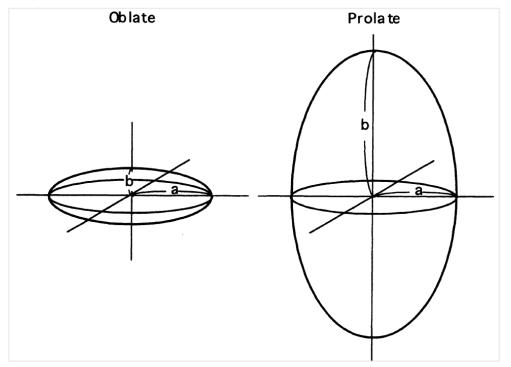
## Spheroid Model: DLS Code Refactoring Notes

A group of randomly oriented, symmetric particles



• Optical characteristics:  $\omega_0$ ,  $\tau_{ext}$  (or  $C_{ext}$ )

$$F(\theta) = \begin{bmatrix} F_{11} & F_{12} & 0 & 0 \\ F_{12} & F_{22} & 0 & 0 \\ 0 & 0 & F_{33} & F_{34} \\ 0 & 0 & -F_{34} & F_{44} \end{bmatrix}, \quad f(\theta) = \frac{F(\theta)}{F_{11}(\theta)}$$

• Aspect ratio

$$\varepsilon = b/a$$

• Size (radius) *r* 

$$V_{Spheroid} = V_{Sphere} = \frac{4}{3} \pi r^3$$

• Size parameter

$$x = 2\pi r/\lambda$$

Kernel (LUT)

$$K_{ii}(\theta, r, n-ik, \varepsilon)$$

• Fixed kernel  $k_{ij}(\theta, r, n-ik) = \int_{\Delta \epsilon} K_{ij}(\theta, r, n-ik, \epsilon) D(\epsilon) d\epsilon \approx \mathbf{K}_{ij} \cdot \mathbf{D} \Delta \epsilon$ 

Log-spline or log-linear interpolation

$$f(x) \rightarrow \log(f(x)) \rightarrow \{i\} \rightarrow \log(f(y)) \rightarrow f(y) = \exp(...)$$

## What is DLS Code?

JOURNAL OF GEOPHYSICAL RESEARCH, VOL. 111, D11208, doi:10.1029/2005JD006619, 2006

## Application of spheroid models to account for aerosol particle nonsphericity in remote sensing of desert dust

Oleg Dubovik, <sup>1,2</sup> Alexander Sinyuk, <sup>1,3</sup> Tatyana Lapyonok, <sup>1,3</sup> Brent N. Holben, <sup>1</sup> Michael Mishchenko, <sup>4</sup> Ping Yang, <sup>5</sup> Tom F. Eck, <sup>1,6</sup> Hester Volten, <sup>7</sup> Olga Muñoz, <sup>8</sup> Ben Veihelmann,<sup>9</sup> Wim J. van der Zande,<sup>10</sup> Jean-Francois Leon,<sup>11</sup> Michael Sorokin,<sup>1,3</sup> and Ilva Slutsker<sup>1,3</sup>

See Sec.2 for theory & numerical details

$$1.33 \le n \le 1.6$$
,

← some absorption remains  $0.0005 \le k \le 0.5$ ,



$$0.3 \le \varepsilon \le 3.0,\tag{23}$$

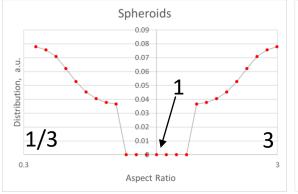
 $0.012 \le x (= 2\pi r/\lambda) \le 625$ ,  $\leftarrow$  wide range – different methods

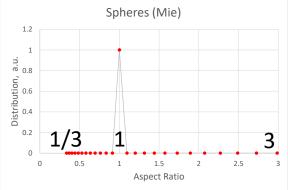


 $\Delta 1^{\circ}$  – resolution for  $K_{ii'}(\Theta, \lambda, n, k, \varepsilon_p, r_k)$ .  $\leftarrow BIG \ Kernels, 5Gb \ in \ ASCII$ 

$$\lambda_{FIX} = 0.340 \, (\mu m)$$
  $\delta_{DLS} \sim 1 - 3\% \, (typical)$ 

Using BIG kernels K(...) and some aspect ratio,  $\varepsilon$ , distribution (note: Mie = spheres) ...

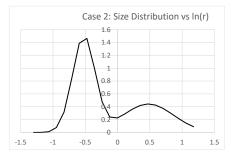




... one generalates fixed kernels k(...) (takes time – save as ASCII LUTs). For MAIAC, we did once in 2012.



Using the fixed kernels k(...), user's wavelength, refractive index, and particle size distribution ( $r_{user}$ ) ...



... one generalates generates optical characteristics for MAIAC RT LUTs (on the fly)

## One Slide Documentation: In → Out



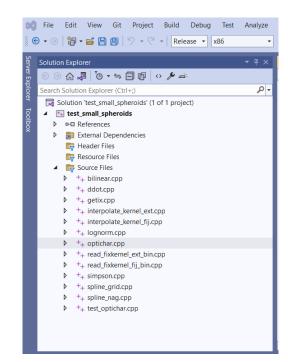
```
#include "const param spheroids.h" // grids (e.g., size grid), constants (e.g., sizes of arrays, pi=3.14...), file names/paths
                  main():
                                                   // Runs Cases 1 & 2; in test optichar.cpp; for the rest: subroutine name = file name
In:
                      +-optichar()
                                                   // for given input returns aerosol extinction, single scattering albedo, and normalized phase matrix
                                    +-getix() // for given x0 and X[] returns indices i1 & i2, so that X[i1] < x0 < X[i2]
         q_{Mie}
                                    +-interpolate_kernel_ext()
                                                                    +-read_fixkernel_ext_bin() // reads extinction and absorption fixed kernels
                                                                    +-bilinear()
                                                                                                            // performs bilinear interpolation (over refractive index)
                                    +-interpolate_kernel_fij()
                                                                    +-read fixkernel fij bin() // reads fixed kernels for phase matrix elements, fij
                                                                    +-bilinear()
                                                 F(\theta) = \begin{bmatrix} F_{11} & f_{12} & 0 & 0 \\ f_{12} & f_{22} & 0 & 0 \\ f_{13} & f_{22} & 0 & 0 \\ 0 & 0 & f_{33} & f_{34} \\ 0 & 0 & -f_{34} & f_{44} \end{bmatrix}, f_{ij} = \frac{F_{ij}}{F_{11}}
F(\theta) = \begin{bmatrix} F_{11} & f_{12} & 0 & 0 \\ f_{12} & f_{22} & 0 & 0 \\ 0 & 0 & f_{33} & f_{34} \\ 0 & 0 & -f_{34} & f_{44} \end{bmatrix}, f_{ij} = \frac{F_{ij}}{F_{11}}
                                   +-lognorm() // calculates lognormal distribution D_V(x = \frac{r}{\lambda}) = \frac{C_V}{\sqrt{2\pi} \sigma} \exp\left(-\frac{\ln(x/x_m)}{2\sigma^2}\right)
                                    +-ddot()
x_0 = \frac{1}{2} \int_0^{\pi} f_{11}(\theta) \sin(\theta) d\theta \approx 1 \quad +-\text{spline\_grid}()
                                                                                     // optional: interpolates from one grid into another using NAG cubic spline
                                                    +-e02baf() & e02bbf() // optional: NAG cubic spline subroutines
                                                                                                                                                                         \frac{\int (D_{VF}(x) + D_{VC}(x)) d \ln(x)}{C + C} \approx 1
x_1 = \frac{1}{2} \int_{0}^{\pi} f_{11}(\theta) \sin(\theta) \cos(\theta) d\theta + \text{simpson}()
                                                                                  // optional: numerical integration using Simpson's rule
```

## See readme.txt for instructions & tests

```
/home/skorkin/spheroids/build - aeronet - Editor - WinSCP
🖫 🖫 🗷 👫 🗙 🔞 🤼 C 📠 🖏 📾 Encoding • □ Color • 🕸 🕝
g++ -Wall -W -c -O3 src/bilinear.cpp
g++ -Wall -W -c -O3 src/ddot.cpp
g++ -Wall -W -c -O3 src/getix.cpp
g++ -Wall -W -c -O3 src/interpolate kernel ext.cpp
g++ -Wall -W -c -O3 src/interpolate kernel fij.cpp
g++ -Wall -W -c -O3 src/lognorm.cpp
g++ -Wall -W -c -O3 src/optichar.cpp
g++ -Wall -W -c -O3 src/read fixkernel fij bin.cpp
g++ -Wall -W -c -O3 src/read fixkernel ext bin.cpp
g++ -Wall -W -c -O3 src/simpson.cpp
g++ -Wall -W -c -O3 src/spline grid.cpp
g++ -Wall -W -c -O3 src/spline_nag.cpp
g++ -Wall -W -O3 src/test optichar.cpp \
bilinear.o \
ddot.o \
getix.o \
interpolate kernel ext.o \
interpolate kernel fij.o \
lognorm.o \
optichar.o \
read fixkernel fij bin.o \
read fixkernel ext bin.o \
simpson.o \
spline grid.o \
spline_nag.o \
-o run
```

rm \*.o

```
/home/skorkin/spheroids/readme.txt - aeronet - Editor - WinSCP
□ □ □ Color · ◎ 2
1. check path to kernels in const param spheroids.h (line 17)
   default is rootdir[path len max] = "./kernels fix bin/"
2. make sure 'build' is executable
   if not run chmod +x build
3. execute 'build' to build (ignore warnings)
4. execute 'run' to run
5. you should get this:
[skorkin@gs618-aerol1 spheroids]$ time ./run
Case 1 inp: wavel = 0.600
            mie frag = 0.700 refre = 1.60 refim = 0.00
            cvf = 0.50 \text{ rad}f = 0.30 \text{ sgm}f = 0.40
            cvc = 1.00 \text{ radc} = 3.00 \text{ sgmc} = 0.90
Case 1 out:
 0.0
         1.016008e+02
                         9.997294e-01
                                         9.997294e-01
                                                          9.994589e-01
                                                                          -0.000000e+00
                                                                                           0.000000e+00
 1.0
         6.220902e+01
                         9.995592e-01
                                         9.995460e-01
                                                          9.991066e-01
                                                                         -1.154759e-04
                                                                                          -2.714780e-03
 2.0
         3.925060e+01
                         9.993048e-01
                                         9.992119e-01
                                                          9.985243e-01
                                                                         -2.712795e-04
                                                                                          -6.797968e-03
 3.0
         2.796145e+01
                         9.990311e-01
                                         9.987746e-01
                                                          9.978275e-01
                                                                         -3.672112e-04
                                                                                          -1.061744e-02
 4.0
         2.172044e+01
                         9.987637e-01
                                         9.982716e-01
                                                          9.970805e-01
                                                                         -3.888452e-04
                                                                                          -1.376277e-02
 5.0
         1.793710e+01
                         9.985168e-01
                                         9.977399e-01
                                                          9.963354e-01
                                                                         -3.531180e-04
                                                                                          -1.621641e-02
  6.0
         1.546706e+01
                         9.982951e-01
                                         9.972065e-01
                                                          9.956238e-01
                                                                         -2.868358e-04
                                                                                          -1.815239e-02
 7.0
         1.374882e+01
                         9.980966e-01
                                         9.966855e-01
                                                          9.949587e-01
                                                                         -2.135548e-04
                                                                                          -1.978601e-02
 8.0
         1.248442e+01
                         9.979169e-01
                                         9.961805e-01
                                                          9.943392e-01
                                                                         -1.504886e-04
                                                                                          -2.130423e-02
 9.0
         1.150547e+01
                         9.977509e-01
                                         9.956875e-01
                                                          9.937566e-01
                                                                         -1.080306e-04
                                                                                          -2.284536e-02
         1.071260e+01
                         9.975948e-01
                                         9.951991e-01
                                                          9.931986e-01
                                                                         -9.368139e-05
                                                                                          -2.449713e-02
10.0
11.0
         1.004511e+01
                         9.974453e-01
                                         9.947061e-01
                                                          9.926523e-01
                                                                         -1.149890e-04
                                                                                          -2.631430e-02
12.0
         9.464612e+00
                         9.972992e-01
                                         9.941965e-01
                                                          9.921028e-01
                                                                         -1.739252e-04
                                                                                          -2.832544e-02
13.0
         8.937836e+00
                         9.971424e-01
                                         9.935101e-01
                                                          9.913892e-01
                                                                         -2.834205e-04
                                                                                          -3.061301e-02
14.0
         8.474269e+00
                         9.970065e-01
                                         9.930801e-01
                                                          9.909372e-01
                                                                         -4.035975e-04
                                                                                          -3.293958e-02
15.0
         8.037483e+00
                         9.968554e-01
                                         9.924524e-01
                                                                         -5.706051e-04
                                                                                          -3.552128e-02
                                                          9.902967e-01
                         9.966984e-01
                                         9.917679e-01
                                                                         -7.689842e-04
                                                                                          -3.826014e-02
16.0
         7.628801e+00
                                                          9.896059e-01
                                                                         -9.946065e-04
                                                                                          -4.113392e-02
17.0
         7.243392e+00
                         9.965340e-01
                                         9.910261e-01
                                                          9.888636e-01
                                                                                          -4.412321e-02
18.0
         6.877935e+00
                         9.963609e-01
                                         9.902331e-01
                                                          9.880755e-01
                                                                         -1.241838e-03
19.0
         6.530111e+00
                         9.961782e-01
                                         9.893970e-01
                                                          9.872494e-01
                                                                         -1.506794e-03
                                                                                          -4.720896e-02
20.0
         6.198333e+00
                         9.959850e-01
                                         9.885220e-01
                                                          9.863895e-01
                                                                         -1.790618e-03
                                                                                          -5.037304e-02
21.0
         5.881550e+00
                         9.957804e-01
                                         9.876013e-01
                                                          9.854891e-01
                                                                         -2.097386e-03
                                                                                          -5.360001e-02
22.0
         5.579034e+00
                         9.955645e-01
                                         9.866233e-01
                                                          9.845358e-01
                                                                         -2.431636e-03
                                                                                          -5.687389e-02
23.0
         5.290212e+00
                         9.953367e-01
                                         9.855760e-01
                                                          9.835179e-01
                                                                         -2.796993e-03
                                                                                          -6.017743e-02
24.0
         5.014601e+00
                         9.950956e-01
                                         9.844490e-01
                                                          9.824258e-01
                                                                         -3.195151e-03
                                                                                          -6.349271e-02
25.0
         4.751790e+00
                         9.948406e-01
                                         9.832355e-01
                                                          9.812527e-01
                                                                         -3.626759e-03
                                                                                          -6.680126e-02
26.0
         4.501395e+00
                         9.945704e-01
                                         9.819297e-01
                                                          9.799935e-01
                                                                         -4.093385e-03
                                                                                          -7.008554e-02
27.0
                         9.942846e-01
                                         9.805282e-01
                                                                         -4.596143e-03
                                                                                          -7.333017e-02
         4.263041e+00
                                                          9.786452e-01
28.0
         4.036377e+00
                         9.939820e-01
                                         9.790268e-01
                                                          9.772042e-01
                                                                         -5.136973e-03
                                                                                          -7.652057e-02
                         9.936619e-01
                                                          9.756676e-01
                                                                         -5.716705e-03
29.0
         3.821034e+00
                                         9.774226e-01
                                                                                          -7.964252e-02
                                         9.757128e-01
                                                                         -6.335532e-03
30.0
         3.616643e+00
                         9.933235e-01
                                                          9.740331e-01
                                                                                          -8.268380e-02
31.0
         3.422803e+00
                         9.929662e-01
                                         9.738952e-01
                                                          9.722991e-01
                                                                         -6.994298e-03
                                                                                          -8.563487e-02
         3.239128e+00
32.0
                         9.925893e-01
                                         9.719659e-01
                                                          9.704621e-01
                                                                         -7.693968e-03
                                                                                          -8.848319e-02
```



## Tests -- 2 cases: q\*Mie+(1-q)\*Srd, Cvf + Cvc

Parameter	Notation	Units	Case 1	Case 2	Comments	
Wavelength	λ	μm	0.6	0.4	Red & blue	
Refractive index: real part	n	-	1.6	1.3	n = [1.29 : 1.70]	
Refractive index: imaginary part	k	-	0.001	0.1	k = [0.0005 : 0.5] > 0	
Mean radius, fine fraction	rvf	μm	0.3	0.3	Same in both cases	
Width parameter, fine fraction	σf	?	0.4	0.4	Same in both cases	
Concentration, fine fraction	Cvf	a. u.	0.5	1.5	a.u. – arbitrary units	
Mean radius, coarse fraction	rvc	μm	3.0	3.0	Same in both	
Width parameter, coarse fraction	σς	?	0.9	0.9	Same in both	
Concentration, coarse fraction	Cvc	a. u.	1.0	1.0	a.u. – arbitrary units	
Mie fraction	q	r. u.	0.7	0.3	q = 1 means Mie only	

$$d_V(r) = \frac{C_V}{\sqrt{2\pi} \sigma} \exp\left(-\frac{\ln\left(r/r_m\right)}{2\sigma^2}\right) \rightarrow d_V(\mathbf{x}) = \frac{C_V}{\sqrt{2\pi} \sigma} \exp\left(-\frac{\ln\left(\mathbf{x}/\mathbf{x}_m\right)}{2\sigma^2}\right); \quad C_V = \int_X d_V(\mathbf{x}) d\ln\mathbf{x}$$

## Numerical results (5 digits) & summary of changes

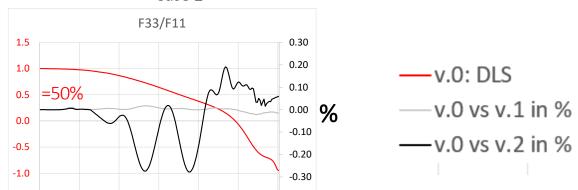
- v.0: DLS original DLS package
- v.1: cpp C version with kernels in \*.bin files, flip sequence of interpolation first over refractive index (bilinear), then r-spline
- v.2: cpp same loglin interpolation for all fij (not reflected in the table); see slide ""
- v.3: cpp lognormal distribution over size parameter (<u>full range as in kernels</u>, no r-spline); no artificial smoothing of f33 & f44 (next slide)

scalef - ?	Parameter	Case 1				Case 2				
		v.0: DLS	v.1: cpp	v.2: cpp	v.3: cpp	v.0: DLS	v.1: cpp	v.2: cpp	v.3: cpp	
$C_{ext}^{Kernels} \times 1000 \left(\frac{\mu m^3}{\mu m^2}?\right) \frac{\lambda_{User}}{\lambda_{Fix}}$	Extinction	5.1080	5.1080	5.1080	5.10 <mark>98</mark>	9.8634	9.8634	9.8634	9.86 <b>43</b>	
	S. S. Albedo	0.98922	0.98922	0.98922	0.989 <mark>13</mark>	0.59104	0.59104	0.59104	0.59100	
$x_0 = -1 f_{11}(\theta) \sin(\theta) d\theta$	x0 = intg{F11}	0.99768	0.997 <mark>20</mark>	0.997 <mark>22</mark>	0.997 <mark>49</mark>	1.00 <mark>01</mark>	0.999 <mark>02</mark>	0.999 <mark>02</mark>	0.999 <mark>65</mark>	
	intg{ F11/x0 }	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	
$C_{Sca}^K F_{ij} \sim K_{ij}$	F11(0)	89.951	89.9 <mark>88</mark>	89.9 <mark>88</mark>	101.60	199.64	199. <mark>86</mark>	199. <mark>86</mark>	<b>220.86</b>	
$F_{ij} \sim \frac{K_{ij}}{C_{Ext}^{K} - C_{Abs}^{K}} \frac{scalef}{scalef}$	F11(90)	0.26762	0.267 <b>71</b>	0.267 <b>71</b>	0.267 <mark>74</mark>	0.067541	0.0675 <mark>97</mark>	0.0675 <mark>97</mark>	0.0675 <b>41</b>	
	F11(180)	0.57250	0.572 <mark>68</mark>	0.572 <mark>68</mark>	0.57 <b>301</b>	0.027849	0.0278 <mark>81</mark>	0.0278 <mark>81</mark>	0.027849	
$x_1 = \frac{1}{2} \int_0^{\pi} f_{11}(\theta) \sin(\theta) \cos(\theta) d\theta$	Aver. S. Cos	0.66682	0.666 <mark>72</mark>	0.666 <mark>72</mark>	0.666 <mark>67</mark>	0.87397	0.873 <mark>87</mark>	0.873 <mark>87</mark>	0.873 <mark>86</mark>	

## Graphical results: smoothing

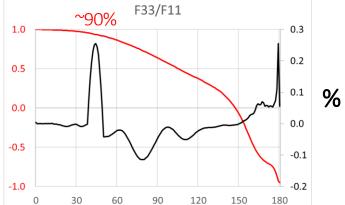
```
Smooth f33 & f44 - as in the DLS code
                                                                                                                               F44 is not used IPOL and many other vRT codes
       // f33:
337
                                                                                                                  isca1 = 48:
338
           isca1 = 38;
                                                        Hard-coded in DLS
                                                                                                                  isca2 = 60;
           isca2 = 50;
339
                                                                                                                  sca1 = sca_fix[isca1];
                                                                                                      349
            sca1 = sca_fix[isca1];
340
                                                                                                                  f1 = log(f44[isca1]);
                                                                                                      350
            f1 = log(f33[isca1]);
341
                                                                                                                  sca2 = sca_fix[isca2];
                                                                                                      351
           sca2 = sca_fix[isca2];
342
                                                                                                                  f2 = log(f44[isca2]);
                                                                                                      352
           f2 = log(f33[isca2]);
343
                                                                                                                  for (isca = isca1; isca < isca2+1; isca++)</pre>
                                                                                                      353
           for (isca = isca1; isca < isca2+1; isca++)</pre>
344
                                                                                                                      f44[isca] = exp( linear(sca_fix[isca], sca1, sca2, f1, f2) );
                                                                                                      354
                f33[isca] = exp( linear(sca_fix[isca], sca1, sca2, f1, f2) );
345
```

## Case 1



-0.40

Smoothed



90

120

150

Not: v.3 vs DLS

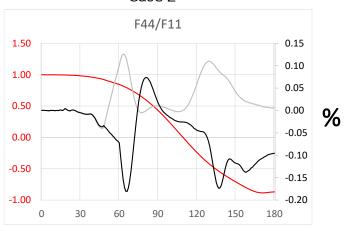
-1.5

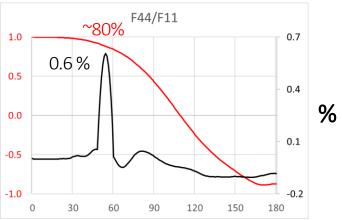
0

30

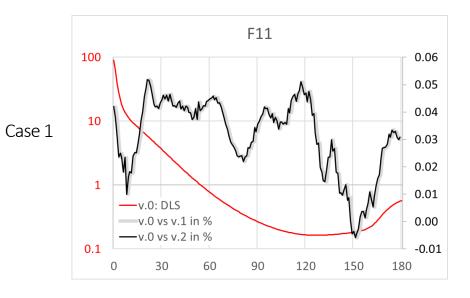
60

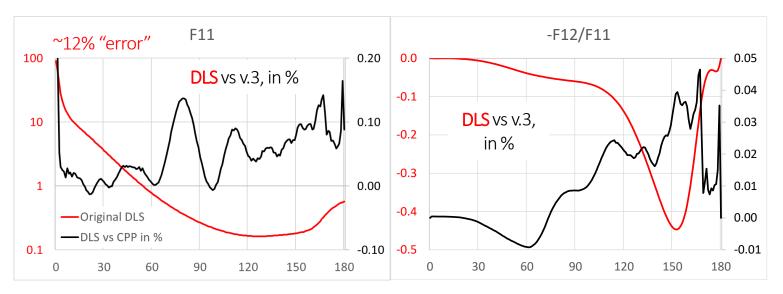


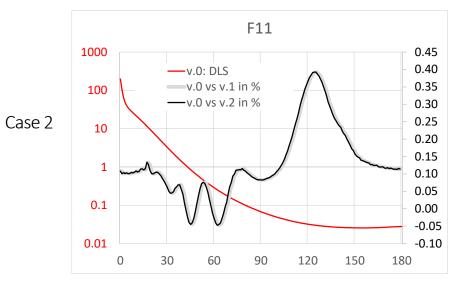


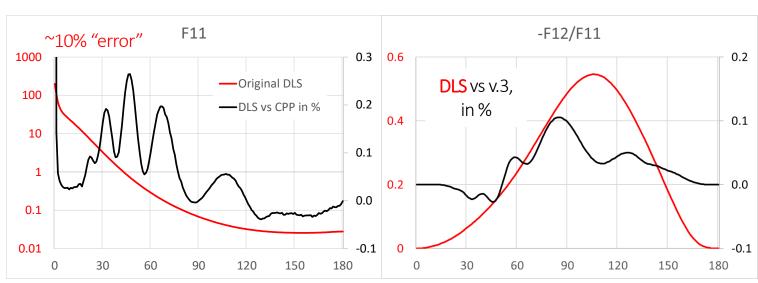


## Graphical results: general





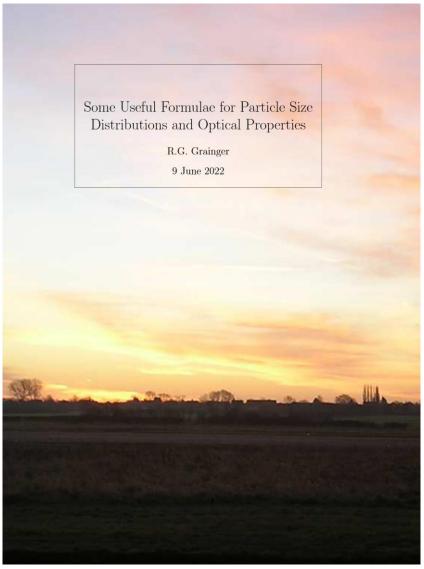




# PS: What if F & C fractions (or Mie & Srd... or both...) have different, e.g. n-ik, ... or other parameters?

**Q:** How to predict unpredictable & account for unaccountable? Where will our research lead us tomorrow? **A:** The new package must have maximum flexibility. Discussion to follow...

## PS: Very good (concise!) summary on the topic



Some Useful Formulae for Particle Size Distributions and Optical Properties

## 1 Describing Particle Size

Atmospheric particles come in a variety of compositions and sizes. There are three main classes: aerosols, water droplets and ice crystals. But that is just a start, a complete description of an ensemble of particles would encompass the composition and geometry of each particle. Such an approach is impracticable. For example atmospheric aerosols have concentrations as high as  $\sim 10,000$  particles per cm<sup>3</sup>. An alternate approach is to use a statistical description of the particle size distribution. This is assisted by the fact that small liquid drops adopt a spherical shape so that for a chemically homogeneous particle the problem becomes one of representing the number distribution of particle radii. The particle size distribution can be represented in tabular form but it is usual to adopt an analytic functional. The success of this approach hinges upon the selection of an appropriate size distribution function that approximates the actual distribution. There is no a priori reason for assuming this can be done.

## 1.1 Particle Size Distribution

A measured distribution of particle sizes can be described by a histogram of the number of particles per unit volume within defined size bins. By making the bin size tend to zero a continuous function is formed called the radius number density distribution N(r) which represents the number of particles with radii between r and r + dr per unit volume. The difficulty with this representation is that is is unmeasurable! This is because there are an infinite number of radius values so that the probability of the radius being any one specific value is zero. The problem is avoided by using the differential radius number density distribution n(r) defined by

$$u(r) = \frac{dN(r)}{dr}.$$
 (1)

The same equation can be written in integral form as

$$dN(r) = \int_{r}^{r+dr} n(r) dr.$$
 (2)

The total number of particles per unit volume,  $N_0$ , is given by

$$N_0 = \int_0^\infty n(r) dr. \qquad ($$

The total surface area of the distribution or surface area density is defined

$$a_{\rm V} = 4\pi \int_0^\infty r^2 n(r) dr.$$
 (4)

Some Useful Formulae for Particle Size Distributions and Optical Properties

## 6.2 Back Scatter

■ to be done ■

## 6.3 Phase Function

The phase function represents the redistribution of the scattered energy. For a collection of particles, the phase function is given by

$$P(\lambda, \theta) = \frac{1}{\beta \text{sca}} \int_{0}^{\infty} \pi r^{2} Q^{\text{sca}}(\lambda, r) P(\lambda, r, \theta) n(r) dr.$$
 (126)

## 6.4 Single Scatter Albedo

The single scatter albedo is the ratio of the energy scattered from a particle to that intercepted by the particle. Hence

$$\omega(\lambda) = \frac{\beta^{\text{sca}}(\lambda)}{\beta^{\text{ext}}(\lambda)}$$
 (127)

## 6.5 Asymmetry Parameter

The asymmetry parameter is the average cosine of the scattering angle, weighted by the intensity of the scattered light as a function of angle. It has the value 1 for perfect forward scattering, 0 for isotropic scattering and -1 for perfect backscatter.

$$g = \frac{1}{\beta^{\text{sca}}} \int_{0}^{\infty} \pi r^{2} Q^{\text{sca}}(\lambda, r) g(\lambda, r) n(r) dr$$
 (128)

## 6.6 Integration

The integration of an optical properties over size is usually reduced from the interval  $r=[0,\infty]$  to  $r=[r_{0},r_{u}]$  as  $n(r)\to 0$  as  $r\to 0$  and  $r\to \infty$ . Numerically an integral over particle size becomes

$$\int_{r_i}^{r_u} f(r)n(r) dr = \sum_{i=1}^{n} w_i f(r_i)$$
(12)

where  $w_i$  are the weights at discrete values of radius,  $r_i$ .

$$\beta^{\text{ext}}(\lambda) = \frac{N_0}{\sigma} \sqrt{\frac{\pi}{2}} \int_{r_1}^{r_u} r Q^{\text{ext}}(\lambda, r) \exp \left[ -\frac{1}{2} \left( \frac{\ln r - \ln r_{\text{m}}}{\sigma} \right)^2 \right] dr$$
 (13)

https://eodg.atm.ox.ac.uk/user/grainger/research/aerosols.pdf