10	1 100	1	0.7	0	0	0	0	0	0	0	0	0	0	0	0;	
	25	0	0	10	-10	1 100	1	0.7	0	0	0	0	0	0	0	0	0	0	0	0;	
	26	0	0	10	-10	1 100	1	1.7	0	0	0	0	0	0	0	0	0	0	0	0;	
	27	0	0		-10		1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	28	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	29	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	30	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	31	0	0	10	-10	1 100	1	0.4		0	0	0	0	0	0	0	0	0	0	0;	
	32	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	33	0	0	10	-10	1 100	1	0.4	0	0	0	0	0	0	0	0	0	0	0	0;	
	];																				

#### **Branch Data**

```
branch data
    fbus
                                                    rateC
                                                             ratio
            tbus
                              b
                                  rateA
                                           rateB
                                                                     angle
                                                                              status
                                                                                       angmin
                          X
                                                                                                angmax
mpc.branch = [ %% (r and x specified in ohms here, converted to p.u. below)
                     0.0470 0
        2
             0.0922
                                       0
                                           0
                                                        1
                                                             -360
                                                                      360;
                                                0
    1
                                   0
                                                    0
             0.4930
                     0.2511
                                                             -360
    2
                                  0
                                       0
                                           0
                                               0
                                                    0
                                                        1
                                                                      360;
    3
             0.3660
                     0.1864
                                       0
                                           0
                                               0
                                                    0
                                                             -360
                                                                      360;
                                                        1
        4
    4
             0.3811
                     0.1941
                                                    0
        5
                                       0
                                               0
                                                             -360
                                                                      360;
                                                        1
    5
             0.8190
                     0.7070
                                           0
        6
                                                0
                                                    0
                                                             -360
                                                                     360;
                                  0
                                       0
                                                        1
    6
             0.1872
                     0.6188
                                       0
                                           0
                                                0
                                                    0
                                                             -360
                                                                      360;
                                                        1
        7
                                   0
             0.7114
                     0.2351
                                                    0
                                                             -360
    7
                                       0
                                               0
                                                                      360;
                                                        1
        8
    8
             1.0300
                     0.7400
                                           0
                                       0
                                                0
                                                    0
                                                        1
                                                             -360
                                                                     360;
                     0.7400
    9
             1.0440
                                           0
                                                0
                                                    0
                                                             -360
                                                                      360;
        10
                                       0
                                                        1
    10
        11
            0.1966
                     0.0650
                                           0
                                                             -360
                                                                     360;
                                               0
                                                    0
                                                        1
                                  0
                                       0
    11
        12
            0.3744
                                           0
                                                    0
                                                             -360
                     0.1238
                                       0
                                                0
                                                                     360;
    12
        13
             1.4680
                     1.1550
                                       0
                                           0
                                                0
                                                    0
                                                             -360
                                                                      360;
                                                        1
                                   0
            0.5416
                     0.7129
                                                             -360
    13
        14
                                       0
                                           0
                                                0
                                                    0
                                                                      360;
                                   0
                                                        1
    14
            0.5910
                     0.5260
                                           0
                                                    0
                                                             -360
        15
                                       0
                                                0
                                                                      360;
                                                        1
            0.7463
                     0.5450
                                                0
                                                    0
    15
        16
                                       0
                                                        1
                                                             -360
                                                                      360;
                                                                     360;
    16
             1.2890
                     1.7210
                                           0
                                                0
                                                    0
                                                             -360
        17
                                       0
                                                        1
                                   0
    17
        18
            0.7320
                     0.5740
                                       0
                                           0
                                                0
                                                    0
                                                             -360
                                                                      360;
                                  0
                                                        1
             0.1640
                     0.1565
    2
                                       0
                                           0
                                                0
                                                    0
                                                             -360
                                                                      360;
        19
    19
        20
             1.5042
                     1.3554
                                           0
                                                0
                                                    0
                                                        1
                                                             -360
                                                                     360;
                                       0
    20
        21
            0.4095
                     0.4784
                                           0
                                                    0
                                       0
                                                0
                                                             -360
                                                                      360;
                                                        1
            0.7089
                     0.9373
    21
        22
                                               0
                                                    0
                                                             -360
                                                                      360;
                                           0
                                       0
                                                        1
    3
        23
            0.4512
                     0.3083
                                       0
                                                0
                                                    0
                                                             -360
                                           0
                                                        1
                                                                      360;
    23
        24
            0.8980
                     0.7091
                                       0
                                                             -360
                                                                      360;
                                   0
                                           0
                                                0
                                                    0
                                                        1
        25 0.8960 0.7011 0
    24
                                  0
                                           0
                                               0
                                                    0
                                                             -360
                                                                      360;
            0.2030 0.1034 0
        26
                                           0
                                                             -360
                                                                      360;
                                       0
                                                    0
                                                    0
    26
        27
            0.2842
                     0.1447
                                       0
                                           0
                                               0
                                                             -360
                                                                      360;
                                                        1
             1.0590
                     0.9337
                                                             -360
    27
        28
                                       0
                                               0
                                                    0
                                                                     360;
                                                        1
            0.8042
                     0.7006
                                           0
                                                    0
                                                             -360
    28
        29
                                       0
                                               0
                                                                     360;
                                                        1
    29
            0.5075
                     0.2585
                                                    0
                                                                      360;
        30
                                               0
                                                             -360
                                                        1
    30
        31
            0.9744
                     0.9630
                                       0
                                           0
                                               0
                                                    0
                                                             -360
                                                                     360;
                     0.3619
            0.3105
    31
        32
                                       0
                                           0
                                               0
                                                    0
                                                             -360
                                                                      360;
                                                        1
            0.3410
                     0.5302
                                                    0
    32
                                       0
                                               0
                                                             -360
                                                                      360;
        33
                                                                     360;
                                           0
                                                    0
    21
        8
             2.0000
                     2.0000
                                       0
                                               0
                                                        0
                                                             -360
        22
            2.0000
                     2.0000
                                           0
                                                    0
    12
                                       0
                                               0
                                                             -360
                                                                     360;
                                                        0
    18
        33
            0.5000
                     0.5000
                                  0
                                       0
                                           0
                                               0
                                                    0
                                                        0
                                                             -360
                                                                     360;
    25
        29 0.5000
                     0.5000
                                       0
                                                0
                                                    0
                                                             -360
                                                                      360;
                                           0
];
```

```
has_critical = [2 3 4 7 8 14 17 18 19 20 21 23 24 25 29 30 31]; has_noncritical = [1 5 6 9 10 11 12 13 15 16 22 26 27 28 32 33];
```

#### Code for bus plot

grid on;

```
%% plot for 33 bus system(before fault)
% Coordinates to match visual layout (can be adjusted as needed)
   % x and y should be the same length as number of buses (33)
   % These are illustrative - you can refine based on your image
   xy - [...
       0 0;
               % Bus 1
       1 0;
              % Bus 2
       2 0;
             % Bus 3
       3 0;
             % Bus 4
             % Bus 5
       4 0;
       5 0;
             % Bus 6
             % Bus 7
       6 0;
             % Bus 8
       7 0;
       8 0;
             % Bus 9
       9 0;
             % Bus 10
       10 0; % Bus 11
             % Bus 12
       11 0;
       12 0;
             % Bus 13
       13 0; % Bus 14
       14 0;
             % Bus 15
       15 0;
             % Bus 16
       16 0;
             % Bus 17
       17 0; % Bus 18
       1 1;
              % Bus 19
             % Bus 20
       2 1;
       3 1;
             % Bus 21
       4 1;
             % Bus 22
       2 -1; % Bus 23
       3 -1; % Bus 24
       4 -1; % Bus 25
       5 -1; % Bus 26
       6 -1; % Bus 27
       7 -1;
             % Bus 28
       8 -1; % Bus 29
       9 -1; % Bus 30
       10 -1; % Bus 31
       11 -1; % Bus 32
       12 -1; % Bus 33
   1;
   % Get branch data
   branch - mpc.branch;
   figure; hold on;
   axis equal;
   title('IEEE 33-Bus System Layout (Only Active Branches)');
   xlabel('X');
   ylabel('Y');
    % Plot all active branches
   for i = 1:size(branch, 1)
       if branch(i, 11) -- 1 % Only plot if status -- 1
           from - branch(i, 1);
           to = branch(i, 2);
           x = [xy(from, 1), xy(to, 1)];
           y = [xy(from, 2), xy(to, 2)];
           plot(x, y, 'b-', 'LineWidth', 2);
       end
    end.
   % Plot buses
   scatter(xy(has_critical, 1), xy(has_critical, 2), 100, 'r', 'filled');
   scatter(xy(has_noncritical, 1), xy(has_noncritical, 2), 100, 'k', 'filled'); % N
   text(xy(:, 1)+0.1, xy(:, 2)+0.1, string(1:size(xy, 1)));
```

#### **Giving Fault**

```
%% giving fault to bus system
% Identify the line to disconnect (e.g., between buses 8 and 9)
i= input('enter the no. of faults: ');
fault = zeros(i,2);

while i>0
  target_fbus = input('enter the from bus: ');
  target_tbus = input('enter the to bus: ');
  fault(i,1) = target_fbus;
  fault(i,2) = target_tbus;
% Find the branch index
  branch_index = find(mpc.branch(:, 1) == target_fbus & mpc.branch(:, 2) == target_tbus);

% Disconnect the line by setting status to 0
  mpc.branch(branch_index, 11) = 0; % Column 11 is BR_STATUS
  i=i-1;
end
```

#### Load shedding calculation

#### Code for finding island buses and total load shed

```
%% applying DFS for finding island buses
visited = zeros(1, 33);
visited(1) = 1; % Start DFS from bus 1
 adj = cell(1, 33);
    for i = 1:size(mpc.branch, 1)
        if mpc.branch(i, 11) == 1
            from = mpc.branch(i, 1);
            to = mpc.branch(i, 2);
            adj{from} = [adj{from}, to];
            adj{to} = [adj{to}, from]; % Assuming undirected connectivity
        end
    end
stack = [1];
    while ~isempty(stack)
        current = stack(end);
        stack(end) = [];
        for neighbor = adj{current}
            if ~visited(neighbor)
                visited(neighbor) = 1;
                stack(end + 1) = neighbor; % push to stack
            end
        end
    end
    total_loadshed = 0;
    % Check unvisited buses (2 to 33)
    for bus = 2:33
        if visited(bus) == 0
            fprintf('Bus %d is isolated.\n', bus);
            total_loadshed = total_loadshed + load_shed(bus);
        end
    end
    display(total_loadshed);
    total_loadshedmin= total_loadshed;
     branch_c= mpc.branch;
```

#### Code for reconfiguration

```
%% Reconfiguration part
for q10=1:2
     if isempty(find(fault(:,1) == 2 & fault(:,2) == 19)) == 0
            if(q10 == 1)
                continue;
            end
        else
    if (q10 == 1)
        mpc.branch(18,11)=1;
    elseif (q10 == 2)
        mpc.branch(18,11)=0;
    end
     end
for q11=1:2
     if isempty(find(fault(:,1) == 20 & fault(:,2) == 21)) == 0
            if(q11 == 1)
                continue;
            end
        else
    if (q11 == 1)
        mpc.branch(20,11)=1;
    elseif (q11 == 2)
        mpc.branch(20,11)=0;
    end
for q12=1:2
     if isempty(find(fault(:,1) == 21 & fault(:,2) == 22)) == 0
            if(q12 == 1)
                continue;
            end
        else
    if (q12 == 1)
        mpc.branch(21,11)=1;
    elseif (q12 ==2)
        mpc.branch(21,11)=0;
    end
     end
for q13=1:2
    if isempty(find(fault(:,1) == 3 & fault(:,2) == 23)) == 0
            if(q13 == 1)
                continue;
            end
        else
    if (q13 == 1)
        mpc.branch(22,11)=1;
    elseif (q13 ==2)
        mpc.branch(22,11)=0;
    end
    end
```

```
for q14=1:2
     if isempty(find(fault(:,1) == 23 & fault(:,2) == 24)) == 0
            if(q14 == 1)
                continue;
            end
        else
    if (q14 == 1)
        mpc.branch(23,11)=1;
    elseif (q14 == 2)
        mpc.branch(23,11)=0;
    end
     end
for q15=1:2
     if isempty(find(fault(:,1) == 24 & fault(:,2) == 25)) == 0
            if(q15 == 1)
                continue;
            end
        else
    if (q15 == 1)
        mpc.branch(24,11)=1;
    elseif (q15 == 2)
        mpc.branch(24,11)=0;
    end
     end
for q16=1:2
    if isempty(find(fault(:,1) == 6 & fault(:,2) == 26)) == 0
            if(q16 == 1)
                continue;
            end
        else
    if (q16 == 1)
        mpc.branch(25,11)=1;
    elseif (q16 ==2)
        mpc.branch(25,11)=0;
    end
     end
for q17=1:2
    if isempty(find(fault(:,1) == 26 & fault(:,2) == 27)) == 0
            if(q17 == 1)
                continue;
            end
        else
    if (q17 == 1)
        mpc.branch(26,11)=1;
    elseif (q17 ==2)
        mpc.branch(26,11)=0;
    end
    end
```

```
for q18=1:2
     if isempty(find(fault(:,1) == 27 & fault(:,2) == 28)) == 0
            if(q18 == 1)
                continue;
            end
        else
    if (q18 == 1)
        mpc.branch(27,11)=1;
    elseif (q18 ==2)
        mpc.branch(27,11)=0;
    end
     end
for q19=1:2
     if isempty(find(fault(:,1) == 29 & fault(:,2) == 30)) == 0
            if(q19 == 1)
                continue;
            end
        else
    if (q19 == 1)
        mpc.branch(29,11)=1;
    elseif (q19 == 2)
        mpc.branch(29,11)=0;
    end
     end
for q20=1:2
    if isempty(find(fault(:,1) == 30 & fault(:,2) == 31)) == 0
            if(q20 == 1)
                continue;
            end
        else
    if (q20 == 1)
        mpc.branch(30,11)=1;
    elseif (q20 ==2)
        mpc.branch(30,11)=0;
    end
     end
for q21=1:2
    if isempty(find(fault(:,1) == 31 & fault(:,2) == 32)) == 0
            if(q21 == 1)
                continue;
            end
        else
    if (q21 == 1)
        mpc.branch(31,11)=1;
    elseif (q21 == 2)
        mpc.branch(31,11)=0;
    end
    end
```

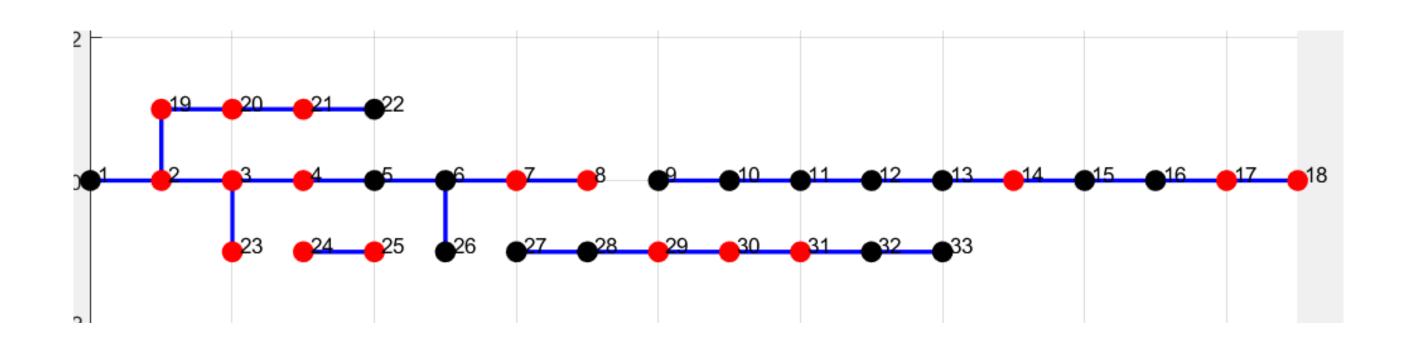
```
for q22=1:2
     if isempty(find(fault(:,1) == 21 & fault(:,2) == 8)) == 0
            if(q22 == 1)
                continue;
            end
        else
    if (q22 == 1)
        mpc.branch(33,11)=1;
    elseif (q22 == 2)
        mpc.branch(33,11)=0;
    end
     end
for q23=1:2
     if isempty(find(fault(:,1) == 12 & fault(:,2) == 22)) == 0
            if(q23 == 1)
                continue;
            end
        else
    if (q23 == 1)
        mpc.branch(34,11)=1;
    elseif (q23 ==2)
        mpc.branch(34,11)=0;
    end
     end
for q24=1:2
    if isempty(find(fault(:,1) == 18 & fault(:,2) == 33)) == 0
           if(q24 == 1)
                continue;
            end
        else
    if (q24 == 1)
        mpc.branch(35,11)=1;
    elseif (q24 ==2)
        mpc.branch(35,11)=0;
    end
    end
for q25=1:2
     if isempty(find(fault(:,1) == 25 & fault(:,2) == 29)) == 0
            if(q25 == 1)
                continue;
            end
        else
    if (q25 == 1)
        mpc.branch(36,11)=1;
    elseif (q25 == 2)
        mpc.branch(36,11)=0;
    end
     end
```

#### Checking radial topology and load shed in the iteration

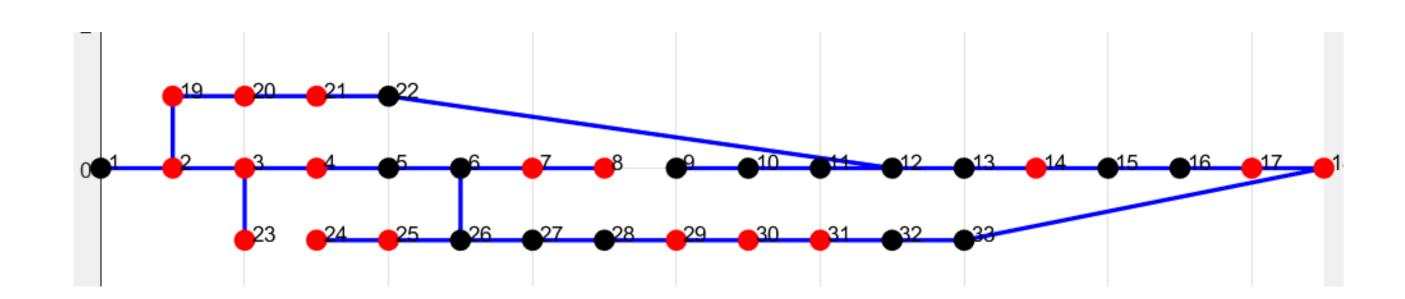
```
num buses = size(mpc.bus, 1);
    island_buses= length(isolated);
    count = 0;
    for k=1:size(mpc.branch,1)
       if isempty(find(isolated == mpc.branch(k,1)))
           if isempty(find(isolated == mpc.branch(k,2)))
           count = count + mpc.branch(k,11);
           end
        end
    end
    % If all buses are visited and there is no loop, it's radial
    if (num_buses - island_buses - 1 == count)
    total_loadshed = 0;
if isempty(isolated) == 0
    for y= 1: length(isolated)
        total loadshed = total loadshed + load shed(isolated(y));
end
if (total_loadshed < total_loadshedmin)</pre>
    total_loadshedmin = total_loadshed;
    branch_c= mpc.branch;
end
    else
        continue;
    end
```

### **Simulation Results:**

#### 3 line outages in line 8-9, line 23-24, line 26-27



#### Optimally reconfigured network topology



#### Load shedding before and after optimization

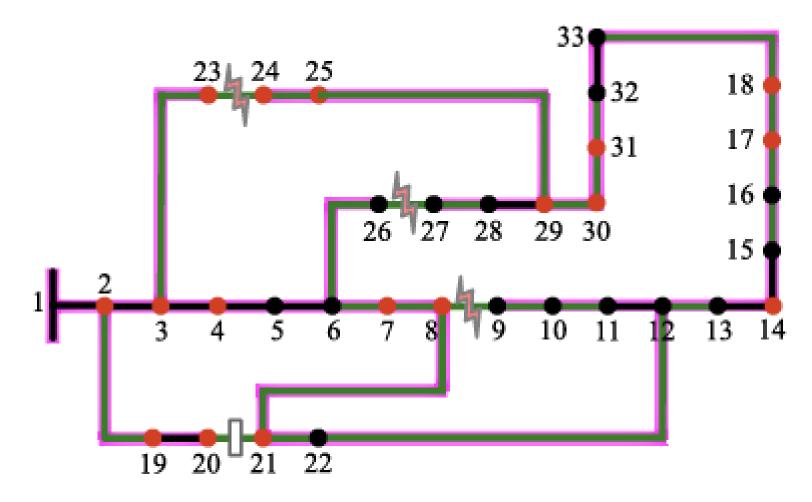
```
total_loadshed =

2.2450

total_loadshedmin =

0
```

### Results from paper

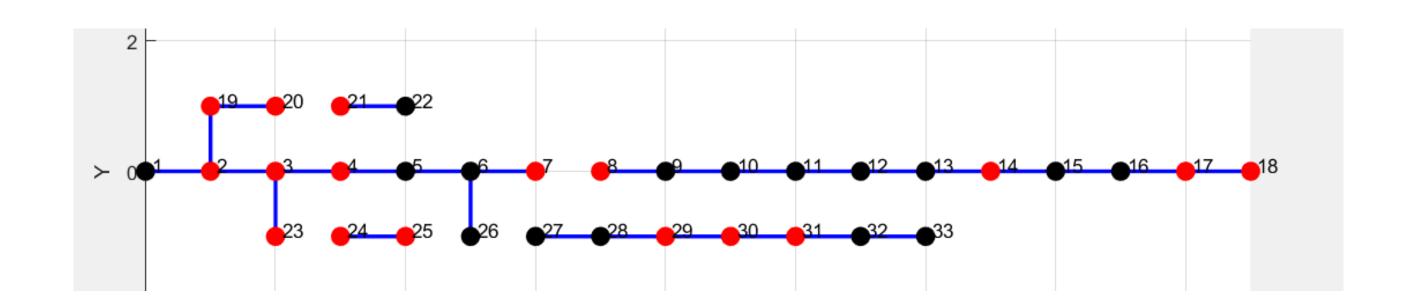


(a) Optimized topology with 3 line outages.

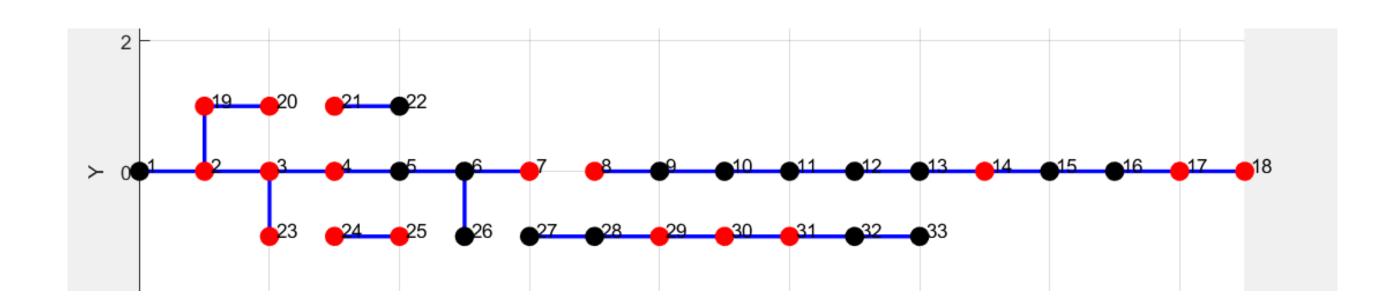
#### Branch data

branch_c =											
1.0000	2.0000	0.0058	0.0029	0	0	0	0	0	0	1.0000 -360.0000	360.0000
2.0000	3.0000	0.0308	0.0157	0	0	0	0	0	0	1.0000 -360.0000	360.0000
3.0000	4.0000	0.0228	0.0116	0	0	0	0	0	0	1.0000 -360.0000	360.0000
4.0000	5.0000	0.0238	0.0121	0	0	0	0	0	0	1.0000 -360.0000	360.0000
5.0000	6.0000	0.0511	0.0441	0	0	0	0	0	0	1.0000 -360.0000	360.0000
6.0000	7.0000	0.0117	0.0386	0	0	0	0	0	0	1.0000 -360.0000	360.0000
7.0000	8.0000	0.0444	0.0147	0	0	0	0	0	0	1.0000 -360.0000	360.0000
8.0000	9.0000	0.0643	0.0462	0	0	0	0	0	0	0 -360.0000	360.0000
9.0000	10.0000	0.0651	0.0462	0	0	0	0	0	0	1.0000 -360.0000	360.0000
10.0000	11.0000	0.0123	0.0041	0	0	0	0	0	0	1.0000 -360.0000	360.0000
11.0000	12.0000	0.0234	0.0077	0	0	0	0	0	0	1.0000 -360.0000	360.0000
12.0000	13.0000	0.0916	0.0721	0	0	0	0	0	0	1.0000 -360.0000	360.0000
13.0000	14.0000	0.0338	0.0445	0	0	0	0	0	0	1.0000 -360.0000	360.0000
14.0000	15.0000	0.0369	0.0328	0	0	0	0	0	0	1.0000 -360.0000	360.0000
15.0000	16.0000	0.0466	0.0340	0	0	0	0	0	0	1.0000 -360.0000	360.0000
16.0000	17.0000	0.0804	0.1074	0	0	0	0	0	0	1.0000 -360.0000	360.0000
17.0000	18.0000	0.0457	0.0358	0	0	0	0	0	0	1.0000 -360.0000	360.0000
2.0000	19.0000	0.0102	0.0098	0	0	0	0	0	0	1.0000 -360.0000	360.0000
19.0000	20.0000	0.0939	0.0846	0	0	0	0	0	0	1.0000 -360.0000	360.0000
20.0000	21.0000	0.0255	0.0298	0	0	0	0	0	0	1.0000 -360.0000	360.0000
21.0000	22.0000	0.0442	0.0585	0	0	0	0	0	0	1.0000 -360.0000	360.0000
3.0000	23.0000	0.0282	0.0192	0	0	0	0	0	0	1.0000 -360.0000	360.0000
23.0000	24.0000	0.0560	0.0442	0	0	0	0	0	0	0 -360.0000	360.0000
24.0000	25.0000	0.0559	0.0437	0	0	0	0	0	0	1.0000 -360.0000	360.0000
6.0000	26.0000	0.0127	0.0065	0	0	0	0	0	0	1.0000 -360.0000	360.0000
26.0000	27.0000	0.0177	0.0090	0	0	0	0	0	0	0 -360.0000	360.0000
27.0000	28.0000	0.0661	0.0583	0	0	0	0	0	0	1.0000 -360.0000	360.0000
28.0000	29.0000	0.0502	0.0437	0	0	0	0	0	0	1.0000 -360.0000	360.0000
29.0000	30.0000	0.0317	0.0161	0	0	0	0	0	0	1.0000 -360.0000	360.0000
30.0000	31.0000	0.0608	0.0601	0	0	0	0	0	0	1.0000 -360.0000	360.0000
31.0000	32.0000	0.0194	0.0226	0	0	0	0	0	0	1.0000 -360.0000	360.0000
32.0000	33.0000	0.0213	0.0331	0	0	0	0	0	0	1.0000 -360.0000	360.0000
21.0000	8.0000	0.1248	0.1248	0	0	0	0	0	0	0 -360.0000	360.0000
12.0000	22.0000	0.1248	0.1248	0	0	0	0	0	0	1.0000 -360.0000	360.0000
18.0000	33.0000	0.0312	0.0312	0	0	0	0	0	0	1.0000 -360.0000	360.0000
25.0000	29.0000	0.0312	0.0312	0	0	0	0	0	0	1.0000 -360.0000	360.0000

#### 4 line outages in line 7-8, line 20-21, line 23-24, line 26-27



#### Optimally reconfigured network topology



#### Load shedding before and after optimization

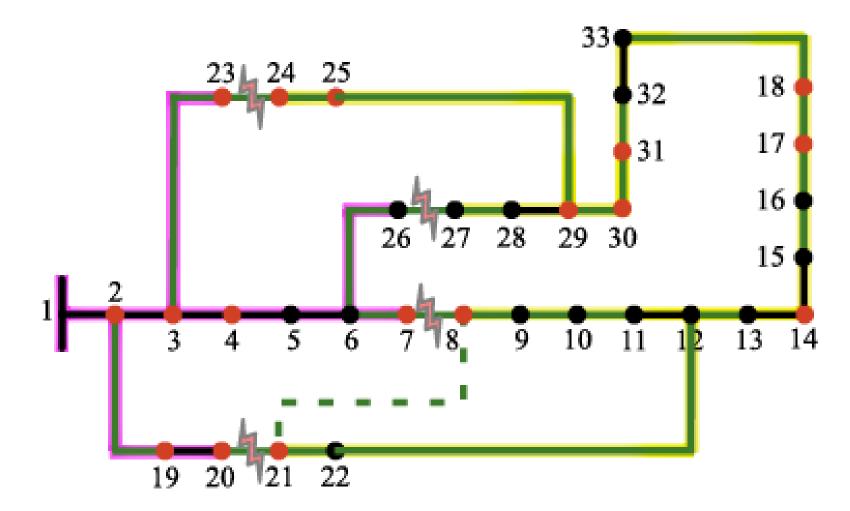
total\_loadshed =

2.5425

total\_loadshedmin =

2.5425

### Results from paper



(b) Optimized topology with 4 line outages.

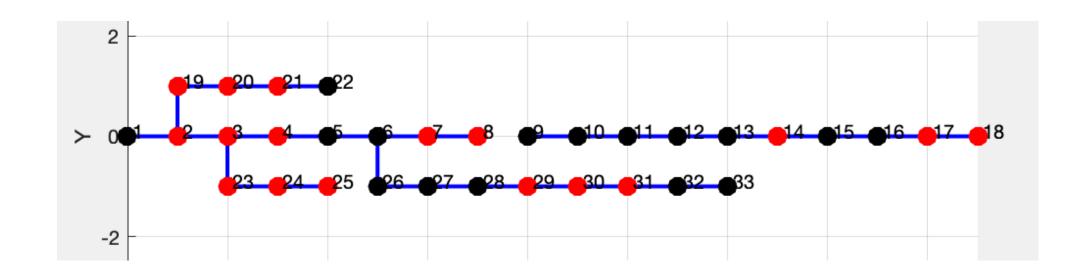
### Branch data

branch_c =											
1.0000	2.0000	0.0058	0.0029	0	0	0	0	0	0	1.0000 -360.0000	360.0000
2.0000	3.0000	0.0308	0.0157	0	0	0	0	0	0	1.0000 -360.0000	360.0000
3.0000	4.0000	0.0228	0.0116	0	0	0	0	0	0	1.0000 -360.0000	360.0000
4.0000	5.0000	0.0238	0.0121	0	0	0	0	0	0	1.0000 -360.0000	360.0000
5.0000	6.0000	0.0511	0.0441	0	0	0	0	0	0	1.0000 -360.0000	360.0000
6.0000	7.0000	0.0117	0.0386	0	0	0	0	0	0	1.0000 -360.0000	360.0000
7.0000	8.0000	0.0444	0.0147	0	0	0	0	0	0	0 -360.0000	360.0000
8.0000	9.0000	0.0643	0.0462	0	0	0	0	0	0	1.0000 -360.0000	360.0000
9.0000	10.0000	0.0651	0.0462	0	0	0	0	0	0	1.0000 -360.0000	360.0000
10.0000	11.0000	0.0123	0.0041	0	0	0	0	0	0	1.0000 -360.0000	360.0000
11.0000	12.0000	0.0234	0.0077	0	0	0	0	0	0	1.0000 -360.0000	360.0000
12.0000	13.0000	0.0916	0.0721	0	0	0	0	0	0	1.0000 -360.0000	360.0000
13.0000	14.0000	0.0338	0.0445	0	0	0	0	0	0	1.0000 -360.0000	360.0000
14.0000	15.0000	0.0369	0.0328	0	0	0	0	0	0	1.0000 -360.0000	360.0000
15.0000	16.0000	0.0466	0.0340	0	0	0	0	0	0	1.0000 -360.0000	360.0000
16.0000	17.0000	0.0804	0.1074	0	0	0	0	0	0	1.0000 -360.0000	360.0000
17.0000	18.0000	0.0457	0.0358	0	0	0	0	0	0	1.0000 -360.0000	360.0000
2.0000	19.0000	0.0102	0.0098	0	0	0	0	0	0	1.0000 -360.0000	360.0000
19.0000	20.0000	0.0939	0.0846	0	0	0	0	0	0	1.0000 -360.0000	360.0000
20.0000	21.0000	0.0255	0.0298	0	0	0	0	0	0	0 -360.0000	360.0000
21.0000	22.0000	0.0442	0.0585	0	0	0	0	0	0	1.0000 -360.0000	360.0000
3.0000	23.0000	0.0282	0.0192	0	0	0	0	0	0	1.0000 -360.0000	360.0000
23.0000	24.0000	0.0560	0.0442	0	0	0	0	0	0	0 -360.0000	360.0000
24.0000	25.0000	0.0559	0.0437	0	0	0	0	0	0	1.0000 -360.0000	360.0000
6.0000	26.0000	0.0127	0.0065	0	0	0	0	0	0	1.0000 -360.0000	360.0000
26.0000	27.0000	0.0177	0.0090	0	0	0	0	0	0	0 -360.0000	360.0000
27.0000	28.0000	0.0661	0.0583	0	0	0	0	0	0	1.0000 -360.0000	360.0000
28.0000	29.0000	0.0502	0.0437	0	0	0	0	0	0	1.0000 -360.0000	360.0000
29.0000	30.0000	0.0317	0.0161	0	0	0	0	0	0	1.0000 -360.0000	360.0000
30.0000	31.0000	0.0608	0.0601	0	0	0	0	0	0	1.0000 -360.0000	360.0000
31.0000	32.0000	0.0194	0.0226	0	0	0	0	0	0	1.0000 -360.0000	360.0000
32.0000	33.0000	0.0213	0.0331	0	0	0	0	0	0	1.0000 -360.0000	360.0000
21.0000	8.0000	0.1248	0.1248	0	0	0	0	0	0	0 -360.0000	360.0000
12.0000	22.0000	0.1248	0.1248	0	0	0	0	0	0	0 -360.0000	360.0000
18.0000	33.0000	0.0312	0.0312	0	0	0	0	0	0	0 -360.0000	360.0000
25.0000	29.0000	0.0312	0.0312	0	0	0	0	0	0	0 -360.0000	360.0000

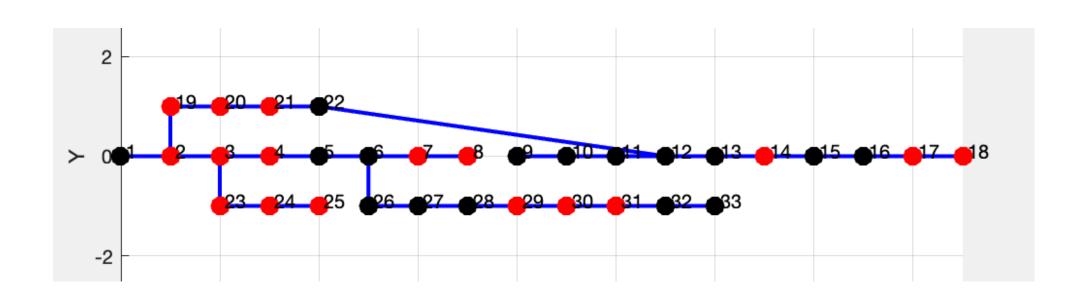
## Single Fault

### line: 8-9

#### **During Fault**



#### After Fault



MATPOWER Version 8.0, 17-May-2024
Power Flow -- AC-polar-power formulation

Newton's method converged in 3 iterations.
PF successful

Converged in 0.26 seconds

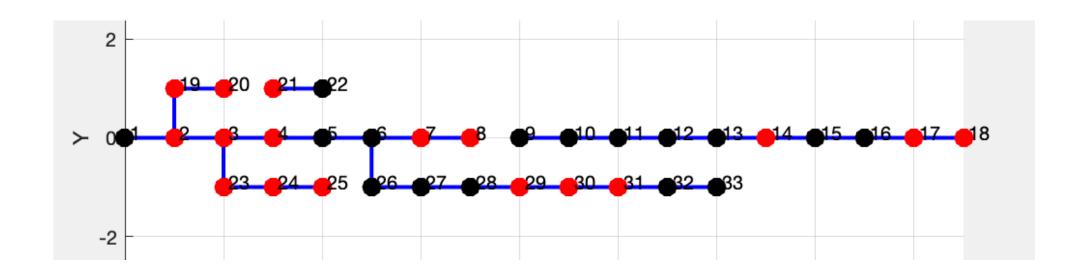
total\_loadshedmin =

How many?		How much?	P (MW)	Q (MVAr)
Buses	33	Total Gen Capacity	10.0	-10.0 to 10.0
Generators	1	On-line Capacity	10.0	-10.0 to 10.0
Committed Gens	1	Generation (actual)	3.9	2.4
Loads	32	Load	3.7	2.3
Fixed	32	Fixed	3.7	2.3
Dispatchable	0	Dispatchable	-0.0 of $-0.0$	-0.0
Shunts	0	Shunt (inj)	-0.0	0.0
Branches	37	Losses $(I^2 * Z)$	0.15	0.11
Transformers	0	Branch Charging (inj)	_	0.0
Inter-ties	0	Total Inter-tie Flow	0.0	0.0
Areas	1			

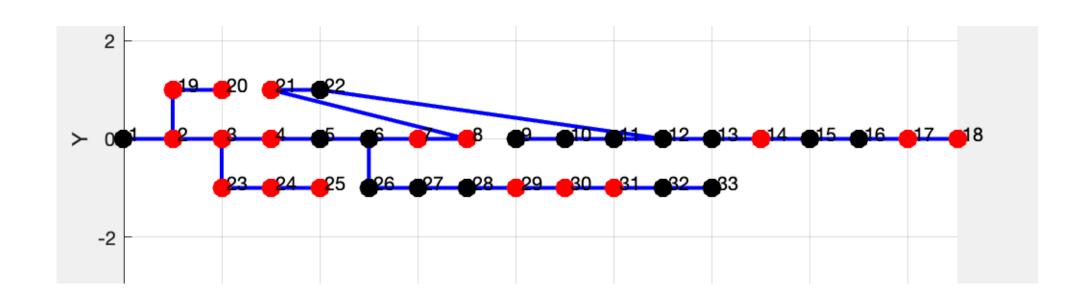
### **Double Fault**

<u>line: 8-9, 20-21</u>

#### **During Fault**



#### **After Fault**



```
MATPOWER Version 8.0, 17-May-2024

Power Flow -- AC-polar-power formulation

Newton's method converged in 4 iterations.

PF successful

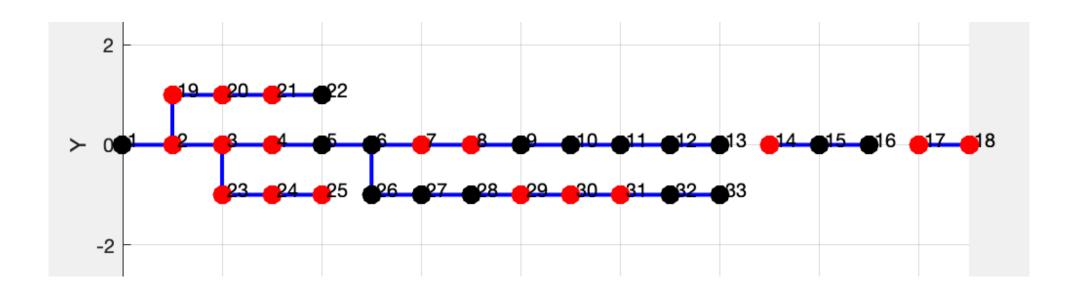
Converged in 0.33 seconds
```

| System Summary

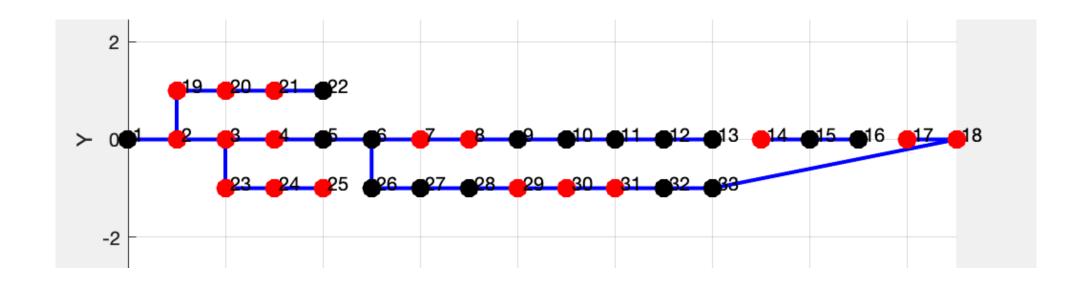
How many?		How much?	P (MW)	Q (MVAr)
Buses	33	Total Gen Capacity	10.0	-10.0 to 10.0
Generators	1	On-line Capacity	10.0	-10.0 to 10.0
Committed Gens	1	Generation (actual)	4.0	2.5
Loads	32	Load	3.7	2.3
Fixed	32	Fixed	3.7	2.3
Dispatchable	0	Dispatchable	-0.0 of $-0.0$	-0.0
Shunts	0	Shunt (inj)	-0.0	0.0
Branches	37	Losses $(I^2 * Z)$	0.24	0.17
Transformers	0	Branch Charging (inj)	_	0.0
Inter-ties	0	Total Inter-tie Flow	0.0	0.0
Areas	1			

### line: 13-14, 16-17

#### **During Fault**



#### **After Fault**



```
Newton's method did not converge in 10 iterations. PF failed >>>> Did NOT converge (0.36 seconds) <>>>
```

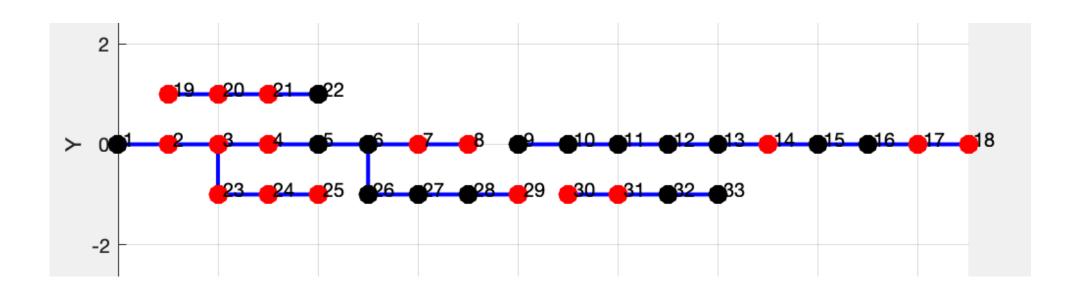
```
total_loadshed =
    0.3900

total_loadshedmin =
    0.2400
```

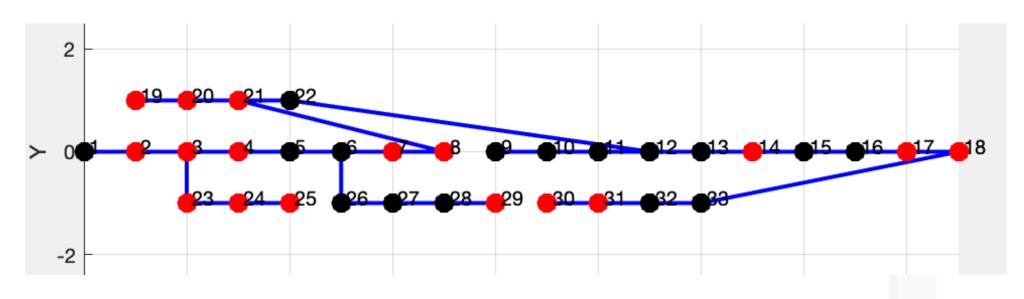
### **Triple Fault**

### <u>line: 2-19, 8-9, 29-30</u>

#### **During Fault**



#### After Fault



MATPOWER Version 8.0, 17-May-2024 Power Flow -- AC-polar-power formulation

Newton's method converged in 5 iterations. PF successful

Converged in 0.30 seconds

total\_loadshed =
 1.6550

total\_loadshedmin =

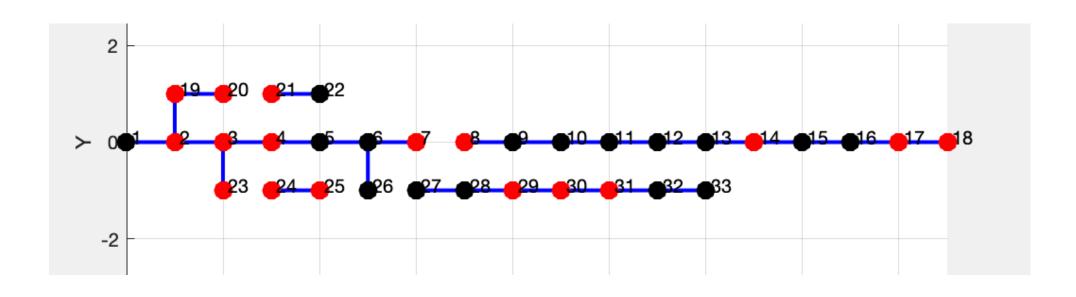
===========	mary ======		========	=======================================
How many?		How much?	P (MW)	Q (MVAr)
Buses	33	Total Gen Capacity	10.0	-10.0 to 10.0
Generators	1	On-line Capacity	10.0	-10.0 to 10.0
Committed Gens	1	Generation (actual)	4.3	2.8

Buses	33	Total Gen Capacity	10.0	-10.0 to 10.0
Generators	1	On-line Capacity	10.0	-10.0 to 10.0
Committed Gens	1	Generation (actual)	4.3	2.8
Loads	32	Load	3.7	2.3
Fixed	32	Fixed	3.7	2.3
Dispatchable	0	Dispatchable	-0.0 of $-0.0$	-0.0
Shunts	0	Shunt (inj)	-0.0	0.0
Branches	37	Losses $(I^2 * Z)$	0.62	0.54
Transformers	0	Branch Charging (inj)	_	0.0
Inter-ties	0	Total Inter-tie Flow	0.0	0.0
Areas	1			

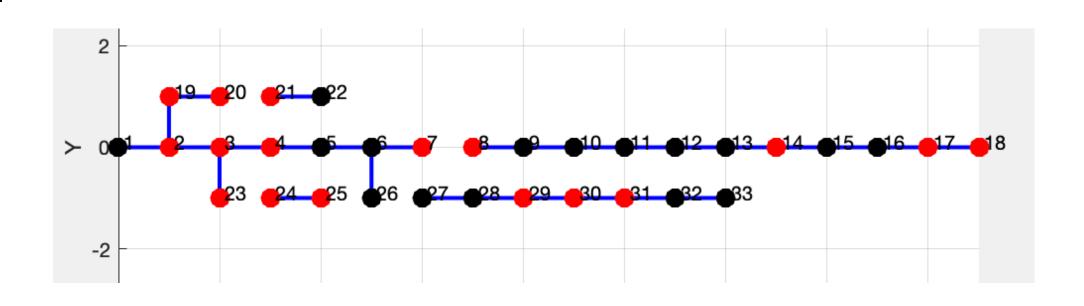
### Four line Fault

### line: 7-8, 20-21, 23-24, 26-27

#### **During Fault**



#### **After Fault**



Newton's method did not converge in 10 iterations. PF failed

>>>> Did NOT converge (0.74 seconds) <<<<<

total\_loadshed =
 2.7550

total\_loadshedmin =
 2.7550

## Discussion

- In the case of the modified IEEE 33-bus system with three line outages, the network was successfully reconfigured to minimize load shedding to zero while maintaining a radial topology.
- In the case of four line outages, as observed from the referenced research paper, the system cannot be fully reconfigured because it would form two separate subsystems. Therefore, the load shedding remains the same even after attempted reconfiguration.
- During testing, it was observed that the modified IEEE 33bus system showed errors while running the power flow analysis (Runpf) in MATLAB.
- This is likely due to insufficient or missing data in the research paper about the modified system, which forced us to make certain assumptions during its creation. These assumptions could have caused errors during the power flow analysis.
- To verify the correctness of our reconfiguration strategy, we tested it on the original IEEE 33-bus system, where we were able to successfully perform reconfiguration and power flow analysis without any errors.

## Conclusion

We have successfully completed the reconfiguration of the modified IEEE 33-bus system. This reconfiguration can be used to minimize load shedding as much as possible for any number of faults. We have used DFS (Depth-First Search) to identify isolated buses in the system and developed our own reconfiguration algorithm in this project. Additionally, we have minimized the time complexity, allowing the algorithm to produce results within seconds. Through this project, we had the opportunity to apply our theoretical knowledge to solve practical problems.

## <u>Modification</u>

referenced primarily addressed The paper reconfiguration of the modified IEEE 33-bus system but did not incorporate any optimization techniques. To address this gap, we developed our own optimization approach for network reconfiguration using a brute-force method, based on the analysis of tie switches. This constituted the first major improvement over the original study. Furthermore, in their initial modified IEEE 33-bus system, the power flow analysis was not functioning as described. Consequently, we applied our optimization method to the standard IEEE 33-bus system, performed the reconfiguration accordingly, and successfully obtained the desired results.

## References

[1] Y. Chen et al., "Optimal Network Reconfiguration and Scheduling With Hardware-in-the-Loop Validation for Improved Microgrid Resilience," in IEEE Access, vol. 13, pp. 8042-8059, 2025, doi: 10.1109/ACCESS.2025.3527329.