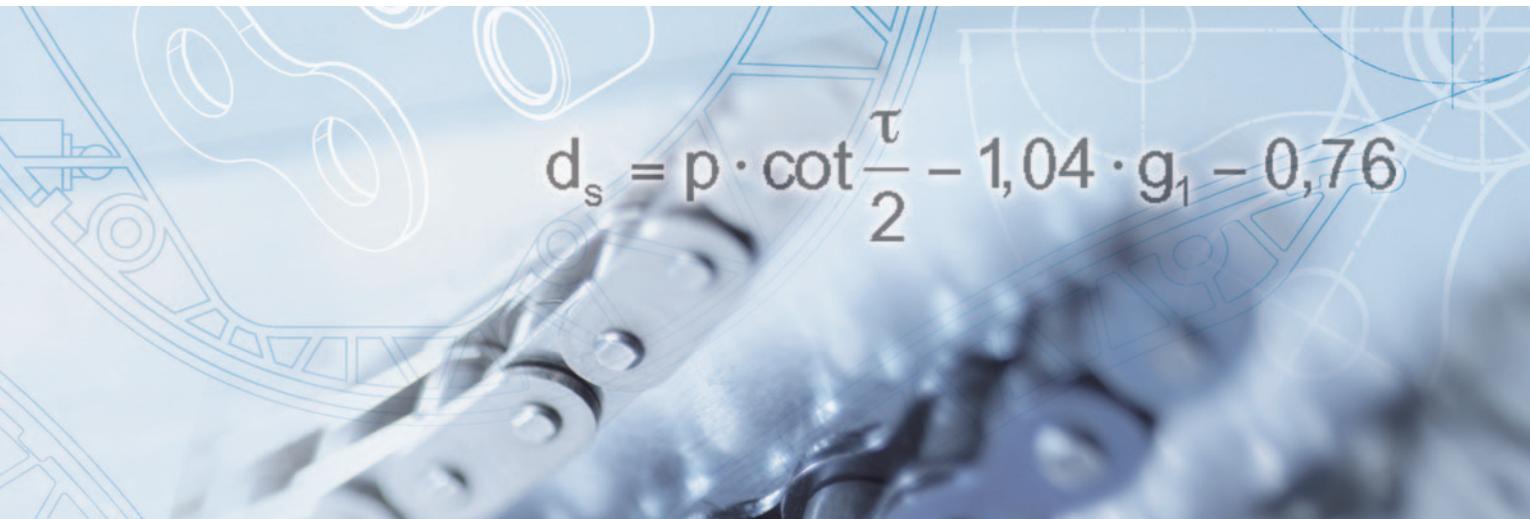


Version 2010



Handbook for chain engineering
Design and construction / Examples of calculation

iwis

Joh. Winklhofer Beteiligungs GmbH & Co. KG

Company Headquarters, Parent of the independent subsidiary companies,
Management Organisation of the Internationally operating companies

iwis motorsysteme GmbH & Co. KG

Subsidiary for the automotive sector, for example chain drives and mass balance drives as well as oil pump drives and gear box chains

iwis antriebssysteme GmbH & Co. KG

Subsidiary for the industrial sector, high precision chains and drive systems for a wide range of applications

iwis antriebssysteme GmbH

A distribution and service company within the chain drive industry

iwis agrisystems (Div.)

Competence centre for the iwis agricultural chain program for combines and maize harvesting

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Together, we are able to offer you even more

Preface

This present **handbook for chain engineering** represents a summary of chain technology that the designer requires: Characteristics of various components, calculating formulae and tables. All this is supplemented by descriptions and examples of calculations.

It is possible to have alternative solutions, which can be supported by calculations, to a number of problems. Optimum results can only be obtained, if the basic information is known and well founded values are available from experience. The User can rely on assistance from our Technical Advisory Dept.

This Department has vast applicational experience of chain drives ranging from the camshaft drive for high-speed racing engines to the conveying of special components through drying ovens, from precision conveyors used in copying equipment, and the stop-go operation encountered with power and free conveyor chains in transfer lines in the motor industry.

Reliable products are identified by their accuracy, close tolerances and proven performance.

These are the products that **iwis** supply. The latest issue of catalogue "Precision Chains for Drive and Conveyor Purposes", which is supplemented by a range of special leaflets, provides information in respect of all available standard and special chains, chain wheels, tensioning devices and other chain drive accessories.

This technical handbook extends the range of **iwis** publications and should help the engineer assess and understand the theory and practice of chain drives and the advantages available when **iwis** products are specified and selected.

Quality can only be assessed under arduous conditions. Exceeding the limits, either upwards or downwards, leads to inevitable expense: Over specification is costly because products and processes are used that are too expensive, equally overload is costly and leads to premature failure.

The correct choice of product is possible only, if the following conditions are known:

- practicable method of calculation and sound theoretical basis
- assured empirical values based on sound experience
- proven figures from practical experience.

iwis offers you all this as a package.

Quality products with a world reputation

QUALITY PLUS POINTS

- Above-average service life due to excellent wear resistance
- High consistency, matchless precision, superior length tolerances
- Breaking strength considerably higher than the DIN/ISO standard, high fatigue strength
- All iwis chains are pre-stretched
- Highly efficient initial greasing and corrosion protection
- Shouldered pins with chains made to DIN 8187 standards

WHAT THIS MEANS FOR THE USER

- Longer times between maintenance, less downtime and thus more economic
- Perfect functioning of chains running in parallel or in pairs, extremely precise positioning, ease of running, and very quiet operation
- Greatly increased factors of safety which provides wider selection opportunities
- Reduced stretching during running-in
- Optimum protection, noise reduction
- Maintenance-friendly, chain which can easily be cut to length

SL – AN IWIS IDEA WINS THROUGH

iwis SL series chains (Super Longlife) have pins with an additional extremely hard surface, under which is a load-bearing high strength hard layer which encloses a tough core.

This special design provides outstanding characteristics:

- Highest resistance to wear and therefore prolonged service life
- Breaking strength and fatigue strength remain high
- Higher resistance to wear at increased temperatures
- Improved surface finishes reduce friction properties and enable the chain to better handle deficient operational lubrication
- Reduced susceptibility to corrosion
- Increased safety with ending stresses

SL chains have proved themselves in practical cases in the most varied chain applications world wide.

iwis chains of this design are designated by the suffix SL.

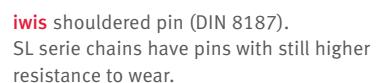
The path to high iwis quality – Each individual part technically perfect

- Use of high-grade heat-treatable steels which are made exclusively for iwis to their material analysis, tolerance and surface quality.
- Each chain part is manufactured a million times daily to the same precision. This production is monitored by SPC (statistical process control).
- All chain parts are heat-treated, using special processes to optimize quality features.
- Constant geometry and high surface quality result from the use of modern production technologies.
- Chains are checked for dimensional accuracy: length tolerance, freedom of articulation and assembly component integrity, inspection of the press-in seating of the pin outer links and bush-inner link interfaces.
- The high standard of quality assurance conforms with the high requirements of the automotive industry, of ISO 9002-1987 and other national and international standards.
- For special applications
 - Surface coatings
 - Special lubrications
 - Reduced length toleranced chains
 - Special materials (e.g. corrosion resistant)

iwis bush – manufactured as a special, surface treated, seamless closed cylinder.



iwis shouldered pin (DIN 8187).
 SL serie chains have pins with still higher resistance to wear.



iwis side plate – optimally dimensioned, shaped with precision, and heat-treated for toughness and hardness.



iwis side plate – optimally dimensioned, shaped with precision, and heat-treated for toughness and hardness.



iwis roller – absolutely cylindrical form, even at the impact point guarantees ideal sliding-contact bearing properties



Your perfect engineering partner



iwis has the largest chain R & D department in Europe, having more than 60 development engineers solely engaged for the engineering of chain drive systems. Besides basic development and designing innovative customer solutions, the main focus of iwis R&D division ranges from calculations, design and testing to wear elongation and fatigue strength analysis.

- Special knowledge of noise emission analysis and vibration engineering
- Our laboratory has the capabilities to carry out many different testing possibilities including microscopy, metallography, evaluation of mechanical properties, chemical composition and qualified analysis of data
- Dynamic simulation/analysis of chain drive systems with regard to chain load, torsional vibrations and friction losses
- FEM analysis of individual chain drive parts – static and dynamic stress and strength investigations
- Evaluation of iwis and customer readings at test facilities for verification of simulation models
- Identification of thermal characteristics of chain drives while testing in the climate-testing laboratory.



Evaluation of chain breaking strength and elongation up to 1000kN

More than 15 pulser are available for testing dynamic fatigue strength according to different testing methods

Testing of chain wear elongation behaviour on more than 20 testing rigs

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1 Introduction

The chain drive assumes a special position in the large group of drive mediums for the transmission of torque and power. The great advantage of this type of positive controlled connection is the constant relative speed between driving and driven shafts and the complete elimination of slip, compared with non-positive drives (e.g. belt drives) where slip very often can only be prevented by high belt tension. Steel roller chains are used as drive, transport or conveyor chains for static or alternating loads with slow or high chain speeds transmitting power between two parallel shafts.

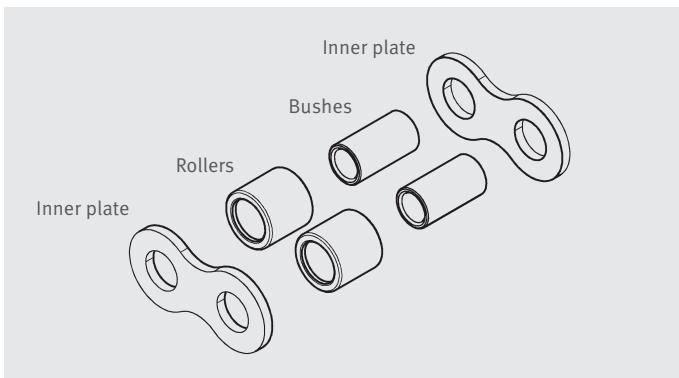
Compared to the use of cables, round link chains, gear and belt drives, the application for steel roller chains must be defined accordingly. The construction of steel roller chain has the advantage of avoiding bending stresses during operation, to which cables are subjected, when they run over pulleys. They are particularly advantageous when long distances between shafts have to be connected, and they are more cost effective than gear drives, due to the fact that no idler gears with bearings are required. Gear drives mean a change of direction. With chain drives the sense of direction remains the same. They constitute a flexible connection between shafts. By using adjustable idler wheels it is possible to control the rotation of two shafts in phase.

Chains can engage with chain wheels on both sides, which is often required for special drives, which need a change of direction. Chain drives are less sensitive to dirt and lack of maintenance than gear and other drives and can also be used under higher operating temperatures. Steel Roller chains are used throughout engineering. They are used in the manufacturing of machine tools, printing machines, in the textile and packaging industry, for material handling, agricultural machinery, in the construction industry, hydraulic engineering and mining industry, and also in the construction of vehicles and engines.

2 Design of steel roller chains

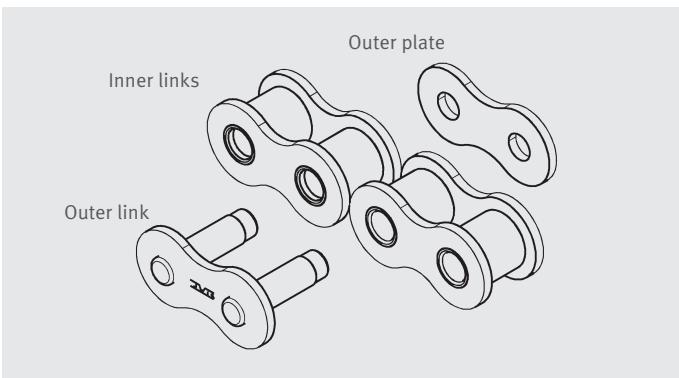
Steel roller chains consist of a range of individual chain links. Each link in turn consists of individual components some of which are designed to transmit tensile loads and others that allow the articulation of two links in respect of each other. The design of the links is of particular importance. Generally speaking, they move only in one plane.

This design of **iwis** high-performance roller chains and of bush chains is illustrated in the following drawings.



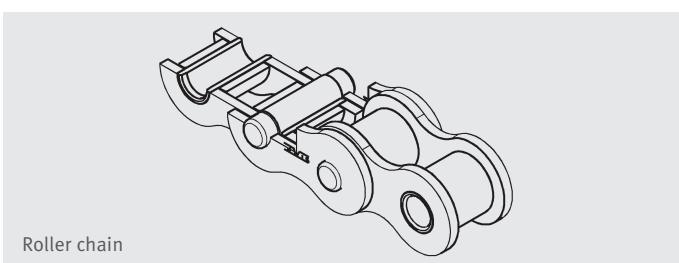
A chain consists of inner and outer links. The inner link consists of two inner plates into which, two bushes are pressed and two rollers, which rotate on the bushes.

In the case of bush chains both rollers are omitted. Thus the bushes are in direct contact with the chain wheel teeth.



The outer link consists of two outer plates and two bearing pins. The connection of the inner links by adding outer links is shown in the above illustration.

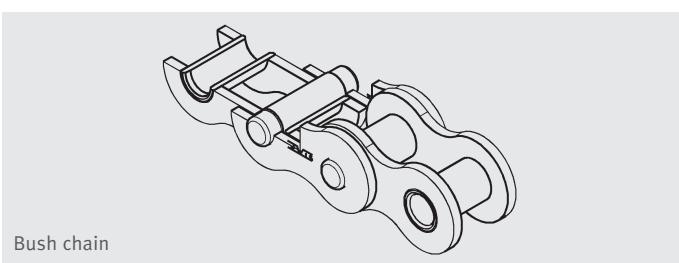
3 Roller and bush chains



iwis manufactures both types of chains. The decision to use one or the other type requires a thorough knowledge of the problems to be solved.

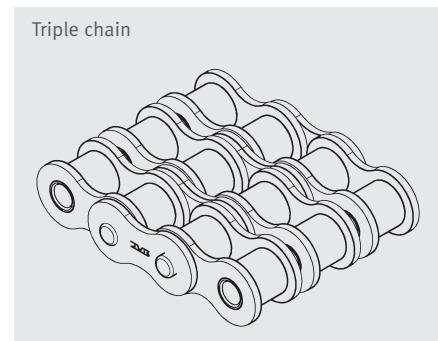
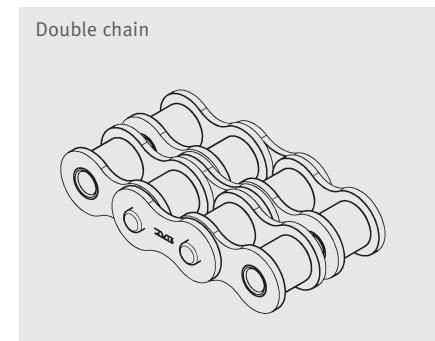
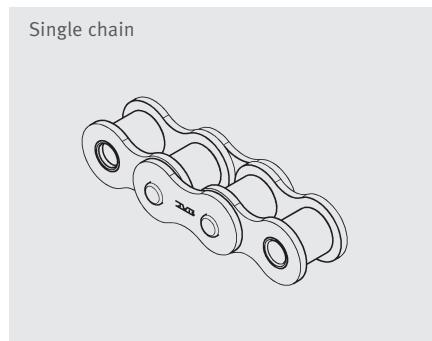
The rollers which rotate on the bushes run with little friction on the teeth of the chainwheel, as there is a constant change in contact area. The grease film between rollers and bushes contributes towards silent running and absorbs shocks.

In the case of a bush chain, the teeth of the chain wheel always contact the stationary bushes at the same point. It is therefore important to provide excellent lubrication when using this type of drive.



The bearing area given in the table for each chain size is the projection of the bearing surface between bush and bearing pin. That is the length of the bush, multiplied by the bearing pin diameter. A higher bearing area results in a lower bearing pressure, and therefore reduces wear rate.

iwis bush chains which are used for heavily stressed camshaft drives in highspeed Diesel engines have been particularly successful.



As soon as the transmission of torque using a single chain requires less than a 15 tooth chainwheel, it is recommended to use a multiple chain with a smaller pitch. This results in a larger number of teeth with the same chain wheel diameter. This improves the polygonal effect of the chain links, and the impact speed of the rollers on the teeth are reduced. Therefore a drive using a multiple smaller pitch chain will run more quietly than a single chain with a larger pitch.

Multiple chains with a smaller pitch than the single chain should also be selected, if single chains exceed the maximum permissible chain speed that is shown on the graphs on pages 29 and 30.

Multiple chains are more sensitive to misalignment of the chainwheels. For reasons of durability it is not recommended to go beyond triplechains. Where a triple chain is insufficient, it is possible to use two double chains or several triple chains. In this case care should be taken to ensure that the chains are matched.

5 Connecting links

If chains are not supplied as endless chains, the ends are connected by a connecting link. On chains up to and including 1" pitch the plate is retained by means of a spring clip.

For chains 1 1/4" pitch and over and chains to DIN 8188 from 3/4" onwards, the link plate is secured by means of a split pin.



Rivetting link

Chains are endlessly riveted together using this type of connecting link.

Standard designation A



Double cranked link

A double cranked link consists of one cranked link and an inner link. They are used to produce chains with an uneven number of links.

Standard designation C



Spring clip connecting link

This spring clip is used to connect chain sections ending with inner links. The closed end of the clip is fitted in the direction of chain motion.

Standard designation E



Single-cranned link with screwed connection

With only one connecting link **A**, **E** or **K** and using this cranked link chains with an uneven number of links can be produced.

Standard designation L



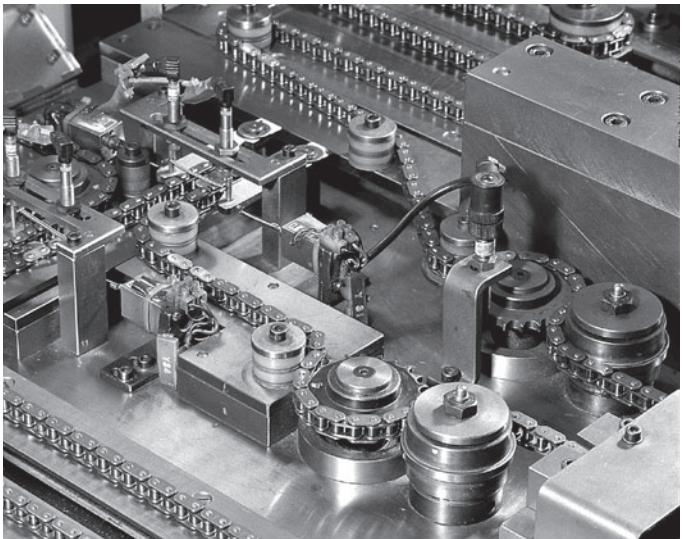
Split pin connecting link

Fulfils the same purpose as the spring clip type.

Standard designation S

A cranked link can should be avoided. It can reduce the breaking strength of the chain by 20 %.

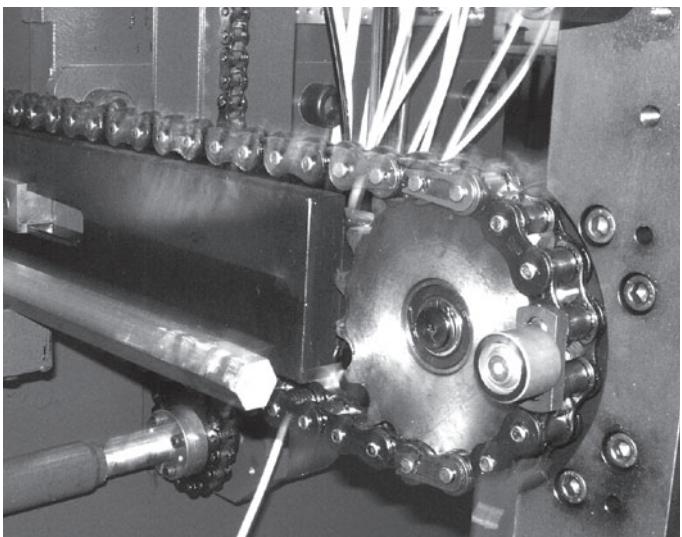
Areas of applications



GENERAL MECHANICAL ENGINEERING

Excellent wear resistance and fatigue strengths for specialized applications

A



HANDLING INDUSTRY

Conveyor chains - reliable, precise and longterm solutions for demanding requirements

B



PACKAGING INDUSTRY

iwis chains with special clamping elements for gripping, retracting and transporting soft foils and other thin-walled materials

C

Layout of
DWTS® chain drives

D

General information
DWTS® chain drives

DWTS® Chains for
industrial use

E

DWTS® Automotive
chain drives

F

Conversion charts,
iwis chain guideline

G

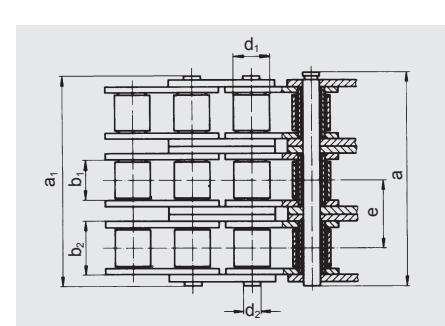
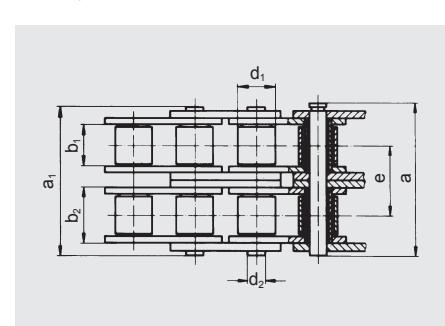
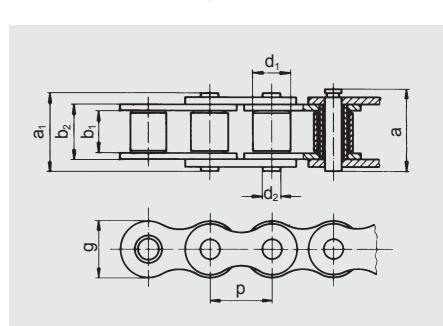
6 iwis-Roller Chains

Standard and works standard embodiment

Table extract

iwis Designation	Designation pitch x inner width		DIN/ISO No.	Pitch p (mm)	inside b ₁ (mm)	outside a ₁ (mm)	Roller dia. d ₁ (mm)	Height of plates g (mm)	Bearing area f (cm ²)	Weight q (kg/m)	Chain made by iwis (N)	Standard (N)
Single chains to DIN 8187												
G 42	6 x 2,8 mm	04	DIN 8187	6	2,80	6,6	4,00	5,00	0,07	0,12	3 200	3 000
G 52	8 mm x 1/8"	05 B-1	DIN 8187	8	3,16	8,1	5,00	7,10	0,11	0,18	6 000	5 000
G 53 H ¹⁾	8 mm x 3/16"	-	Works standards	8	4,76	11,7	5,003)	7,60	0,25	0,34	9 000	-
G 62 1/2 ²⁾	3/8 x 5/32"	-	Works standards	9,525	3,94	11,0	6,35	8,20	0,22	0,34	11 000	-
G 67 ²⁾	3/8 x 7/32"	06 B-1	DIN 8187	9,525	5,72	12,9	6,35	8,20	0,28	0,41	10 500	9 000
P 83 V	1/2 x 3/16"	-	Works standards	12,7	4,88	13,2	7,75	10,20	0,29	0,44	15 500	-
S 84 V	1/2 x 1/4"	-	Works standards	12,7	6,40	15,0	7,75	12,00	0,38	0,58	18 000	-
L 85 SL	1/2 x 5/16"	08 B-1	DIN 8187	12,7	7,75	16,9	8,51	12,20	0,50	0,70	22 000	18 000
M 106 SL	5/8 x 3/8"	10 B-1	DIN 8187	15,875	9,65	19,5	10,16	14,40	0,67	0,95	27 000	22 400
M 127 SL	3/4 x 7/16"	12 B-1	DIN 8187	19,05	11,75	22,7	12,07	16,40	0,89	1,25	34 000	29 000
M 1611	1"x17 mm	16 B-1	DIN 8187	25,4	17,02	36,1	15,88	21,10	2,10	2,70	75 000	60 000
M 2012	1 1/4 x 3/4"	20 B-1	DIN 8187	31,75	19,56	40,5	19,05	25,40	2,92	3,72	120 000	95 000
M 2416	1 1/2 x 1"	24 B-1	DIN 8187	38,1	25,40	53,1	25,40	33,50	5,50	7,05	211 000	160 000
M 2819	1 3/4 x 31 mm	28 B-1	DIN 8187	44,45	30,95	65,1	27,94	37,00	7,35	8,96	250 000	200 000
M 3219	2"x 31 mm	32 B-1	DIN 8187	50,8	30,95	63,6	29,21	42,30	8,05	10,00	315 000	250 000
Double chains to DIN 8187												
D 52	8 mm x 1/8"	05 B-2	DIN 8187	8	3,16	13,9	5,00	7,10	0,22	0,36	9 100	7 800
D 67 ²⁾	3/8 x 7/32"	06 B-2	DIN 8187	9,525	5,72	23,4	6,35	8,20	0,56	0,78	20 000	16 900
D 85 SL	1/2 x 5/16"	08 B-2	DIN 8187	12,7	7,75	30,8	8,51	12,20	1,00	1,35	40 000	32 000
D 106 SL	5/8 x 3/8"	10 B-2	DIN 8187	15,875	9,65	36,0	10,16	14,40	1,34	1,85	56 000	44 500
D 127	3/4 x 7/16"	12 B-2	DIN 8187	19,05	11,75	42,1	12,07	16,40	1,78	2,50	68 000	57 800
D 1611	1"x17 mm	16 B-2	DIN 8187	25,4	17,02	68,0	15,88	21,10	4,21	5,40	150 000	106 000
D 2012	1 1/4 x 3/4"	20 B-2	DIN 8187	31,75	19,56	79,7	19,05	25,40	5,84	7,36	210 000	170 000
D 2416	1 1/2 x 1"	24 B-2	DIN 8187	38,1	25,40	101,8	25,40	33,50	11,00	13,85	370 000	280 000
D 2819	1 3/4 x 31 mm	28 B-2	DIN 8187	44,45	30,95	124,7	27,94	37,00	14,70	18,80	500 000	360 000
D 3219	2"x 31 mm	32 B-2	DIN 8187	50,8	30,95	126,0	29,21	42,30	16,10	19,80	530 000	450 000
Triple chains to DIN 8187												
Tr 85	1/2 x 5/16"	08 B-3	DIN 8187	12,7	7,75	44,7	8,51	12,20	1,50	2,00	58 000	47 500
Tr 106	5/8 x 3/8"	10 B-3	DIN 8187	15,875	9,65	52,5	10,16	14,40	2,02	2,80	80 000	66 700
Tr 127	3/4 x 7/16"	12 B-3	DIN 8187	19,05	11,75	61,5	12,07	16,40	2,68	3,80	100 000	86 700
Tr 1611	1"x17 mm	16 B-3	DIN 8187	25,4	17,02	99,2	15,88	21,10	6,32	8,00	220 000	160 000
Tr 2012	1 1/4 x 3/4"	20 B-3	DIN 8187	31,75	19,56	116,1	19,05	25,40	8,76	11,00	315 000	250 000
Tr 2416	1 1/2 x 1"	24 B-3	DIN 8187	38,1	25,40	150,2	25,40	33,50	16,50	20,31	560 000	425 000
Tr 2819	1 3/4 x 31 mm	28 B-3	DIN 8187	44,45	30,95	184,5	27,94	37,00	22,05	28,00	750 000	530 000
Tr 3219	2"x 31 mm	32 B-3	DIN 8187	50,8	30,95	184,5	29,21	42,30	24,15	29,60	795 000	670 000

¹⁾ bush chain ²⁾ straight side plates ³⁾ bush Ø Chains with the SL suffix have pins with increased resistance to wear.



<i>iwis</i> Designation	Designation pitch \times inner width	DIN/ISO No.	Pitch p (mm)	Inside b_1 (mm)	Outside a_1 (mm)	Width	Roller dia. d_1 (mm)	Height of plates g (mm)	Bearing area f (cm 2)	Weight q (kg/m)	Chain made by iwis (N)	Breaking load F_B	Standard (N)
Single chains to DIN 8188 (ANSI-Standard)													
L 85 A	1/2 x 8/16"	ANSI 40	08 A-1	DIN 8188	12,7	7,94	16,6	7,95	12,00	0,44	0,60	18 000	14 100
M 106 A	5/8 x 3/8"	ANSI 50	10 A-1	DIN 8188	15,875	9,53	20,4	10,16	14,40	0,70	1,00	29 000	22 200
M 128 A SL ¹⁾	3/4 x 1/2"	ANSI 60	12 A-1	DIN 8188	19,05	12,70	25,3	11,91	18,00	1,06	1,47	42 000	31 800
M 1610 A	1 x 5/8"	ANSI 80	16 A-1	DIN 8188	25,4	15,88	32,1	15,88	22,80	1,79	2,57	68 000	56 700

Double chains to DIN 8188 (ANSI-Standard)

D 85 A	1/2 x 5/16"	ANSI 40-2	08 A-2	DIN 8188	12,7	7,94	31,0	7,95	12,00	0,88	1,19	36 000	28 200
D 106 A	5/8 x 3/8"	ANSI 50-2	10 A-2	DIN 8188	15,875	9,53	38,6	10,16	14,40	1,40	1,92	56 000	44 400
D 128 A ¹⁾	3/4 x 1/2"	ANSI 60-2	12 A-2	DIN 8188	19,05	12,70	48,1	11,91	18,00	2,12	2,90	84 000	63 600
D 1610 A	1 x 5/8"	ANSI 80-2	16 A-2	DIN 8188	25,4	15,88	61,4	15,88	22,80	3,58	5,01	145 000	113 400

Triple chains to DIN 8188 (ANSI-Standard)

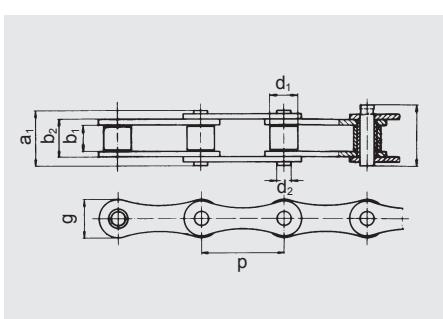
Tr 85 A	1/2 x 8/16"	ANSI 40-3	08 A-3	DIN 8188	12,7	7,94	45,4	7,95	12,00	1,32	1,78	50 000	42 300
Tr 106 A	5/8 x 3/8"	ANSI 50-3	10 A-3	DIN 8188	15,875	9,53	56,7	10,16	14,40	2,10	2,89	80 000	66 600
Tr 128 A	3/4 x 1/2"	ANSI 60-3	12 A-3	DIN 8188	19,05	12,70	71,0	11,91	18,00	3,18	4,28	125 000	95 400
Tr 1610 A	1 x 5/8"	ANSI 80-3	16 A-3	DIN 8188	25,4	15,88	90,7	15,88	22,80	5,37	7,47	210 000	170 100

¹⁾ also available with straight side plates

Chains with the SL suffix have pins with increased resistance to wear.

Overall programme with technical data in catalogue
 „Precision chains for Drive and Conveyor Purposes“

<i>iwis</i> Designation	Designation pitch \times inner width	DIN/ISO No.	Pitch p (mm)	Inside b_1 (mm)	Outside a_1 (mm)	Width	Roller dia. d_1 (mm)	Height of plates g (mm)	Weight q (kg/m)	Chain made by iwis (N)	Breaking load F_B	Standard (N)
Long pitch chains to DIN 8181												
LR 165 SL	1 x 5/16"	208 B	DIN 8181	25,4	7,75	16,9	8,51	11,80	0,52	22 000	18 000	
LR 206 SL	1 1/4 x 3/8"	210 B	DIN 8181	31,75	9,65	19,5	10,16	15,0	0,63	28 000	22 400	
LR 247 SL	1 1/2 x 7/16"	212 B	DIN 8181	38,1	11,75	22,7	12,07	16,10	0,85	34 000	29 000	
LR 3211	1" x 17 mm	216 B	DIN 8181	50,8	17,02	36,1	15,88	20,60	2,10	75 000	60 000	



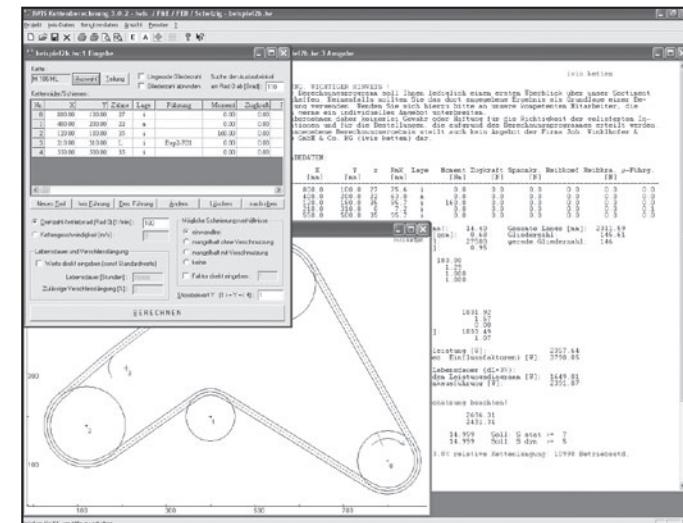
7 Chain calculation program

iwis presents a special PC software package to support you in chain drive layout and pre-selection of suitable chains.

Industrial chain drives are

- drive chains for power transmission of parallel axis shafts,
- which transfer static and dynamic loads,
- as transport or conveyor chains in the application in this program.

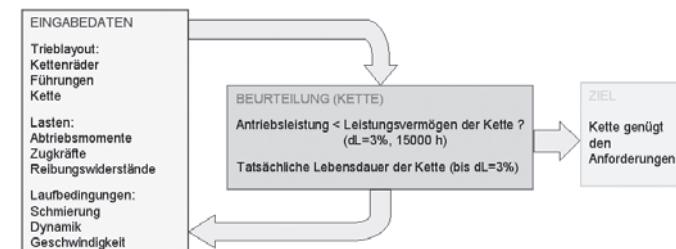
The idea behind the program is based on the calculation of necessary drive capacity in chain transmissions which is required due to their use (engine torque, chain load in the chain section in transport tasks and the friction from the friction ratios on the tension and guide rails and the bearing friction). If the required objective is not met regarding the life of the chain and the operating conditions (e.g. lubrication and dynamics), then it is the responsibility of the user to make amendments or choose another type of chain.



The first result always has the minimum life of the chain of 15,000h (relating to a wear distortion of 3%) as a layout criterion. In addition, the actually calculated (expected) life is given; target life of this drive would then be crucial.

A drive chain cannot be calculated directly with the program, when only the drive capacity of the drive motor is given. It is necessary to specify either a load bearing chain shaft or a taut span depending on the drive sprocket wheel. The motor capacity must be greater than the drive capacity in all cases.

The program is designed in such a way that the user can use one of the chain data banks provided by iwis in which all calculation and capacity characteristics of iwis chains as well as according to DIN 1817, DIN 8188 or ISO 606 can be stored.



It is also possible with the proper knowledge to construct a chain database. A drive can be calculated from a number of axles and conveyor or guide rails in a 2D plane. Sprocket wheels or guides can be defined as tension elements. The chain line is automatically determined by positions of the drive components (wheels, guides).

New discoveries in chain theory and results of tests as well as program updates and corrections are continually being incorporated and are identified by version numbers.

CAUTION, IMPORTANT NOTICE!

Our calculation program is only intended to provide an initial overview of our product range. Under no circumstances should the generated results be used as the basis for placing an order. Please speak to one of our specialist representatives who will be pleased to supply you with a tailor made quotation.

We give no guarantee and accept no liability for the accuracy of the information provided or for any orders which are placed on the basis of the calculation program. The generated results do not constitute an offer by the iwis antriebssysteme GmbH & Co. KG.

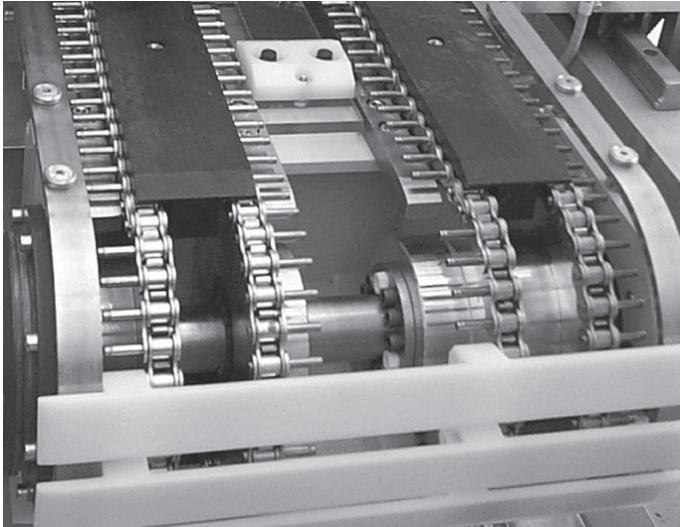
The program is called up by a user code with individual password. After installation it is therefore necessary to request a user file from iwis. All future program developments and corrections will automatically be sent to all registered users. In case support questions arise it is thus guaranteed that the calculations are the same in relation to the program file.

Instructions, wishes and error reports to:
Michael.Panas@iwi.com or Ulrich.Schelzig@iwi.com

System requirement, minimum equipment:

- Processor 586 (Pentium/AMD)
- 64 MB Main memory (RAM)
- Graphic card with 800x600 Pixel resolution
- CD-ROM drive
- Windows 98/NT

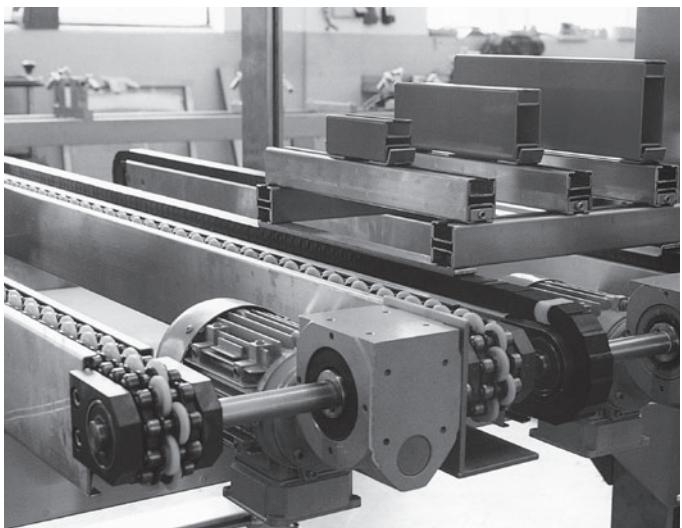
Areas of applications



PACKAGING INDUSTRY:

Special applications für conveyor chains in the Food & Non-Food fieldsh

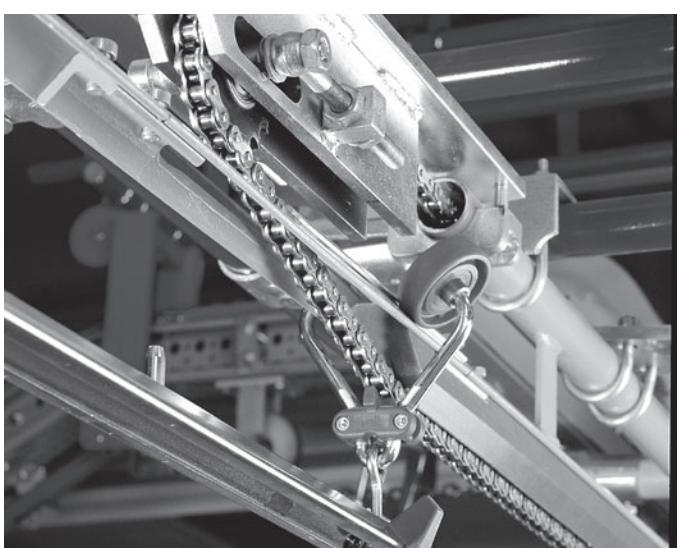
A



MACHINE LINKAGE:

iwis power and free conveyor chains convey, store, accelerare, retard workpieces and workpiece carriers

B



CONVEYING APPLICATIONS:

iwis high performance chains with attachments

C

General information
DWIS® chain drives

D

DWIS® Chains for
industrial use

E

DWIS® Automotive
chain drives

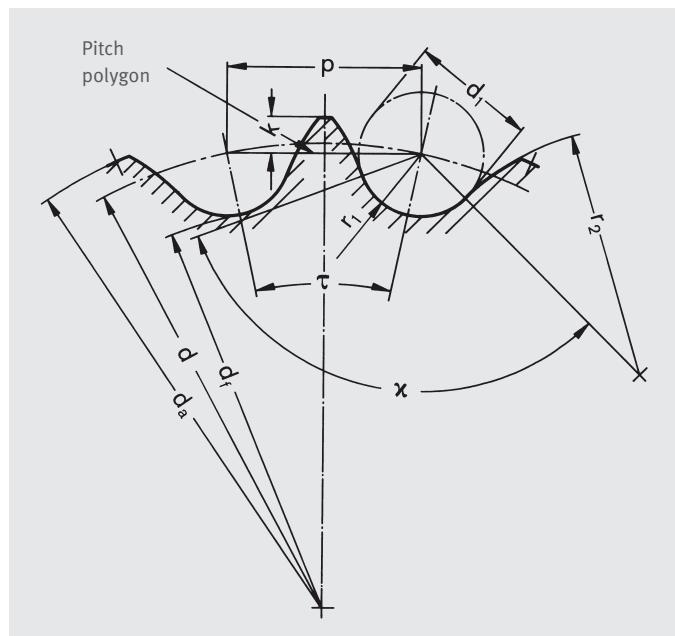
F

Conversion charts,
iwis chain guideline

1 Design and construction

The shape of the chainwheels is determined by the chain size, number of teeth and the torque to be transmitted. Wheels with hubs allow the transmission of a higher torque, whereas plate wheels may be used only for the transmission of smaller torques.

The tooth form is designed in accordance with DIN 8196. The calculation of the required values is summarized below.



- p chain pitch
- d_1 roller diameter max.
- d pitch circle diameter
- d_f root circle diameter
- d_a top diameter
- r_1 tooth radius
- τ tooth angle
- x roller contact angle
- r_2 tooth profile radius
- k tooth height above pitch polygon
- z number of teeth

Pitch circle diameter

$$d = \frac{p}{\sin \frac{\tau}{2}}$$

Root circle diameter

$$\frac{\tau}{2} = \frac{180^\circ}{z}$$

$$d_f = d - d_1$$

Top diameter

$$d_{a \max} = d + 1,25 \cdot p - d_1$$

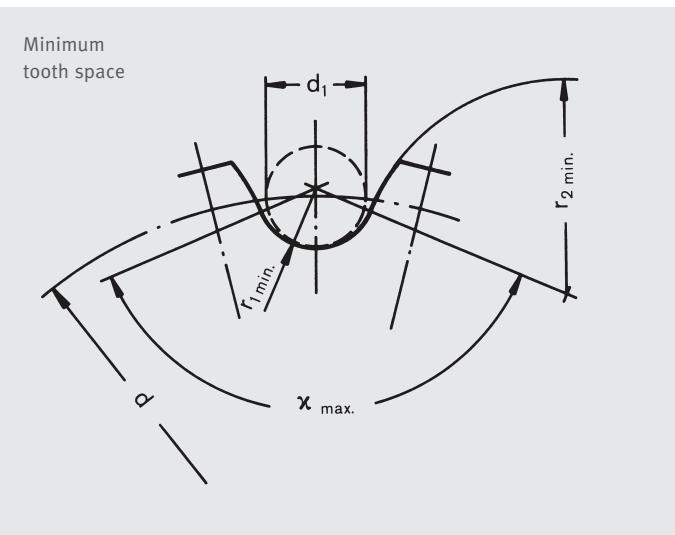
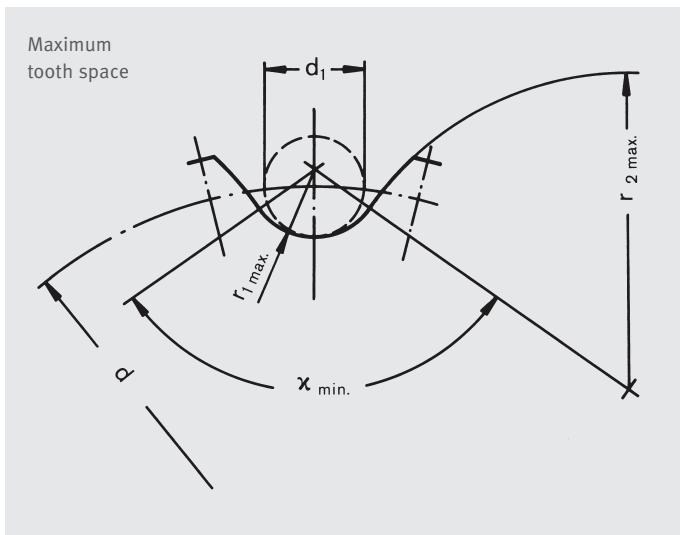
Tooth height

$$k_{\max} = 0,625 \cdot p - 0,5d_1 + \frac{0,8}{z} \cdot p$$

$$d_{a \min} = d + \left(1 - \frac{1,6}{z}\right) \cdot p - d_1$$

$$k_{\min} = 0,5 \cdot (p - d_1)$$

If crossovers occur when interlocking, the effective maximum tip diameter is determined by the interlocking tool



$$r_{1\max} = 0,505 \cdot d_1 + 0,069 \sqrt[3]{d_1}$$

$$r_{1\min} = 0,505 \cdot d_1$$

$$\chi_{\min} = 120^\circ - \frac{90^\circ}{z}$$

$$\chi_{\max} = 140^\circ - \frac{90^\circ}{z}$$

$$r_{2\max} = 0,008 \cdot d_1 (z^2 + 180)$$

$$r_{2\min} = 0,12 \cdot d_1 (z + 2)$$

TOOTH WIDTH

Tooth width B_1 is narrower than the inner width b_1 of the chain

Chain pitch B_1 $p \leq 12,7$ $p > 12,7$

Tolerance for tooth width B_1 : h14

for Single chain wheels $0,93 \cdot b_1$ $0,95 \cdot b_1$

Tooth width B_2, B_3 etc.
 \triangleq (Number of chain strands - 1) · e + B_1

for Double and Triple chain wheels $0,91 \cdot b_1$ $0,93 \cdot b_1$

Tooth width bevel
 (applicable for bicycle and moped sprockets) $c = 0,1 \text{ bis } 0,15 \cdot p$
 $c = 0,05 \text{ bis } 0,07 \cdot p$

for Quadruple chain wheels and over $0,88 \cdot b_1$ $0,93 \cdot b_1$
 $(b_1 \text{ inner width of the chain})$

Zahnfassenradius $r_3 \geq p$

Radfasenradius r_4

Diameter of relief
 Below the root circle (maximum hub diameter)

$$d_s = p \cdot \cot \frac{\tau}{2} - 1,04 \cdot g_1 - 0,76$$

(g_1 max. height of plates)

$$\frac{\tau}{2} = \frac{180^\circ}{z}$$

For further chain wheel dimensions see chart on page 18.

	Chain pitch p	r_4	
		minimal	maximal
	up to 9,525	0,2	1
over 9,525	up to 19,05	0,3	1,6
over 19,05	up to 38,1	0,4	2,5
over 38,1		0,5	6

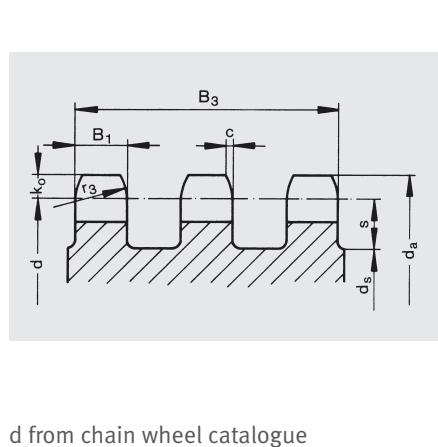
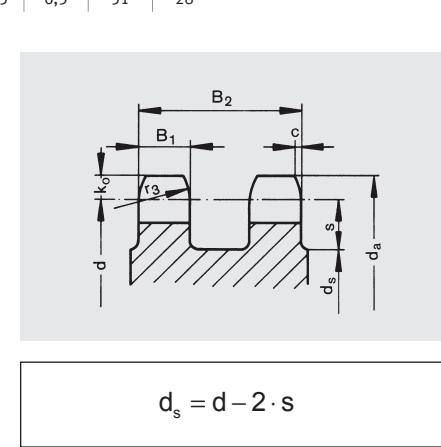
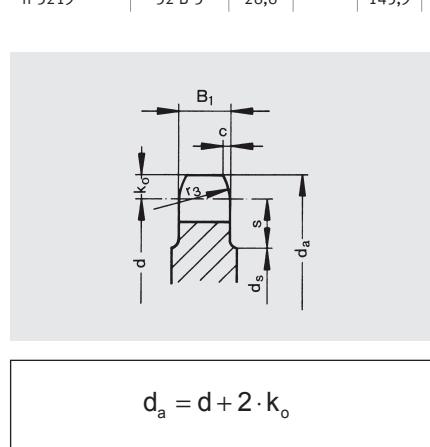
2 Chain wheel sizes

Designation								
iwiS	DIN ISO	B_1 h_{14}	B_2 h_{13}	B_3 h_{12}	k_o ⁽¹⁾	c	r_s	s ⁽²⁾
Single chains to DIN 8187, Works standard								
G 42	04	2,6	-	-	1,2	0,8	6	4
G 52	05 B-1	2,7	-	-	1,8	1,0	8	5,5
G 53 H	-	4,4	-	-	1,8	1,0	8	6
G 62 1/2	-	3,6	-	-	2,0	1,2	10	6,5
G 67	06 B-1	5,3	-	-	2,0	1,2	10	6,5
P 83 V	-	4,5	-	-	2,6	0,8	13	8
S 84	-	5,9	-	-	2,6	1,6	13	8
L 85 SL	08 B-1	7,2	-	-	2,6	1,6	13	9
M 106 SL	10 B-1	9,1	-	-	3,5	2,0	16	11
M 127 SL	12 B-1	11,1	-	-	4,2	2,4	19	12
M 1611	16 B-1	16,1	-	-	5,5	3,2	26	17
M 2012	20 B-1	18,5	-	-	7,0	4,0	32	21
M 2416	24 B-1	24,1	-	-	8,0	4,8	38	25
M 2819	28 B-1	29,4	-	-	10,0	5,6	44	26
M 3219	32 B-1	29,4	-	-	12,5	6,3	51	28
Double chains to DIN 8187, DIN 8154, Works standards								
D 52	05 B-2	2,7	8,3	-	1,8	1,0	8	5,5
D 67	06 B-2	5,2	15,4	-	2,0	1,2	10	6,5
D 85 SL	08 B-2	7,0	20,9	-	2,6	1,6	13	9
D 106 SL	10 B-2	8,9	25,4	-	3,5	2,0	16	11
D 127	12 B-2	10,8	30,2	-	4,2	2,4	19	12
D 1611	16 B-2	15,8	47,6	-	5,5	3,2	26	17
D 2012	20 B-2	18,1	54,5	-	7,0	4,0	32	21
D 2416	24 B-2	23,6	71,9	-	8,0	4,8	38	25
D 2819	28 B-2	28,8	88,3	-	10,0	5,6	44	26
D 3219	32 B-2	28,8	87,3	-	12,5	6,3	51	28
Triple chains to DIN 8187, DIN 8154								
Tr 67	06 B-3	5,2	-	25,6	2,0	1,2	10	6,5
Tr 85	08 B-3	7,0	-	34,8	2,6	1,6	13	9
Tr 106	10 B-3	8,9	-	42,0	3,5	2,0	16	11
Tr 127	12 B-3	10,8	-	49,7	4,2	2,4	19	12
Tr 1611	16 B-3	15,8	-	79,5	5,5	3,2	26	17
Tr 2012	20 B-3	18,1	-	91,0	7,0	4,0	32	21
Tr 2416	24 B-3	23,6	-	120,3	8,0	4,8	38	25
Tr 2819	28 B-3	28,8	-	147,9	10,0	5,6	44	26
Tr 3219	32 B-3	28,8	-	145,9	12,5	6,3	51	28

Designation								
iwiS	DIN ISO	B_1 h_{14}	B_2 h_{13}	B_3 h_{12}	k_o ⁽¹⁾	c	r_s	s ⁽²⁾
Single chains to DIN 8188								
L 85 A	08 A-1	7,3	-	-	2,6	1,6	13	9
M 106 A	10 A-1	9,0	-	-	3,5	2,0	16	11
M 128 ASL	12 A-1	12,0	-	-	4,2	2,4	19	13
M 128 AG	12 A-1	12,0	-	-	4,2	2,4	19	13
M 1610 A	16 A-1	15,0	-	-	5,5	3,2	26	17
Double chains to DIN 8188								
D 85 A	08 A-2	7,2	21,5	-	2,6	1,6	13	9
D 106 A	10 A-2	8,8	26,9	-	3,5	2,0	16	11
D 128 A	12 A-2	11,8	34,5	-	4,2	2,4	19	13
D 1610 A	16 A-2	14,7	43,9	-	5,5	3,2	26	17
Triple chains to DIN 8188								
Tr 85 A	08 A-3	7,2	-	35,9	2,6	1,6	13	9
Tr 106 A	10 A-3	8,8	-	45,0	3,5	2,0	16	11
Tr 128 A	12 A-3	11,8	-	57,3	4,2	2,4	19	13
Tr 1610 A	16 A-3	14,7	-	73,2	5,5	3,2	26	17
Long pitch chains to DIN 8181								
LR 165 SL	208 B	7,2	-	-	2,7	1,6	13	10,5
LR 206 SL	210 B	9,1	-	-	3,7	2,0	16	12,5
LR 247 SL	212 B	11,1	-	-	4,5	2,4	19	15,0
LR 3211	216 B	16,1	-	-	6,0	3,2	26	19,5
Side bow chains								
L 85 A-SB	-	7,3	-	-	2,6	1,6	13	9
M 106 A-SB	-	9,0	-	-	3,5	2,0	16	11
M 128 A-SB	-	12,0	-	-	4,2	2,4	19	13

¹⁾ Value for k_o , only approx. For 17 teeth and below and application in limit conditions, d_a is calculated in accordance with formula on page 14.

²⁾ Value for s only approx. For application in limit conditions d_s is calculated in accordance with formula on page 15.



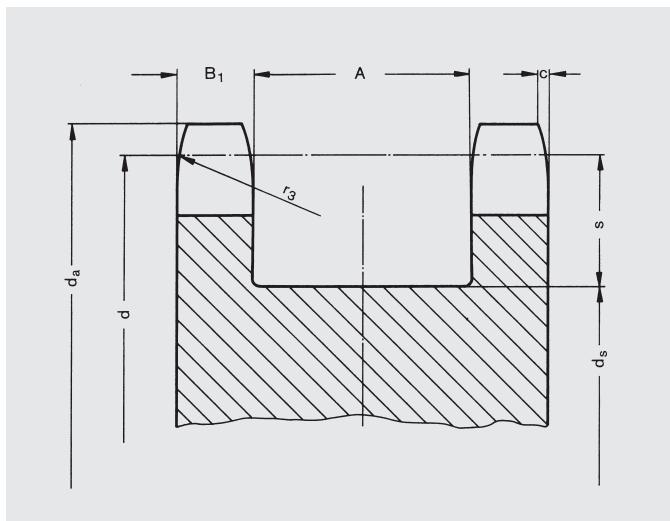
PITCH CIRCLE CORRECTION FOR LONG PITCH CHAINS

In the case of roller chains to DIN 8181 (long pitch type) the chain wheels with normal pitch to DIN 8187/88 are often used, in order to avoid a special design. If on the other hand an accurate wrap around these chain wheels has to be achieved, it is necessary to correct the pitch circle diameter. The tooth forming is carried out on a larger pitch circle diameter. The correction is made in accordance with the following formula:

$$d = \frac{2 \cdot p}{\sin \frac{360^\circ}{z}}$$

p = pitch
 z = no. of teeth
 for chain wheels to DIN 8187/88

CHAIN WHEEL SECTION FOR POWER AND FREE CONVEYOR CHAIN



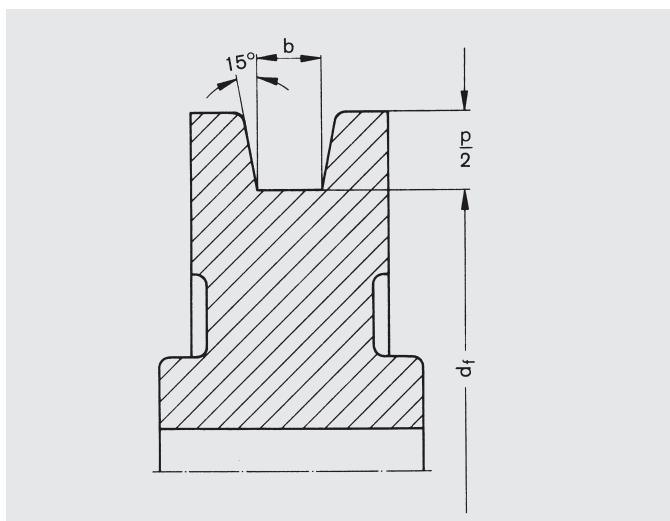
$$d = \frac{p}{\sin \frac{180^\circ}{z}}$$

$$d_s = d - 2s$$

z = no. of teeth
 d_a, c, r_3 see page 16

iwis designation	Pitch p	B ₁	s	A
M 127 SFS/K	19,05	10,8	15	20,7
LR 247 SFS/K	38,1	10,8	15	20,7
M 1611 SFS/K	25,4	11,6	20,5	33,3
LR 3211 SFS/K	50,8	11,6	26	33,3

GUIDE PULLEY FOR HIGH-PERFORMANCE LEAF CHAINS



Sizes/dimensions:

Inner roller width
 b = a₁ · 1,15

Permissible min. root circle diameter

$$d_{f\min} = p \cdot 5$$

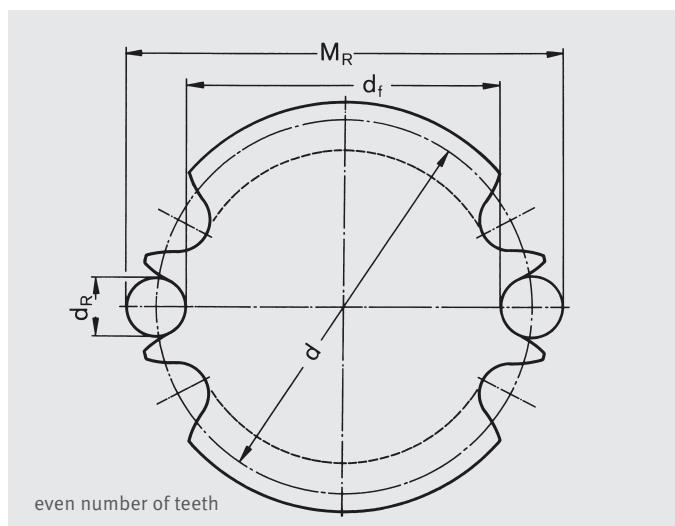
a₁ = width of chain from catalogue
 „Precision chain systems for drive and conveyor purposes“
 p = chain pitch

A 3 Checking chain wheels

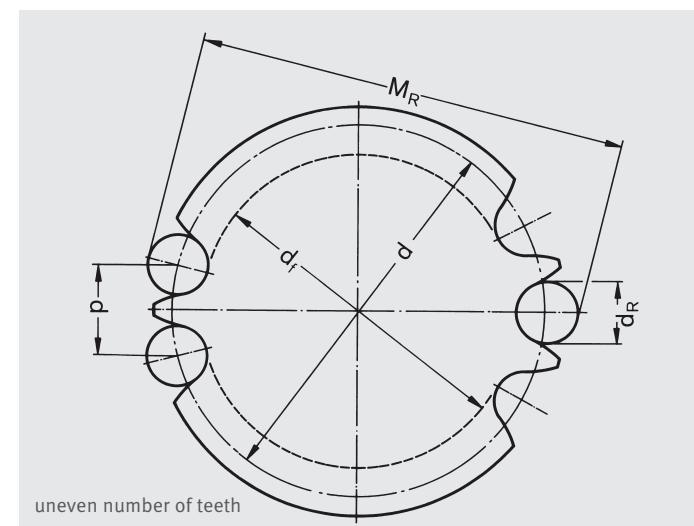
The dimensions indicated on pages 16 to 19 must be checked. This applies also to the surface finish.

The root circle diameter, together with the longitudinal tolerance of the chain provides the initial gearing between the chain and the chainwheel. With an excessively small root circle diameter the chain is located relatively high in the tooth form from the very beginning. Thus the capacity for absorbing wear is reduced. Particular care

should be taken in the manufacture of chain wheels with a small number of teeth. The accuracy of the root circle diameter can be checked by placing a new chain on the machined teeth. If the individual chain links can be lifted out of the teeth the root circle diameter is too small. The check thus described can only be used for low requirements. A more accurate check should be carried out by measurement taken over checking pins as shown – M_R .



$$M_R = d + d_{R \min}$$



$$M_R = d \cdot \cos \frac{90^\circ}{z} + d_{R \min}$$

$d_R = d_1$
but with permissible + 0,01
tolerance – 0

Dimensions d and M_R
see the tables from page 21 onwards

In addition the chainwheels should be checked for run-out and eccentricity. DIN 8196 gives the following recommendations:

Concentricity

Max. discrepancy in concentricity between chain wheel bore and root circle diameter when locating the wheel in the bore: $0,0008 \cdot d_f + 0,08$ or $0,15$ (according to which value is the higher), **but a maximum of 0,76 mm.**

Run-out

Max. run-out allowable between chain wheel bore and face of chain wheel, with the wheel located in the bore is: $0,0009 d_f + 0,08$, **with a maximum of 1,14 mm**

Dimension d – pitch circle diameter and z – no. of teeth – see tables in catalogue "Chain Wheels and Plate Wheels"

Chain wheel bore

Unless otherwise agreed between Manufacturer and Costumer, the chain wheel bores shall have a tolerance range of H 8.

Choice of material

The choice of material depends on the drive conditions, number of teeth, speed and trans-mitted torque. For small chain wheels with fewer than 30 teeth and an average chain speeds up to approx. 7 m/sec. Steel of a higher strength is used. In the case of higher chain speeds tempered, case hardened or flame hardened steel is used. For the manufacture of large chain wheels with more than 30 teeth, grey iron or steel castings are used for average speeds, whereas tempered steel is usual for higher chain speeds.

The performance and longevity of a sprocket is not only determined by the precision of the chain, but also by its quality.

1 Fundamental principles

The suitability of a chain drive for a specific purpose depends upon whether it can sustain the stresses that arise for an assumed period of time. When designing it is necessary to take into account

all influencing factors which in their entirety determine the durability of a chain. The following diagram is designed to provide an idea of the interdependence of the influencing factors.

Load factors

Specific drive factors
Link movement
Drive arrangement
Tension/Guide
Lubrication

Static influencing factors
chain pull centrifugal force

Dynamic influences
Load shocks
Polygon effect
Run in load
Load alternation/ frequency
Dynamic load

Chain factors

- Breaking strength
- Wear resistance
- Durability

Selection factors

Size
Components Total assembly

Materials
Type
Quality
Heat treatment
Surface treatment

Finish
Component manufacture
Accuracy of assembly
Initial lubrication at factory

THERE ARE THREE SIGNIFICANT FACTORS THAT DETERMINE THE OPERATIONAL CHARACTERISTICS OF THE CHAIN:

Breaking strength:

If the load on a chain is increased until the chain breaks, this load will equal the breaking strength and the fracture that occurs is referred to as a forced fracture.

The test can be repeated with reduced loads, until finally there are no more fractures and the fatigue resistance figure has been established.

Bearing pressure, friction travel (page 27) and quality of lubrication are important factors that affect chain wear. The selection can be affected by multiplying the capacity to be transmitted by the following factors.

Wear resistance

The wear in the chain links and the resulting chain elongation determine the permissible load for roller and bush chains. In the case of optimum operating conditions, the expected life is 15.000 operating hours with a max. 2 % chain elongation.

Fatigue resistance

The influencing factors arising from the operational conditions subject the chain to alternating loads. These loads can be recreated on a Pulsator and the cycles required to cause failure can be determined.

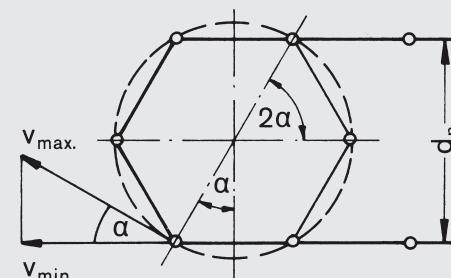
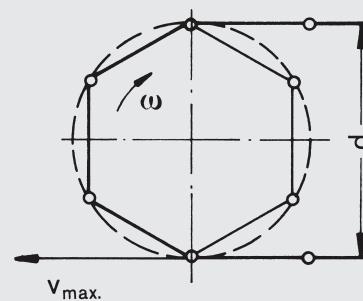
1.1 Influencing factors

Number of teeth

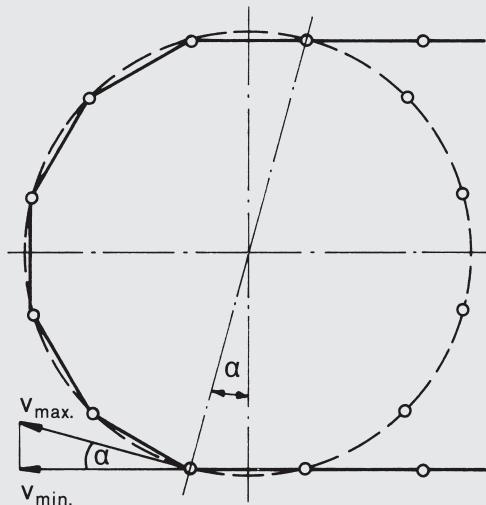
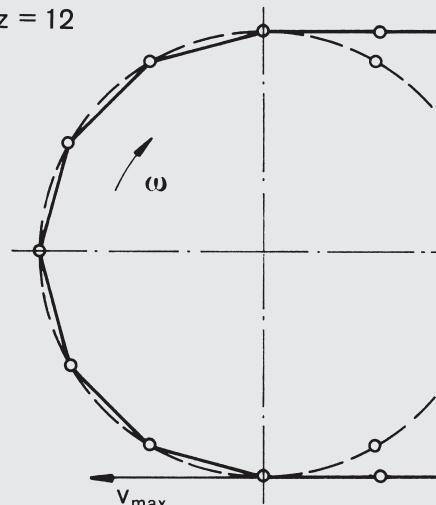
The influence of the number of teeth z in a small chain wheel is taken into account by factor f_1 .

z	11	13	15	17	19	21	23	25
f_1	1,72	1,46	1,27	1,2	1,0	0,91	0,83	0,76

$$z = 6$$



$$z = 12$$



Each chain wheel is a polygon whose number of corners corresponds with the number of teeth. With a constant angular velocity the chain speed v is thus subject to periodic fluctuations between the limit values v_{\max} and v_{\min} (polygonal effect). In this way the chain is alternately accelerated and decelerated and there are increased loads.

$$v_{\min} = \frac{d_n}{2} \cdot \omega = \frac{p \cdot n}{19100 \cdot \tan \frac{180^\circ}{z}}$$

$\left[\frac{m}{s} \right]$

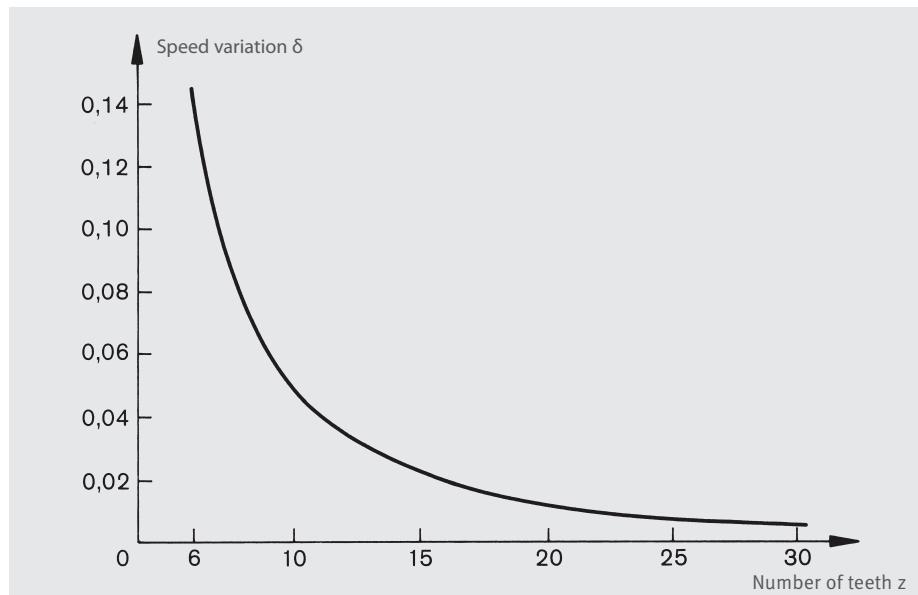
p = Pitch in mm
 n = Rev./Min.
 z = Number of teeth

$$v_{\max} = \frac{d}{2} \cdot \omega = \frac{p \cdot n}{19100 \cdot \sin \frac{180^\circ}{z}}$$

$\left[\frac{m}{s} \right]$

The speed variation due to the alternating speed v_{\max} and v_{\min} is calculated as follows:

$$\delta = \frac{v_{\max} - v_{\min}}{v_{\text{mittel}}}$$



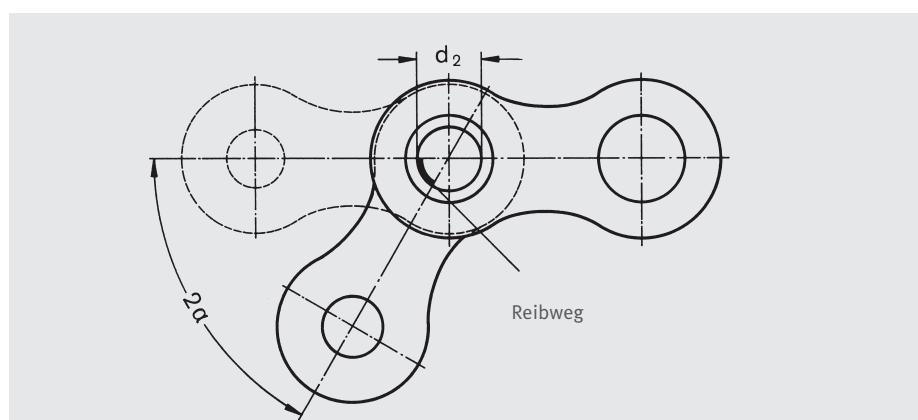
The speed variation is only dependent on the number of teeth z . It increases with the number of teeth $z < 19$ to a considerable extent. This is the reason why small numbers of teeth, particularly in conjunction with higher speeds should be avoided. With $z > 19$ the speed variation approaches but does not meet the datum (zero) line asymptotically, that is the polygonal effect is without any influence from $z = 19$ onwards.

When the chain runs on the chainwheel the link angle is as follows: Consequently the deflection (angle of friction) increases with a decreasing number of teeth and wear increases. The friction travel is calculated as follows: d_2 = Diameter of bearing pin in mm

$$2\alpha = \frac{360^\circ}{z}$$

$$s = \frac{d_2 \cdot \pi}{z}$$

[mm]



The lower the number of teeth the lower the permissible bearing pressure and the higher the poly-gonal effect.

A Speed – Chain speed

As speed n of the driving wheel increases, the number of chain revolutions increases correspondingly. Each link is deflected more frequently and thus the friction travel and consequently the wear increases. In order to reach the desired durability of 15.000 operating hours with a max. of 2 % chain elongation; it is necessary to reduce the bearing pressure.

The number of chain revolutions per minute is

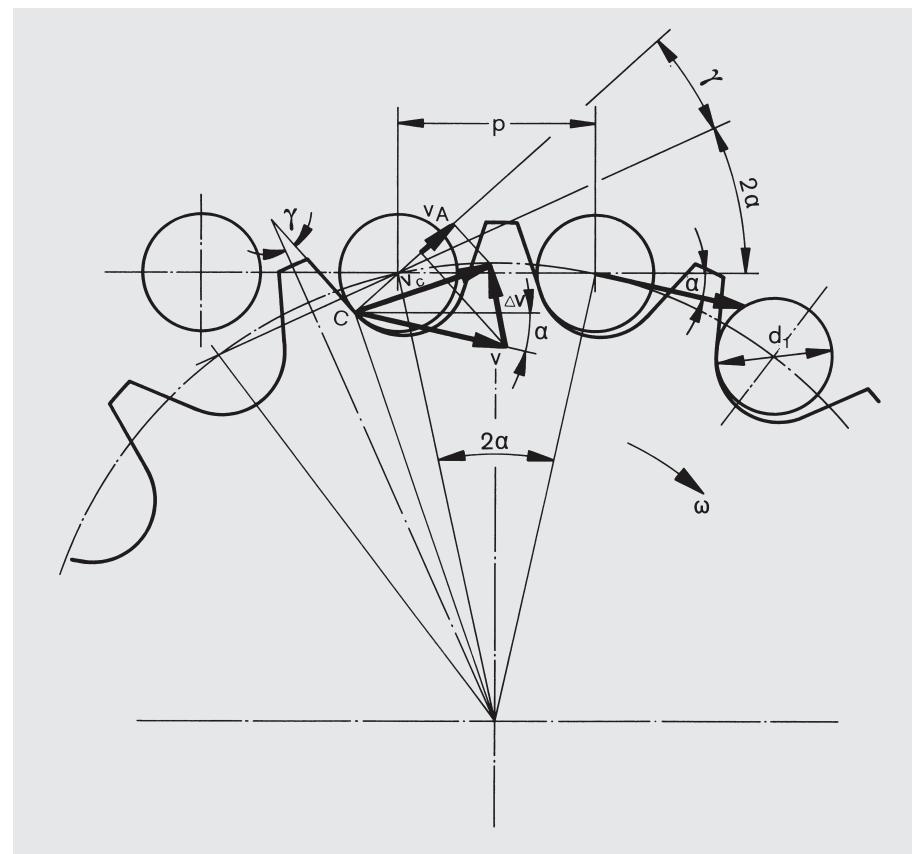
$$\frac{n_1 \cdot z_1}{X} \text{ bzw. } \frac{n_2 \cdot z_2}{X}$$

X = Number of links

Chain speed in meters per second

$$v = \frac{d \cdot n \cdot \pi}{60000} \quad [\frac{m}{s}]$$

d = Pitch circle diameter in mm



As the chain speed increases the permissible bearing pressure must be reduced.

20 m/s should be considered as the maximum chain speed, with 30 m/s under certain circumstances. These figures drop considerably with an increase in pitch size. The chain speed is a decisive factor for the impact speed v_A of the chain wheel against the chain roller, as can be seen from the formula:

$$v_A = \frac{\pi \cdot n \cdot p}{30000} \cdot \sin\left(\frac{360}{z} + \gamma\right)$$

[\frac{m}{s}]

γ = angle of pressure

According to chain size a limit value of approx. 4 m/s is acceptable for v_A . A high impact speed causes high impact energy with a corresponding load on the chain rollers. With a given chain speed v the impact speed is to be kept low by means of a large number of teeth z .

As the chain gears on the wheel the chain rollers impact on the teeth with a shock. The kinetic energy of the impacting mass has to be absorbed by the roller.

Impact energy E_A :
in Newtonmeters

$$E_A = \frac{q \cdot p}{2000} \cdot v_A^2 \quad [\text{Nm}]$$

Impact force F_A :
in Newtons

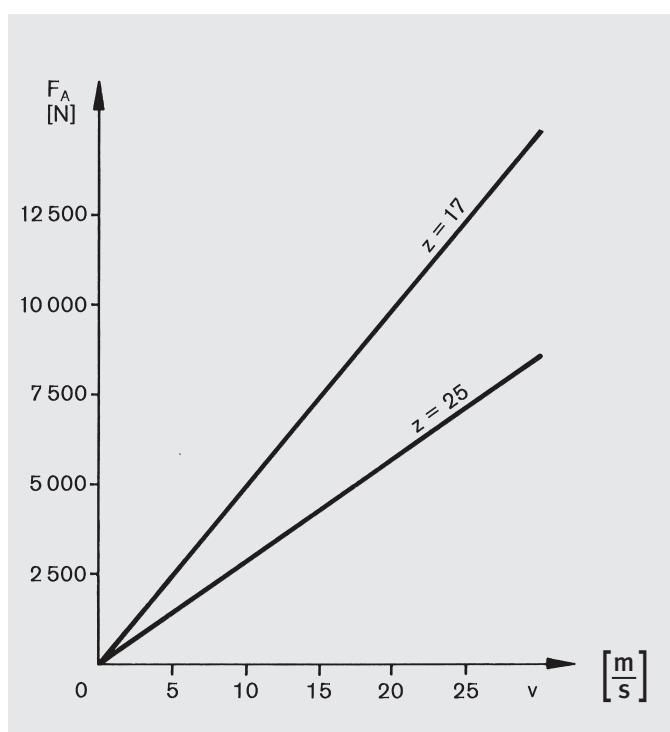
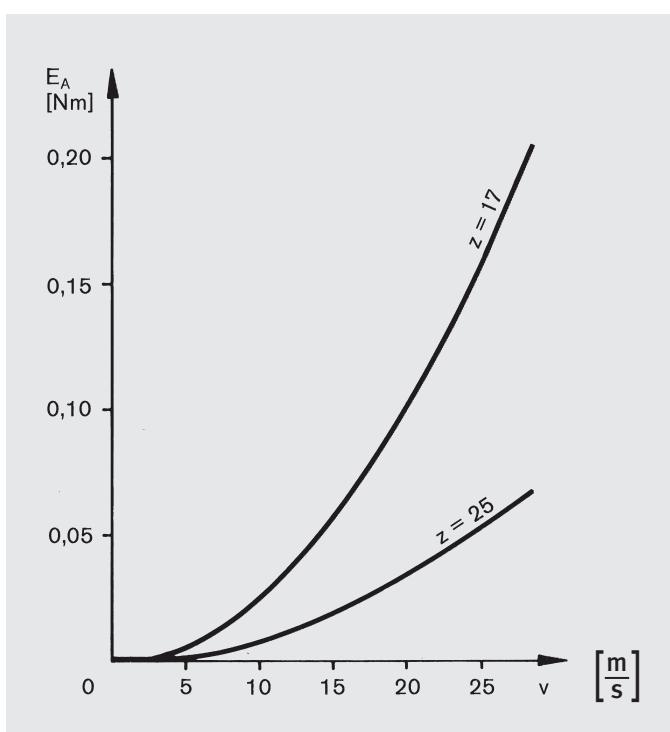
$$F_A = \sqrt{\frac{q \cdot p \cdot b_z \cdot E}{3}} \cdot v_A \quad [\text{N}]$$

The impact force F_A is absorbed as flank pressure. With a higher speed, and in particular with a low number of teeth z it requires a high degree of flank strength (high degree of surface hardness).

b_z = Width of teeth in mm

q = Weight of chain in $\frac{\text{kg}}{\text{m}}$

E = Modulus of elasticity $\frac{\text{N}}{\text{mm}^2}$

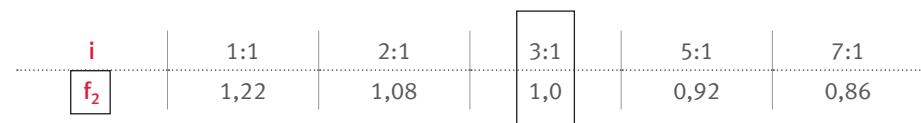


The above diagrams show the impact energy and force in the case of a $1/2 \times 5/16$ " chain, **iwis** reference L 85, depending on speed and number of teeth.

Layout of chain drives

Ratio

Effect of ratio i



When $i = 1:1$ the friction travel is identical on both chain wheels.

$$\frac{d_2 \cdot \pi}{z_1} = \frac{d_2 \cdot \pi}{z_2}$$

$$\frac{d_2 \cdot \pi}{z_1} \text{ und } \frac{d_2 \cdot \pi}{z_2}$$

wodurch der Gesamtreibweg geringer wird.

The higher the ratio the higher the permissible bearing pressure.

The table quotes for i_{max} 7:1. This ratio should only be used in extreme cases and with a very slow running chain drive. As a result of the large arc of contact at the large

chain wheel and the high number of teeth in mesh, the chain on the non tensioned side will not engage positively. In this case a ratio of 4:1 should not be exceeded.

Shock factor

Effect of shock factor Y



Many chains are subjected to shock loads whose size depends on the type and performance of the driving and driven machines. These shocks lead to an increased load in the chain compared with a shockfree operation.

When designing the chain drive, this shock loading, which represents an increase in the chain pull and affects in particular the durability, must be taken into consideration.

The following shock factors can be taken as an illustration.

Shock factor Y = 1

For machines with shockfree operation, i.e. machines driven by electric motors, i.e. lathes, drilling machines, etc.

Shock factor Y = 2

For planers and shapers, presses of all types, weaver's looms, continuous conveyors, etc.

For more detailed information see table on page 27

Shock factor Y = 3

for twin-cylinder piston pumps, mixing drums, stampers, lifting gears etc.

Shock factor Y = 4

for single-stage centrifugal compressors, etc.

Shock factors Y for chain drives (Examples)

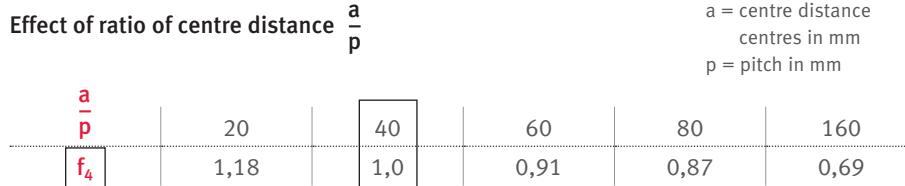
The figures given are mean values with a centre distance $a = 40 \times$ no. of pitches
 Allowances have to be made for unfavourable conditions.

Equipment driven

		Driving Machine							
		Elektromotoren	slow	Combustion engines		fast	water turbines		
		1 Zylinder	2 Zylinder	bis 2 Zylinder	4 Zylinder	6 Zylinder und darüber	schnell	langsam	Dampfturbinen
									Kolben-Dampfmaschinen
Lathes, drilling machines		1							
Milling machines		1,5							
Planing machines		2,3							
Shaping machines		2							
Drawing machines		1,8							
Presses	hydraulic	1,8		2,8	2,5	2,2			
	eccentric	2,5							
	toggle	2							
Woodworking machines		1,8	4,5	4	3,7	3	2,5	3,5	3,5
Weaving looms		2							2
Knitting machines	rotating	1,5							
	reciprocating	2							
Spinning machines		1,5							1,5
Piston compressors	single stage	2,5		5	4,5	4	3,5		
	twin stage	2		4,5	4	3,5	3		
Centrifugal compressors	single stage	1,6	4	3,2	3	2,5	2		
	twin stage	1,3	3	2,7	2,5	2	1,6		
Blowers		1,5		3	2,7	2,5	2		
Fans		2,5		3,7				3,5	2,5
Piston	1 cylinder	2	5	4	3,5	3	2,6	2,5	3,5
	2 cylinder	1,8	4	3,5	3	2,7	2,3	2,2	2,7
Centrifugal pumps		1,5	3	2,8	2,5	2,2	2		2,5
Rolling mills	via gearbox	2,5							
	direct	3							
Press rollers		2							2
Ball mills		1,8							1,8
Tube mills		2							2
Hammer mills		2,5		5	4,5	4	3,5		2,5
Calendar mills	via gearbox	2,5							
	direct	3							
Cellulose grinders		1,8					2,2	3	3,5
Oscillating screens		2		4	3,5	3,2	2,8		4
Stampers		2	5	4	3,5	3,2			
Mixers		1,7	4	3,2	3	2,5	2		
Excavators		3		5	4,5	4			5
Bodenfräse		5	4,5	4					
Agitators		1,6							1,6
Continous conveyors for bulk material		1,5	3	2,8	2,5	2,2	2		2,8
Continous conveyors for indiv. items		2	4	3,5	3	2,7	2		1,5
Lifting gears		2,5	5	4	3,5	3	2,6		
Fork lift trucks			3		4,5	3,5			
Winch drives		2,5							
Generators	Large installation	1		2			1,2	1,5	1
	Small installation	1,5		2,8			1,7	2,5	1,5
Transmissionen lines (driven)		1,5			2,3	2	2	2,5	1,5
									2,5
									1,5

Centre distance

Effect of ratio of centre distance $\frac{a}{p}$



a = centre distance
centres in mm
p = pitch in mm

If the shaft centre distance is increased, the chain must be increased in length and the number of chain rotations is therefore reduced.

Consequently individual chain links are deflected less frequently, therefore the total friction travel and the wear must be reduced.

A shaft centre distance should be chosen to provide an even number of chain links. A chain with an uneven number of links makes it necessary to use a cranked link, which reduces the chain breaking strength by 20 %.

The greater the centre distance the higher the permissible bearing pressure.

Lubrication

Effect of lubrication f_5

		Chain speed v in $\frac{m}{s}$	< 4	4-7	> 7
f_5	Lubrication	Perfect	1,0	1,0	1,0
		Inadequate with clean conditions	1,4	2,5	not permissible
		Inadequate with unclean conditions	2,5	4,0	
		None	5,0	not permissible	

Suitable lubrication is an important condition for the durability of a chain whose individual links perform like friction bearings carrying out a pivoting movement. An efficient lubrication system should therefore

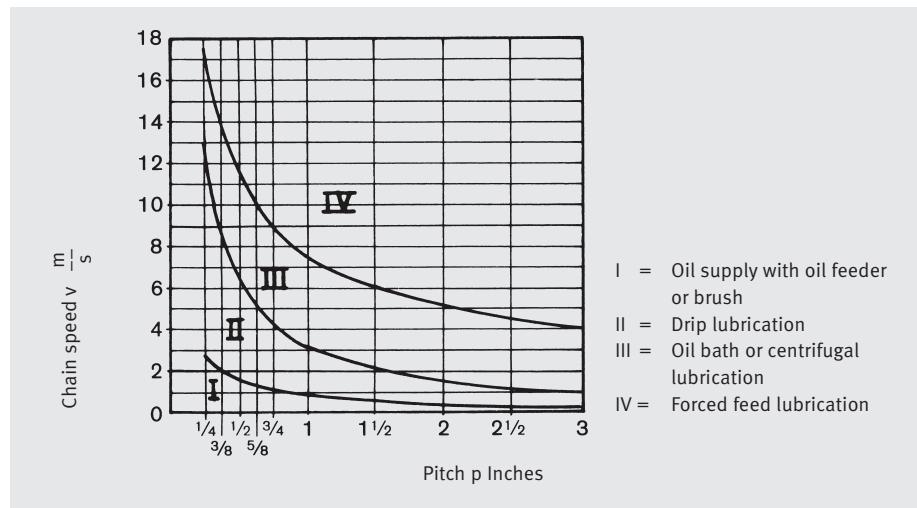
be used as a matter of course, to ensure that the lubrication film in the link remains intact, thus avoiding unlubricated movements causing a high degree of wear. With inadequate lubrication and un-clean oper-

ating conditions the transmittable power is reduced by up to 20 %. Thus the efficiency of the chain is reduced more dramatically than by any other factor.

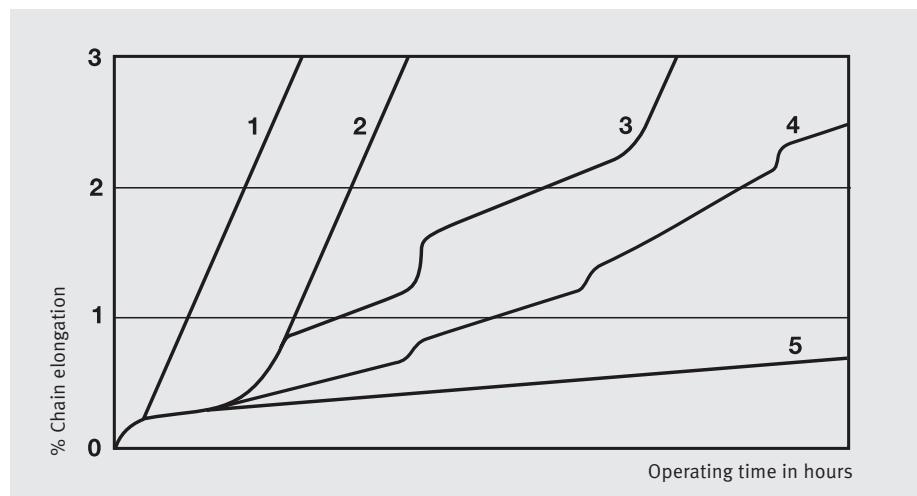
Transmittable power

Chain speed	perfect lubrication	inadequate lubrication		
		clean conditions	unclean	without lubrication
up to 4 $\frac{m}{s}$	100 %	70%	40 %	20 %
up to 7 $\frac{m}{s}$		40%	25 %	not permissible

Types of lubrication



If adequate lubrication is not possible, an oversized chain must be selected, unless a shorter working life is acceptable, as an alternative. The most suitable lubrication system depends also on the chain speed.



Chain elongation compared with operating time and various lubrication conditions is illustrated by the following graph:

Graph 1

Dry running, heavy wear, deterioration of chain within the shortest possible time.

Graph 2

One single lubrication, delayed wear until lubrication is exhausted.

Graph 3

Occasional dry running with manual lubrication, if lubrication intervals are neglected.

Graph 4

Faulty lubrication, irregular wear caused by low quality, unclean, unsuitable or insufficient lubrication.

Graph 5

Complete lubrication, considerable reduction of wear, highest guarantee for long chain life.

The permissible bearing area pressing is directly related to the effectiveness of the lubrication.

A Multi shaft drives

Where more than two shafts are driven by a chain, the power should be increased by the factor f_6 . The use of additional shafts increases the friction travel between chain pin and bush by

$$\frac{d_2 \cdot \pi}{z_1} + \frac{d_2 \cdot \pi}{z_2} + \frac{d_2 \cdot \pi}{z_3} + \dots$$

during one chain revolution.

Consequently, factor f_6 should be taken into account for the bearing pressure.

$$f_6 = \sqrt[3]{\left(\frac{\frac{1}{z_1} + \frac{1}{z_2} + \frac{1}{z_3} + \dots}{0,584} \right) X} \cdot 10^3$$

X = Number of links.

If the number of shafts is increased, the permissible bearing pressure is reduced.

SUMMARY

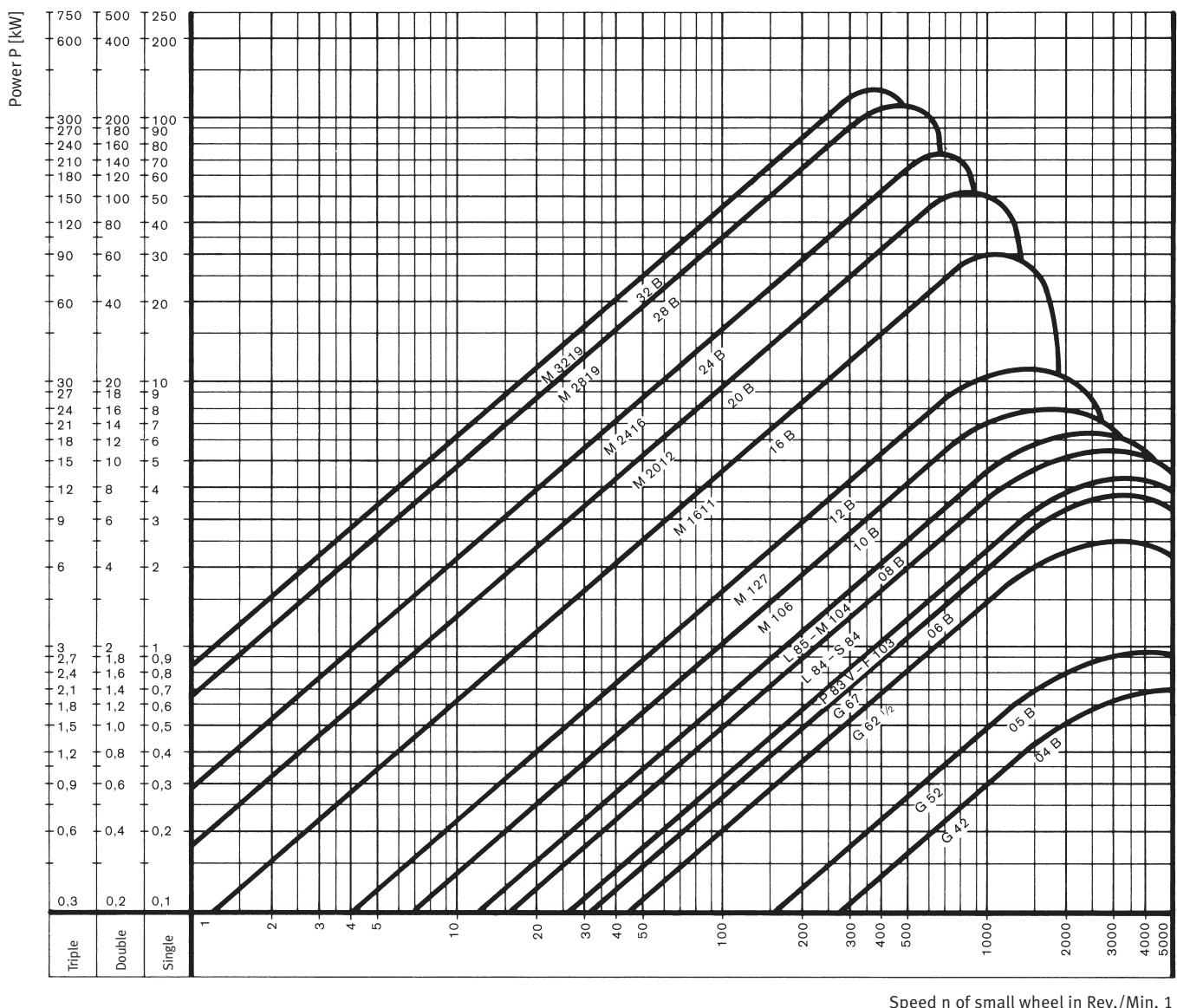
The previously mentioned factors f_1-f_6 determine significantly the permissible bearing pressure.

Relevant determining factors are given in the table on page 35.

2 Chain calculation

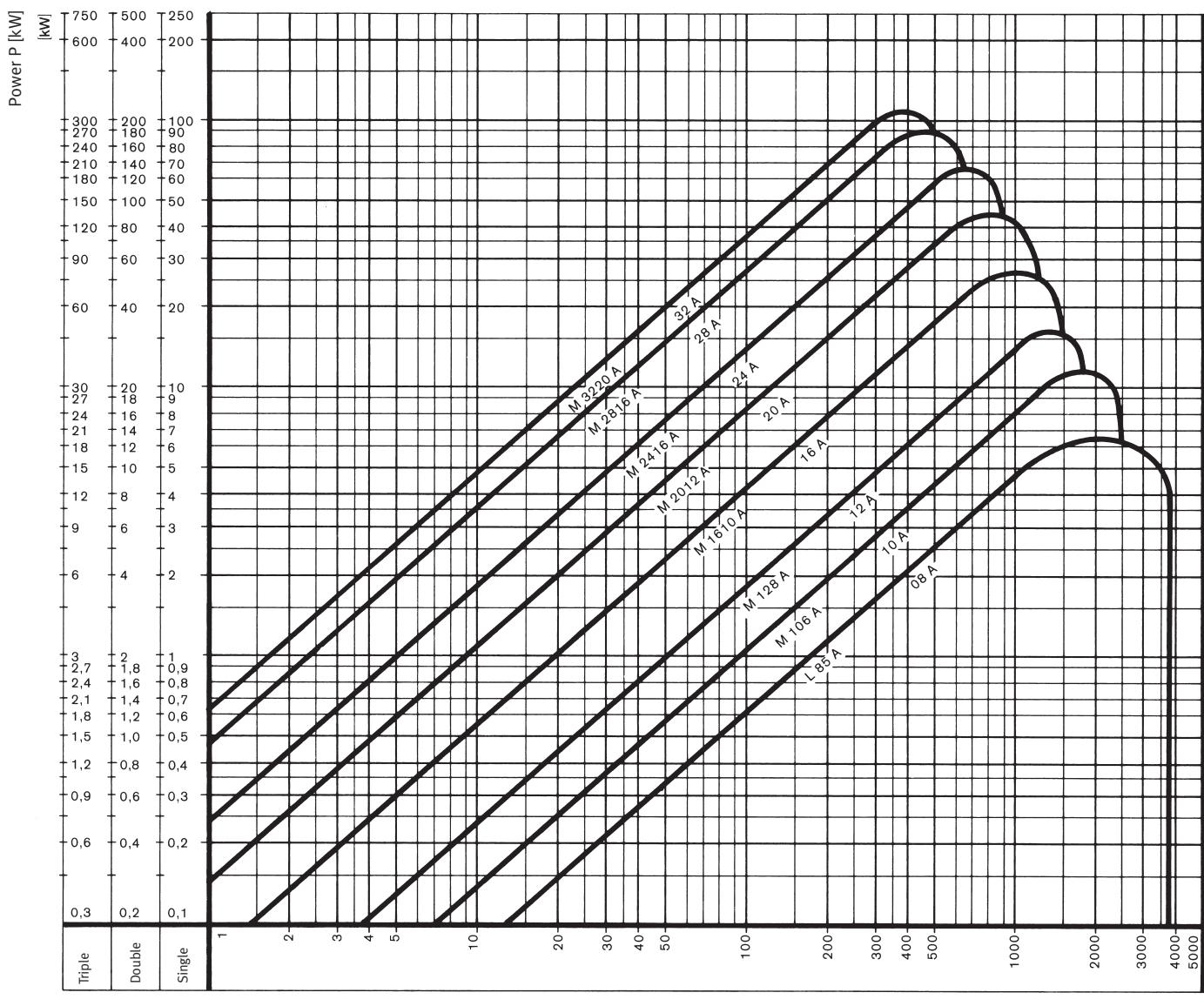
2.1 Pre-selection

BRITISH STANDARD CHAINS PERFORMANCE DIAGRAM DIN 8187



2.1 Pre-selection

AMERICAN STANDARD CHAINS PERFORMANCE DIAGRAM DIN 8188



Speed n of small wheel in Rev./Min. 1

Initial selection by performance diagram

The plotting of the performance curve was based on the following initial values:

Number of teeth of small chain wheel $z_1 = 19$,
 ratio $i = 3:1$, shockfree operation
 $Y = 1$, centre distance $40 \times p$
 (p = pitch), perfect lubrication, 2 shafts.

Since these conditions are met in very few cases only, the power to be transmitted P will be corrected to the diagram power P_D , taking into consideration the variable factors f_1 to f_6 .

To pre-select a chain the following factors should be taken into account:

Factors:

f_1 Effect of the number of teeth of the small chain wheel z

z	11	13	15	17	19	21	23	25
f_1	1,72	1,46	1,27	0,12	1,0	0,91	0,83	0,76

f_2 Effect of ratio i

i	1:1	2:1	3:1	5:1	7:1
f_2	1,22	1,08	1,0	0,92	0,86

f_3 Effect of Shock factor Y

Y	1	2	3	4
f_3	1	1,37	1,59	1,72

f_4 Effect of ratio of centre distance $\frac{a}{p}$

$\frac{a}{p}$	20	40	60	80	160
f_4	1,18	1,0	0,91	0,87	0,69

f_5 Effect of lubrication

f_5	Lubrication	Chain speed v in $\frac{m}{s}$			f_5
		< 4	4-7	> 7	
perfect		1,0	1,0	1,0	
inadequate with clean conditions		1,4	2,5	unacceptable	
inadequate with unclean conditions		2,5	4,0		
none		5,0	unacceptable		

f_6 Effect of number of chain wheels

$$f_6 = \sqrt[3]{\left(\frac{1}{Z_1} + \frac{1}{Z_2} + \frac{1}{Z_3} + \dots \right) \frac{10^3}{X}} \\ 0,584$$

$f_6 = 1$ for drive comprising two shafts

Overall factor

$$P_D = P \cdot f_G$$

$$f_G = f_1 \cdot f_2 \cdot f_3 \cdot f_4 \cdot f_5 \cdot f_6$$

Pre-selection of a chain from DIN 8187 performance curve – Example:

In the performance curve the power (0,25 kW) crosses the vertical speed line (40 min^{-1}) in the upper area of chain L 85. This chain would be adequate, without taking into account the various factors.

Determining diagram power P_D and factor f_G :

The factors are taken from the adjacent tables. Intermediate values are interpolated.

No. of teeth chosen for small chain wheel

$$z_1 = 17 \quad f_1 = 1,12$$

Ratio

$$i = 4 \quad f_2 = 0,96$$

Assumed shock factor

$$Y = 2 \quad f_3 = 1,37$$

Ratio of centre distance

$$\frac{a}{p} = \frac{380}{12,7} = 30$$

$$f_4 = 1,09$$

Perfect lubrication

$$f_5 = 1$$

Chain drive with 2 chain wheels

$$f_6 = 1$$

$$f_G = 1,12 \cdot 0,96 \cdot 1,37 \cdot 1,09 \cdot 1 \cdot 1 = 1,60$$

$$P_D = P \cdot f_G = 0,25 \cdot 1,60 = 0,40 \text{ kW}$$

If $P_D = 0,40 \text{ kW}$ is checked at $n = 40 \text{ min}^{-1}$ in the power curve, it will be found that the L 85 chain is not strong enough. The next stronger chain M 106 is selected and verified by calculation.

For calculation examples see page 36.

2.2 Calculation

Summary of formulae

Item to be calculated	Des.	Formula or reference		Item to be calculated	Des.	Formula or reference	
Power transmitted	P	$P = \frac{F \cdot v}{1000} = \frac{M \cdot n}{9550}$	kW	Determining factors for bearing pressure	p_v	see table on page 35	$\frac{N}{cm^2}$
Diagram performance	P_D	$P_D = P \cdot f_G$	kW	Friction travel factor	l	see table on page 35	--
Influencing factors	f_G	$f_G = f_1 \cdot f_2 \cdot f_3 \cdot f_4 \cdot f_5 \cdot f_6$	--	Breaking load of chain	F_B	see table on page 12	N
Torque	M	$M = \frac{9550 \cdot P}{n} = \frac{F \cdot d}{2000}$	Nm	Static breaking load safety factor	γ_{st}	$\gamma_{st} = \frac{F_B}{F_G}$	--
Speed	n	$n = \frac{60000 \cdot v}{d \cdot \pi} = \frac{60000 \cdot v}{z \cdot p}$	min ⁻¹	Dynamic breaking load safety factor	γ_d	$\gamma_d = \frac{F_B}{F_G \cdot Y}$	--
Ratio	i	$i = \frac{n_1}{n_2} = \frac{z_2}{z_1}$	--	Shock factor	Y	see table on page 27	--
Pitch circle diameter	d	$d = \frac{p}{\sin 180^\circ / z}$	mm	No. of links	X	$X = 2 \frac{a}{p} + \frac{z_1 + z_2}{2} + \frac{A \cdot p}{a}$	--
Chain speed	v	$v = \frac{z \cdot n \cdot p}{60000} = \frac{d \cdot \pi \cdot n}{60000} = \frac{1000 \cdot P}{F}$	$\frac{m}{s}$	Pitch	p	see table on page 12	mm
Chain pull	F	$F = \frac{1000 \cdot P}{v} = \frac{2000 \cdot M}{d}$	N	Compensating factor	A	$A = \left(\frac{z_2 - z_1}{2\pi} \right)^2$ see table on page 41	--
Centrifugal force	F_f	$F_f = q \cdot v^2$	N	Centre distance $z_1 = z_2$	a	$a = \frac{X - z}{2} \cdot p$	mm
Total pull	F_G	$F_G = F + F_f$	N	Centre distance z_1 not equal to z_2	a	$a = [2X - (z_1 + z_2)] \cdot C \cdot p$	mm
Chain weight per metre	q	see table on page 12	$\frac{kg}{m}$	Factor for centre distance	C	see table with calculation on page 41	--
Bearing pressure, calculated	p_r	$p_r = \frac{F_G}{f}$	$\frac{N}{cm^2}$	Impact speed	v_A	$v_A = \frac{\pi \cdot n \cdot p}{30000} \cdot \sin \left(\frac{360^\circ}{z} + \gamma \right)$	$\frac{m}{s}$
Bearing pressure, permissible	p_{zul}	$p_{zul} = \frac{p_v \cdot \lambda}{f_5 \cdot f_6}$	$\frac{N}{cm^2}$	Angle of pressure	γ		Grad
Bearing area	f	$f = b_2 \cdot d_2$ see table on page 12	cm ²				

Determining factors for bearing pressure p_v in N/cm²

Chain speed v in $\frac{m}{s}$	No. of teeth of small wheel														
	11	12	13	14	15	16	17	18	19	20	21	22	23	24	≥ 25
0,1	3020	3060	3110	3160	3205	3235	3255	3285	3335	3365	3385	3415	3430	3460	3480
0,2	2755	2795	2825	2875	2920	2940	2970	3000	3040	3060	3080	3110	3130	3160	3175
0,4	2650	2685	2725	2775	2815	2835	2855	2895	2920	2940	2960	2990	3010	3040	3060
0,6	2530	2570	2600	2650	2685	2705	2725	2765	2795	2815	2835	2855	2875	2905	2920
0,8	2440	2480	2510	2560	2600	2620	2630	2665	2695	2715	2735	2755	2775	2805	2825
1,0	2335	2375	2405	2440	2470	2490	2510	2540	2570	2590	2610	2630	2650	2665	2685
1,5	2245	2285	2315	2355	2385	2405	2420	2450	2480	2500	2520	2540	2560	2580	2600
2,0	2165	2195	2225	2265	2305	2325	2335	2365	2395	2410	2420	2440	2460	2480	2500
2,5	2090	2120	2150	2185	2215	2235	2245	2275	2305	2325	2335	2355	2395	2420	2450
3	2010	2040	2070	2100	2130	2150	2165	2195	2215	2245	2275	2305	2335	2375	2410
4	1705	1795	1885	1960	2030	2060	2090	2120	2140	2175	2215	2255	2295	2335	2375
5	1375	1520	1655	1735	1805	1875	1930	1970	2010	2060	2110	2140	2165	2200	2235
6	1030	1206	1385	1510	1610	1695	1775	1845	1910	1950	2000	2030	2070	2100	2140
7	835	980	1130	1255	1375	1480	1590	1705	1815	1835	1865	1900	1940	1980	2020
8	-	785	1000	1090	1175	1285	1395	1530	1665	1705	1745	1785	1835	1875	1920
10	-	-	795	885	1000	1090	1177	1295	1400	1430	1470	1540	1610	1670	1735
12	-	-	-	-	805	890	1050	1145	1235	1275	1325	1385	1450	1510	1570
15	-	-	-	-	-	-	875	950	1030	1080	1130	1185	1245	1305	1375
18	-	-	-	-	-	-	-	-	865	940	1030	1090	1155	1215	1275

Guide figures below the line should be avoided.

Friction travel factor λ

Shock factor	Chains to DIN	$a = 20 \cdot p$ $z_2 : z_1$					$a = 40 \cdot p$ $z_2 : z_1$					$a = 60 \cdot p$ $z_2 : z_1$					$a = 80 \cdot p$ $z_2 : z_1$					$a = 160 \cdot p$ $z_2 : z_1$				
		1:1	2:1	3:1	5:1	7:1	1:1	2:1	3:1	5:1	7:1	1:1	2:1	3:1	5:1	7:1	1:1	2:1	3:1	5:1	7:1	1:1	2:1	3:1	5:1	7:1
1	8187, 8188, 8154	0,70	0,79	0,85	0,92	0,99	0,82	0,93	1,00	1,09	1,16	0,90	1,02	1,10	1,20	1,28	0,94	1,06	1,15	1,25	1,34	1,19	1,35	1,45	1,58	1,68
	8181	0,56	0,63	0,68	0,74	0,79	0,66	0,74	0,80	0,87	0,93	0,72	0,82	0,88	0,96	1,03	0,75	0,85	0,92	1,00	1,07	0,95	1,08	1,16	1,26	1,35
2	8187, 8188, 8154	0,51	0,57	0,62	0,67	0,72	0,60	0,68	0,73	0,79	0,85	0,66	0,74	0,80	0,87	0,93	0,69	0,78	0,84	0,91	0,98	0,87	0,99	1,06	1,15	1,23
	8181	0,41	0,46	0,50	0,54	0,58	0,48	0,54	0,58	0,63	0,68	0,53	0,59	0,64	0,70	0,74	0,55	0,62	0,67	0,73	0,78	0,70	0,79	0,85	0,93	0,99
3	8187, 8188, 8154	0,44	0,49	0,53	0,58	0,62	0,52	0,59	0,63	0,69	0,73	0,57	0,64	0,69	0,75	0,80	0,59	0,67	0,72	0,78	0,84	0,75	0,85	0,91	0,99	1,06
	8181	0,35	0,39	0,42	0,46	0,50	0,42	0,47	0,50	0,55	0,58	0,46	0,51	0,55	0,60	0,64	0,47	0,54	0,57	0,62	0,67	0,60	0,68	0,73	0,80	0,85
4	8187, 8188, 8154	0,40	0,45	0,49	0,53	0,57	0,48	0,54	0,58	0,63	0,67	0,53	0,59	0,64	0,69	0,74	0,55	0,62	0,67	0,73	0,78	0,69	0,78	0,84	0,92	0,97
	8181	0,32	0,36	0,39	0,42	0,46	0,38	0,43	0,46	0,50	0,54	0,42	0,47	0,51	0,55	0,59	0,44	0,50	0,54	0,58	0,62	0,55	0,62	0,67	0,73	0,78

2.3 Examples of calculations

Example 1:

A conveyor belt driven by a roller chain from a geared motor.

a) Preselection of chain from DIN 8187 power diagram, page 31

The intersection between the horizontal power curve (for 0,96 kW) and the vertical speed curve (for 20 min⁻¹) is situated in the upper area of the chain M 1611. This chain would be adequate without taking into consideration the various factors.

Establishing diagram power P_D

For factors see page 33

Number of pinion teeth, selected

$$z_1 = 17 \quad f_1 = 1,12$$

Ratio n₁ : n₂

$$i = 2 \quad f_2 = 1,08$$

Shock factor, assumed

$$Y = 2 \quad f_3 = 1,37$$

Ratio for centre distance

$$\frac{a}{p} = \frac{1900}{25,4} = 75 \quad f_4 = 0,88$$

Lubrication, perfect

$$f_5 = 1$$

Drive with 2 chain wheels

$$f_6 = 1$$

$$f_G = f_1 \cdot f_2 \cdot f_3 \cdot f_4 \cdot f_5 \cdot f_6$$

$$= 1,12 \cdot 1,08 \cdot 1,37 \cdot 0,88 \cdot 1 \cdot 1 \\ = 1,46$$

$$P_D = P \cdot f_G$$

$$= 0,96 \cdot 1,46 \\ = 1,4 \text{ kW}$$

If P_D is located again in the power diagram at n = 20 Rev./Min., it will be found that chain M 1611 is unsuitable. The next stronger chain M 2012 is selected.

b) Re-calculating selected chain Roller chain M 2012

Pitch p = 31,75 mm

Breaking load F_B = 100 000 N

Bearing area f = 2,94 cm²

Chain weight q = 3,32 kg/m

Chain wheel

Pitch circle diameter at

$$z_1 = 17 \quad d = 172,79 \text{ mm}$$

1) Chain speed:

$$v = \frac{d \cdot \pi \cdot n_1}{60000} = \frac{172,79 \cdot \pi \cdot 20}{60000} = 0,18 \frac{\text{m}}{\text{s}}$$

2) Chain pull:

$$F = \frac{1000 \cdot P}{v} = \frac{1000 \cdot 0,96}{0,18} = 5333 \text{ N}$$

3) Centrifugal force:

$$F_f = q \cdot v^2 = 3,32 \cdot 0,18^2 = 0,11 \text{ N}$$

4) Total pull:

$$F_G = F + F_f = 5333 \text{ N} \quad - \text{Centrifugal force ignored}$$

5) Bearing pressure arithmetic:

$$p_r = \frac{F_G}{f} = \frac{5333}{2,94} = 1813,9 \frac{\text{N}}{\text{cm}^2}$$

6) Bearing pressure permissible:

$$p_{zul} = \frac{p_v \cdot \lambda}{f_5 \cdot f_6} = \frac{3027 \cdot 0,77}{1 \cdot 1} = 2240 \frac{\text{N}}{\text{cm}^2}$$

The arithmetic bearing pressure should not exceed the permissible value.

The approx. Value p_v and the friction travel λ are determined by interpolation from the tables on page 35.

7) Static breaking load safety factor:

$$\gamma_{st} = \frac{F_B}{F_G} = \frac{100000}{5333} = 18,7$$

– higher than the recommended minimum value 7

8) Dynamic breaking load safety factor:

$$\gamma_d = \frac{F_B}{F_G \cdot Y} = \frac{100000}{5333 \cdot 2} = 9,4$$

– higher than the recommended minimum value 5

According to the table for types of lubrication on page 29, manual lubrication is sufficient.

The re-calculation shows that chain M 2012 was selected correctly.

Thus it is possible to establish the exact length of the chain (see page 40).

If space restrictions are present, double or triple strand chains of a smaller pitch could be selected.

2.3 Examples of calculations

Example 2:

Chain drive to a hydraulic pump. For this the following information is available.

Torque	M = 45,7 Nm
Driving Speed	n ₁ = 200 min ⁻¹
Ratio	i = 2
Centre distance	a = ca. 750 mm
Max. permissible external diameter, including chain on wheel: d _A = 70 mm	

a) Pre-selection chain from DIN 8187 power curve, page 31

Power:

$$P = \frac{M \cdot n_1}{9550} = \frac{45,7 \cdot 200}{9550} = 0,96 \text{ kW}$$

The diagram shows that chain L 85 should be used. In view of the higher operating conditions and the maximum diameter restriction on wheel selection preference is given to the Double chain D 67 which has a smaller pitch, but nearly the same breaking load. Furthermore, this provides a sufficient number of teeth with the specified limitation of the chain wheel diameter.

Determining diagram power P_D

Factors, see page 33	$z_1 = 17$	$f_1 = 1,12$
No. of teeth of pinon, selected	$i = 2$	$f_2 = 1,08$
Ratio	$Y = 2$	$f_3 = 1,37$
Shock factor, assumed	$\frac{a}{p} = \frac{750}{9,525} = 78,7$	$f_4 = 0,87$
Ratio for centre distance		$f_5 = 1$
Lubrication, perfect		$f_6 = 1$

Drive with 2 chain wheels

$$f_G = f_1 \cdot f_2 \cdot f_3 \cdot f_4 \cdot f_5 \cdot f_6 = 1,12 \cdot 1,08 \cdot 1,37 \cdot 0,87 \cdot 1 \cdot 1 = 1,44$$

$$P_D = P \cdot f_G = 0,96 \cdot 1,44 = 1,38 \text{ kW}$$

A new check using this calculated power shows that chain D 67 is not adequate. Therefore Triple chain Tr 67 is selected

b) Re-calculating selected chain Roller chain Tr 67

Pitch	p = 9,525 mm
Breaking load	F _B = 29 000 N
Bearing area	f = 0,83 cm ²
Chain weight	q = 1,18 kg/m

Chain wheel

Pitch circle diameter at z₁ = 17 d = 51,84 mm

Checking top diameter d_A including chain

$$d_A = d + g$$

= 51,84 + 8,26 = 60,1 mm – this is smaller than 70 mm

g = height of link plate

1) Chain speed:

$$v = \frac{z \cdot n_1 \cdot p}{60000} = \frac{17 \cdot 200 \cdot 9,525}{60000} = 0,54 \frac{\text{m}}{\text{s}}$$

2) Chain pull:

$$F = \frac{1000 \cdot P}{v} = \frac{1000 \cdot 0,96}{0,54} = 1778 \text{ N}$$

3) Centrifugal force:

$$F_f = q \cdot v^2 = 1,18 \cdot 0,54^2 = 0,34 \text{ N}$$

4) Total pull:

$$F_G = F + F_f = 1778 \text{ N} \quad - \text{Centrifugal force ignored}$$

5) Bearing pressure arithmetic:

$$p_r = \frac{F_G}{f} = \frac{1778}{0,83} = 2142,17 \frac{\text{N}}{\text{cm}^2}$$

6) Bearing pressure permissible:

$$p_{zul} = \frac{p_v \cdot \lambda}{f_5 \cdot f_6} = \frac{2764 \cdot 0,78}{1 \cdot 1} = 2156 \frac{\text{N}}{\text{cm}^2} \quad p_r \text{ smaller than } p_{zul}$$

The approx. value p_v and the friction travel λ are determined by interpolation from the tables on page 35

7) Static breaking load safety factor:

$$\gamma_{st} = \frac{F_B}{F_G} = \frac{29000}{1778} = 16,3$$

– higher than the recommended minimum value 7

8) Dynamic breaking load safety factor:

$$\gamma_d = \frac{F_B}{F_G \cdot Y} = \frac{29000}{1778 \cdot 2} = 8,16$$

– higher than the recommended minimum value 5

According to table on page 29, types of lubrication, manual lubrication is sufficient.

The exact chain length can be established in accordance with item 3, page 40.



3 Determining length of chain

3.1 Number of links and centre distance

Chain drive with 2 shafts

If the chain size has been determined, it is possible to calculate the number of links, the length of the chain and the exact centre distance.

Data required:

Pitch	p
No. of teeth, drive wheel	z_1
No. of teeth, driven wheel	z_2
Approx. centre distance in mm	a

1 Chain wheels with identical numbers of teeth $z_1 = z_2$

No. of links:

$$X = \frac{2a}{p} + z$$

Centre distance:

$$a = \frac{X - z}{2} \cdot p$$

2 Chain wheels with different numbers of teeth $z_1 \neq z_2$

No. of links:

$$X = 2 \frac{a}{p} + \frac{z_1 + z_2}{2} + A \cdot p$$

Compensating factor:

$$A = \left(\frac{z_2 - z_1}{2 \cdot \pi} \right)^2 \quad \text{or from table on page 41}$$

Centre distance:

$$a = [2X - (z_1 + z_2)] \cdot C \cdot p \quad [\text{mm}]$$

C = Factor for centre distance from table on page 41

In most cases the approximate centre distance is given, for which very often an uneven number of links X is obtained. This figure is rounded up to the next even figure, or rounded down, as the case maybe, in order to avoid an uneven number of links. The centre distance is then again calculated with the corrected number of links.

The smallest centre distance for a chain drive consisting of two chain wheels shall always be higher than the arithmetic mean of the outside diameters of both wheels.

With a fixed centre distance and given chain wheel diameter the slack of the chain is compensated by means of a tensioner. See also page 58, drive arrangement.

$$a > \frac{d_{a1} + d_{a2}}{2}$$

Compensating factor A

$z_2 - z_1$	A	$z_2 - z_1$	A	$z_2 - z_1$	A	$z_2 - z_1$	A	$z_2 - z_1$	A
1	0,0253	21	11,171	41	42,580	61	94,254	81	166,191
2	0,1013	22	12,260	42	44,683	62	97,370	82	170,320
3	0,2280	23	13,400	43	46,836	63	100,536	83	174,450
4	0,4053	24	14,590	44	49,040	64	103,753	84	178,730
5	0,6333	25	15,831	45	51,294	65	107,021	85	183,011
6	0,912	26	17,123	46	53,599	66	110,339	86	187,342
7	1,241	27	18,466	47	55,955	67	113,708	87	191,724
8	1,621	28	19,859	48	58,361	68	117,128	88	196,157
9	2,052	29	21,303	49	60,818	69	120,598	89	200,640
10	2,533	30	22,797	50	63,326	70	124,119	90	205,174
11	3,065	31	24,342	51	65,884	71	127,690	91	209,759
12	3,648	32	25,938	52	68,493	72	131,313	92	214,395
13	4,281	33	27,585	53	71,153	73	134,986	93	219,081
14	4,965	34	29,282	54	73,863	74	138,709	94	223,817
15	5,699	35	31,030	55	76,624	75	142,483	95	228,605
16	6,485	36	32,828	56	79,436	76	146,308	96	233,443
17	7,320	37	34,677	57	82,298	77	150,184	97	238,322
18	8,207	38	36,577	58	85,211	78	154,110	98	243,271
19	9,144	39	38,527	59	88,175	79	158,087	99	248,261
20	10,132	40	40,529	60	91,189	80	162,115	100	253,302

Factor for centre distance C

$\frac{X - z_1}{z_2 - z_1}$	F	C	D	$\frac{X - z_1}{z_2 - z_1}$	F	C	D	$\frac{X - z_1}{z_2 - z_1}$	F	C	D
13		0,24 991		2,00		0,24 421		1,33		0,22 968	
12		990	1	1,95		380	41	1,32		912	56
11		988	2	1,90		333	47	1,31		854	58
10		986	2	1,85	20	281	52	1,30		793	61
9	1	983	3	1,80		222	59	1,29		729	64
8		978	5	1,75		156	66	1,28		662	67
7		970	8	1,70		081	75	1,27		593	69
6		958	12	1,68		048	33	1,26		520	73
5		937	21	1,66		013	35	1,25		443	77
4,8		931	6	1,64		0,23 977	36	1,24		361	82
4,6		925	8	1,62		938	41	1,23		275	86
4,4		917	10	1,60		897	43	1,22		185	90
4,2		907	11	1,58		854	47	1,21		090	95
4,0	5	896	13	1,56	50	807	49	1,20	100	0,21 990	106
3,8		883	15	1,54		758	53	1,19		884	113
3,6		868	19	1,52		705	57	1,18		771	119
3,4		849	24	1,50		648	60	1,17		652	126
3,2		825	30	1,48		588	64	1,16		526	136
3,0		795	17	1,46		524	69	1,15		390	145
2,9		778	20	1,44		455	74	1,14		245	155
2,8		758	23	1,42		381	80	1,13		090	167
2,7		735	27	1,40		301	42	1,12		0,20 923	179
2,6		708	30	1,39		259	44	1,11		744	195
2,5	10	678	35	1,38		215	45	1,10		549	213
2,4		643	41	1,37	100	170	47	1,09		336	232
2,3		602	50	1,36		123	50	1,08		104	256
2,2		552	59	1,35		073	51	1,07		0,19 848	284
2,1		493	72	1,34		022	54	1,06		564	
2,0		421		1,33		0,22 968					

Examples for calculating z_1 not equal to z_2

The following is given for a chain drive:

Approx. centre distance

$$a = 370 \text{ mm}$$

No. of teeth, drive wheel

$$z_1 = 19$$

No. of teeth, driven wheel

$$z_2 = 60$$

Pitch

$$p = 25,4 \text{ mm}$$

a) No. of links

$$X = 2 \frac{a}{p} + \frac{z_1 + z_2}{2} + \frac{A \cdot p}{a}$$

$$z_2 - z_1 = 41$$

from table on page 41 A = 42,58

$$X = 2 \cdot \frac{370}{25,4} + \frac{19 + 60}{2} + \frac{42,58 \cdot 25,4}{370}$$

$$X = 71,55$$

The Value X = 71,55 is rounded

up to the even figure of X = 72.

The exact centre distance is then calculated with this value.

b) Centre distance $a = [2X - (z_1 + z_2)] \cdot C \cdot p$

Establishing value C from table on page 41 and interpolation:

$$1. \quad \frac{X - z_1}{z_2 - z_1} = \frac{72 - 19}{60 - 19} = 1,29268$$

$$2. \quad \text{Nearest table figure} = 1,29$$

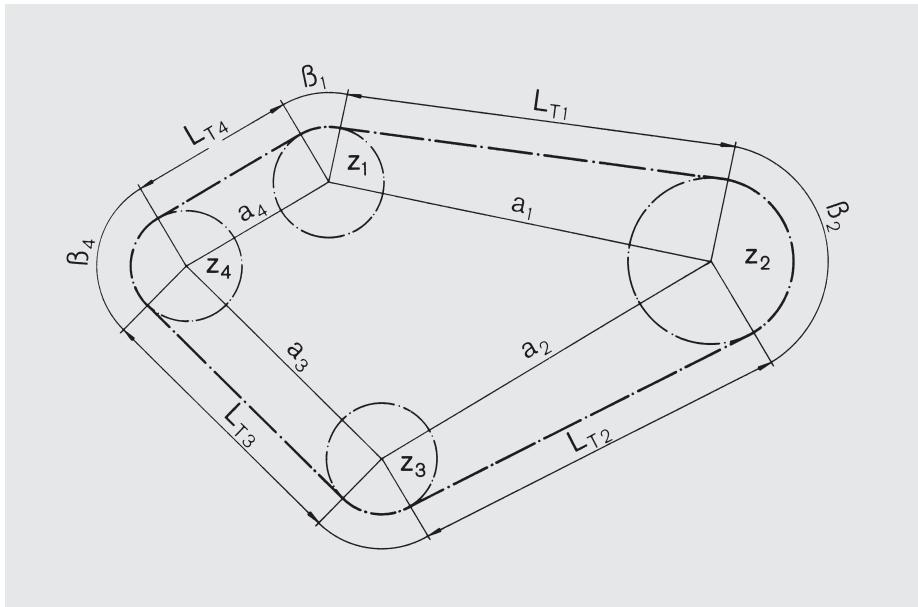
$$3. \quad \text{Residual value } R = 1,29268 - 1,29 = 0,00268$$

$$\begin{aligned} 4. \quad \text{Interpolated value} &= I = D \cdot F \cdot R \\ &\text{from table: Difference} & D = 64 \\ &\text{Factor} & F = 100 \\ &I = 64 \cdot 100 \cdot 0,00268 \\ &= 17 \end{aligned}$$

$$\begin{aligned} 5. \quad \text{Calculation of } C: \text{from table} & \quad C_{1,29} = 0,22729 \\ &+ I = 17 \\ \hline & C = 0,22746 \end{aligned}$$

$$\begin{aligned} a &= [2 \cdot 72 - (19 + 60)] \cdot 0,22746 \cdot 25,4 \\ &= 375,54 \text{ mm} \end{aligned}$$

Chain drive with several shafts



It is possible to produce equations for the calculation of the number of links for chain drives with more than two chain wheels. However, the mathematical calculation is complicated and graphical determination of the chain length is thus easier and in most cases it can be carried out with sufficient accuracy. The basic procedure is shown below.

A large scale should be chosen when the drive details are being drawn. This will minimize errors in chain length calculation.

The pitch circle diameter for the wheels is used as a basis for determining the number of links. The theoretical chain length X' is calculated by the addition of all L_{Ti} and β_i values.

$$X' = \frac{1}{p} \cdot \sum_i L_{Ti} + \sum_i \frac{\beta_i \cdot z_i}{360^\circ}$$

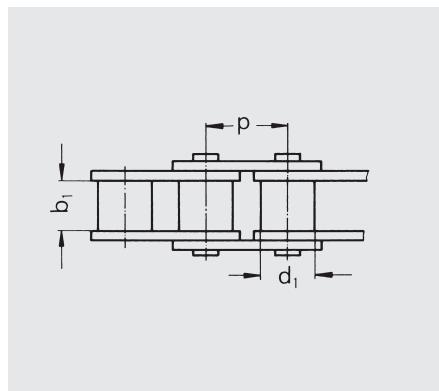
X' = calculated number of links
 p = chain pitch
 z = number of teeth

In the special case where all chain wheels have the same number of teeth and are situated within the chain, the simplified formulae applies for the calculation of the number of links.

The number of links calculated is generally speaking not a full figure and must therefore be rounded up to the next highest even number.

Where it is possible to provide adjustment, this method is sufficiently accurate, otherwise the centre distances or number of teeth should be modified until the correct chain tension is achieved.

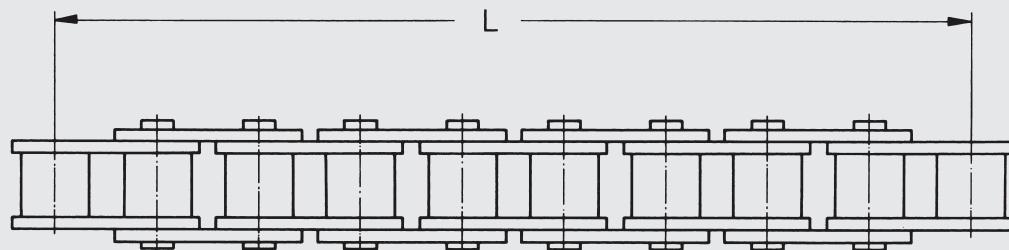
3.2 Measuring chain length



The size of the chain is determined by the pitch p , the inner width b_1 and the diameters of the rollers or bushes d_1 respectively. Multiplying pitch p with the number of links X gives the length L of the chain.

$$L = p \cdot X \quad [\text{mm}]$$

ESTABLISHING LENGTH AND TOLERANCE OF A CHAIN



In the case of **open** chains the stretched (actual) length is measured under load by applying the standard measuring load. The length established is then compared with the nominal lengths to DIN standards, which are listed in the following tables for many pitches and numbers of links.

In the case of **endless** chains a circumferential measurement using twice the measuring force is used.

Further note:

With a new chain the tedious counting of links can be left out, if the total chain length is established (in mm) and the relevant number of links for the pitch in question is read off the tables on pages 45 – 50.

The standard length tolerance for **iwis** chains are better than those specified by normal standards. In addition it is possible to produce chains to closer tolerances still

The permissible tolerance in length may be $+0,15\%$ for roller and bush chains with a measuring length $49 \times$ pitch. The measurement should be taken with the chain clean and free of lubrication and with the application of the measuring force. The tolerance for differing chain lengths of certain pitches can be calculated, using the following formula:

$$\begin{aligned} (+) \text{ tolerance} &= p \cdot X \cdot 0,0015 \quad [\text{mm}] \\ &\text{(DIN 8187/88/81, 8154)} \\ p &= \text{pitch} \\ X &= \text{number of links} \end{aligned}$$

The measuring forces specified for the pitch and type of construction can be taken from the following tables:

Lengths and tolerances

Roller chains with pitch p = 12,7 mm (1/2")

iwis Designation	ISO 606	Measuring load in N
P 83 V	-	155
S 84	-	180
L 85	08B-1	120
D 85	08B-2	250
Tr 85	08B-3	370
iwis Designation	ISO 606	Measuring load in N
L 85 A	08A-1	120
D 85 A	08A-2	250
Tr 85 A	08A-3	370

Roller chains with pitch p = 15,875 mm (5/8")

iwis Designation	ISO 606	Measuring load in N
M 106	10B-1	200
D 106	10B-2	390
Tr 106	10B-3	590
iwis Designation	ISO 606	Measuring load in N
M 106 A	10A-1	200
D 106 A	10A-2	390
Tr 106 A	10A-3	590

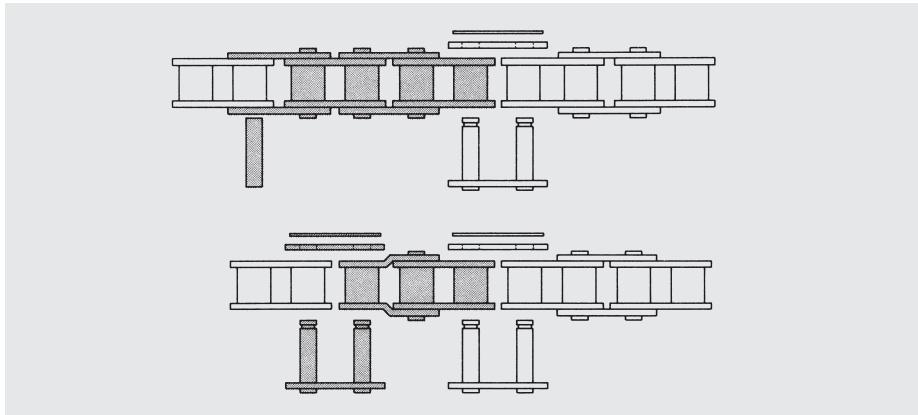
No. of links	Absolute length mm	+Tol. mm	No. of links	Absolute length mm	+Tol. mm	No. of links	Absolute length mm	+Tol. mm	No. of links	Absolute length mm	+Tol. mm	No. of links	Absolute length mm	+Tol. mm	No. of links	Absolute length mm	+Tol. mm	No. of links	Absolute length mm	+Tol. mm	No. of links	Absolute length mm	+Tol. mm	No. of links	Absolute length mm	+Tol. mm	No. of links	Absolute length mm	+Tol. mm	No. of links	Absolute length mm	+Tol. mm	
11	139,7	0,21	51	647,7	0,97	91	1155,7	1,73	131	1663,7	2,50	11	174,63	0,26	51	809,63	1,21	91	1444,63	2,17	131	2079,63	3,12										
12	152,4	0,23	52	660,4	0,99	92	1168,4	1,75	132	1676,4	2,52	12	190,50	0,29	52	825,50	1,24	92	1460,50	2,19	132	2095,50	3,14										
13	165,1	0,25	53	673,1	1,01	93	1181,1	1,77	133	1689,1	2,53	13	206,38	0,31	53	841,38	1,26	93	1476,38	2,21	133	2111,38	3,17										
14	177,8	0,27	54	685,8	1,03	94	1193,8	1,79	134	1701,8	2,55	14	222,25	0,33	54	857,25	1,29	94	1492,25	2,24	134	2127,25	3,19										
15	190,5	0,29	55	698,5	1,05	95	1206,5	1,81	135	1714,5	2,57	15	238,13	0,36	55	873,13	1,31	95	1508,13	2,26	135	2143,13	3,21										
16	203,2	0,30	56	711,2	1,07	96	1219,2	1,83	136	1727,2	2,59	16	254,00	0,38	56	889,00	1,33	96	1524,00	2,29	136	2159,00	3,24										
17	215,9	0,32	57	723,9	1,09	97	1231,9	1,85	137	1739,9	2,61	17	269,88	0,40	57	904,88	1,36	97	1539,88	2,31	137	2174,88	3,26										
18	228,6	0,34	58	736,6	1,10	98	1244,6	1,87	138	1752,6	2,63	18	285,75	0,43	58	920,75	1,38	98	1555,75	2,33	138	2190,75	3,29										
19	241,3	0,36	59	749,3	1,12	99	1257,3	1,89	139	1765,3	2,65	19	301,63	0,45	59	936,63	1,40	99	1571,63	2,36	139	2206,63	3,31										
20	254,0	0,38	60	762,0	1,14	100	1270,0	1,91	140	1778,0	2,67	20	317,50	0,48	60	952,50	1,43	100	1587,50	2,38	140	2222,50	3,33										
21	266,7	0,40	61	774,7	1,16	101	1282,7	1,92	141	1790,7	2,69	21	333,38	0,50	61	968,38	1,45	101	1603,38	2,41	141	2238,38	3,36										
22	279,4	0,42	62	787,4	1,18	102	1295,4	1,94	142	1803,4	2,71	22	349,25	0,52	62	984,25	1,48	102	1619,25	2,43	142	2254,25	3,38										
23	292,1	0,44	63	800,1	1,20	103	1308,1	1,96	143	1816,1	2,72	23	365,13	0,55	63	1000,13	1,50	103	1635,13	2,45	143	2270,13	3,41										
24	304,8	0,46	64	812,8	1,22	104	1320,8	1,98	144	1828,8	2,74	24	381,00	0,57	64	1016,00	1,52	104	1651,00	2,48	144	2286,00	3,43										
25	317,5	0,48	65	825,5	1,24	105	1333,5	2,00	145	1841,5	2,76	25	396,88	0,60	65	1031,88	1,55	105	1666,88	2,50	145	2301,88	3,45										
26	330,2	0,50	66	838,2	1,26	106	1346,2	2,02	146	1854,2	2,78	26	412,75	0,62	66	1047,75	1,57	106	1682,75	2,52	146	2317,75	3,48										
27	342,9	0,51	67	850,9	1,28	107	1358,9	2,04	147	1866,9	2,80	27	428,63	0,64	67	1063,63	1,60	107	1698,63	2,55	147	2333,63	3,50										
28	355,6	0,53	68	863,6	1,30	108	1371,6	2,06	148	1879,6	2,82	28	444,50	0,67	68	1079,50	1,62	108	1714,50	2,57	148	2349,50	3,52										
29	368,3	0,55	69	876,3	1,31	109	1384,3	2,08	149	1892,3	2,84	29	460,38	0,69	69	1095,38	1,64	109	1730,38	2,60	149	2365,38	3,55										
30	381,0	0,57	70	889,0	1,33	110	1397,0	2,10	150	1905,0	2,86	30	476,25	0,71	70	1111,25	1,67	110	1746,25	2,62	150	2381,25	3,57										
31	393,7	0,59	71	901,7	1,35	111	1409,7	2,12	151	1917,7	2,88	31	492,13	0,74	71	1127,13	1,69	111	1762,13	2,64	151	2397,13	3,60										
32	406,4	0,61	72	914,4	1,37	112	1422,4	2,13	152	1930,4	2,90	32	508,00	0,76	72	1143,00	1,71	112	1778,00	2,67	152	2413,00	3,62										
33	419,1	0,63	73	927,1	1,39	113	1435,1	2,15	153	1943,1	2,91	33	523,88	0,79	73	1158,88	1,74	113	1793,88	2,69	153	2428,88	3,64										
34	431,8	0,65	74	939,8	1,41	114	1447,8	2,17	154	1955,8	2,93	34	539,75	0,81	74	1174,75	1,76	114	1809,75	2,71	154	2444,75	3,67										
35	444,5	0,67	75	952,5	1,43	115	1460,5	2,19	155	1968,5	2,95	35	555,63	0,83	75	1190,63	1,79	115	1825,63	2,74	155	2460,63	3,69										
36	457,2	0,69	76	965,2	1,45	116	1473,2	2,21	156	1981,2	2,97	36	571,50	0,86	76	1206,50	1,81	116	1841,50	2,76	156	2476,50	3,71										
37	469,9	0,70	77	977,9	1,47	117	1485,9	2,23	157	1993,9	2,99	37	587,38	0,88	77	1222,38	1,83	117	1857,38	2,79	157	2492,38	3,74										
38	482,6	0,72	78	990,6	1,49	118	1498,6	2,25	158	2006,6	3,01	38	603,25	0,90	78	1238,25	1,86	118	1873,25	2,81	158	2508,25	3,76										
39	495,3	0,74	79	1003,3	1,50	119	1511,3	2,27	159	2019,3	3,03	39	619,13	0,93	79	1254,13	1,88	119	1889,13	2,83	159	2524,13	3,79										
40	508,0	0,76	80	1016,0	1,52	120	1524,0	2,29	160	2032,0	3,05	40	635,00	0,95	80	1270,00	1,91	120	1905,00	2,86	160	2540,00	3,81										
41	520,7	0,78	81	1028,7	1,54	121	1536,7	2,31	161	2044,7	3,07	41	650,88	0,98	81	1285,88	1,93	121	1920,88	2,88	161	2555,88	3,83										
42	533,4	0,80	82	1041,4	1,56	122	1549,4	2,32	162	2057,4	3,09	42	666,75	1,00	82	1301,75	1,95	122	1936,75	2,91	162	2571,75	3,86										
43	546,1	0,82	83	1054,1	1,58	123	1562,1	2,34	163	2070,1	3,11	43	682,63	1,02	83	1317,63	1,98	123	1952,63	2,93	163	2587,63	3,88										
44	558,8	0,84	84	1066,8	1,60	124	1574,8	2,36	164	2082,8	3,12	44	698,50	1,05	84	1333,50	2,00	124	1968,50	2,95	164												

3.3 Shortening and lengthening chain

Shortening by one link

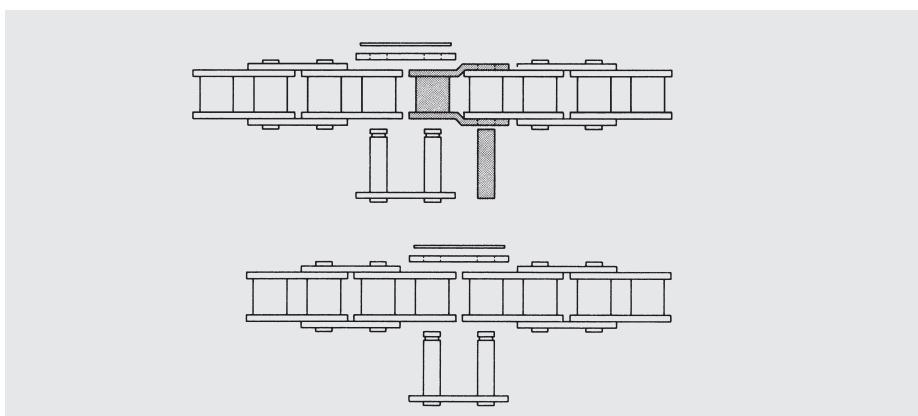
1) A chain with even number of links:

To shorten the chain by one link, remove two inner links and two outer links adjacent to the connector link and fit a double cranked link together with a further connector link.



2) A chain with uneven number of links:

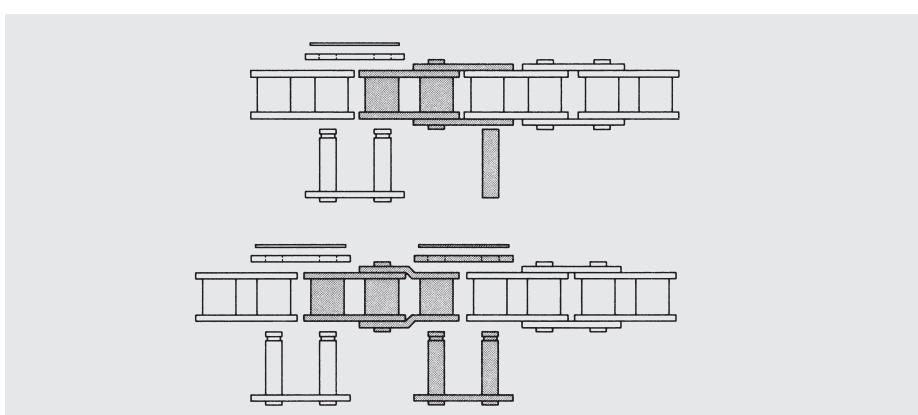
To shorten the chain remove the cranked link.



Extending chain by one link

1) A Chain with even number of links:

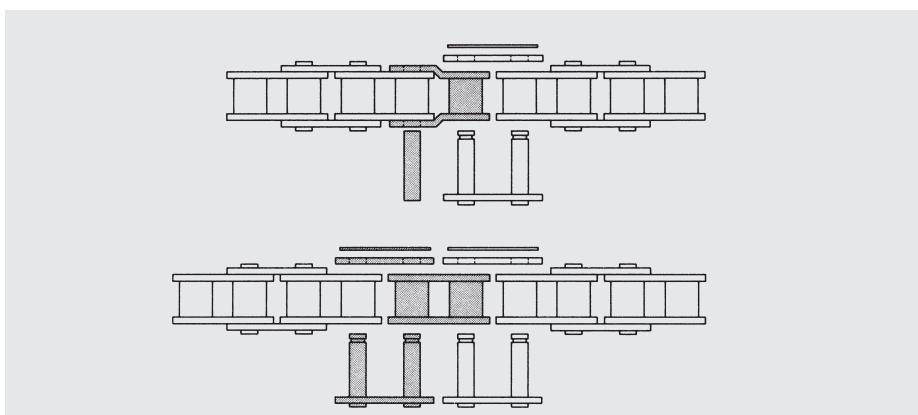
To extend chain by one link remove one inner link and one outer link and fit one double cranked link with a further connector link.



2) A chain with uneven number of links:

To extend the chain by one link, remove the single cranked link and fit an inner link with an additional connector link.

Various tools are available to **separate** and **connect** roller and bush chains, to cover the shouldered bearing pin to DIN 8187 and the plain bearing pin to DIN 8188. The types and dimensions are indicated in a separate leaflet.



1 Arrangement of drive

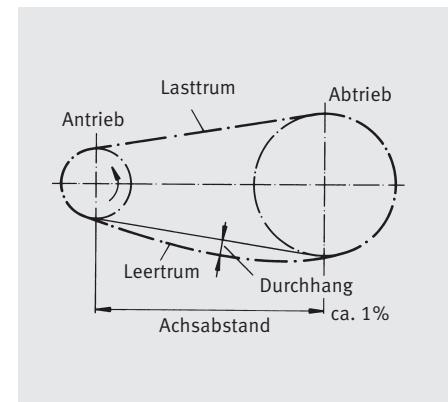
When designing a chain drive it is very often impossible to realize the theoretical best arrangement of the chainwheels.

A horizontal position for the chain wheel shafts is preferable, where the driven/taught span should be at the top and the slack span below.

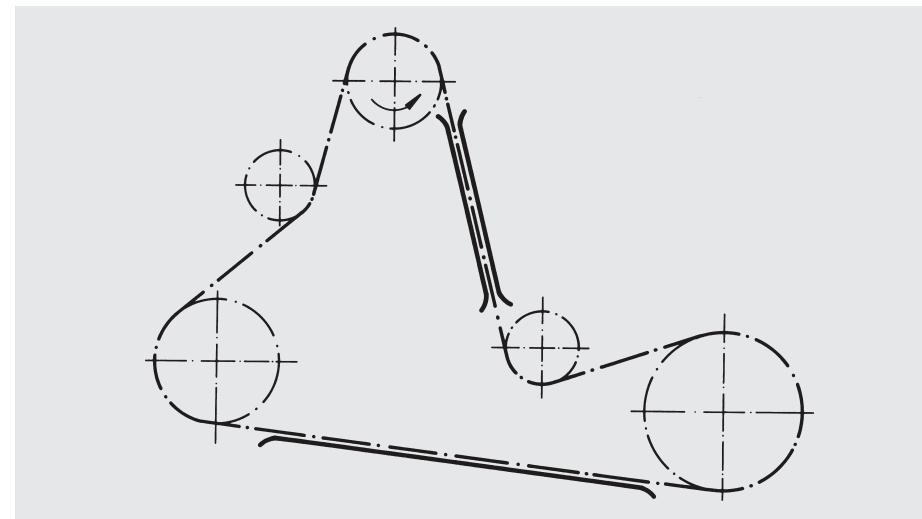
For chain drives arranged in the normal position the slack should be approx. 1 % of the centre distance. The mean centre distance can be assumed to be 30 – 60 pitches p. The angle of arc α depends on the following:

$$z_1 \leq 21 \quad \alpha \geq 120^\circ$$

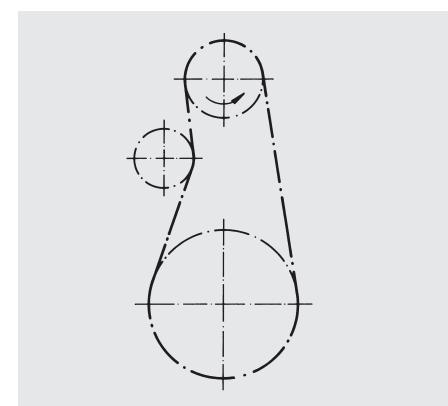
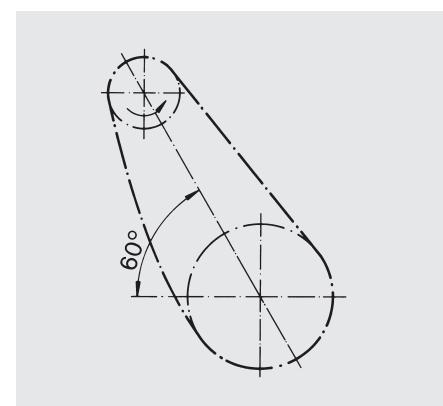
$$z_1 > 21 \quad \alpha \geq 90^\circ$$



Further examples of chain drive layout:



When adapting a drive to a restricted space it is possible to use idler wheels. Where the distance between centres is considerable, chain guides can be used to support the chains.



With the driven chain side below, only a short centre distance and minimum slack is permissible, to ensure that the slack chain does not interfere or compact between the wheels.

With chain wheels arranged horizontally and up to 60° a tensioner and or guide is not necessarily required.

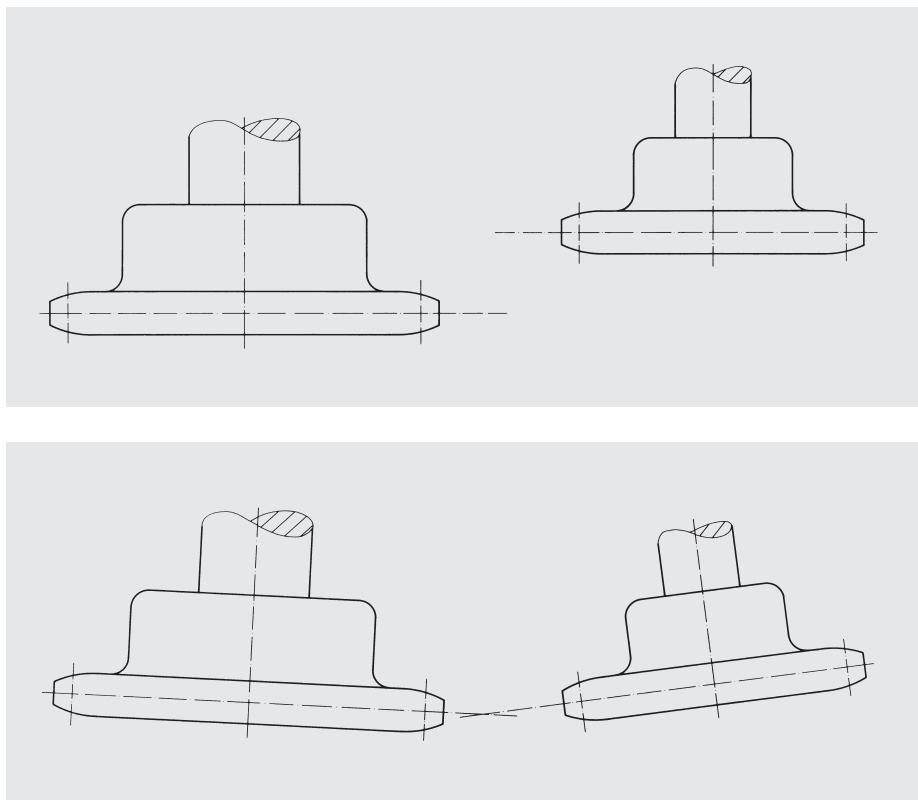
With the chain vertical, a tensioning roller or blade should be provided. An excessive chain length can be compensated by means of a tensioning roller in the case of fixed centre distances.

2 Chain and chain wheel alignment

Accurate chain alignment has a significant effect on chain life. Particular care should be paid to ensure that the shafts are parallel and to the alignment of the chain wheels. As a guide for slow running chain drives a tolerance of 0,2 mm per 100 mm centre distance is given for misalignment. In the case of faster running drives, such as in combustion engines and with short centre distances misalignment of the wheels should not exceed 0,1 mm.

With short centre distance drives and vertical chain wheel centres the chain should be supported by means of a guide.

Where the misalignment exceeds the specified value or if there is no support in the case of vertical chain wheel centres, the inner links interfere with the chain wheel teeth, resulting in continuous knocking of the inner link plates, which are eventually pushed outwards until they contact the outer link plates and thus reduce the freedom of link movement. In addition, lateral vibrations are set up, which accelerate chain wear.



3 Chain tension

Vibrations cause wear and increase the noise level of chain drives. They can be caused by:

- Uneven rotational speed of driver or driven sprocket
- Polygon effect
- Inaccurate alignment
- Vertical and horizontal run-out of sprockets
- Long, loose chain sections
- Insufficient lubrication

A distinction is made between longitudinal and transverse oscillations of the chain.

In the case of **longitudinal oscillations** there is a constant change in chain tension between the chain wheels.

Transverse oscillations are set up with long and loose chain sections as a result of super-imposing pulse and natural frequencies of the drive.

With the correct tension and guiding of the chain the above oscillations can be reduced or even prevented.

Chain tensioners

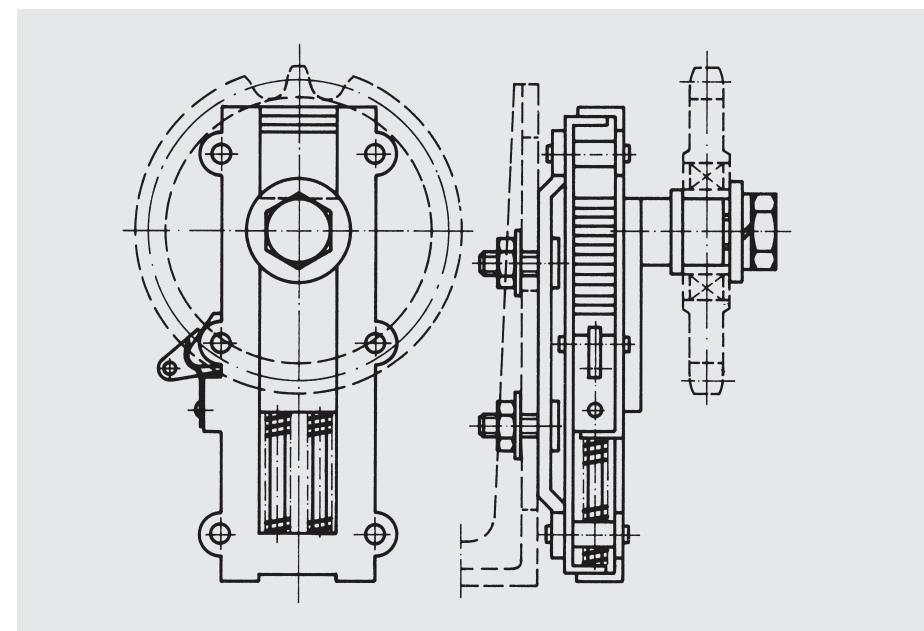
The life of a chain drive is increased considerably if a tensioner is used. A chain works satisfactorily up to an elongation due to wear amounting to max. 2 %, provided it is continuously re-tensioned. If this is not done, the slack span begins to hang to an increasing degree and the chain runs unevenly causing additional wear.

The initial load must be sufficient to stabilize the chain running, to eliminate the wear and to prevent jumping of the chain over the teeth. Excessive high initial tensioner load has to be avoided, since this can increase the chain load and bearing pressure beyond an acceptable level.

CHAIN TENSIONER AMS TYPE

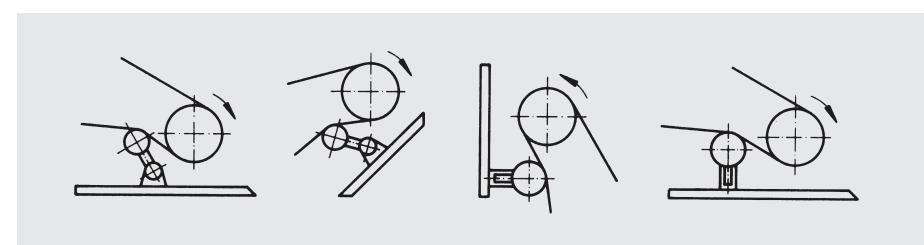
With automatic adjustment and non-return mechanism. This tensioner ensures constant damping of oscillations. Two fixing bolts in a groove enable the complete chain tensioner to be moved, thus increasing the range of adjustment.

Detailed information is provided in a special brochure.



Installation:

The tensioners offered by **iwis** can be fitted in many positions. They are always fitted on the slack span of the chain drive.



Chain guides

Chain guides are used to support chains where the centre distance is long, in order to reduce the stress as a result of the chain weight. They also reduce trans-verse and longitudinal oscillations, which increase the wear rate.

In addition, chain guides are used to absorb or reduce the force due to the mass, as it occurs when the chain runs off the wheel. Chain guides can be effectively used for noise damping purposes.

4 Maintenance and Lubrication of Chain Drives

Regular maintenance and lubrication are preconditions for low wear and long service life of the chain drive.

Maintenance and lubrication frequency, as well as the related relubrication, is determined by operating conditions (tensile forces, temperature, contamination, aggressive media).

Maintenance

During **regular visual inspections** special attention should be paid to **stretching due to wear, tension, lubrication condition, and evidence of wear due to tracking errors**.

Checking the maximum permissible stretching due to wear:

The length of a chain is defined by the pitch p and the number of links X . In the course of time stretching due to wear occurs, and usually this can be measured without removing the chain. The difference from precise measurement with a specified measurement load is slight if measurements are conducted over the highest possible number of chain links, approximately 20 to 40.

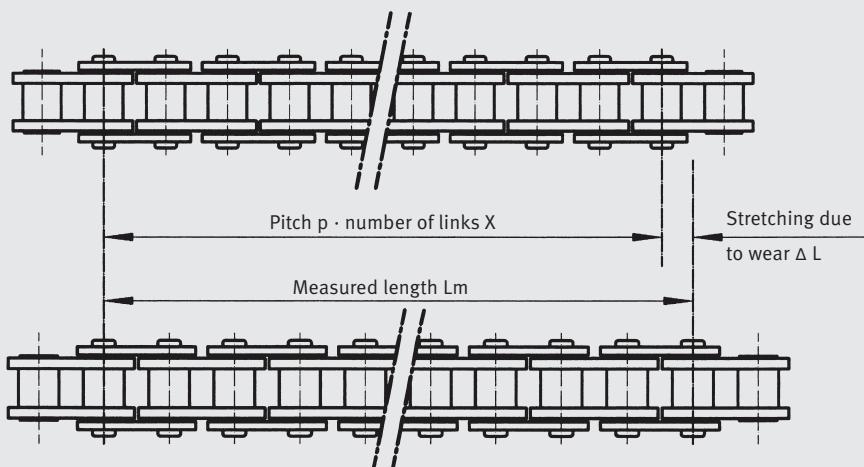
The chain should be replaced at:

max. 3% for simple drives
ca. 2% for high-performance drives
ca. 1% for special applications (synchronous operation, positioning)

Controlled **retensioning** of the chains has a very positive effect on chain life. Extreme retensioning should be avoided just as much as excessive slack. A guideline figure would be approx. 5 % of the actual chain pulling force. In the case of chains running in parallel both strands must be tensioned equally, at best by a common shaft for both sprockets. If no automatic chain tensioning device is available the chain must be adjusted by hand, by altering the distance between the sprocket shafts.

A further possibility with long drives is to shorten the chain by removing individual links, provided that wear is relatively light. Various tools are available for dismantling and reassembling the chain. These tools are available for parallel pin and shoulder pin chains.

Measurement of stretching due to wear



$$\Delta L = \frac{L_m - (p \cdot X)}{p \cdot X} \cdot 100 [\%]$$

Before **relubrication** the chains and sprockets should be **cleaned** to remove obstinate contamination and to permit the lubricant to penetrate via the back of the plates. The surface of the chain can also be cleaned using an appropriate solvent. Complete immersion and washing is not recommended as the cleaning agent does not evaporate completely from within the chain and thus the penetration of the fresh lubricant is obstructed.

During **visual inspection**, attention should be paid to evidence of chain linkplate marking and wear due to tracking errors. These are caused by misaligned sprockets or guides or by chains which are not in parallel.

Guide figure for alignment deviations per 100 mm axle separation:

0.1 mm with fast-running drives and close axle spacing;

0.2 mm with slow-running drives. The sprockets should be constantly inspected and if necessary replaced. We do not recommend that new chains are used with worn sprockets.

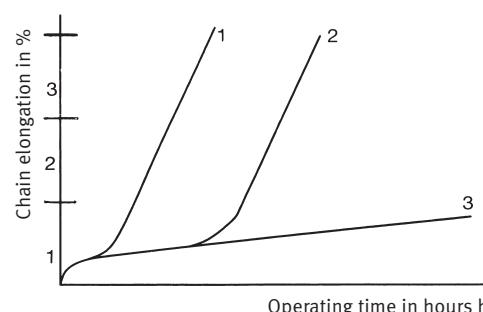
Lubrication

Correct and effective lubrication will protect against high wear resulting from bearing pressure, articulation of pin and bush bore and rotation of the roller.

It will considerably lengthen the service life of the chain. An adequate supply of lubricant must be present in the chain parts at all times and under all load conditions.

Only then can the lubricant do its job of reducing wear, protecting against corrosion and providing a damping action.

Influence of lubrication on wear and chain stretching

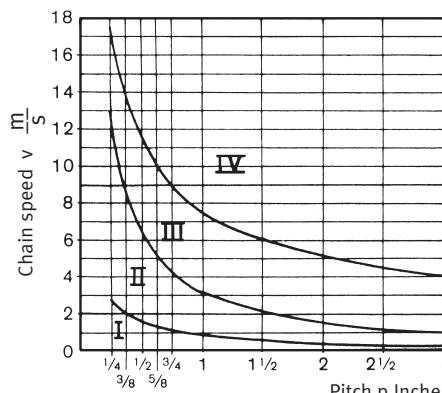


Graph 1 without lubrication, immediate wear is unavoidable

Graph 2 optimum initial lubrication, no re-lubrication, high wear after a short time

Graph 3 optimum initial lubrication and re-lubrication, low wear and long service life

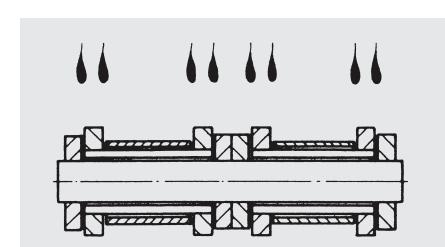
Depending upon the application, **iwis** chains are given the appropriate highgrade lubrication. Due to the articulation of the chain parts the lubricant is used in the course of time. For this reason regular re-lubrication is imperative. Selection of the most suitable lubricating method will depend upon the chain speed and chain pitch.



- I = Oil added with the oil gun or brush
- II = drip-feed lubrication
- III = oil bath or centrifugal lubrication
- IV = pressure circulation lubrication

Chain lubricants must provide a combination of the following properties: Adhesiveness, compatibility with initial lubricant, corrosion protection, load-carrying capacity of the oil film, creep capability, anti-seizing lubrication, high viscosity coupled with good flow properties, stability at high temperatures, water repel-

lency, resistance to different media, etc. Recommendations for the selection of the most suitable lubricant may be obtained from the applications advisory service or a competent tribologist.

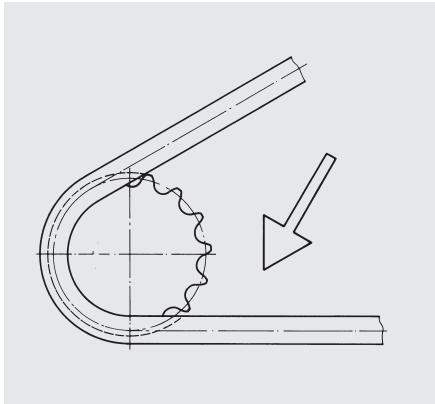


Note:

Connecting links, when supplied separately, have only been immersion-protected against rust and must be greased upon installation. If the connecting links are supplied together with the chains, they will have been greased with the same lubricant as the chains.

Lubrication methods

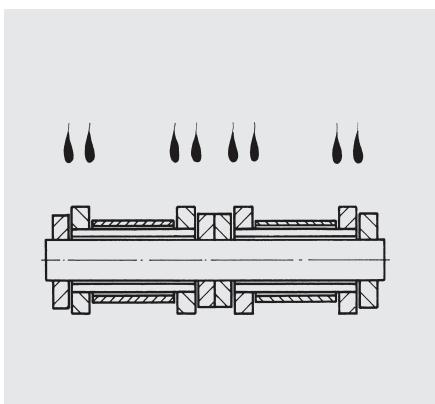
A



MANUAL LUBRICATION

With oil can or brush – very unreliable. Thus it is suitable only for drives that are not in constant service or for drives with slow chain speeds.

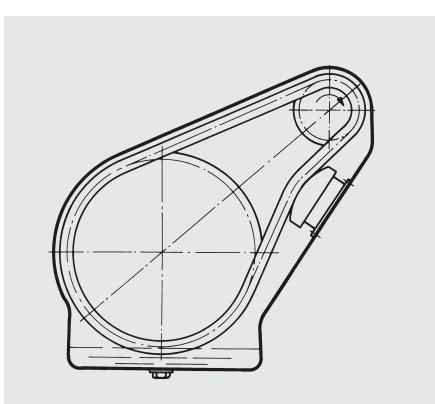
B



DRIP FEED LUBRICATION

Drip feed is suitable for chain drives that are not highly stressed. In order to reach the joints, the drip tube should be carefully positioned as shown.

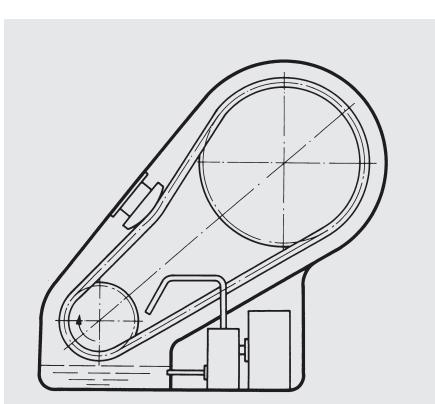
C



OIL BATH LUBRICATION

A chain casing absorbs noise and should be as large as possible, to prevent the chain knocking against the casing wall if the chain elongates due to wear. There is no loss of lubricant in an oil bath. The chain linkplates and rollers should be submerged in the bath. Too great a depth leads to overheating of the oil and its premature oxidation, and causes power loss due to the increased running resistance.

D



PRESSURE LUBRICATION

Required for high-speed chain drives and high loads. The oil supply can be connected to an existing pressure pipe or it can be provided by a pump. A tube ejects the oil in the direction of the chain travel over the entire width of the chain, onto the inside of the taught span of the chain. The amount of oil feed depends on the size of the drive and the heat to be dissipated.

E

F

G

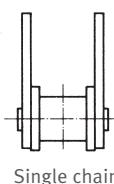
1 Conveyor chains – Roller chains with attachments

1.1 Attachments

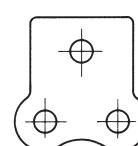
Roller chains are converted into conveyor chains by combining the elements of the standard chain with special attachments, i.e. the straight and bent attachment plates.

All attachments are fitted in place of the outer link plates, and the chain breaking load remains unchanged. These attachments can be fitted on one side, both sides and at any distance to single, double and triple chains.

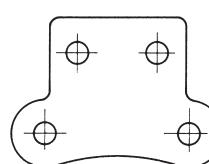
STRAIGHT ATTACHMENT PLATES



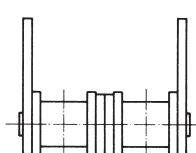
Single chain



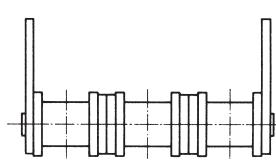
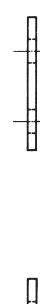
Narrow attachment



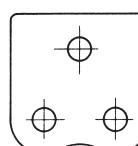
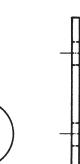
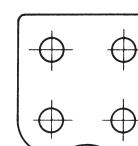
Double pitch attachment



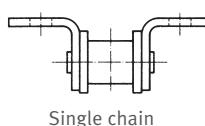
Double chain



Triple chain

Wide design with one
or two drill holes

BENT ATTACHMENT PLATES



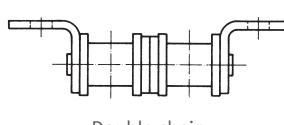
Single chain



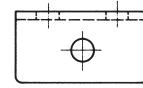
Narrow attachment



Double pitch attachment



Double chain



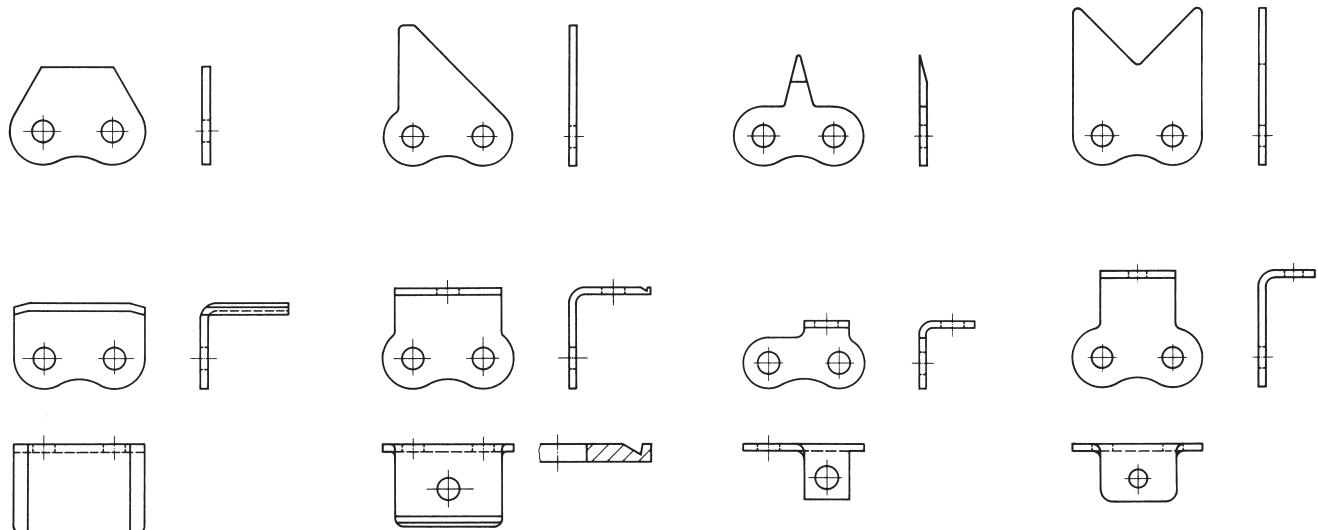
Triple chain

Wide design with one
or two drill holes

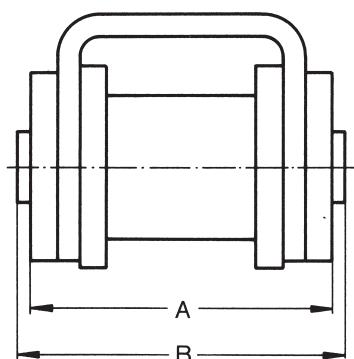
Detailed dimensions are included in catalogue "Precision chains for Drive and Conveyor Purposes"
Further shapes are given in catalogue "Precision chains for Drive and Conveyor Purposes"

SPECIAL LINK PLATES

These may be straight, cranked, bent and drilled and can be adapted to suit the customer's requirements. A few examples are shown below. Further shapes are given in catalogue 11.



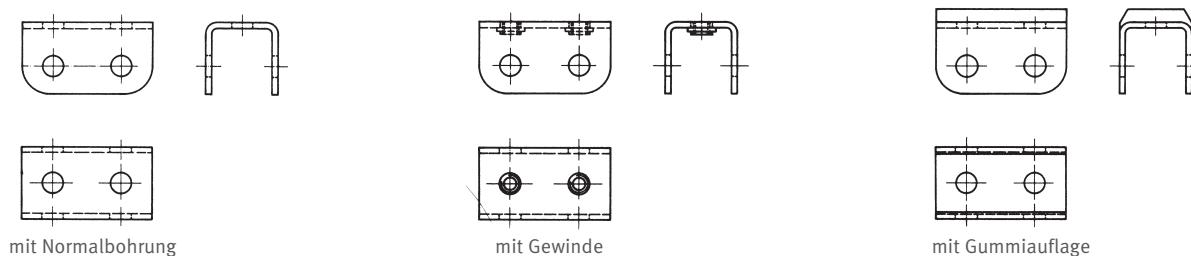
U-PLATES



U-Plates are fitted between inner and outer plates.
 The chain width is larger than standard. See chart.

Chain	Chain width	
	A	B
L 85 SL	17,8	19,8
D 85 SL	31,8	33,9
M 106 SL	20,0	22,0
M 1610A	33,7	36,5

Chain connectors with longer pins are required



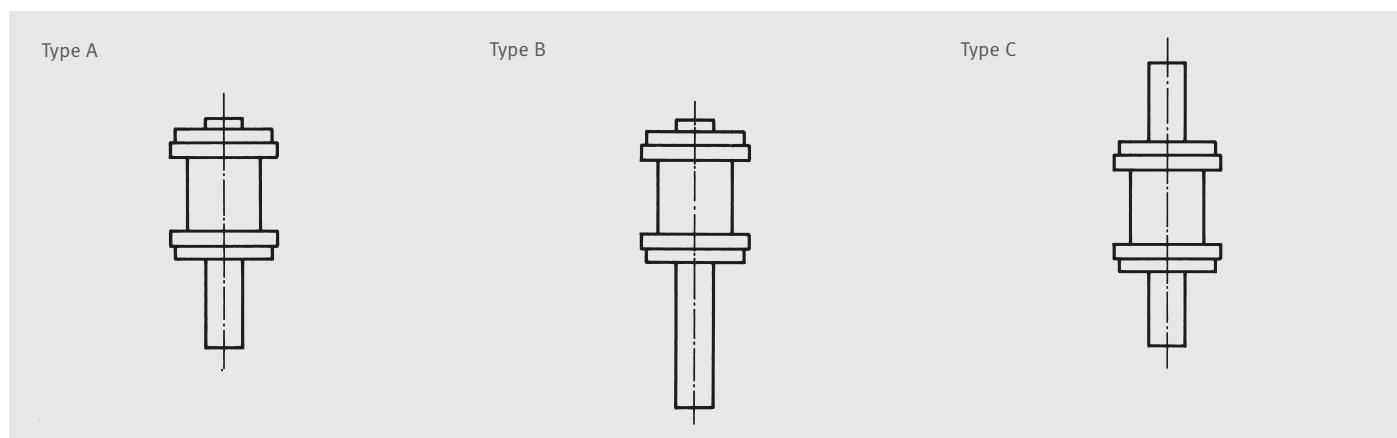
Detailed dimensions are included in catalogue "Precision chains for Drive and Conveyor Purposes"
 Further shapes are given in catalogue "Precision chains for Drive and Conveyor Purposes"

1.2 Extended pins

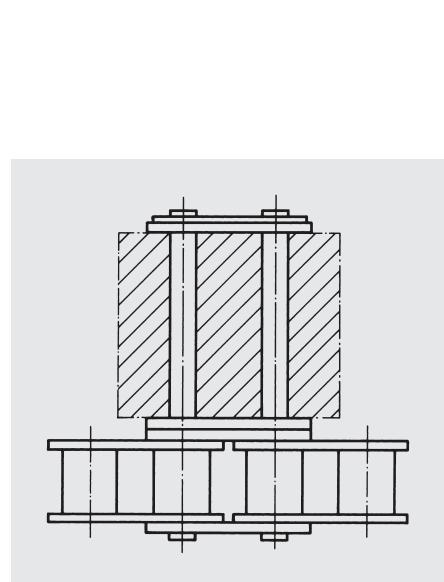
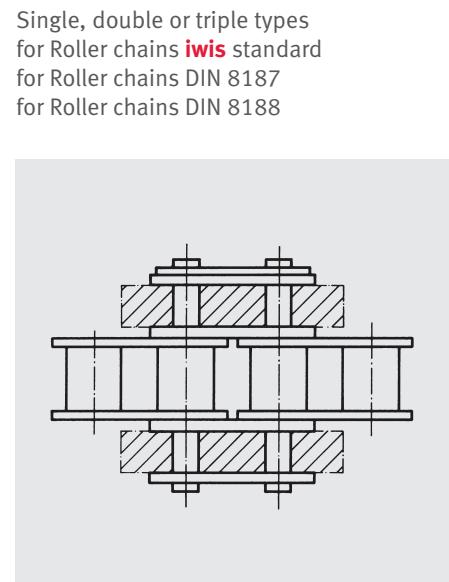
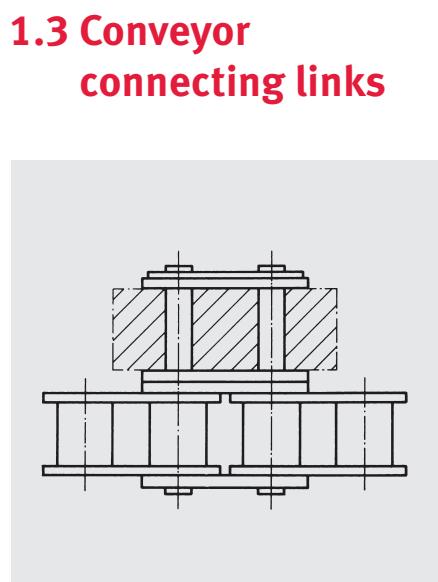
The extended pins can be fitted on one or both sides of the chain and at any distance. There is a press fit between the extended pin and the outer link plates, to secure against rotation.

A significant advantage of this conveyor chain design, compared to vertical attachment plates for example, is the central application of turning moments, which will reduce the risk of moving the chain from the guide.

Applicable for
Roller chain **iwis** standard
Roller chains DIN 8187
Roller chains DIN 8188
Roller chains DIN 8181



Detailed dimensions are included in catalogue "Precision chains for Drive and Conveyor Purposes"



Detailed dimensions are included in catalogue "Precision chains for Drive and Conveyor Purposes"

E

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A

PRINTING INDUSTRY:

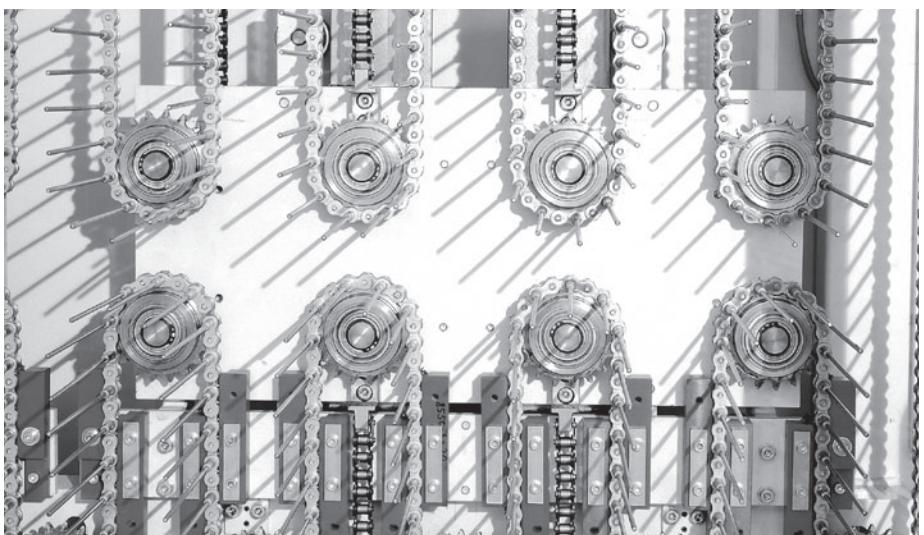
iwis high performance chains running in parallel and accurate synchronous



B

GENERAL MECHANICAL ENGINEERING:

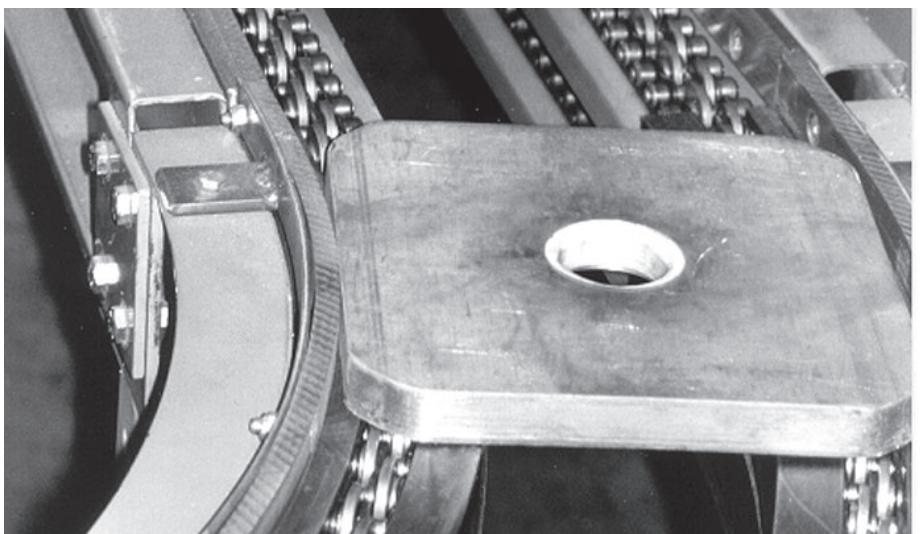
Excellent wear resistance and fatigue strengths for specialized applications



C

CONVEYOR SYSTEMS:

Side bow power and free conveyor chains – the solution for modular changes of direction in conveyor systems.



D

 DWS® chain drives

General information
 DWS® chain drives

E

 DWS® Chains for industrial use
 DWS® chain drives

Conversion charts,
iwis chain guideline

G

2 Chains for special applications

2.1 MEGAlife I maintenance free chains

MEGAlife Maintenance-free roller chains can be used wherever lubrication is difficult or impossible to implement. This includes dry ambient conditions, clean-rooms, installations with restricted maintenance access and applications in which a contamination of plant and conveyed product must be prevented.

MEGAlife chains are available as roller chains conforming to the DIN 8187/ISO 606 standard for drive applications and as conveyor chains with attachments. Simplex, duplex and triplex (single, double and triple versions) with a pitch from 9.525 mm to 25.40 mm are available. The nickel-plated chain components are corrosion-resistant and can be used in a temperature range from -40 °C to 150 °C.

The chains are supplied either dry or with special-purpose lubrication to suit the intended application. According to the manufacturer they have an outstanding service life, which, although it depends on the operating conditions, can be further extended through careful periodic lubrication. Under some conditions, the chains can even be permanently operated without maintenance.

DIN ISO no.	Ref. no. iwiS	Pitch p (")	Pitch p (mm)	iwiS (N) med.	Standard (N) min.	Bearing area f (cm)	Weight per m q (kg/m)	b ₁ (mm) min.	b ₂ (mm) min.	g (mm) max.	a ¹ (mm) max. ¹⁾	Outer link a (mm) max. ¹⁾	Roller d ₁ (mm) max.	Pin d ₂ (mm) max.	e (mm)	Article No.
Single																
06 B-1	G 67 ML*	3/8"	9,525	11.000	9.000	0,28	0,41	5,72	8,53	8,20	12,90	16,70	6,35	3,31	-	50033917
08 B-1	L 85 ML	1/2"	12,70	22.000	18.000	0,50	0,70	7,75	11,30	12,20	16,90	18,50	8,51	4,45	-	50026256
08 A-1 ANSI 40	L 85 AML	1/2"	12,70	17.500	14.100	0,44	0,60	7,94	11,15	12,00	16,60	17,50	7,95	3,96	-	50036841
10 B-1	M 106 ML	5/8"	15,875	25.000	22.400	0,67	0,95	9,65	13,28	14,40	19,50	20,90	10,16	5,08	-	50026257
12 B-1	M 127 ML	3/4"	19,05	30.000	29.000	0,89	1,25	11,75	15,62	16,20	22,70	23,60	12,07	5,72	-	50026258
12 A-1 ANSI 60	M 128 AML	3/4"	19,05	41.000	31.800	1,06	1,47	12,70	17,75	18,00	25,30	26,70	11,91	5,96	-	50038464
16 B-1	M 1611 ML	1"	25,4	75.000	60.000	2,10	2,70	17,02	25,45	21,10	36,10	36,90	15,88	8,28	-	50028923
Double																
06 B-2	D 67 ML	3/8"	9,525	19.000	16.900	0,56	0,78	5,72	8,53	8,20	23,40	24,60	6,35	3,31	10,24	50033832
08 B-2	D 85 ML	1/2"	12,70	40.000	32.000	1,00	1,35	7,75	11,30	12,20	30,80	32,40	8,51	4,45	13,92	50027439
10 B-2	D 106 ML	5/8"	15,875	50.000	44.500	1,34	1,85	9,65	13,28	14,40	36,00	37,50	10,16	5,08	16,59	50027509
12 B-2	D 127 ML	3/4"	19,05	60.000	57.800	1,78	2,50	11,75	15,62	16,40	42,10	43,00	12,07	5,72	19,46	50027457
16 B-2	D 1611 ML	1"	25,40	150.000	106.000	4,21	5,40	17,02	29,45	21,10	68,00	68,80	15,85	8,28	31,88	50033161
20 B-2	D 2012 ML	1 1/4"	31,75	210.000	170.000	5,84	7,36	19,56	29,01	25,40	79,70	82,90	19,05	10,19	36,45	50033771
Triple																
08 B-3	TR 85 ML	1/2"	12,70	58.000	47.500	1,50	2,00	7,75	11,30	12,20	44,70	46,30	8,51	4,45	13,92	50027510
10 B-3	TR 106 ML	5/8"	15,875	75.000	66.700	2,02	2,80	9,65	13,28	14,40	52,50	54,00	10,16	5,08	16,59	50027511
12 B-3	TR 127 ML	3/4"	19,05	89.000	86.700	2,68	3,80	11,75	15,62	16,40	61,50	62,50	12,07	5,72	19,46	50027512
16 B-3	TR 1611 ML	1"	25,40	219.000	160.000	6,32	8,00	17,02	25,45	21,10	99,20	100,70	15,88	8,28	31,88	50033628
Single/Double - MEGAlife I – roller chains with straight side plates																
10 B-1	M 106 ML-GL	5/8"	15,875	24.000	22.400	0,67	0,95	9,65	13,28	13,90	19,50	20,90	10,16	5,08	-	50035304
10 B-2	D 106 ML-GL	5/8"	15,875	47.500	44.500	1,34	1,85	9,65	13,28	13,90	36,00	37,50	10,16	5,08	16,59	50034083
12 B-1	M 127 ML-GL	3/4"	19,05	30.000	29.000	0,89	1,30	11,75	15,62	16,10	22,70	23,60	12,07	5,72	-	50037351
12 B-2	D 127 ML-GL	3/4"	19,05	63.000	57.800	1,78	2,50	11,75	15,62	16,10	42,10	43,00	12,07	5,72	19,46	50034084

* also available in 10 m length (Art. 50035181) ¹⁾ Differing dimensions for cranked links If cranked links are fitted, it should be noted that the breaking strength of the chain may be reduced by approximately 20 %.

2.2 MEGAlife II – roller chains

(complying with DIN 8187-1, ISO 606: 1994)

For high-speed and other demanding applications, the Megalife 2 series with its exceptionally long service life is the ideal choice.

Its outstanding surface hardness, which is achieved with a special thermo chemical process, ensures wear resistance even at speeds of over 3 m/s.

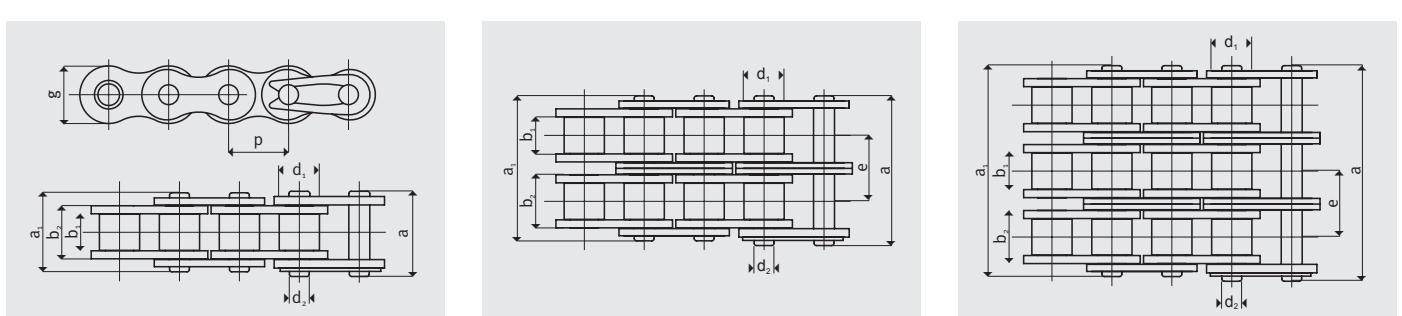
DIN/ISO no.	Ref. no. iwis	Pitch p (")	Pitch p (mm)	iwis (N) med.	Standard (N) min.	Bearing area f (cm) ²	Weight perm q (kg/m)	b ₁ (mm) min.	b ₂ (mm) min.	g (mm) max.	Inner link	Outer link	a (mm) max. ^v	Roller d ₁ (mm) max.	Pin d ₂ (mm) max.	Transverse pitch e (mm)	5 m Versions	Article No.
Single																		
06 B-1	G 67 ML-2*	3/8"	9,525	11.000	9.000	0,28	0,41	5,72	8,53	8,20	12,90	14,10	6,35	3,31	-	50030791		
08 B-1	L 85 ML-2	1/2"	12,70	22.000	18.000	0,50	0,70	7,75	11,30	12,20	16,90	18,50	8,51	4,45	-	50030461		
10 B-1	M 106 ML-2	5/8"	15,875	27.500	22.400	0,67	0,95	9,65	13,28	14,40	19,50	20,90	10,16	5,08	-	50030462		
12 B-1	M 127 ML-2	3/4"	19,05	34.000	29.000	0,89	1,25	11,75	15,62	16,40	22,70	23,60	12,07	5,72	-	50030463		
16 B-1	M 1611 ML-2	1"	25,40	75.000	60.000	2,10	2,70	17,02	25,45	21,10	36,10	36,90	15,88	8,28	-	50030464		
20 B-1	M 2012 ML-2	1 1/4"	31,75	120.000	95.000	5,84	7,36	19,56	29,10	26,60	77,00	79,70	19,05	10,17	36,45	50033036		
Double																		
06 B-2	D 67 ML-2	3/8"	9,525	19.000	16.900	0,56	0,78	5,72	8,53	8,20	23,40	24,60	6,35	3,31	10,24	50031074		
08 B-2	D 85 ML-2	1/2"	12,70	40.000	32.000	1,00	1,35	7,75	11,30	12,20	30,80	32,40	8,51	4,45	13,92	50030465		
10 B-2	D 106 ML-2	5/8"	15,875	49.000	44.500	1,34	1,85	9,65	13,28	14,40	36,00	37,50	10,16	5,08	16,59	50030466		
12 B-2	D 127 ML-2	3/4"	19,05	61.000	57.800	1,78	2,50	11,75	15,62	16,40	42,10	43,00	12,07	5,72	19,46	50030467		
Triple - ML-2 roller chains on request																		

Single ANSI roller chains, complying with DIN 8188-1, American standard, ISO 606: 1994

08 A-1 ANSI 40	L 85 AML-2	1/2"	12,70	17.500	14.100	0,44	0,60	7,94	11,15	12,00	16,60	17,50	7,95	3,96	-	50033770	
12 A-1 ANSI 60	M 128 AML-2	3/4"	19,05	41.000	31.800	1,06	1,47	12,70	17,75	18,00	25,30	26,70	11,91	5,96	-	50031073	
16 A-1 ANSI 80	M 1610 AML-2	1"	25,40	68.000	56.700	1,79	2,57	15,88	22,40	22,80	32,00	33,90	15,88	7,94	-	50032667	

ML-2 conveyor chains on request

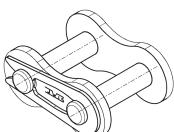
¹⁾ Differing dimensions for cranked links. If cranked links are fitted, it should be noted that the breaking strength of the chain may be reduced by approximately 20 %. * straight side plates



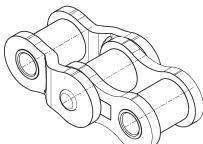
INDIVIDUAL COMPONENTS AND CONNECTING LINKS



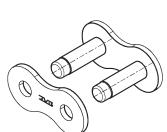
No. 2 Inner link
Standard designation B



No. 3 Connecting link with spring clip
Standard designation E



No. 7 Double cranked link
Standard designation C



No. 8 Outer link
Standard designation A

2.3 Corrosion-protected chains

Where conditions are less severe, chains with surface-protected parts can be used. IWIS chains are produced with nickel- and zinc-plated surface coatings.

Surface-coated chains provide good corrosion protection: nickel-plated against the effects of moisture, and zinc-plated also against weak organic acids. Nickel-plated surfaces are permitted in the food-stuffs industry.

For technical reasons the pins of these chains are made of normal high-grade steel for chain pins (not SL).

More detailed information is available on request.

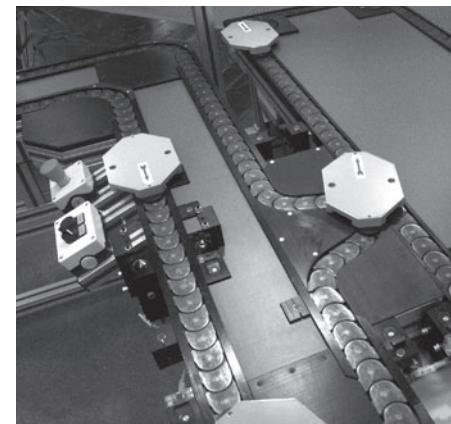
2.4 Apron chains

Conveying and storage of components through the tightest curves.

The apron chain is a long-link roller chain 1 1/2 x 7/16" made to DIN 8181 with vertical extended chain pins. Each link is designed as a cranked link with cotter pin. On the extended head of the pin a steel plate is pressure fitted. The meshing shapes of the plates always ensures a constant surface for receiving the components even on the curves.

The apron chain's ability to run around very tight radius curves provides the advantage that long conveyor sections can be concentrated into much smaller spaces.

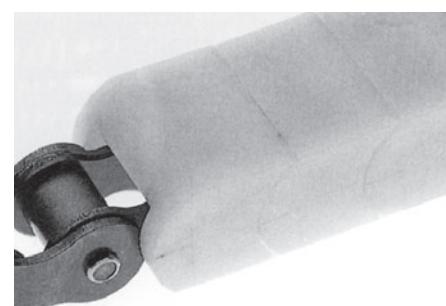
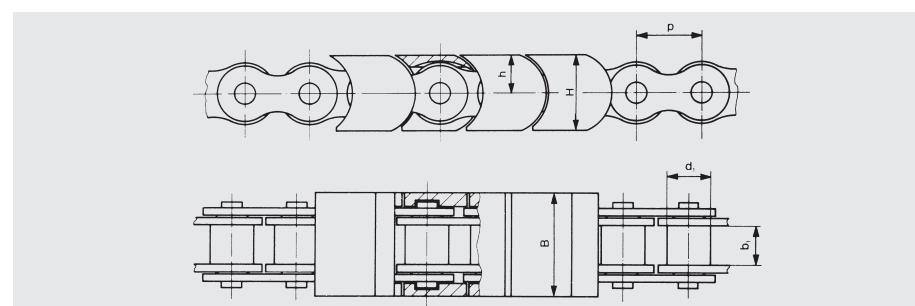
Plate width: 50 / 80 mm
Minimum radius: 60 mm/150 mm
Minimum tooth number: 20 bei 50 mm
30 bei 80 mm
Number of links:
Only possible with an even number of links.



iwis-designation: conveyor chain LR 247 (apron chain).

2.5 Transfer chains

CONVEYING, TRANSPORTING, SYNCHRONIZING CONTAINERS, COMPONENT PALETS ...



<i>iwis</i> -chain no.	Pitch <i>p</i> (mm)	Permissible weight load per chain strand	Breaking strength <i>iwis F_B</i> (N)	Weight (kg/m)	Width <i>B</i> (mm)	Carrier Attachment Height <i>H</i> (mm)	Height <i>h</i> (mm)	max. load per plastic Attachment blugel (N)
L 85 TF	12,7	6250	22.000	0,82	19,8	15,2	8,0	12
M 106 TF	15,875	8000	27.500	1,18	24,8	17,5	9,5	26
M 127 TF	19,05	9750	34.000	1,59	29,8	19,8	11,0	43

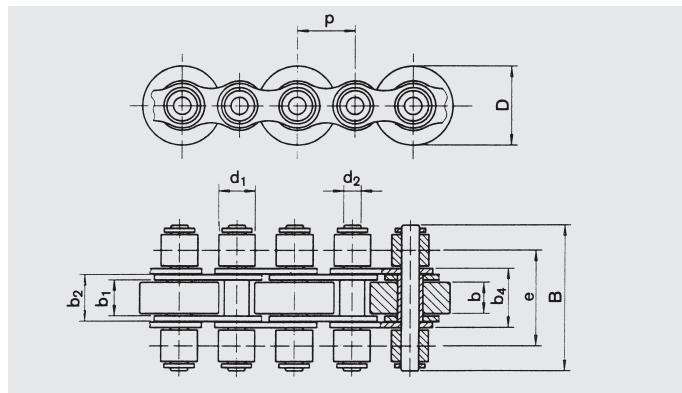
These chains are made to dimensions shown on page 10 under **iwis** reference L 85 SL, M 106 SL and M 127 SL.

The carriers made from high-grade wear-resistant plastic convey the transported items and seal off the chain's functional area. Guide values for chain selection: friction factor 0.1 for determining the pulling

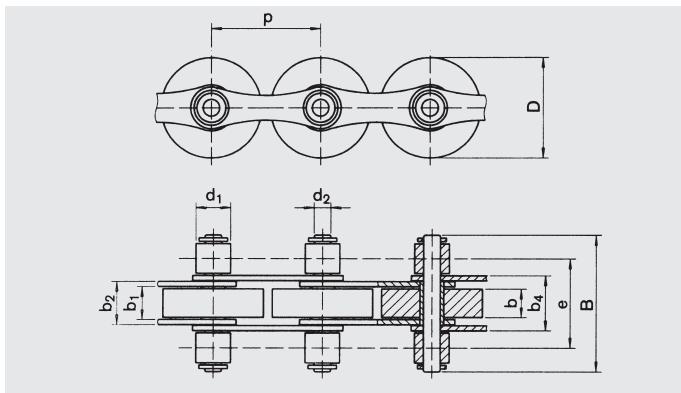
capacity of the chain; friction factor 0.25 for calculating the drive power. For normal loads, a bridge-shaped chain guide on which the chain rollers are carried will be adequate.

2.6 Power and free conveyor chains

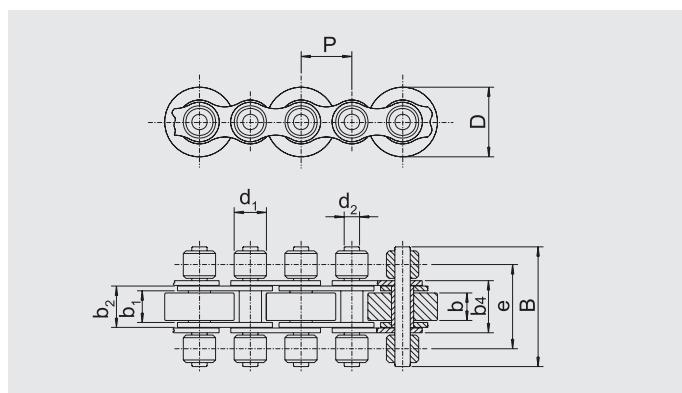
CONVEYING, STOPPING, ACCELERATING, ACCUMULATING



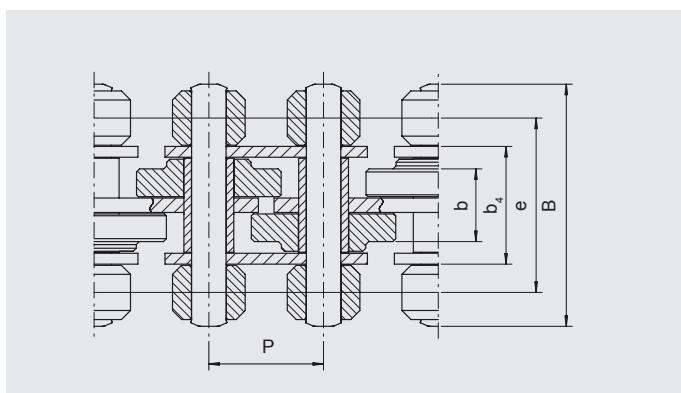
Design M normal pitch



Design LR double pitch



Design OS devoid of washers



Design VS, staggered accumulation roller

Dimensions - new power and free chains

<i>iwis</i> chain type	Pitch P (mm)	B (mm)	b (mm)	b4 (mm)	e (mm)	Diameter (mm)	Transport roller	
							Loading capacity (kg)	Weight (kg/m)
L 88 SFK	12,70	27	9,2	14,50	18,70	16,00 ¹⁾	6	0,85
L 88 SFS	12,70	27	9,2	14,50	18,70	16,00	8	1,40
M 120 SFK	19,05	40	11,70	19,55	29,0	24,01 / 26,0 / 27,01 / 28,0	10	1,8
M 120 SFK	19,05	45	11,70	19,55	31,5	24,0 / 26,0 / 27,0 / 28,0	10	1,8
M 120 SFS	19,05	40	11,70	19,55	29,0	24,01 / 26,0 / 27,01 / 28,0	15	2,8
M 120 SFS	19,05	45	11,70	19,55	31,5	24,0 / 26,0 / 27,0 / 28,0	15	2,8

¹⁾ Supplied ex stock

SFK - with plastic transport rollers

SFS - with hardened steel transport rollers

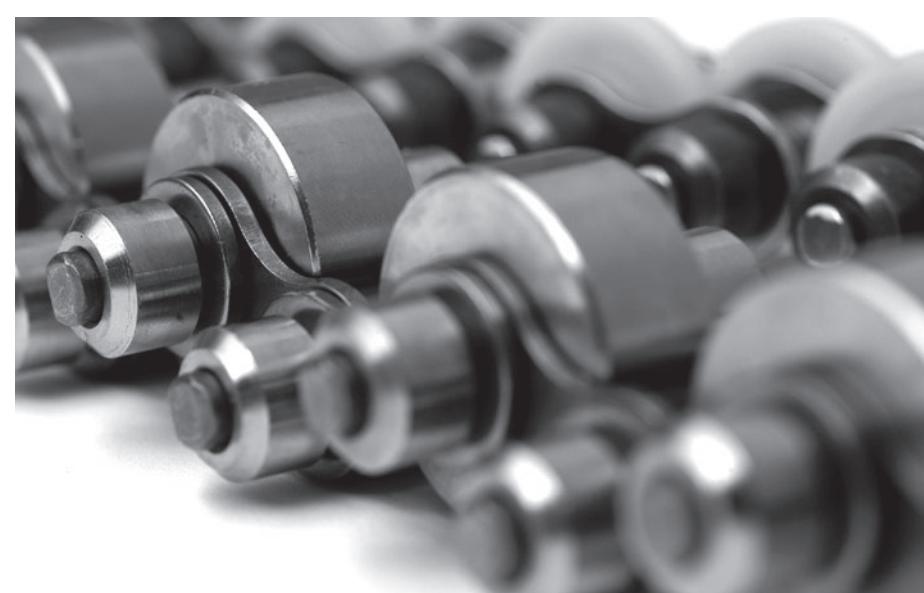
Design	iwi chain no.	Pitch p (mm)	Chain width B (mm)	e (mm)	b ₁ (mm)	b ₂ (mm) max.	b ₄ (mm) max.	Width b (mm)	Diameter	Transport roller		Diameter	
										Load capacity (kg)	Roller d ₁ (mm)	Pin d ₂ (mm)	Weight (kg/m)
OS	L 85 SFK	12,70	27	18,70	—	—	14,50	9,2	16,00	6	—	—	0,85
	L 85 SFS	12,70	27	18,70	—	—	14,50	9,2	16,00	8	—	—	1,40
M	M 127 SFK	19,05	40	27,5	11,75	15,62	19,55	11,0	24,0	26,0	28,0	10	12,07 5,72 2,3
	M 127 SFS	19,05	40	27,5	11,75	15,62	19,55	11,0	24,0	26,0	28,0	—	12,07 5,72 3,1
M	M 127 SFK	19,05	40	27,5	11,75	15,62	19,55	11,0	24,0	26,0	28,0	10	12,07 5,72 2,3
	M 127 SFK	19,05	43	29,0	11,75	15,62	19,55	11,0	24,0	26,01)	28,0	10	12,07 5,72 2,3
M	M 127 SFK	19,05	48	31,5	11,75	15,62	19,55	11,0	24,0	26,0	28,0	10	12,07 5,72 2,3
	M 127 SFS	19,05	40	27,5	11,75	15,62	19,55	11,0	24,0	26,0	28,0	15	12,07 5,72 3,1
M	M 127 SFS	19,05	43	29,0	11,75	15,62	19,55	11,0	24,0	26,0	28,0	15	12,07 5,72 3,1
	M 127 SFS	19,05	48	31,5	11,75	15,62	19,55	11,0	24,01)	26,0	28,0	15	12,07 5,72 3,1
M	M 1611 SFK	25,4	67,9	44,9	17,02	25,45	32,0	16,5	38,5	—	—	25	15,88 8,28 4,9
	M 1611 SFS	25,4	67,9	44,9	17,02	25,45	32,0	16,5	38,5	—	—	30	15,88 8,28 7,2
LR	LR 165 SFK	25,4	30,7	20,0	7,75	11,30	14,65	7,5	24,0	—	—	6	8,52 4,45 1,3
	LR 247 SFK	38,1	48	31,5	11,75	15,62	19,55	11,0	24,0	35	—	10	12,07 5,72 2,6
LR	LR 247 SFS	38,1	48	31,5	11,75	15,62	19,55	11,0	24,0	35	—	10	12,07 5,72 2,6
	LR 3211 SFK	50,8	67,9	44,9	17,02	25,45	32,0	16,5	50,0	38,5	—	25	15,88 8,28 3,6
LR	LR 3211 SFS	50,8	67,9	44,9	17,02	25,45	32,0	16,5	50,0	38,5	—	30	15,88 8,28 7,6

¹⁾ Supplied ex stock SFK - with plastic conveyor rollers SFS - with hardened steel conveyor rollers

Special designs with guide plates, other transport roller diameters and roller arrangements are available on request.

Maximum permissible conveyor length, depending on load, approx. 30 m. In the case of conveyor sections longer than approx. 10 m, guide plates are recommended as compensation for any misalignment in the guides which may be present. The decisive factor in selecting chain size is the load-bearing capacity of the transport rollers and the permissible chain pulling power. Depending on loading, chain guides can be made of plastic or steel.

Option: Chains **M 127 SFK/SFS** with transport rollers 24 and 26 mm diameter can also be supplied with wear-resistant plastic inserts, which seal off the gaps between the transport rollers and protect the chain from ingress of foreign matters.

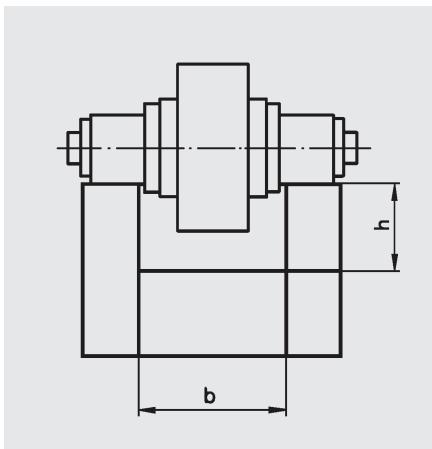


Maintenance power and free conveyor chains with special redesigned joint and transport rollers made of sintered steel,

can be applied in cases where Lubrication is not at all or only partly possible.

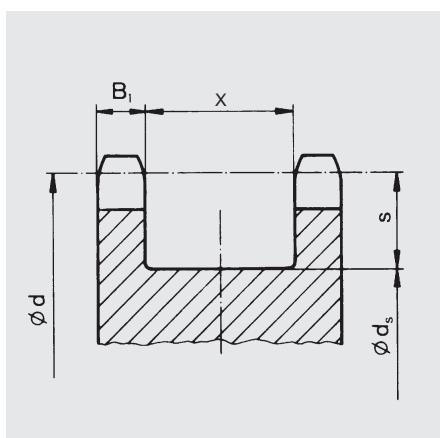
CHAIN GUIDE

iwis chain	b (mm)	h (mm)
L 88 SF	15	10
L 88 SF SB	15,5	10
M 120 SF	20	15
M 120 SF SB	21	15
M 127 SF	20	15
M 1611 SF	33	20



CHAIN WHEELS

iwis chain	Pitch p (mm)	B ₁ (mm)	X (mm)	s (mm)
L 88 SF	12,7	4	15,5	10
M 120 SF-B40	19,05	8,3	20,7	15,0
M 127 SF-B40/B43	19,05	8,3	20,7	15,0
M 120 SF-B45	19,05	10,8	20,7	15,0
M 127 SF-B48	19,05	10,8	20,7	15,0
M 1611 SF	25,4	11,6	33,3	20,5



$$d_s = d - 2s$$

$$d = p : (\sin 180^\circ : z)$$

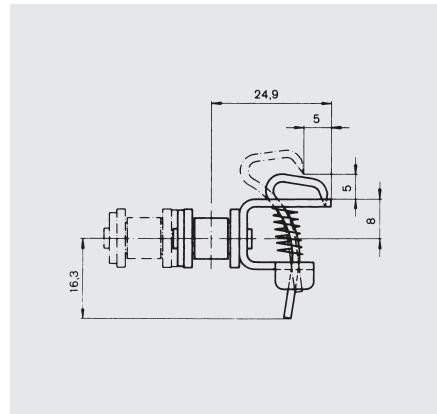
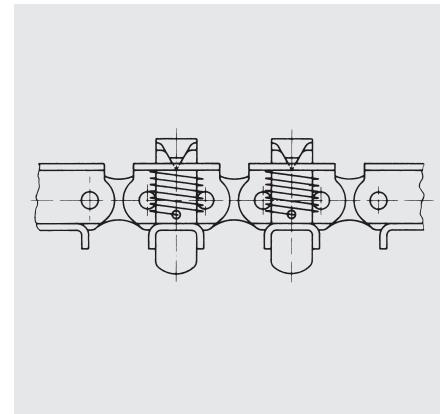
Recommended number of teeth minimum z = 15

2.7 Grip chains

GRIPPING, CARRYING AND CONVEYING

iwi-chain no.	Pitch p (mm)	Weight q (kg/m)
Single strand chain L 85 Grip	12,7	1,15
Double strand chain D 85 Grip	12,7	1,8

Dimensions and values not given are identical to iwi chains L 85 SL and D 85 SL.



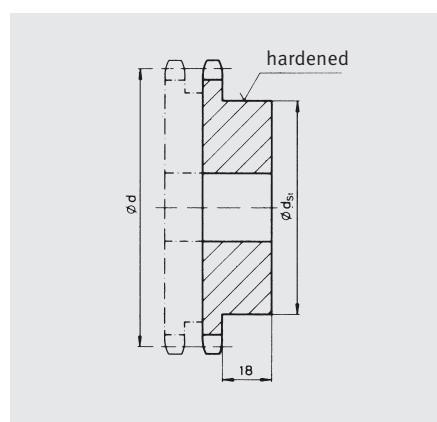
The gripper elements are mounted continuously or at defined intervals on the chain. The entire chain is corrosion-protected by nickel-plating, while the grippers themselves consist of a corrosion-resistant, hardened steel.

In the standard version, the gripper is provided with a point, and it operates within U-shaped plates fitted on one side of the chain at each outer link.

The gripper opens when it runs onto a control disk which can be the hardened sprocket boss. The gripper then swings outwards and permits the transported item to be loaded or unloaded.

The type of control disk will depend on the machine design, available space and mounting possibilities.

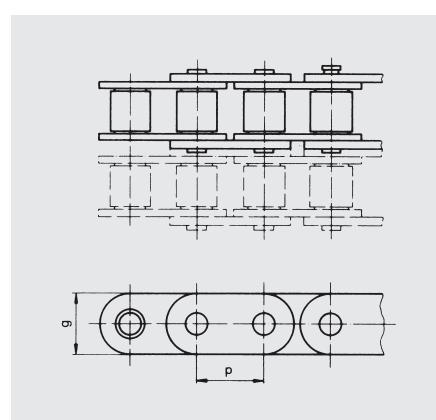
Detailed information is provided in a special brochure.



Example cam

2.8 Pallet transport chains

ROLLER CHAINS WITH STRAIGHT SIDE PLATES FOR TRANSPORTING COMPONENTS OR MATERIALS



iwi-chain no.	Pitch p (mm)	g (mm)	Breaking strength FB iwi mean (N)	Weight (kg/m)
Single strand chain M 128 AG	19,05	18,0	42.000	1,75
Double strand chain D 128 AG	19,05	18,0	84.000	3,50

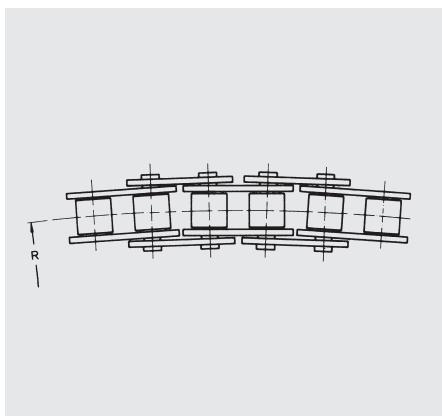
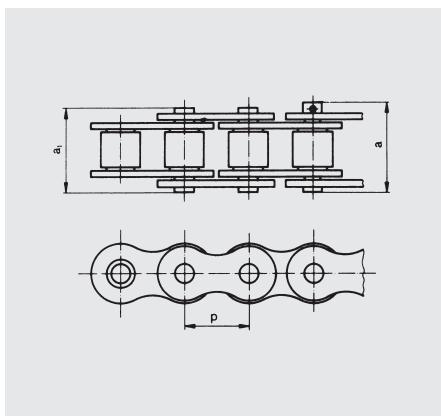
The top and bottom of all link plates are straight. These form a continuous support for material being conveyed.

Dimensions and values not given are identical to those of iwi chains M 128 A SL or D 128 A to DIN 8188.

Other dimensions available on request.

2.9 Side bow chains

TRANSPORTING, CONVEYING, DRIVING ON CURVED TRACKS



Side bow chains are constructed in the same way as roller chains to DIN 8188. They only deviate from standard dimensions in their pins and outside width.

The symmetrically conical pins with a central running surface enable the inner and outer links to run at an angle to one another which means that power can be transferred or loads carried on curved tracks.

iwiS-chain no.	Pitch p (mm)	a1 (mm)	a (mm)	Radius R (mm)	Mindest Bruchkraft iwiS (N)	Dauer	Kurzzeitig	Gewicht (kg/m)	Lieferbare Verbindungsglieder
L 85 A-SB	12,7	16,8	17,8	425	10.000	600	1500	0,65	2, 4, 8
M 106 A-SB	15,875	21,0	22,3	500	18.000	900	2500	1,00	2, 4, 8
M 128 A-SB	19,05	26,3	27,7	750	26.000	1200	3700	1,50	2, 4, 8

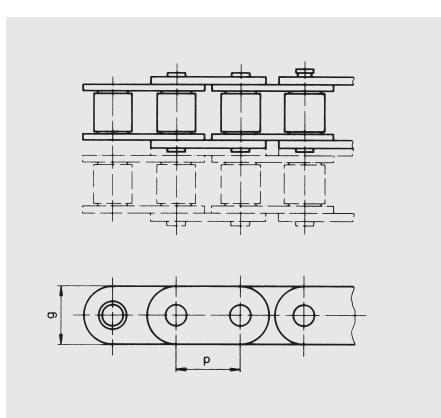
SB chains are also suitable to a limited extent for cases of use where the slanting position of the shafts determined by design factors makes slight torsion of the chains necessary.

The breaking strength of the chain and the service life to be expected are lower than with conventional chains, as the chain joint cannot be so heavily loaded due to the special pin design. Side bow chains with straight or bent connecting plates can be used as conveyor chains in many applications.

The transmission of a load on a curved track requires suitable chain guides on both the driven and the drive sections of the chain – for example, cage rails of high-molecular low-pressure polyethylene.

2.10 Hollow bearing pin chains

SIMPLE FITTING OF MOUNTED PARTS AND CROSS-MEMBERS



iwiS-chain no.	Pitch p (mm)	g (mm)	B (mm)	D (mm)	Breaking strength iwiS (N)	Weight (kg/m)
M 128 HB	19,05	18,0	25,5	6	36.500 ¹⁾	1,23

¹⁾ Breaking strength without inserted pins 34 500 N

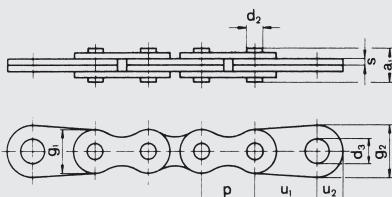
The main dimensions of the special sleeve chain are identical to those of iwiS chain M 128 A SL to DIN 8188.

The hollow pins can be located at any pitch point or at any pitch interval. Pins of 6 mm diameter can simply be inserted into the hollow bearing pins.

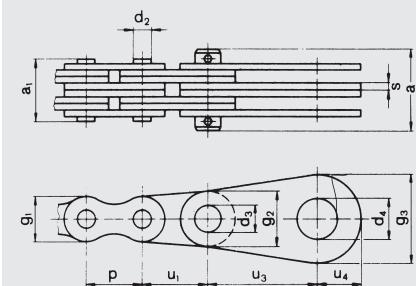
2.11 Leaf chains

LOAD CHAINS FOR LIFTING AND PULLING

End link design A



End link design B
(from combination 4 x 4)



iwi's-chain no.	General information										End link dimensions									
	p (Zoll)	p (mm)	Plate combination	Arrangement	Breaking load F _B iwi's min (N)	Bearing area f (cm ²)	Weight q (kg/m)	Bearing pin diameter d ² (mm)	a (mm)	Overall width	Plate height g ₁ (mm)	Plate thickness s (mm)	d ₃ (mm)	d ₄ (mm)	g ₂ (mm)	g ₃ (mm)	u ₁ (mm)	u ₂ (mm)	u ₃ (mm)	u ₄ (mm)
FL 522	-	8,0	2 x 2	■■■	5.000	0,05	0,15	2,31	5,6	-	6,3	1,0	6,2	-	16,0	-	15,0	10,0	-	-
FL 523	-	8,0	2 x 3	■■■	7.000	0,05	0,19	2,31	6,7	-	6,3	1,0	6,2	-	16,0	-	15,0	10,0	-	-
FL 623 ¹⁾	3/8	9,525	2 x 3	■■■	10.000	0,08	0,32	3,31	8,3	-	8,1	1,2	6,2	-	16,0	-	15,0	10,0	-	-
FL 623 b ¹⁾	3/8	9,525	2 x 3	■■■	20.000	0,20	0,46	3,31	10,9	-	8,2	2,0	6,2	-	-	-	-	-	-	-
FL 823 b	1/2	12,70	2 x 3	■■■	28.000	0,18	0,65	4,45	12,4	-	10,8	2,0	8,2	-	18,0	-	20,0	11,0	-	-
FL 834 a	3/8	12,70	3 x 4	■■■■	21.000	0,17	0,42	3,68	13,1	-	9,1	1,5	8,2	-	18,0	-	20,0	11,0	-	-
FL 834 b	1/2	12,70	3 x 4	■■■■	42.000	0,27	0,91	4,45	16,5	-	10,8	2,0	8,2	-	18,0	-	20,0	11,0	-	-
FL 845 a	1/2	12,70	4 x 5	■■■■■	34.000	0,24	0,67	3,68	16,9	25	9,1	1,6	8,2	12,2	18,0	25,0	20,0	11,0	30,0	15,0
FL 845 b	1/2	12,70	4 x 5	■■■■■	52.000	0,32	1,00	4,45	19,0	25	10,8	1,8	8,2	12,2	18,0	25,0	20,0	11,0	30,0	15,0
FL 866 a	1/2	12,70	6 x 6	■■■■■■	44.000	0,36	0,88	3,68	21,7	28	9,1	1,6	8,2	12,2	18,0	25,0	20,0	11,0	30,0	15,0
FL 866 bd	1/2	12,70	3 x 3 ²⁾	■■■■	62.000	0,40	1,17	4,45	20,6	28	10,8	1,5	8,2	12,2	18,0	25,0	20,0	11,0	30,0	15,0
FL 1044 bd	5/8	15,875	2 x 2 ²⁾	■■■	57.000	0,37	1,12	5,08	16,8	28	13,7	1,8	10,4	16,2	20,0	35,0	25,0	12,0	45,0	21,0
FL 1066 bd	5/8	15,875	3 x 3 ²⁾	■■■■	86.000	0,55	1,68	5,08	24,0	35	13,7	1,8	10,4	16,2	20,0	35,0	25,0	12,0	45,0	21,0
FL 1266 bd	3/4	19,05	3 x 3 ²⁾	■■■■	115.000	0,76	2,18	5,72	30,0	40	14,9	2,2	10,4	16,2	20,0	35,0	25,0	12,0	45,0	21,0
FL 1644 d	1	25,40	2 x 2 ²⁾	■■■	157.000	1,00	2,92	8,28	28,0	40	20,8	3,0	12,2	18,2	25,0	40,0	30,0	15,0	50,0	24,0
FL 1666 d	1	25,40	3 x 3 ²⁾	■■■■	231.000	1,50	4,35	8,28	41,0	50	20,8	3,0	12,2	18,2	25,0	40,0	30,0	15,0	50,0	24,0

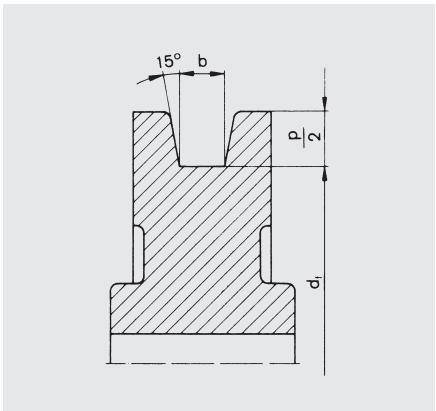
¹⁾ Straight side plates ²⁾ double

End link design A is arranged only as an inner link, which enables the connection of end link B as an outer link.

iwi's leaf chains are manufactured from precision iwi's chain parts to DIN 8187. The chain selection will be determined by the size and frequency of shock loading and the appropriate national lifting regulations.



EXAMPLE OF A LEAF CHAIN GUIDE ROLLER



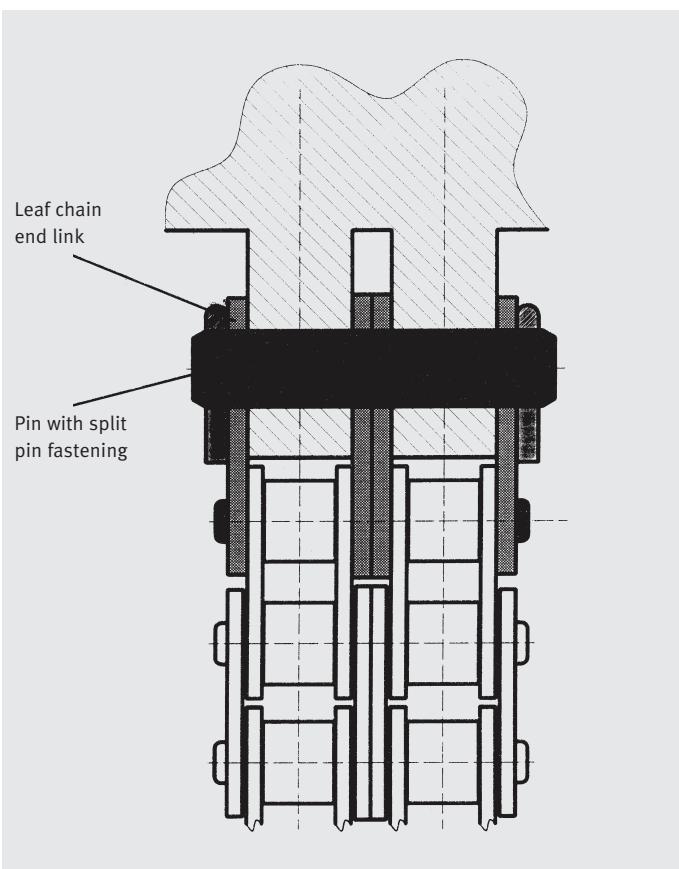
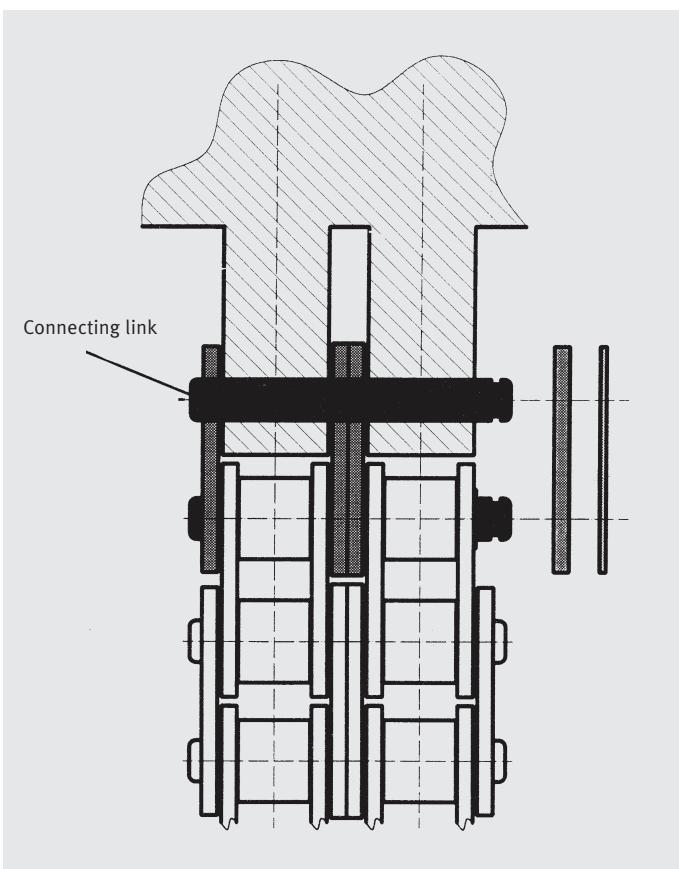
Inside width of roller:
 $b = a_1 \cdot 1,15$

Minimum diameter:
 $d_{f\min} = p \cdot 5$

Use the largest possible diameter.

Special applications – fastening of roller chains

iwis-roller chains can also be used as load chains. Roller chain connecting links (spring clip links) or leaf chain end links are examples of fastening possibilities.



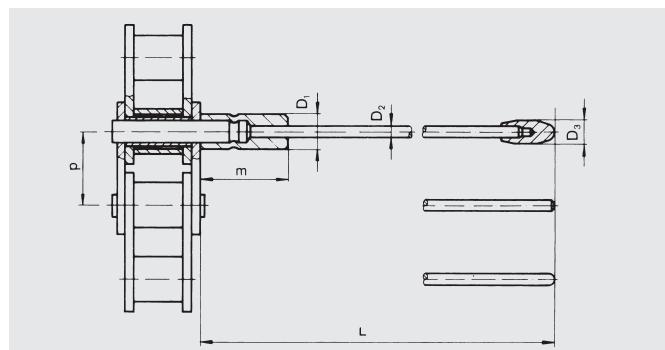
2.12 Tube or can conveyor chains

CAREFUL TAKE-UP AND TRANSPORTATION OF THIN-WALLED HOLLOW ARTICLES

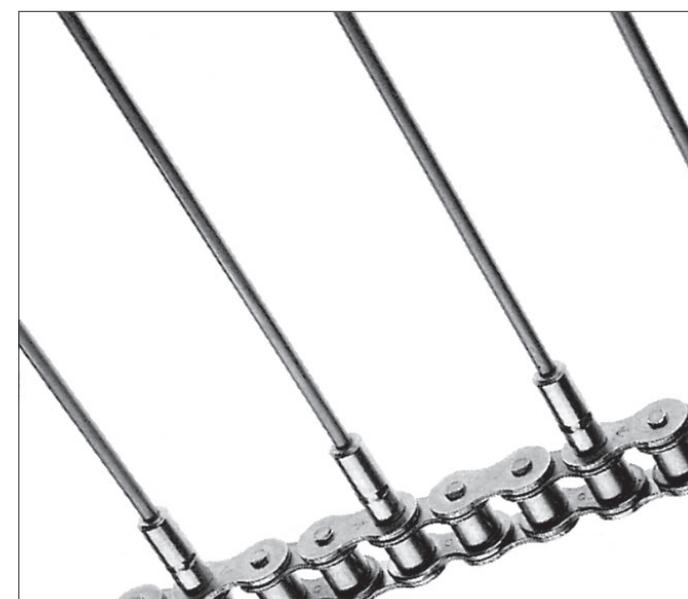
The field in which these conveyor chains are most frequently used is in the production of tubes and cans. These hollow articles, which are usually light, thin-walled and sensitive, must run through numerous processing stations and are there cleaned, lacquered, dried, packed and so on. These items are conveyed in large quantities at high speed over long transportation paths. Depending on the individual process, other stresses are strong contamination and temperature influences.

In the **production of tubes** as a rule high-performance roller chains with pitches between 1/2" and 1" are used. The hollow articles are taken up by spring steel pins whose spacing and length will depend on the size of the work-piece. The spring steel pins are pressed onto extended bearing pins and secured against rotation. The shape of the pin end can be made to match requirements. In the case of repairs it must be possible to replace the pin easily and rapidly. A special tool is available for chains L 85 SL, M 106 SL and M 127 SL.

iwis-chain no.	Pitch p (mm)	$L_{max.}$	D_1	m	D_2	D_3
L 85 SL	12,7	300	8,0	22,0	3,5	7,0
M 106 SL	15,875	300	8,0	22,0	4,0	8,0
M 127 SL	19,05	300	8,0	22,0	4,0	8,0
M 1611	25,4	300	12,0	30,0	4,0	8,0

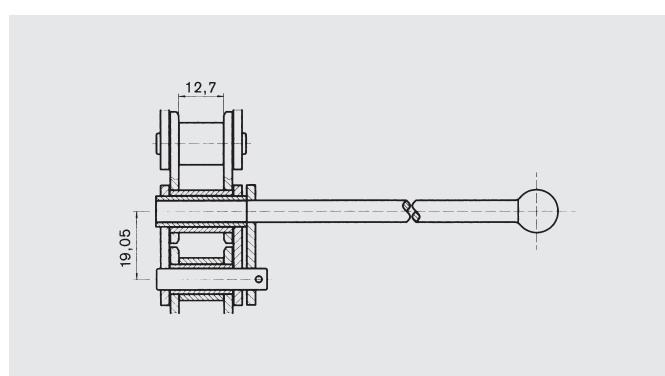


In the **production of cans**, a high-performance 3/4 x 1/2" roller chain to DIN 8188 is to be preferred which is fitted with hollow pins at the straight attachment fastening points (M 128 HB).



Here predominantly solid pins are inserted into the hollow pins at defined intervals and secured against rotation by means of screws, splints or other special fittings. Depending on the items being conveyed, the pins are available in various lengths and shapes.

EXAMPLES

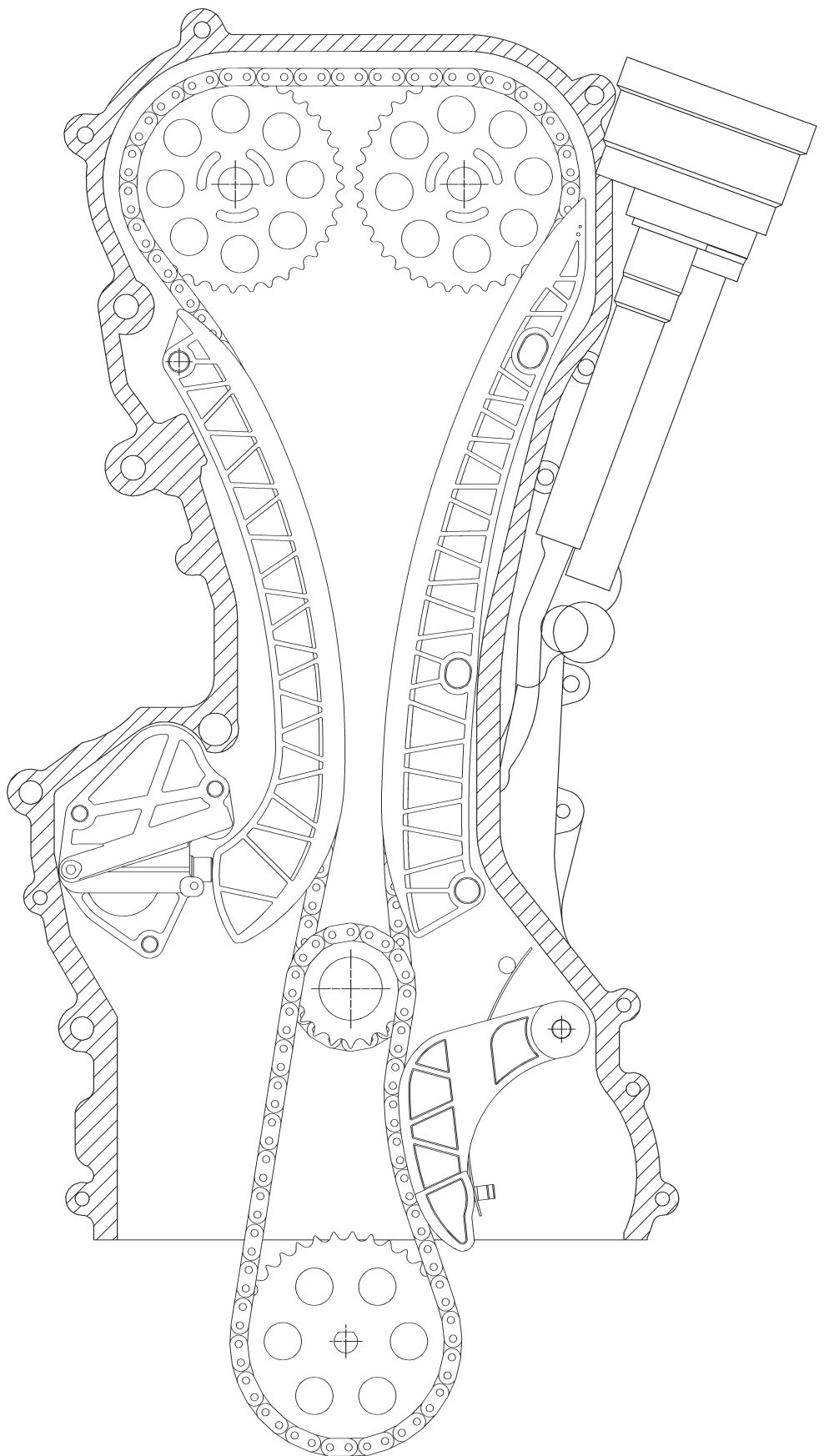


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 Power
 transmission chain



iwis simplex chains for timing and oil pump drives in a 3-cylinder-DOHC-engine

A

 Chain wheels

B

 Layout of
chain drives

C

 General information
chain drives

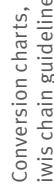
D

 Chains for
industrial use

E

 Automotive
chain drives

F

 Conversion charts,
iweis chain guideline

Amongst the various applications for chain drives the engine and gear design covering vehicles and stationary equipment require particularly high levels of precision, performance, and durability.

In the course of many decades roller and bush type chains of certain standard dimensions have proved to be particularly suitable.

iwis have influenced the development in this sector from the very beginning and have become leaders in this field.

iwis Programme:

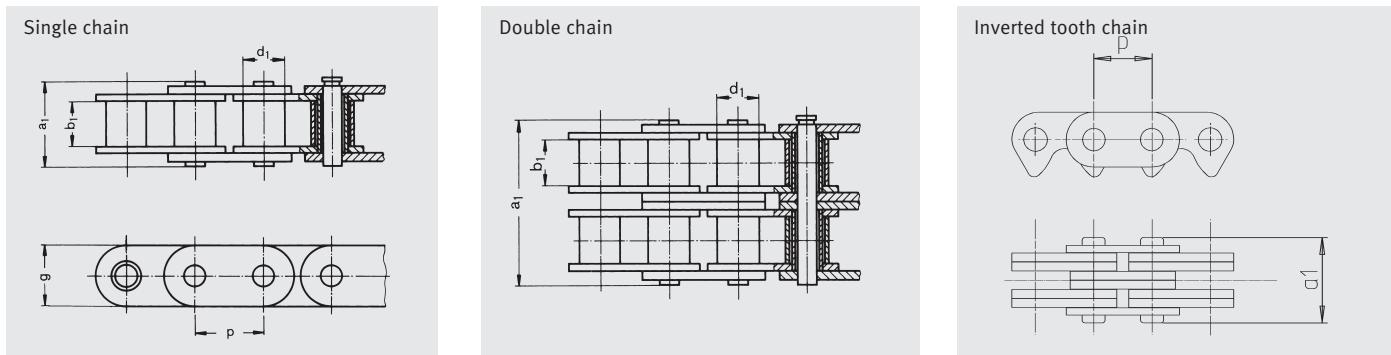
This comprises a number of single and double chains designed as roller or bush chains. Each one of these types has certain characteristics which make them particularly suitable for certain applications. New types are being developed in conjunction with new engine developments. The best materials and precision production processing together with the highest quality standards ensure a timing chain that will satisfy the demanding requirements of today's high performance engines.

Higher engine loads and operating speeds, along with new extremes of torsional vibration and temperatures make it essential to utilize a timing chain that combines high strength and low wear elongation. This will result in more precise camshaft timing as well as reducing timing variation over the life of the engine. The table on page 70 shows a summary of roller and bush chains for engines.

Characteristics and typical applications of selected types of chains

	Characteristics:	Principal applications:
7 mm x $\frac{2}{16}$ " – G 44 H – 8 mm x $\frac{3}{16}$ " – G 53 H / D53H – bush chains	Single bush chains, 8 mm pitch, large bearing pin diameter, large bearing area. Standard gearing as with 8 mm roller chain.	Reduced weight due to small pitch, compared with $3/8$ " chain, thus reduced centrifugal force and impact speed. Particularly suitable for drives with high speeds (e.g. mass balancing) or as timing chains on small engines (motorcycles) or drive chains for auxiliary equipment.
8 mm x $\frac{5}{16}$ " – Z 53 R – 6,35 mm x $\frac{5}{16}$ " – Z 46 – inverted tooth chain (silent chain)	Acoustic optimized inverted tooth chain with 8 mm pitch. Chain sprockets with special toothing.	timing drives with an optimized acoustic demand
$\frac{3}{8}$ x $\frac{7}{32}$ " – G 67/G 68/D 67 – roller chains	Single and double roller chains, type G 68 with increased bearing area compared with G 67.	Timing drives, oil pump drives, drives for auxiliary equipment, gearbox chains. G 68 is used increasingly as a replacement of double roller chains of a similar pitch.
$\frac{3}{8}$ x $\frac{7}{32}$ " – G 67H/D 67 H – bush chains	Single and double chains, bush type for standard chainwheels as used for $3/8$ " roller chains. Large bearing pin diameter, large bearing area.	Heavy duty drives, e.g. Diesel engines with a highly impulsive load.

Dimensions



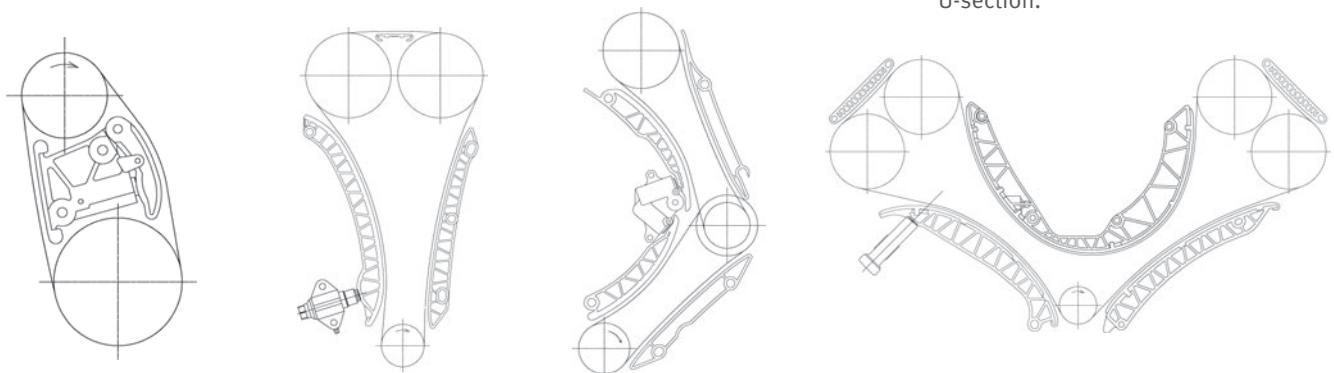
iwis-chain no.	Designation pitch \times inner width	DIN/ISO N:	Zoll	Pitch p mm	inside b^1 (mm) max.	outside a^1 (mm) max.	roller/bush d^1 (mm) max.	height of plates	bearing area f (cm 2)	chain weight q (kg/m)	iwis-breaking load F_B (N)
Single chains											
G 44 H 1) 2)	7 mm x 2/16"	–	–	7,000	3,5	9,9	4,00	6,8	0,165	0,26	7000
G 53 H 1) 2)	8 mm x 3/16"	–	–	8,000	4,76	11,8	5,00	7,60	0,25	0,34	9000
G 67	3/8 x 7/32"	06 B-1	3/8	9,525	5,72	12,9	6,35	8,26	0,28	0,41	12000
G 68 2)	3/8 x 7/32"	–	3/8	9,525	5,72	14,0	6,35	8,26	0,32	0,44	12500
G 68 H 1) 2)	3/8 x 7/32"	–	3/8	9,525	5,5	13,9	6,35	9,60	0,47	0,59	14000
Double chains											
D 53 H 1) 2)	8 mm x 3/16"	–	–	8,000	4,76	20,9	5,00	7,60	0,49	0,62	12000
D 67	3/8 x 7/32"	06 B-2	3/8	9,525	5,72	23,4	6,35	8,26	0,56	0,78	19000
D 67 H 1) 2)	3/8 x 7/32"	–	3/8	9,525	5,5	23,7	6,35	9,60	0,76	0,89	19000
Inverted tooth chain											
Z 53 R 2)	8 mm x 5/16"	–	–	8,000	–	11,7	–	–	0,15	0,45	17000
Z 46 2)	6,35 mm x 5/16"	–	–	6,350	–	10,9	–	–	0,15	0,37	11500

¹⁾ Bush type chains ²⁾ iwis standard

Chain drives used on combustion engines are subjected to an inherent sequence of unequal loads. In addition to the engine characteristics, the number of cylinders, arrangement of drive components and the type and number of auxiliary drives are factors of significance.

By using tensioning and guide elements which are carefully designed to the relevant engine, it is possible to optimize the life of the chain drive to match that of the engine without requiring any additional maintenance, apart from the specified engine maintenance.

Simple rails made of plastic or metal with plastic or rubber linings are used as guides, depending whether the chain track is straight or curved. If there is a danger that the chain may be subjected to lateral oscillations, rails with lateral guides are used, which guide either between the inner link plates or enclose the chain in a U-section.



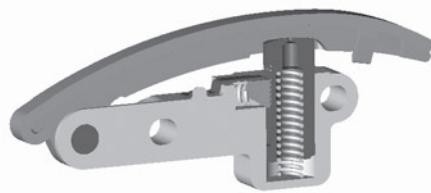
A Tensioning elements

The **tensioners** have a number of functional characteristics which are available in a combination to suit the application.

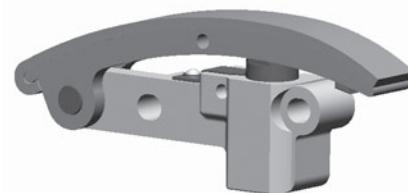
These are:

- Effort created by mechanical spring
- Effort created by oil pressure, which also acts as a damper
- Damping by oil supplied without pressure. Non-return valve
- Lubrication hole in the tensioning pad for chain lubrication and aeration
- Nonreturn mechanism to limit the reverse travel
- Device to return the tensioner without the need to dismantle.
- Tensioner with rubber pad for direct contact with chain
- Double piston for simultaneous tensioning/damping of several chains

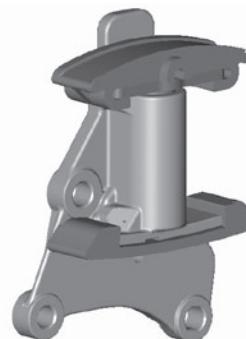
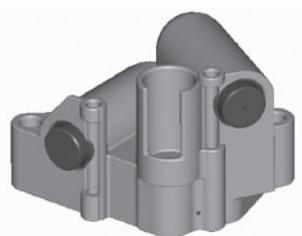
EXAMPLES:



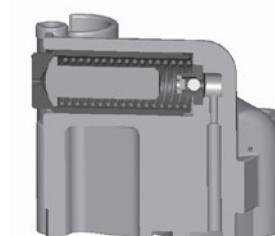
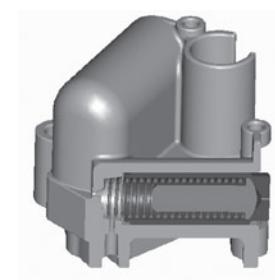
Tensioning effort by means of spring, oil pressure damping and non-return mechanism. Splash hole for chain lubrication



Tensioner with non-return mechanism and piston resetting mechanism, oil pressure damping



Type for tensioning/guide rail



Double piston type for direct tensioning of two chain sections.
Oil filled, non-return valve

With pressure pin to operate articulating tensioner or guide rail. Fitted in engine casing

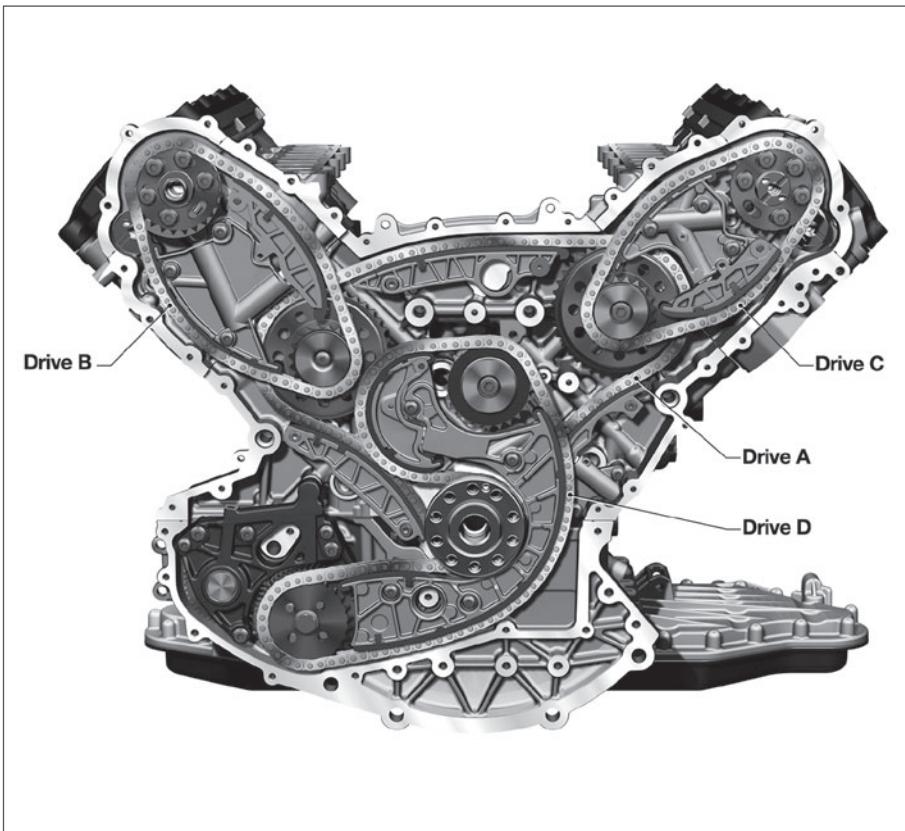
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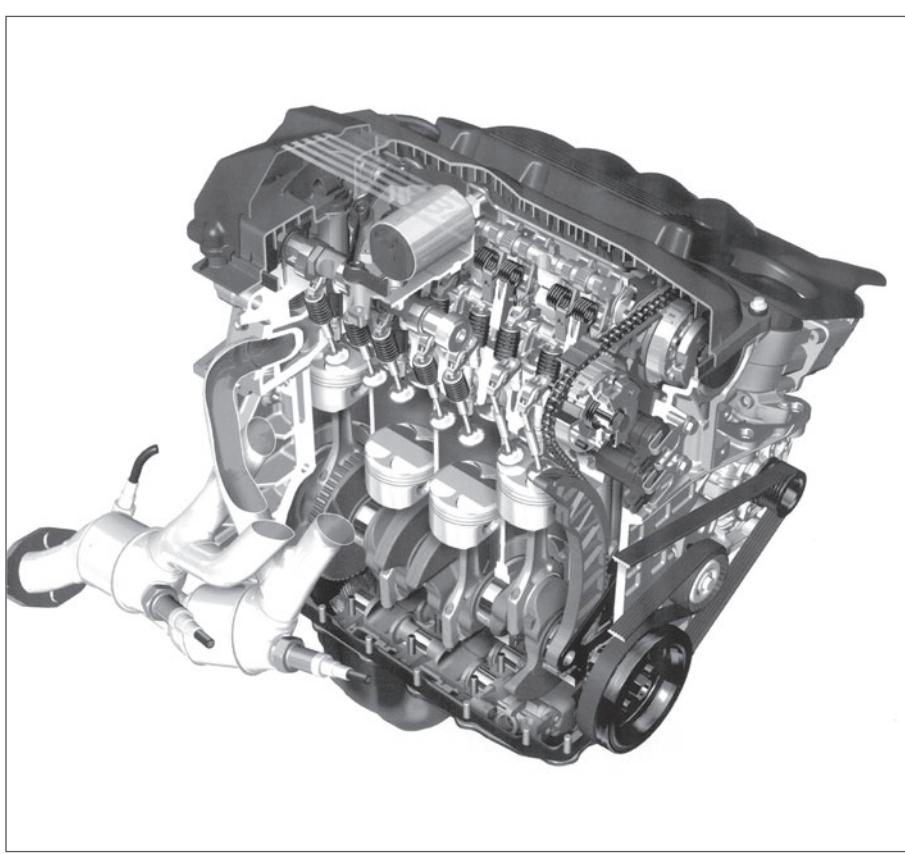
A



Cam shaft timing with **iwis** chains
in a V8-engine

DWTS® Chain wheels

B



Cam shaft drive with **iwis** simplex chain
in a 4-cylinder-DOHC-engine

DWTS® chain drives

C

General information
DWTS® chain drives

D

DWTS® Chains for
industrial use

E

DWTS® Automotive
chain drives

F

Conversion charts,
iwis chain guideline

New chain types

Over the past years, the main requirements for chains focused on minimum elongation throughout the vehicle's life cycle and high strength. Recently, however engine designers have expressed a further wish for reduced noise emission and improved chain dynamics.

This new demand arises from the realization of smoother combustion processes due to new injection technology and the reduction in noise emission from accessory drives in the combustion engine, through which the timing chain drive is being perceived to a greater extent as a source of noise.

In response to these demands, two new chain generations have been developed and are represented by the **iwiSUPREME** and **iwiSTAR** versions. Both chains combine standard **iwi** chain characteristics with additionally optimised acoustic and dynamic performance.

iwiSUPREME

Due to their kinematics characteristics, inverted tooth chains in particular, display major potential for an improvement in dynamic and acoustic performance. Whereas inverted tooth chain drives have proven their performance for many years in timing chain drives with less dynamic loading, up to present it has not been possible worldwide to implement them on engines with challenging dynamic demands (e.g. diesel engines) due their greater chain elongations in comparison to bush and roller chains.

The **iwiSUPREME** version is based on the operating principle of an inverted tooth chain (see figure 1). By optimising the kinematical motion sequence at the chain

infeed and outfeed, the infeed pulse and irregularity of motion and power transmission (chordal action) could be reduced. Extensive engine trials indicated an improvement in chain dynamics as well as in acoustic performance. The link plate contour was designed so that even very small teeth numbers of 18 on the smallest chain sprocket could be achieved, which has a very positive effect on the demand of radial design space.

A bush was integrated in the inner link of the tooth link plates to improve the wear and tear characteristic. Whereas on conventional inverted tooth chains the articulated movement takes place between the tooth link plate and the pin at the

chain sprocket infeed and outfeed, on the **iwiSUPREME** version, the interaction between bushing and pin is analogous to that of bush and roller chains. The design-related improvement in tribological conditions is reflected in perceptibly lower wear and tear values in comparison to conventional inverted tooth chains and permits even implementation in diesel engines. Due to the compact design of inverted tooth chains, in which a greater number of transmitting link plates can be featured in comparison to roller and bush chains, a significant benefit in terms of strength can also be observed on the **iwiSUPREME**.

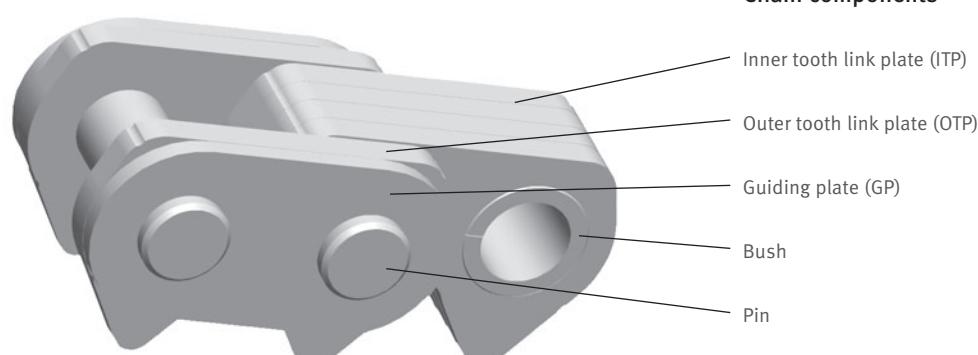


Figure 1: Design of the **iwiSUPREME** chain variant

New chain types

iwistar

The inner dynamics of a chain drive and acoustic behaviour perceived by the customer are mainly determined by the polygonal effect of chains that increases as the number of teeth on the chain sprocket decreases.

The **iwistar** variant was developed on the basis of proven bush and roller chains with the objective to improve the dynamics and acoustic performance (see figure 2).

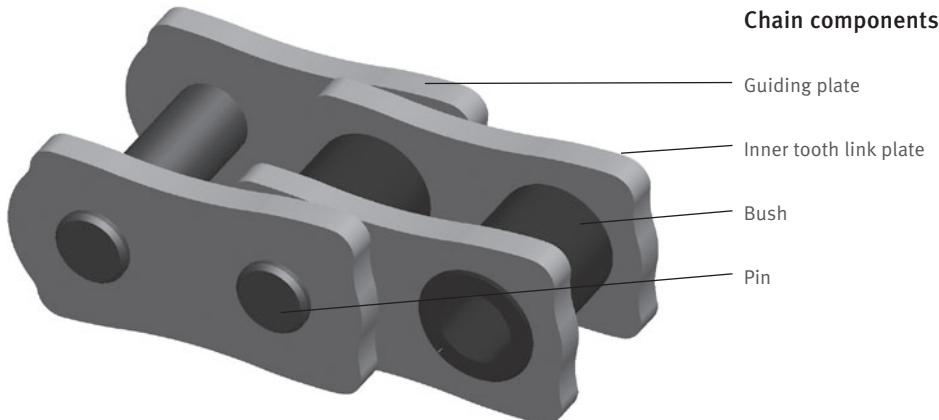


Figure 2: Design of the **iwistar** chain variant

In order to reduce the unevenness at chain infeed and outfeed, the chain rests on a supporting ring by its specially shaped outer and inner link plates (see figure 3). As it runs into the chain sprocket, the chain is lifted by the interaction of link plate contours and supporting ring.

The design of the geometry of the link plate contours intends the inner tooth link plate to roll off the supporting disc while the chain wheel turns and at the same time, the lifting of the chain is counteracted by the engagement of the chain sprocket.

As such, the polygonal effect can be almost completely eliminated and smooth chain running assured.



Figure 3: Chain infeed motion sequence

By implementing the **iwistar** variant, a perceptible reduction in inner chain excitation and an improvement in acoustic performance can be achieved.

As the wear and tear and strength values of the **iwistar** variant are identical to that of standard bushing chains, users can implement the chains without any restrictions.

Both newly developed variants, **iwisUPREME** and **iwistar**, are available in pitches of 7 mm, 8 mm and 9.525 mm. The main geometrical dimensions have been selected so that when converting a bush or roller chain drive, there is no need to replace the rails.

Conversion chart

Inch ("') in mm						English feet (ft) to cm		PS to kW		kW to PS	
Inch	Inch	mm	Inch	Inch	mm	Fuß	cm	PS	kW	kW	PS
1/32	0,031	0,794	13/16	1	20,637	1,0	30,5	1,0	0,73	1,0	1,36
1/16	0,062	1,587	27/32	0,844	21,431	1,1	33,5	1,5	1,10	1,5	2,04
3/32	0,094	2,381	7/8	0,875	22,225	1,2	36,6	2,0	1,47	2,0	2,72
1/8	0,125	3,175	29/32	0,906	23,019	1,3	39,6	2,5	1,83	2,5	3,4
5/32	0,156	3,969	15/16	0,937	23,812	1,4	42,7	3,0	2,20	3,0	4,08
3/16	0,187	4,762	31/32	0,969	24,606	1,5	45,7	3,5	2,57	3,5	4,76
7/32	0,219	5,556	1	1	25,4	1,6	48,8	4,0	2,94	4,0	5,44
1/4	0,25	6,35	1 1/32	1,031	26,194	1,7	51,8	5,0	3,67	5,0	6,8
9/32	0,281	7,144	1 1/16	1,062	26,987	1,8	54,9	6,0	4,41	6,0	8,16
5/16	0,312	7,937	1 3/32	1,094	27,781	1,9	57,9	7,0	5,14	7,0	9,52
11/32	0,344	8,731	1 1/8	1,125	28,575	2,0	61,0	8,0	5,83	8,0	10,88
3/8	0,375	9,525	1 5/32	1,156	29,369	2,5	76,2	9,0	6,61	9,0	12,24
13/32	0,406	10,319	1 3/16	1,187	30,162	3,0	91,4	10,0	7,35	10,0	13,6
7/16	0,437	11,112	1 7/32	1,219	30,956	3,5	106,7	11,0	8,09	11,0	14,96
15/32	0,469	11,906	1 1/4	1,25	31,75	4,0	121,9	12,0	8,82	12,0	16,32
1/2	0,5	12,7	1 9/32	1,281	32,544	4,5	137,2	13,0	9,56	13,0	17,68
17/32	0,531	13,494	1 5/16	1,312	33,337	5,0	152,4	14,0	10,30	14,0	19,04
9/16	0,562	14,287	1 11/32	1,344	34,131	10,0	304,8	15,0	11,03	15,0	20,4
19/32	0,594	15,081	1 3/8	1,375	34,925	15,0	457,2	16,0	11,76	16,0	21,76
5/8	0,625	15,875	1 13/32	1,406	35,719	20,0	609,6	17,0	12,5	17,0	23,12
21/32	0,656	16,669	1 7/16	1,437	36,512	25,0	762,0	18,0	13,23	18,0	24,48
11/16	0,687	17,462	1 15/32	1,469	37,306	30,0	914,4	19,0	13,97	19,0	25,84
23/32	0,719	18,256	1 1/2	1,5	38,1	35,0	1066,8	20,0	14,70	20,0	27,20
3/4	0,75	19,05	1 3/4	1,75	44,45	40,0	1219,2	25,0	18,38	25,0	34,0
25/32	0,781	19,844	2	2	50,8	50,0	1524,0	50,0	36,76	50,0	68,0

1" english = 25,399956 mm

1 m/s = 196,8 ft/min

1 inch = 0,0833 feet = 0,0278 yard

1" american = 25,40005 mm

1 m/s = 3,28 ft/s

1 foot = 12 inch = 0,333 yard

1 lb = 0,454 kp

1 m/s = 3,6 km/h

1 yard = 36 inch = 3 feet

1 kp = 2,205 lb

1 km/h = 0,278 m/s

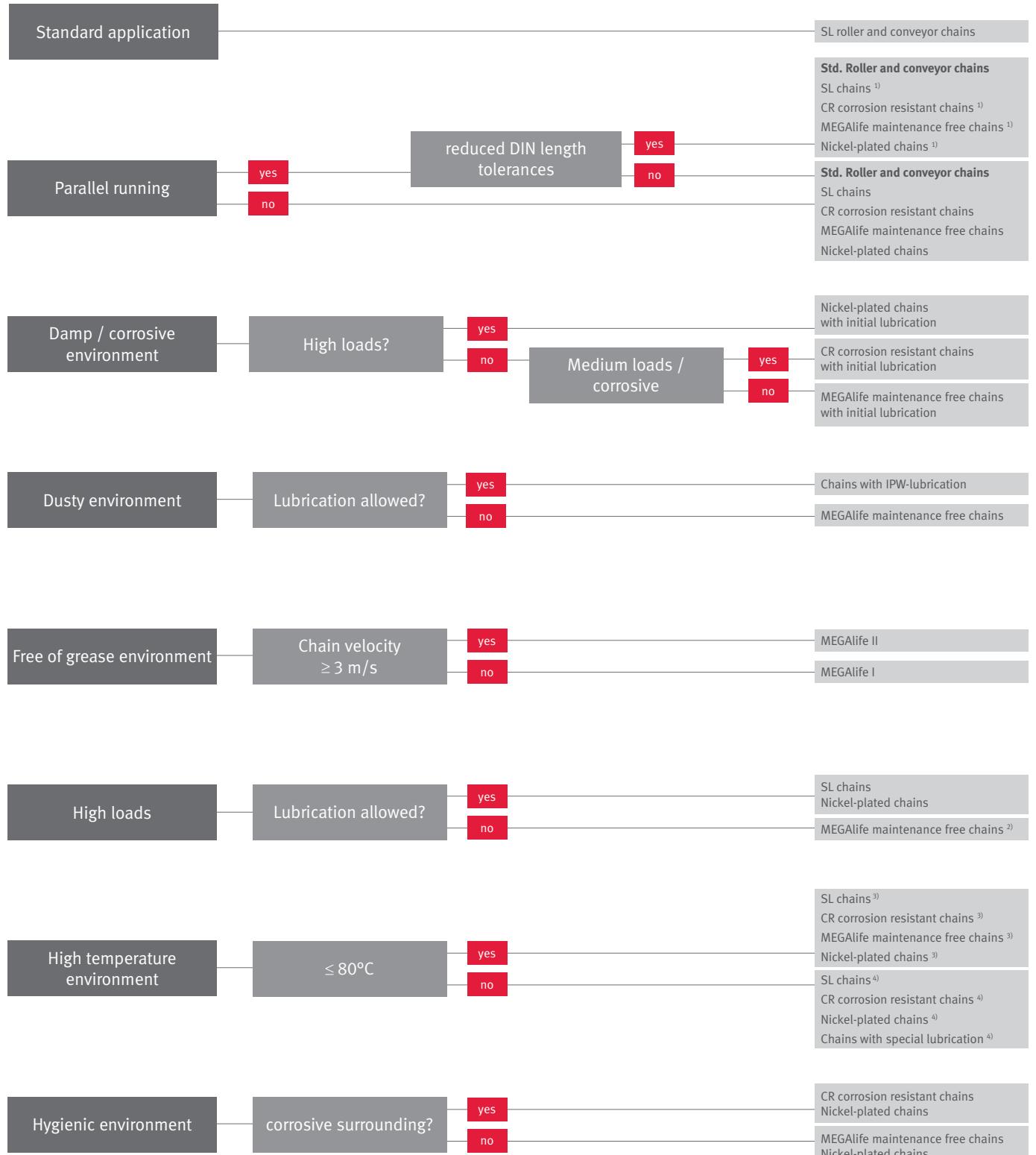
1 PS = 0,98 HP

1 ft/s = 0,305 m/s

1 HP = 1,014 PS

iwis® chain guideline for industrial applications

Which application demands which chain type?



important detail! The following guidelines support you in choosing the right chain. However, please note that each application is individual. The result should in no case serve as a basis for your order.

Therefore please refer to our professional employees who are happy to submit an individual order to you. We do not assume any guarantee or liability.

iwis® Questionnaire for chain drives

Enquiry from: _____ Date: _____

Address: _____ Dealt with by: _____

Telephone: _____

Drive (input)

Electric, hydraulic, pneumatic combustion engines/motors (2, 4 or 6 cyls)?

Power output? kW

RPM? min⁻¹

Max. torque? at n = min⁻¹ Nm

Continuous power or peak power?

Speed constant, varying or impulsive?

Operating time, cyclic operation?

Are shock absorbing transmission-elements present (friction clutch)?

Output

Type of driven machine?

RPM? min⁻¹

Power requirement? for starting - normal running - max. kW

Load even, varying or impulsive?

Direction of rotation continuous or alternating? (show in diagram)

Chain drive

Centre distance mm

Does the design allow the centre distance to be modified? ±

Possibility to provide tensioner? (adjustability, idler, chain guide)

Could the centre distance alter in service? e.g. rear wheel suspension on a motorcycle

Required or current ratio respectively?

Shafts horizontal or vertical?

Can the drive be protected against dirt and dust or can it be enclosed?

What type of lubrication is possible? (manual, drip, oil bath, pressure)

External factors? (temperature in °C, dust, moisture, fibres)

Chain

Chains planned or existing drive?

Is the chain replacing an existing drive?

Max. permissible chain width? mm

Chain wheels

No. of teeth? $z_1 =$ $z_2 =$

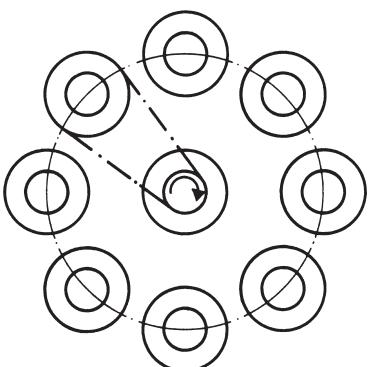
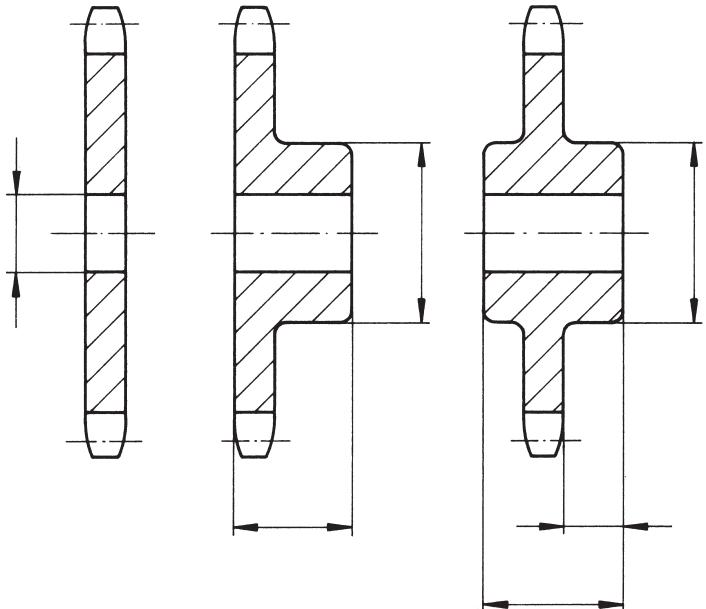
Max. permissible outside diameter, incl. chain? mm

Chain wheel as a disc or with hub, predrilled or with finished bore?

iwis[®] Questionnaire for chain drives

A

The relevant dimensions with permissible tolerances should be entered in the diagram below.



Example used:
 Drive running in clockwise direction, in
 inclined arrangement, speed reducing ratio

B

C

D

E

F

G

Drawing of drive layout

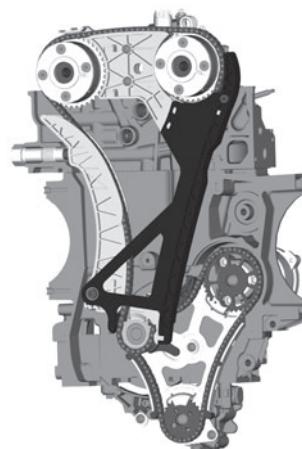
The iwis group

iwis – Joh. Winklhofer Beteiligungs GmbH & Co. KG is a medium sized company group in the automotive supply industry and drive technology industry for general engineering. The following divisions are part of the Company:

iwis motorsysteme GmbH & Co. KG

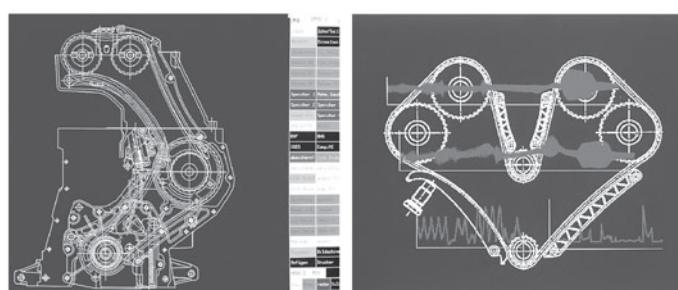
System supplier to the automobile industry

Over the course of time, the subsidiary firm specializing in automobile applications established a reputation within Germany as a leading global system supplier. Apart from the production of control chains and chain tensioners, iwis is a global supplier of control systems and systems for camshafts, mass balancing and oil pumps. iwis chain drive systems run for long periods in millions of petrol and diesel motors without the need for servicing. In accordance with the needs of the client, the control assembly module is developed and produced from the appropriate ‘building block’ components (the control chain, chain tensioners, guidance rails and the sprocket). Due to the depth of production experience with chains and distinct expertise – especially in the field of chain tensioners and chain drive modules – iwis is able to guarantee consistently high levels of quality in large scale production.



Research and development

Research and development offers engineering support for timing drives, compensation and oil pump systems, as well as for drive systems for general engineering. We work with our customers during the development phase, accompanying them right through to being ready to go into production. Simultaneous engineering is guaranteed at all times by special test rigs and modern design and calculating methods. This ensures the most rapid reaction times in the joint development process.



iwis antriebssysteme GmbH & Co. KG (München)

Dynamic drive systems for winners

The subsidiary responsible for industrial applications supplies iwis drive systems, precision chains, sprocket wheels and chain tensioner products for drives and material handling for a wide range of industrial applications. The all round product range includes roller chains, conveyor chains, maintenance free MEGALife chains, corrosion resistant CR chains, power and free conveyor chains, special conveyor chains, chain guides, sprocket wheels, chain tensioners, tools and the necessary chain lubricants. Our strength is producing chains far over the DIN standard in extremely tight length tolerances. As a systems supplier in drive technology we offer innovative and customer specific solutions to problems.

iwis antriebssysteme GmbH (Wilnsdorf)

The work of a whole series of specialists

iwis antriebssysteme GmbH, Wilnsdorf (formerly Flexon) has been actively in the business of drive technology and conveyor systems since 1980 and in doing so, has consistently orientated its range to match the needs of its customers. Today we supply a comprehensive, highly differentiated range of products from high quality chains and sprockets through to accessories for all applications. Apart from our product's high level of quality and reliability, industry and agriculture (and many other sectors besides) especially benefit from the services we provide.

The ELITE and FLEXON brandnames represent the values we stand for. Our flexibility ensures you the best possible solutions, even in the case of demanding and difficult tasks. We can be sure of this as it is backed up by the combined expertise of our many specialists in fields of development, production, quality control, sales and service. Just taking the field of development alone, the close partnership that we share with TU Chemnitz (an institution, which in the field of drive technology and conveyor systems, is internationally seen as one the leading scientific centres) is exemplary within the sector and a decisive factor in the technological standards of our products.

iwis agrisystems (Sontra)

The centre for agricultural expertise

As agricultural machinery is practically always located outdoors, the chains used in them are directly exposed to adverse influences such as dust and dirt as well as cold and wet conditions. Apart from this, their reliability is consistently put to the test after long periods of non-operation in winter. In view of this, we are especially proud of being able to claim a leading market position in the business of agricultural chains. On the one hand, this is thankfully attributed to their robust design and on the other hand, their availability.

The range of products and brands that make up iwis drive systems

JWIS



High performance precision chains for all industrial sectors

In the field of drive technology and conveyor systems, iwis supplies recognised top quality products for a whole range of industrial applications. Our strength lies in producing the chains with extremely close length tolerances that go way beyond the DIN standard. As a system supplier, we offer innovative and tailored solutions related to drive technology. We work to ensure that the benefits to the customer take centre stage.

ELITE



Top quality roller chains

The elite roller chain range offers high performance and operational reliability which doesn't just fulfil ISO standards, DIN and ANSI, but also attains top marks when it comes to creep resistance. The comprehensive family of products and the possibility of developing special designs open up an unlimited range of applications from industrial plant to use in clean rooms. Careful preparation on modern production lines, quality materials and optimum heat treatment guarantee a high level of resistance to creep as well as wear and tear. After installation, all chains are pre-stretched: The guarantee for low level run-in stretching!

iwis agrisystems: ELITE



Chains for agricultural applications

The iwis range comprises chains and complete kits for nearly all types of agricultural machines which are established around the world. For many years now we have been supplying to original equipment manufacturers as well as the market for spare parts. Today we are a market leader in chains for agricultural applications. By placing an emphasis on the highest technical and logistical abilities, we are able to immediately supply urgent spare parts during the harvest season.



FLEXON flat top chains and modular belts

Our maxxTop flat top chains in plastic and/or stainless steel and our maxxBelt modular belts represent the perfect solution for your transport operations. Whether in the drinks industry, in packaging plants or in other industries, our FLEXON chains are used everywhere where level transfer surfaces are required. With expertise and commitment we meet the diverse needs of our customers and in doing so, ensure strict compliance with the quality level of our products and services.



Accessories

iwis rounds off its extensive range of products with a wide selection of accessories. The range includes (among other things) chain tensions, guidance rails, tools (e.g. stud pulling machines (see photo above) and lubricants.



Sprockets

iwis has a wide range of standard sprockets in stock. Special designs are also available quickly – bore holes and grooves will be finished to meet your needs.

90 years success history iwi's

- 1916** → Company founded by the councillor of commerce Johann Baptist Winklhofer
- Following this, the production of ignition devices in a disused factory.
- Among other things, bicycle chains were also produced after the 1st World War.
- 1933** → Dr. Rudolph and Otto Winklhofer, sons of the company's founder, join their father's company.
- 1939** → Incorporation of timing chains into the product range and becoming BMW and Skoda's supplier.
- 1972** → Starting to supply chain tensioners.
- 1975** → Graduate engineer Gerhard Winklhofer takes over the management role in the 3rd generation.
- 1988** → iwi's successfully passes the first audit for quality.
- 1990** → iwi's receives the first order from the automobile industry to deliver a complete system.
- 1991** → iwi's receives the Q1 award from Ford and is certified the DIN ISO 9002.
- 1992** → iwi's successfully passes the first VDA-6 audits. (VDA is the Association of German Automobile Manufacturers)
- 1993** → orwi's ketten in Strakonice is founded as an independent company in the Czech Republic.
- 1994** → DIN ISO 9001 certification.
- 1996** → iwi's is awarded the Bavarian Prize for Quality (Bayerischen Qualitätspreis).
- 1997** → iwi's fulfills the conditions of the EC Eco-Audit Regulation for environmental stewardship.
- 1998** → iwi's is awarded the Prize for Environmental Awareness for the City of Munich.
- 1999** → Johannes Winklhofer, graduate businessman, takes over the management role in the 4th generation.
- Certification QS 9000, DIN EN ISO 14001, DIN ISO 9001:2000

- 2000** → Opening of the modern factory in Landsberg.
- In 2000, the EC Eco-Audit Regulation was successfully recertified.
- 2001** → VDA 6.1 certification.
- 2002** → ISO TS 16949 certification.
- DIN EN ISO 14001 recertification (Munich factory).
- DIN EN ISO 14001 certification (Landsberg factory).
- iwi's receives the Bayerischer Qualitätspreis 2002 and the Bayerischer Frauenförderpreis 2002.
- 2004** → Factory 3 which is based in Landsberg wins the "Location Champion" award in the "Factory of the Year" competition.
- 2005** → iwi's is the overall winner in the "Factory of the Year" competition.
- Extension to the certificate for the 'career and family' audit by the Hertie foundation (for family friendly staffing policies).
- 2006** → iwi's celebrates their **90th anniversary** and is listed under Bavaria's Top 50 companies.
- Aquisition of the Flexon GmbH.
- iwi's makes the drive systems division independent
- iwi's takes over the Flexon group
- 2007** → Listed on the "Top 100" List of the best German employers of medium-sized businesses.
- Establishment of a Holding structure
- 2008** → TOP employer - Automotive 2008/2009
- iwi's drive systems, LLC is awarded the ACHIEVING EXCELLENCE PARTNERSHIP AWARD 2008 by John Deere for excellent partnership
- 2009** → "Engine of the year 2009" award – 7 out of the 9 motors which are awarded prizes feature iwi's chain control assemblies
- ACHIEVING EXCELLENCE AWARD 2009 – iwi's drive systems, LLC and iwi's antriebssysteme GmbH, Sontra (agrisystems) are awarded prizes by John Deere for excellent partnership



A



High precision chains

iwis[®]



Chain engineering

iwis[®]



Flat Top chains

FLEXON



Modular belts

FLEXON

iwis[®] Chainwheels

B



Roller- and conveyor chains

ELITE



Leaf chains

ELITE



Agricultural chains

ELITE



Sprockets and drive components

iwis[®] chain drives

C



Drive- and conveyor chains

EURO CHAIN[®]
 powered by iwis



Transmission roller chains

ecoplus[®]

iwis[®] Chains for industrial use

D

All catalogues can be downloaded on iwi.com/kataloge

iwis[®] Automotive chain drives

F

Conversion charts,
 iwis chain guideline

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