

# Optical Communication

## Minor-II solutions

Q.1. Given that,

The p-i-n photodiode generates 1 electron-hole pair / 3 photons  
wave length incident light  $\lambda = 0.8 \mu\text{m}$

Received optical power  $P_{in} = 10^{-7} \text{ W}$ .

(a) Quantum efficiency of the photodiode

$$\eta = \frac{\text{no. of } e^- \text{ collected}}{\text{no. of photons incident}} = \frac{q_e}{q_p}$$

$$\boxed{\eta = \frac{1}{3} = 0.333}$$

$\therefore$  At  $0.8 \mu\text{m}$ , the quantum efficiency is 33.3%

(b) The maximum possible band gap energy  $E_g = \frac{hc}{\lambda}$

$$E_g = \frac{6.626 \times 10^{-34} \times 3 \times 10^8}{0.8 \times 10^{-6}} \text{ J}$$

$$\boxed{E_g = 24.8475 \times 10^{-20} \text{ J}}$$

(c) The mean output photo current  $I_p = R P_{in}$

where  $R \rightarrow$  responsivity

$$R = \frac{nq}{E_g} = \frac{0.33 \times 1.602 \times 10^{-19}}{24.8475 \times 10^{-20}}$$

$$= 0.2127$$

$$\therefore I_p = 0.2127 \times 10^{-7} \text{ A} = \boxed{21.27 \text{ nA}}$$

Q2

Given that,

For p-i-n photo diode, area of photon capture  $A = 1.5 \text{ mm}^2$

load resistance  $R_L = 100 \Omega$

electron drift velocity  $v_d = 10^7 \text{ m/s}$

The permittivity of Si  $\epsilon = 1.04 \times 10^{-10} \text{ F/m}$

The junction (intrinsic layer) capacitance

$$C_j = \frac{\epsilon A}{w} \quad ; \quad \text{where } w = \text{thickness of the i-layer}$$

$$\text{For fast response time, } R_L C_j = \frac{w}{v_d}$$

$$R_L \frac{\epsilon A}{w} = \frac{w}{v_d}$$

$$w = \sqrt{v_d R_L \epsilon A} = 3.95 \times 10^{-4} \text{ m}$$

$$\therefore w = 395 \mu\text{m}$$

Q 3.

Given that,

Incoming signal power  $P_{in} = 1.28 \text{ nW}$ 

$$\text{SNR} = 9 \text{ dB}$$

Quantum efficiency of the photodetector  $\eta = 75\%$ Transmission bandwidth  $B = 400 \text{ MHz}$ .

$$\text{SNR} = \frac{I_p^2}{\sigma_s^2} \quad (\text{Assume shot noise is dominated component})$$

where

$$\text{shot noise } \sigma_s^2 = 2q I_p B$$

$$10^{0.9} = \frac{I_p}{2qB} \Rightarrow I_p = 15.8869 B \rightarrow (1)$$

$$\text{We know that } \eta = \frac{I_p/q}{P_{in}/E_{ph}} \Rightarrow$$

$$E_{ph} = \frac{hc}{\lambda} = \frac{\eta P_{in}}{I_p/q} \Rightarrow \lambda = \frac{hc (I_p/q)}{\eta P_{in}}$$

$$\therefore \lambda = \frac{6.626 \times 10^{-34} \times 3 \times 10^8 \times 15.886 \times 400 \times 10^6}{0.75 \times 1.28 \times 10^{-9}} \text{ m}$$

$$\boxed{\lambda = 1.3157 \text{ } \mu\text{m}}$$

Q.4

Given that

For a digital single mode optical fiber system,

the operating wavelength  $\lambda = 1.5 \mu\text{m}$ 

Transmission rate = 560 Mbps

length of the fiber link  $L = 50 \text{ km}$ Mean optical power launched into fiber  $P_{in} = -13 \text{ dBm}$ fiber loss  $\alpha_{\text{fiber}} = 0.25 \text{ dB/km}$ splice loss  $\alpha_{\text{splice}} = 0.1 \text{ dB}$  (at 1 km interval  
i.e., 49 splices) $\alpha_{\text{connector}} = 0.5 \text{ dB}$  (only one at  
the receiver)system margin  $\alpha_{\text{system}} = 1 \text{ dB}$ Receiver sensitivity  $P_s = -39 \text{ dBm}$ 

The total power loss =  $L \alpha_{\text{fiber}} + 49 \alpha_{\text{splices}} + \alpha_{\text{connector}} + \alpha_{\text{system}}$

$$= 50 \times 0.25 + 49 \times 0.1 + 0.5 + 1$$

$$= 18.9 \text{ dB}$$

The maximum allowable loss =  $P_{in} - P_s = 26 \text{ dB}$ .

$\therefore$  The maximum safety margin for this system is

$$\alpha_{\text{safety margin}} = 26 - 18.9 = \boxed{7.1 \text{ dB}}$$

A 5

Given that, the number of homes subscribed for FTTH service is 280

The power budget = 23 dB ; fiber loss ( $\alpha$ ) = 0.2 dB/km

$$P_{\text{budget}}(\text{dB}) > \alpha L + P_{L,\text{split}} + M_s(\text{dB})$$

where  $L$  = length of the fiber

$P_{L,\text{split}}$  = Power loss due to splitter

$M_s$  = system margin (can be neglected)

because  $M_s \approx 1$ ,  $10 \log_{10}(M_s) = 0 \text{ dB}$ .

$$P_{\text{budget}}(\text{dB}) = 23 \text{ dB} > \alpha L + P_{L,\text{split}}$$

The FTTH system uses a PON architecture and star topology.

⇒ For proper network development, the total loss due to the power splitter and fiber loss must be less than 23 dB.

⇒ According to the architecture of FTTH, there might be multiple splitter stages between OLT and homes

⇒ In general, the FTTH uses 1:32 power splitter or less splitter ratio

$$\therefore P_{L,\text{split}}(32) = 10 \log_{10}(32) \approx 15 \text{ dB}$$

$$\text{Similarly } P_{L,\text{split}}(16) \approx 12 ; P_{L,\text{split}}(8) = 9 \text{ dB}$$



Here, the total fiber link loss from central office to end is more than the maximum allowable fiber link loss.  
 $\therefore$  It is required to use optical amplifier any-where between OLT to ONU.

Now  $P_{\text{budget}} \geq \alpha L + P_{\text{split}} - A$   
where  $A = \text{gain of the amplifier}$

Here based on the distance between OLT and ONU, power splitter ratio, we can adjust the amplifier gain.