Flywheel

energy-storage device. absorbs A flywheel inertial lt mechanical is an energy and serves as а reservoir, storing energy during the period when the supply of energy is more than the requirement and releases it during the period when the requirement of energy is more than the supply.

Flywheels-Function need and Operation

The main function of a fly wheel is to smoothen out variations in of a shaft caused by torque fluctuations. If the source of torque or load torque is fluctuating in nature, then a flywheel is called Many machines have load patterns usually for. that cause torque time function vary over the cycle. Internal combustion to cylinders engines with one or two are а typical example. Piston compressors, punch presses, rock crushers etc. are the other systems that have fly wheel.

Flywheel absorbs mechanical energy by increasing its angular velocity and delivers the stored energy by decreasing its velocity

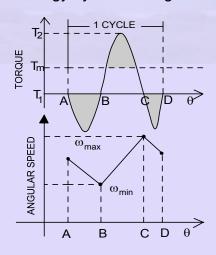


Figure 3.3.1

Design Approach

There are two stages to the design of a flywheel.

First, the amount of energy required for the desired degree of smoothening must be found and the (mass) moment of inertia needed to absorb that energy determined.

Then flywheel geometry must be defined that caters the required moment of inertia in a reasonably sized package and is safe against failure at the designed speeds of operation.

Design Parameters

Flywheel inertia (size) needed directly depends upon the acceptable changes in the speed.

Speed fluctuation

The change in the shaft speed during a cycle is called the speed fluctuation and is equal to $\omega_{\mbox{max}^-}\,\omega_{\mbox{min}}$

$$Fl = \omega_{max} - \omega_{min}$$

We can normalize this to a dimensionless ratio by dividing it by the average or nominal shaft speed $(\omega_{\mbox{ave}})$.

$$C_f = \frac{\omega_{max} - \omega_{min}}{\omega}$$

Where ω_{avg} is nominal angular velocity

Co-efficient of speed fluctuation

The above ratio is termed as coefficient of speed fluctuation C_f and it is defined as

$$C_f = \frac{\omega_{max} - \omega_{min}}{\omega}$$

nominal angular velocity, and ω_{ave} Where ω is the average or mean shaft desired. This coefficient design speed is а parameter be chosen by the designer.

The smaller this chosen value, the larger the flywheel have to be and more the cost and weight to be added to the system. However the smaller this value more smoother the operation of the device

typically set to а value between 0.01 to 0.05 for precision applications machinery and high 0.20 for like crusher as as hammering machinery.

Design Equation

The kinetic energy E_k in a rotating system

$$= \frac{1}{2}I(\omega^2)$$

Hence the change in kinetic energy of a system can be given as,

$$E_{K} = \frac{1}{2}I_{m} \left(\omega^{2}_{max} - \omega^{2}_{min}\right)$$

$$E_{K} = E_{2} - E_{1}$$

$$\omega_{avg} = \frac{\left(\omega_{max} + \omega_{min}\right)}{2}$$

$$E_{K} = \frac{1}{2}I_{s} \left(2\omega_{avg}\right) \left(C_{f} \omega_{avg}\right)$$

$$E_{2} - E_{1} = C_{f} I\omega^{2}$$

$$I_{s} = \frac{E_{k}}{C_{f} \omega_{avg}^{2}}$$

entire Thus the mass moment of inertia needed in the rotating system in order to obtain selected coefficient of speed fluctuation determined using the relation

$$E_{K} = \frac{1}{2}I_{s} (2\omega_{avg}) (C_{f} \omega_{avg})$$

$$I_{s} = \frac{E_{k}}{C_{f} \omega_{avg}^{2}}$$

The above equation can be used to obtain appropriate flywheel inertia I_{m} corresponding to the known energy change E_{k} for a specific value coefficient of speed fluctuation C_{f} ,

Torque Variation and Energy

The required change in kinetic energy E_k is obtained from the known torque time relation or curve by integrating it for one cycle.

$$\int\limits_{\theta \text{ @ }\omega_{min}}^{\theta \text{ @ }\omega_{max}}\left(T_{l}-T_{avg}\right)\!\!d\theta=E_{K}$$

Computing the kinetic energy Ek needed is illustrated in the following example

Torque Time Relation without Flywheel

A typical torque time relation for example of a mechanical punching press without a fly wheel in shown in the figure.

In the absence of fly wheel surplus or positive enregy avalible initially and intermedialty and enery absorbtion negative energy A large magitidue of speed during punching and stripping operations. smoothen out the fluctuation can be noted. To speed fluctuation fly wheel is to be added and the fly wheel energy needed is computed as illustrated below

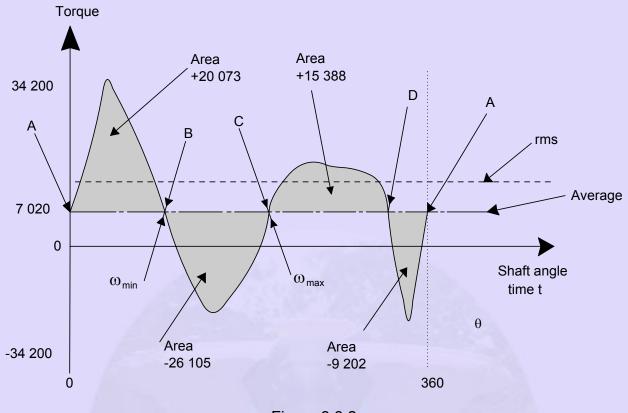


Figure 3.3.2

| Accumulation of Energy pulses under a Torque- Time curve | | | | |
|--|-----------|---|---------------------|--|
| From | △ Area=△E | Accumulated sum =E | Min & max | |
| A to B | +20 073 | +20 073 | ω _{min} @Β | |
| B to C | -26 105 | -6 032 | ω _{max} @C | |
| C to D | +15 388 | +9 356 | | |
| D to A | -9 202 | +154 | | |
| | | Total Energy= E@ ω_{min} - E@ ω_{min} =(-6 032)-(+20 073)= 26 105 Nmm ² | | |

Figure 3.3.3

Torque Time Relation with Flywheel

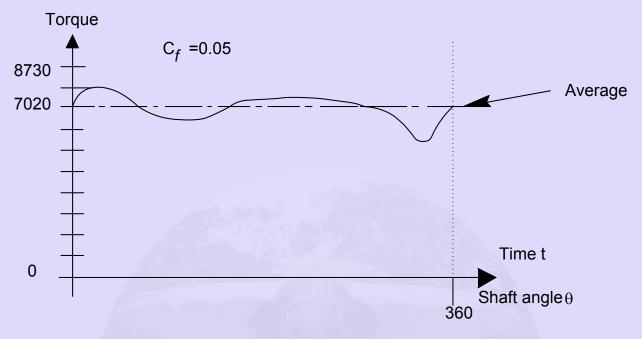


Figure 3.3.4

Geometry of Flywheel

The geometry of a flywheel may be as simple as a cylindrical disc of solid material, or may be of spoked construction like conventional wheels with a hub and rim connected by spokes or arms Small fly wheels are solid discs of hollow circular cross section. As the energy flywheel requirements and size of the increases the geometry changes to disc of central hub and peripheral rim connected by webs and to hollow wheels with multiple arms.

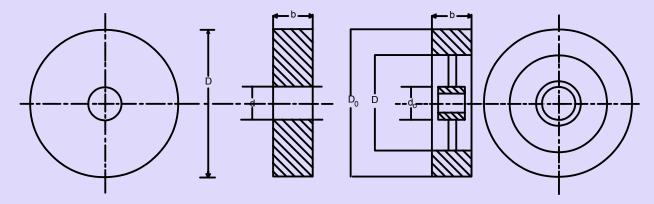
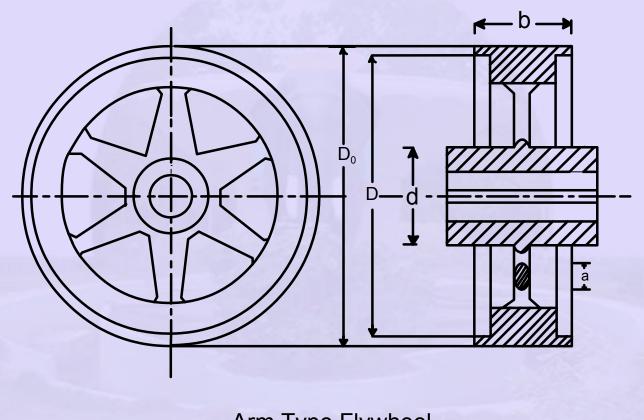


Figure 3.3.5



Arm Type Flywheel

Figure 3.3.6

The latter arrangement is a more efficient of material especially for large flywheels, as it concentrates the bulk of its mass in the rim which is at the largest radius. Mass at largest radius contributes much more since the mass moment of inertia is proportional to mr²

For a solid disc geometry with inside radius r_{i} and out side radius r_{o} , the mass moment of inertia I is

$$I_{m} = mk^{2} = \frac{m}{2}(r_{o}^{2} + r_{i}^{2})$$

The mass of a hollow circular disc of constant thickness t is

$$m = \frac{W}{g} = \pi \frac{\gamma}{g} \Big(r_o^2 - r_i^2 \Big) t$$

Combing the two equations we can write

$$I_{m} = \frac{\pi}{2} \frac{\gamma}{g} \left(r_{o}^{4} - r_{i}^{4} \right) t$$

Where γ is material's weight density

The equation is better solved by geometric proportions i.e by assuming inside to out side radius ratio and radius to thickness ratio.

Stresses in Flywheel

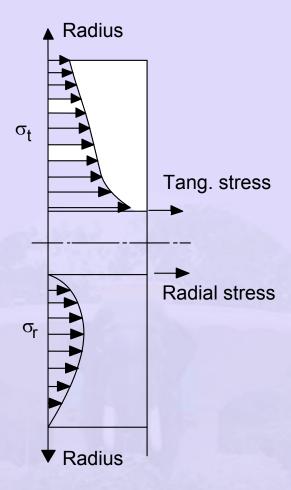
Flywheel being rotating disc. centrifugal stresses upon acts its distributed to pull mass and attempts it apart. similar Its to those caused by an internally pressurized cylinder

$$\sigma_{t} = \frac{\gamma}{g} \omega^{2} \left(\frac{3+v}{8} \right) \left(r_{i}^{2} + r_{o}^{2} - \frac{1+3v}{3+v} r^{2} \right)$$

$$\sigma_{r} = \frac{\gamma}{g} \omega^{2} \left(\frac{3+v}{8} \right) \left(r_{i}^{2} + r_{o}^{2} - \frac{r_{i}^{2} r_{o}^{2}}{r^{2}} - r^{2} \right)$$

 γ = material weight density, ω = angular velocity in rad/sec. v= Poisson's ratio, is the radius to a point of interest, r_i and r_o are inside and outside radii of the solid disc flywheel.

Analogous to a thick cylinder under internal pressure the tangential and radial stress in a solid disc flywheel as a function of its radius r is given by:



point of most interest is the inside radius where the stress is a maximum. What causes failure in a flywheel is typically tangential the point from where fracture originated stress at that and upon fracture fragments explode resulting extremely dangerous consequences, can forces causing the stresses are a function of the the rotational Since also, instead of checking for stresses, the maximum speed at speed the stresses reach the critical value can be determined and safe operating speed can be calculated or specified based on safety factor. Generally some means to preclude its operation beyond this speed is desirable, for example like a governor.

Consequently

F.O.S (N) =
$$N_{os} = \frac{\omega}{\omega_{yield}}$$

WORKED OUT EXAMPLE 1

A 2.2 kw, 960 rpm motor powers the cam driven ram of a press through a gearing of 6:1 ratio. The rated capacity of the press is 20 kN and has a stroke of 200 mm. Assuming that the cam driven ram is capable of delivering the rated load at a constant velocity during the last 15% of a constant velocity stroke. Design a suitable flywheel that can maintain a coefficient of Speed fluctuation of 0.02. Assume that the maximum diameter of the flywheel is not to exceed 0.6m.

Work done by the press=

$$U = 20*10^{3}*0.2*0.15$$
$$= 600 \text{Nm}$$

Energy absorbed= work done= 600 Nm

Mean torque on the shaft:

$$\frac{2.2*10^3}{2*\pi*\frac{960}{60}} = 21.88$$
Nm

Energy supplied= work don per cycle

$$=2\pi*21.88*6$$

= 825 Nm

Thus the mechanical efficiency of the system is =

$$\eta = \frac{600}{825} = 0.727 = 72\%$$

There fore the fluctuation in energy is =

$$E_k$$
 = Energy absorbed - Energy supplied

$$600 - 825*0.075(21.88*6*\pi*0.15)$$
 538.125 Nm
 E_k
 538.125

$$I = \frac{E_k}{C_f \left(\omega_{avg}\right)^2} = \frac{538.125}{0.02 \left(2\pi * \frac{960}{60}\right)^2}$$

$$= 2.6622 \text{ kg m}^2$$

$$I = \frac{\pi}{2} \cdot \frac{r}{g} \left(r_0^2 - r_i^2 \right) . t$$

Assuming
$$\frac{r_i}{r_o} = 0.8$$

$$2.6622 = \frac{\pi}{2} * \frac{78500}{9.86} (0.30^4 - 0.24^4) t$$
$$= 59.805t$$

$$\therefore t = \frac{2.6622}{59.805} = 0.0445$$

or

= 0.556MPa

45 mm

$$\begin{split} &\sigma_t = \frac{r}{g}\omega^2 \left(\frac{3+\gamma}{8}\right) \left(r_i^2 + r_o^2 - \frac{1+3\gamma}{3+\gamma}r^2\right) \\ &\sigma_t = \frac{78500}{9.81}.\omega^2 \left(\frac{3+0.3}{8}\right) \left(0.24^2 + 0.3^2 - \frac{1.9}{3.3}*0.24^2\right) \\ &\sigma_t = 0.543* \left(2\pi*\frac{960}{60}\right)^2 \\ &= 55667N/m^2 \end{split}$$

or if
$$\sigma_t = 150 \text{ MPa}$$

 $150*10^6 = 7961.4\omega^2 (0.4125)(0.0376)(0.090)(0.0331)$
 $= 0.548\omega^2$
 $\omega = 16544 \text{ rad/sec}^2$

$$N_{OS} = \frac{\omega_{yield}}{\omega} = \frac{16544}{32\pi}$$
$$= 164.65$$